T

MATERIALS SCIENCE PRODUCTS
PFIZER INC., 640 NORTH 13TH STREET, EASTON, PENNSYLVANIA 18042-1497

1 plant shut down
1 plant - fiberfree talc

215 250-3000

July 24, 1987

Mr. John Copeland
Office of Air Quality Planning and Standards
USEPA
Research Triangle Park, NC 27711

RE: Hazardous Air Pollutants

Dear Mr. Copeland,

The USEPA request (from J. F. Farmer) for information on air emissions of asbestos and other mineral fibers addressed to Dr. G. Laubach was forwarded to this department for response.

The Pfizer Inc., MSP Group presently operates two talc processing facilities which are located in Victorville, CA and Dillon, MT.

The plant located in Victorville, CA will be permanently closed on July 30, 1987. Since this plant will not be operating after that date, data from the plant on air emissions prior to July 31, 1987 will not be relevant to the need for future national emissions standards.

The plant located south of Dillon, MT processes only fiber-free Montana talc. The fiber-free characteristic of this talc deposit is a critical part of our product quality and samples are examined monthly with an electron microscope for presence of fibers at Pfizer MSP Group analytical lab in Easton, PA. No tremolite or asbestos fibers have been found since the Pfizer acquisition in 1969. Tests by MSHA and NIOSH have confirmed the lack of fibers in the many samples they have examined. Geologically, the nature of the talc deposit indicates that no fibers are expected to be found. Since the talc processed at this plant has been proven to be fiber-free there are no fibrous emissions from the facility. Thus the plant is not applicable for the study.

Very truly yours,

Wayne E. McCoy for
Wayne E. McCoy
Director of Divisional Engineering
and Production Services

WEM/

TALC

Mr. Gerald Laubach
President
Pfizer, Inc.
235 East 42nd Street
New York, NY 10017

~~Ack sent 1/4/88~~

Contact: Wayne McCoy (215) 250-3000

~~No ack. sent~~

114 Response Rec'd 7/24/87

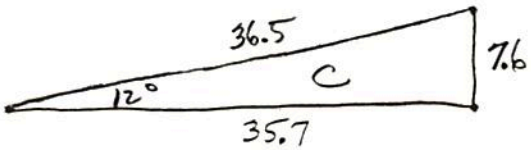
- one plant in Victorville, CA to be closed 7/30/87
- Dillon, MT plant processes only fiber-free talc
- Plant N/A for this project

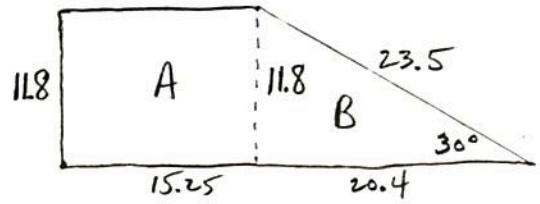
/ closed

/ open

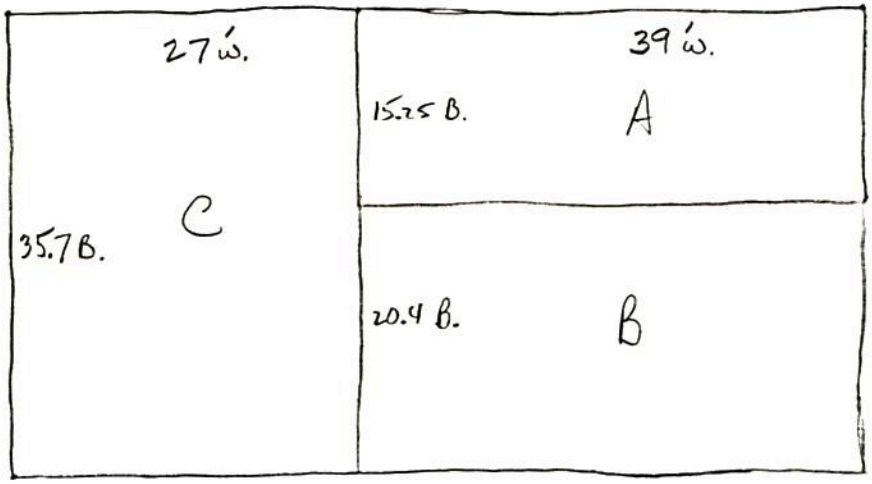
no fibers - (no analysis)

VAN HORN 2-3-87 TOM WHITE @ MINE





NORTH FACE @ 90°



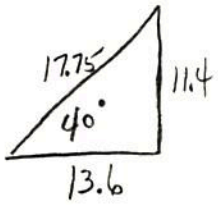
A = 15.25 × 39 × 11.8 × 125 #/ft³ ÷ 2000 = 438.63

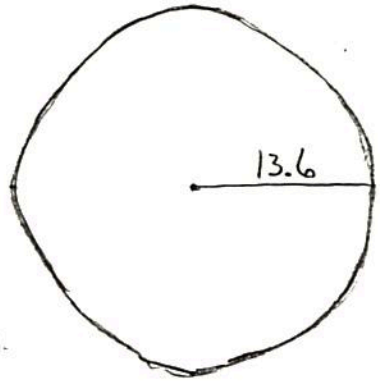
B = 20.4 × 39 × 11.8 ÷ 2 × 125 ÷ 2000 = 293.38

C = 35.7 × 27 × 7.6 ÷ 2 × 125 ÷ 2000 = 228.93

960.94

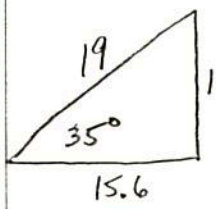
VAN HORN 2-3-87 TOM LIGHT GREY @ MINE

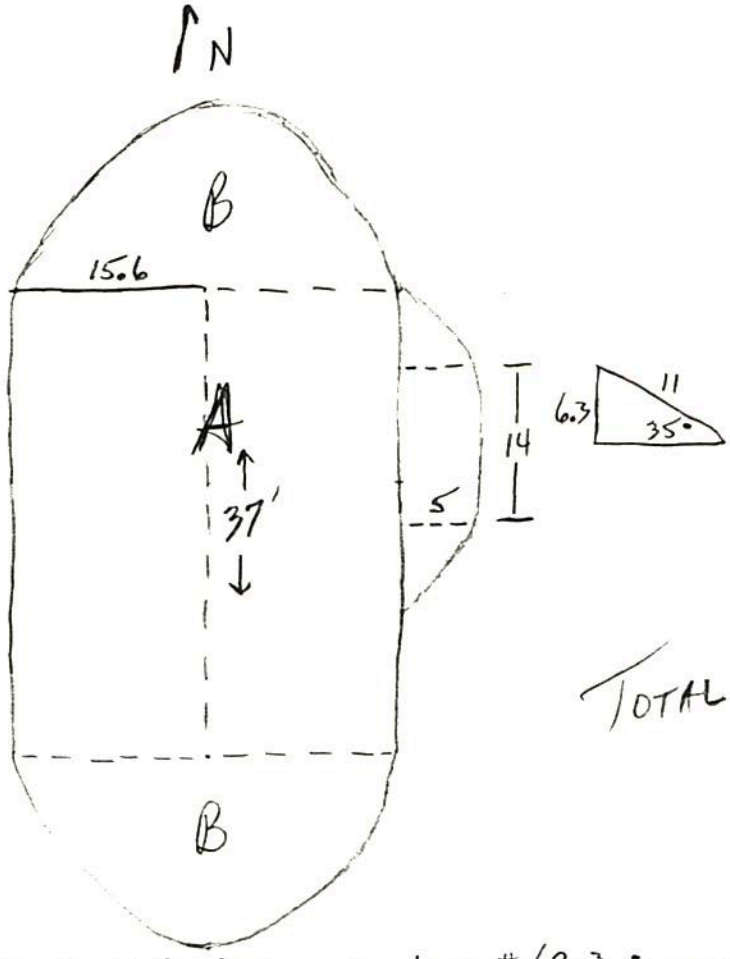




CONE = $13.6^2 \times \pi \times 11.4 \div 3 \times 125\ \#/ft^3 \div 2000 = 138.00$

TOM DARK @ MINE





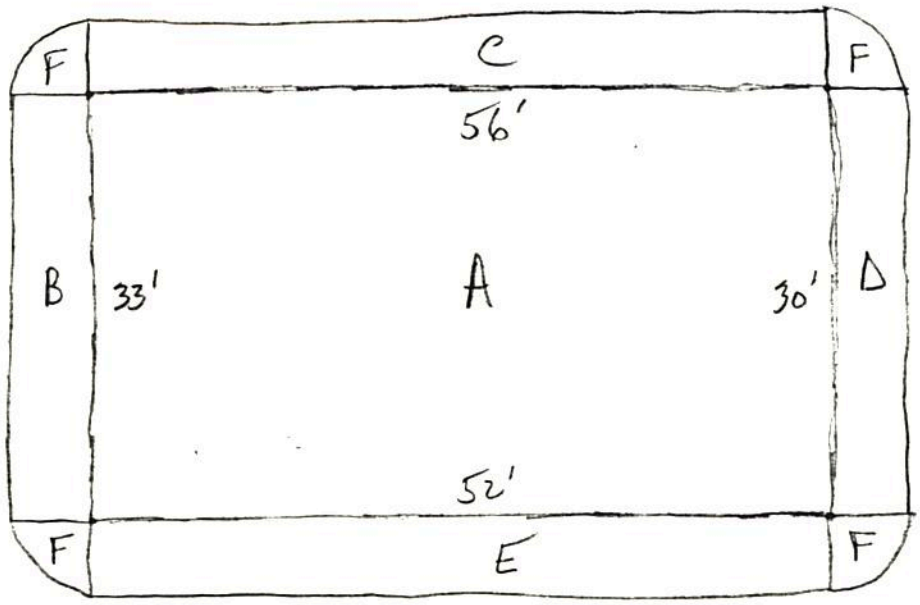
TOTAL = 584.89

A= $31.2 \times 37 \times 10.9 \div 2 \times 123\ \#/ft^3 \div 2000 = 386.93$

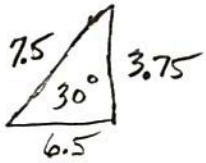
B= $15.6^2 \times \pi \times 10.9 \div 3 \times 123 \div 2000 = 170.84$

C= $5 \times 14 \times 6.3 \times 12.3 \div 2000 = 27.12$

VAN HORN 2-3-87 TDM DARK @ UPPER RELAY



N ↑



$A = \frac{56+52}{2} \times \frac{33+30}{2} \times 3.75 \times 123\ \#/ft^3 \div 2000 = 392.29$

$B = 33 \times 3.75 \times 6.5 \div 2 \times 123 \div 2000 = 24.73$

$C = 56 \times 3.75 \times 6.5 \div 2 \times 123 \div 2000 = 41.97$

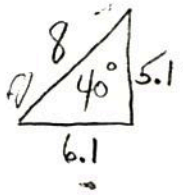
$D = 30 \times 3.75 \times 6.5 \div 2 \times 123 \div 2000 = 22.49$

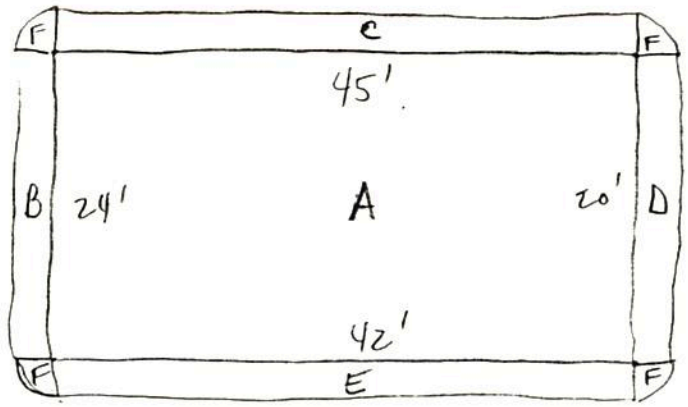
$E = 52 \times 3.75 \times 6.5 \div 2 \times 123 \div 2000 = 38.98$

$F = 6.5^2 \times \pi \times 3.75 \div 3 \times 123 \div 2000 = 10.20$

530.66

VAN HORN 2-3-87 TOM LIGHT GREY @ UPPER RELAY





N 1

$A = \frac{45+42}{2} \times \frac{24+20}{2} \times 5.1 \times 125\ \#/ft^3 \div 2000 = 305.04$

$B = 24 \times 5.1 \times 6.1 \div 2 \times 125 \div 2000 = 23.33$

$C = 45 \times 5.1 \times 6.1 \div 2 \times 125 \div 2000 = 43.75$

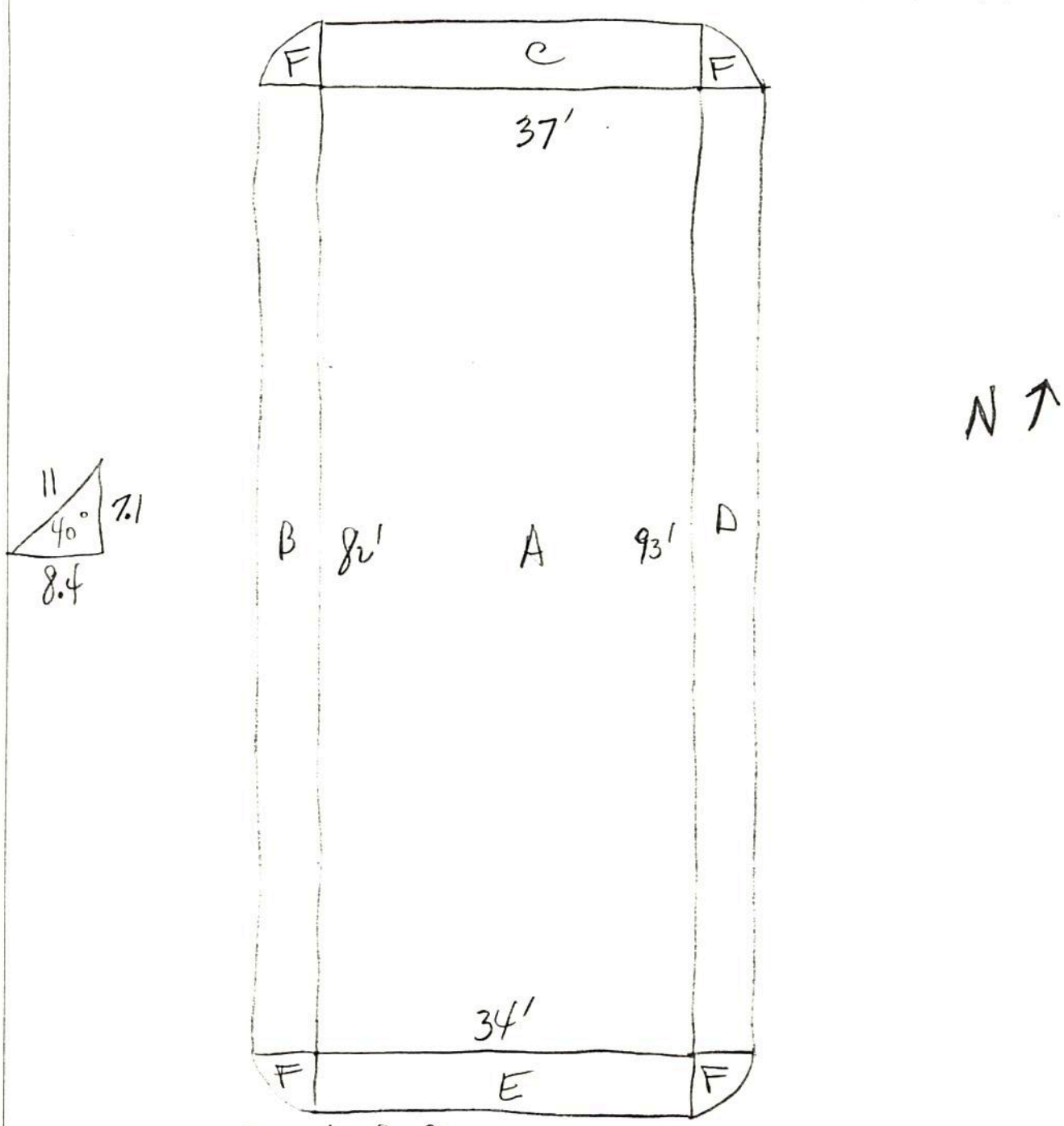
$D = 20 \times 5.1 \times 6.1 \div 2 \times 125 \div 2000 = 19.44$

$E = 42 \times 5.1 \times 6.1 \div 2 \times 125 \div 2000 = 40.83$

$F = 6.1^2 \times \pi \times 5.1 \div 3 \times 125 \div 2000 = 12.42$

444.81

VAN HORN 2-3-87 TDM DARK @ LOWER RELAY



$A = \frac{37+34}{2} \times \frac{82+93}{2} \times 7.1 \times 123\ \#/ft^3 \div 2000 = 1356.34$

$B = 82 \times 7.1 \times 8.4 \times 123 \div 2000 = 300.76$

$C = 37 \times 7.1 \times 8.4 \times 123 \div 2000 = 135.71$

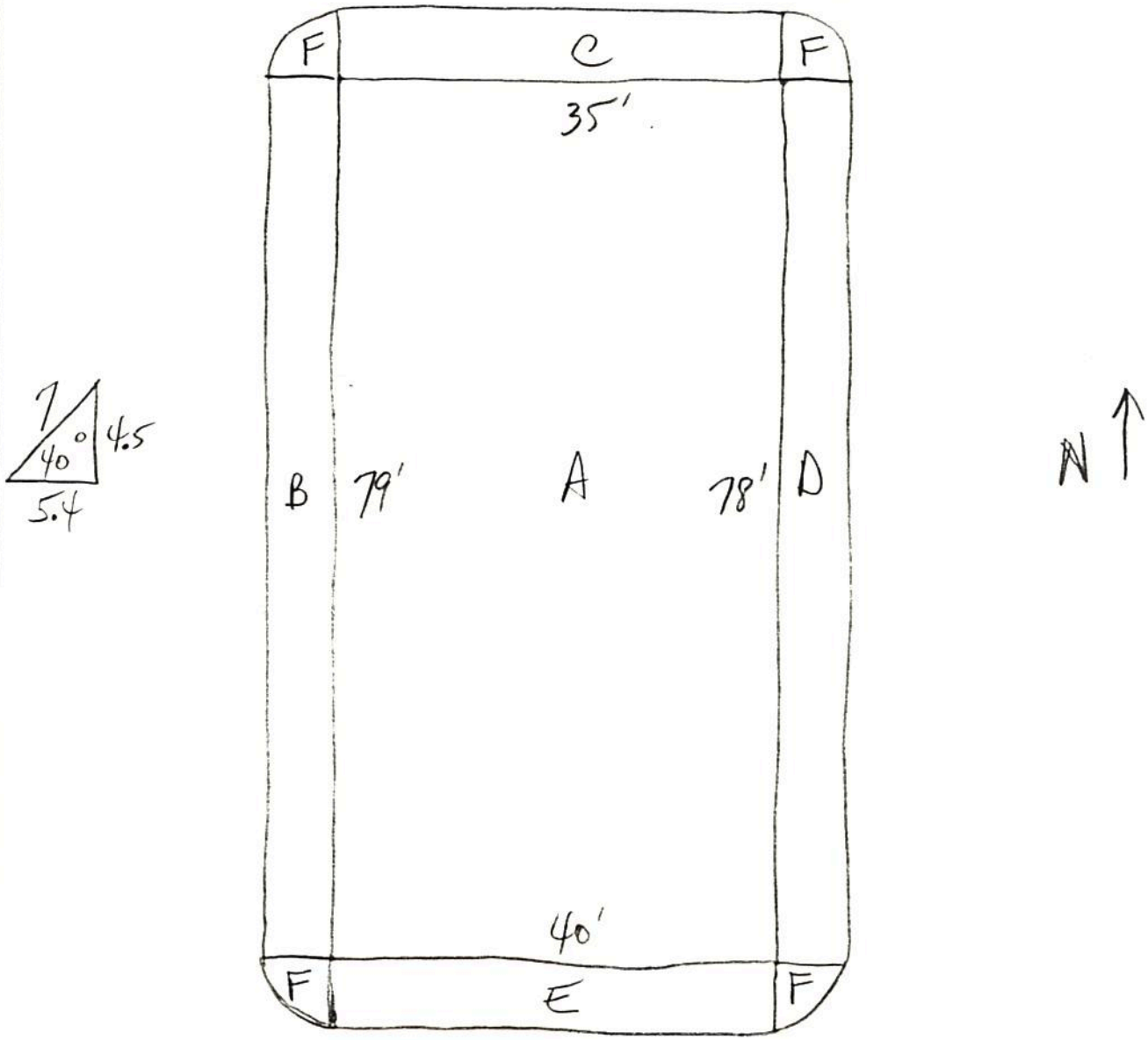
$D = 93 \times 7.1 \times 8.4 \times 123 \div 2000 = 341.11$

$E = 34 \times 7.1 \times 8.4 \times 123 \div 2000 = 124.71$

$F = 8.4^2 \times \pi \times 7.1 \div 3 \times 123 \div 2000 = 32.26$

2290.89

VAN HORN 2-3-87 TDM LIGHT GREY @ LOWER RELAY



$A = \frac{35+40}{2} \times \frac{79+78}{2} \times 4.5 \times 125\ \#/ft^3 \div 2000 = 827.93$

$B = 79 \times 4.5 \times 5.4 \div 2 \times 125 \div 2000 = 59.99$

$C = 35 \times 4.5 \times 5.4 \div 2 \times 125 \div 2000 = 26.58$

$D = 78 \times 4.5 \times 5.4 \div 2 \times 125 \div 2000 = 59.23$

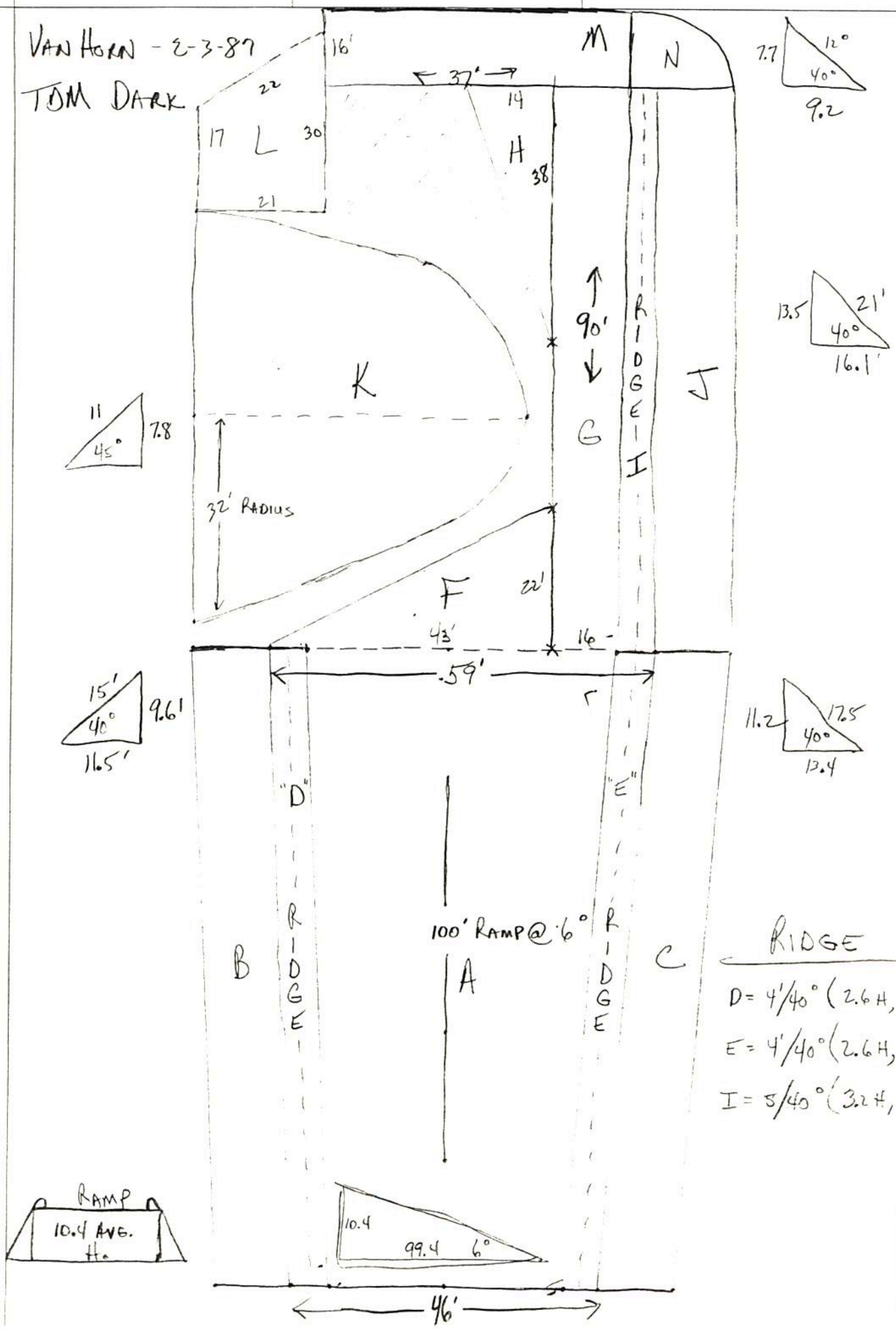
$E = 40 \times 4.5 \times 5.4 \div 2 \times 125 \div 2000 = 30.38$

$F = 5.4^2 \times \pi \times 4.5 \div 3 \times 125 \div 2000 = 8.59$

1012.70

VAN HORN - 2-3-87

TOM DARK



RIDGE

D = 4'/40° (2.6 H, 6.1 W)

E = 4'/40° (2.6 H, 6.1 W)

I = 8/40° (3.2 H, 7.7 W)

$A = \frac{59+46}{2} \times 10.4 \times 99.4 \times 123\ \#/ft^3 \div 2000 = 3337.75$

$B = 11.5 \times 9.6 \times 99.4 \div 2 \times 123 \div 2000 = 337.44$

$C = 13.4 \times 11.2 \times 99.4 \div 2 \times 123 \div 2000 = 458.73$

$D = 6.1 \times 2.6 \times 99.4 \div 2 \times 123 \div 2000 = 48.48$

$E = 6.1 \times 2.6 \times 99.4 \div 2 \times 123 \div 2000 = 48.48$

$F = 43 \times 22 \times 10.4 \div 2 \times 123 \div 2000 = 302.53$

$G = 90 \times 16 \times 13.5 \times 123 \div 2000 = 1195.56$

$H = 38 \times 14 \times 13.5 \div 2 \times 123 \div 2000 = 220.85$

$I = 7.7 \times 3.2 \times 90 \div 2 \times 123 \div 2000 = 68.19$

$J = 90 \times 13.5 \times 16.1 \div 2 \times 123 \div 2000 = 601.52$

$K = 32^2 \times \pi \times 7.8 \div 2 \times 123 \div 2000 = 771.60$

$L = \frac{17+30}{2} \times \frac{22+21}{2} \times 7.8 \times 123 \div 2000 = 242.37$

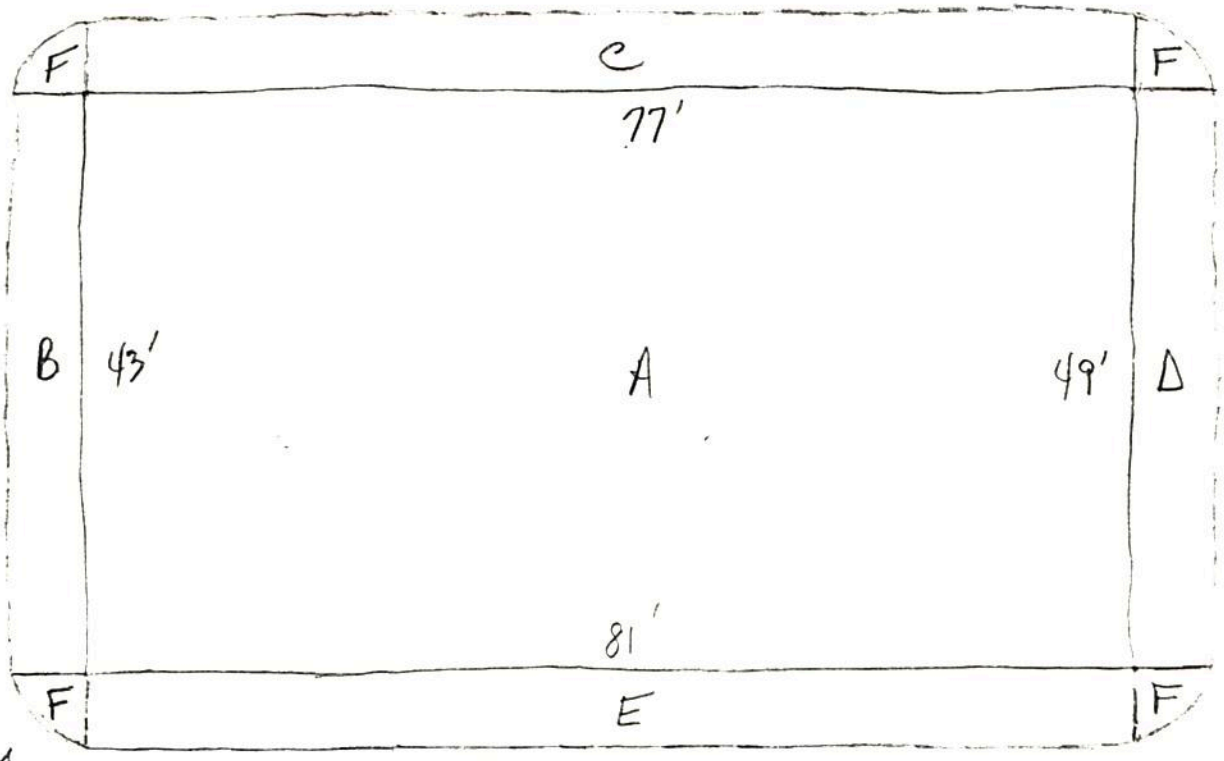
$M = 37 \times 16 \times 7.7 \times 123 \div 2000 = 280.34$

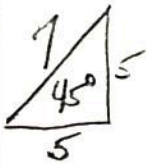
$N = 9.2^2 \times \pi \times 7.7 \div 3 \div 4 \times 123 \div 2000 = 10.49$

7924.33

TDM DARK

VAN HORN 2-3-87 TDM- WHITE @ UPPER RELAY





$A = \frac{77+81}{2} \times \frac{49+43}{2} \times 5 \times 125^{\#}/ft^3 \div 2000 = 1135.63$

$B = 43 \times 5 \times 5 \div 2 \times 125 \div 2000 = 33.59$

$C = 77 \times 5 \times 5 \div 2 \times 125 \div 2000 = 60.16$

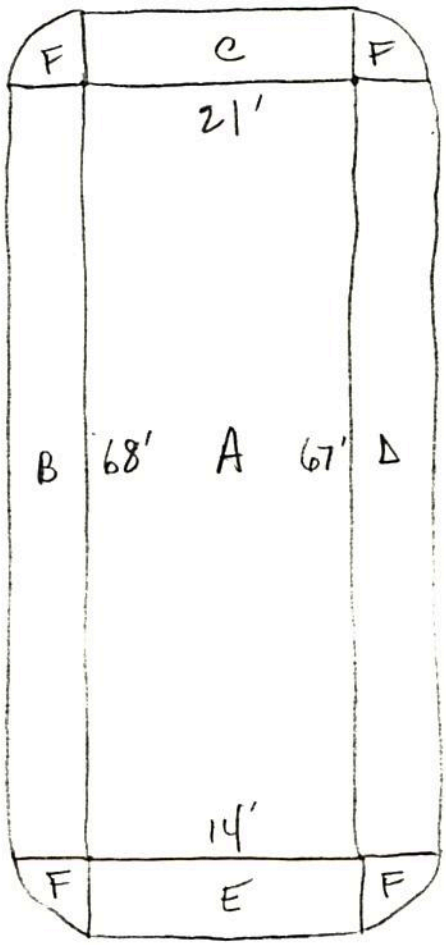
$D = 49 \times 5 \times 5 \div 2 \times 125 \div 2000 = 38.28$

$E = 81 \times 5 \times 5 \div 2 \times 125 \div 2000 = 63.28$

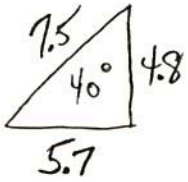
$F = 5^2 \times \pi \times 5 \div 3 \times 125 \div 2000 = 8.18$

1339.12

VAN HORN 2-3-87 TDM WHITE @ LOWER RELAY



N ↑



$A = \frac{21+14}{2} \times \frac{68+67}{2} \times 4.8 \times 125\ \#/ft^3 \div 2000 = 354.38$

$B = 68 \times 4.8 \times 5.7 \div 2 \times 125 \div 2000 = 58.14$

$C = 21 \times 4.8 \times 5.7 \div 2 \times 125 \div 2000 = 17.96$

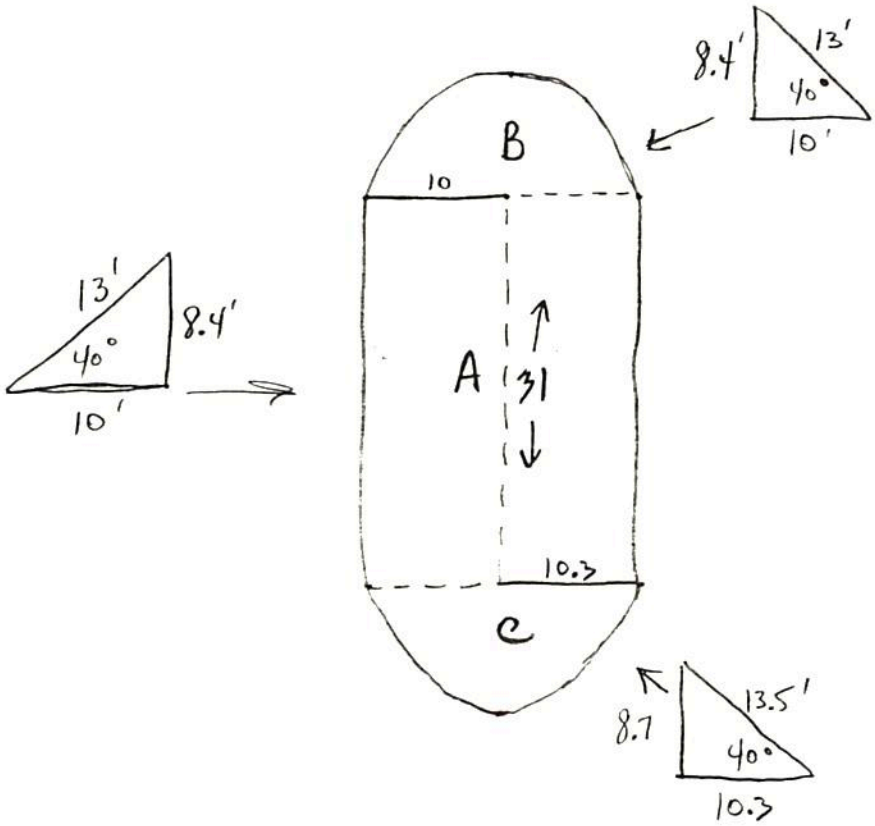
$D = 67 \times 4.8 \times 5.7 \div 2 \times 125 \div 2000 = 57.29$

$E = 14 \times 4.8 \times 5.7 \div 2 \times 125 \div 2000 = 11.97$

$F = 5.7^2 \times \pi \times 4.8 \div 3 \times 125 \div 2000 = 10.21$

509.95

VAN HORN 2-3-87 TOM WHITE @ PLANT



GROSS WT. 155

BOX WT. <30>

NET WT 125 #/ft³

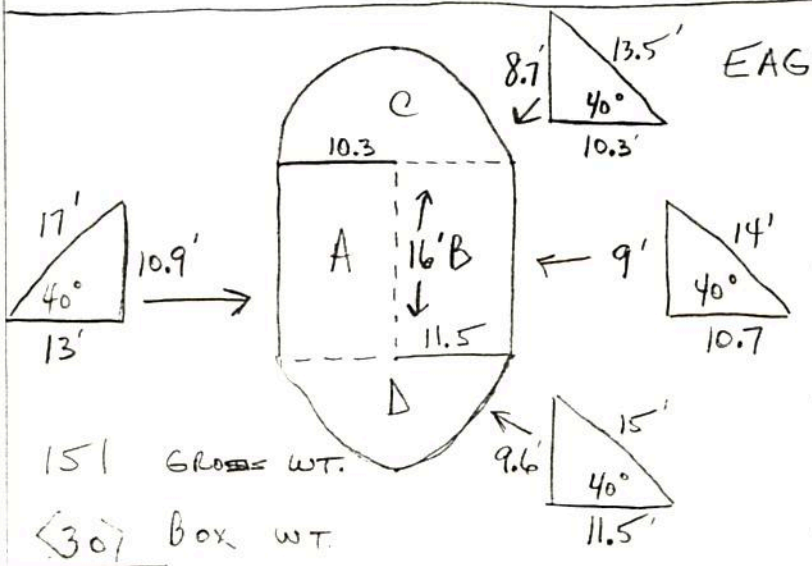
A = 31 × 8.4 × 20.3 ÷ 2 × 125 #/ft³ ÷ 2000 = 165.19

B = 10² × π × 8.4 ÷ 3 ÷ 2 × 125 ÷ 2000 = 27.49

C = 10.3² × π × 8.7 ÷ 3 ÷ 2 × 125 ÷ 2000 = 30.20

222.88

EAGLE FLAT CW @ PLANT



151 GROSS WT.

<30> BOX WT.

121 NET WT.

A = 16 × 10.9 × 13 ÷ 2 × 121 #/ft³ ÷ 2000 = 68.58

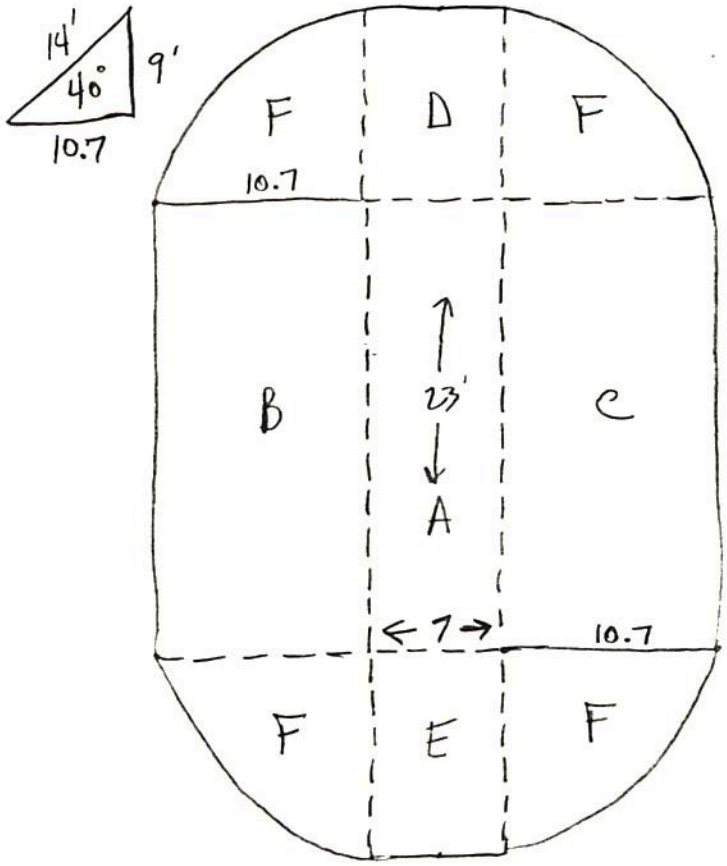
B = 16 × 9 × 10.7 ÷ 2 × 121 ÷ 2000 = 46.61

C = 10.3² × π × 8.7 ÷ 3 ÷ 2 × 121 ÷ 2000 = 29.24

D = 11.5² × π × 9.6 ÷ 3 ÷ 2 × 121 ÷ 2000 = 40.22

TOTAL = 184.65

VAN HORN 2-3-87 SPINKS DRIED CLAY @ PLANT



GROSS WT. 126

BOX WT <30>

NET WT. 96 #/ft³

A= 23 × 7 × 9 × 96 #/ft³ ÷ 2000 = 69.55

B= 23 × 10.7 × 9 ÷ 2 × 96 ÷ 2000 = 53.16

C= 23 × 10.7 × 9 ÷ 2 × 96 ÷ 2000 = 53.16

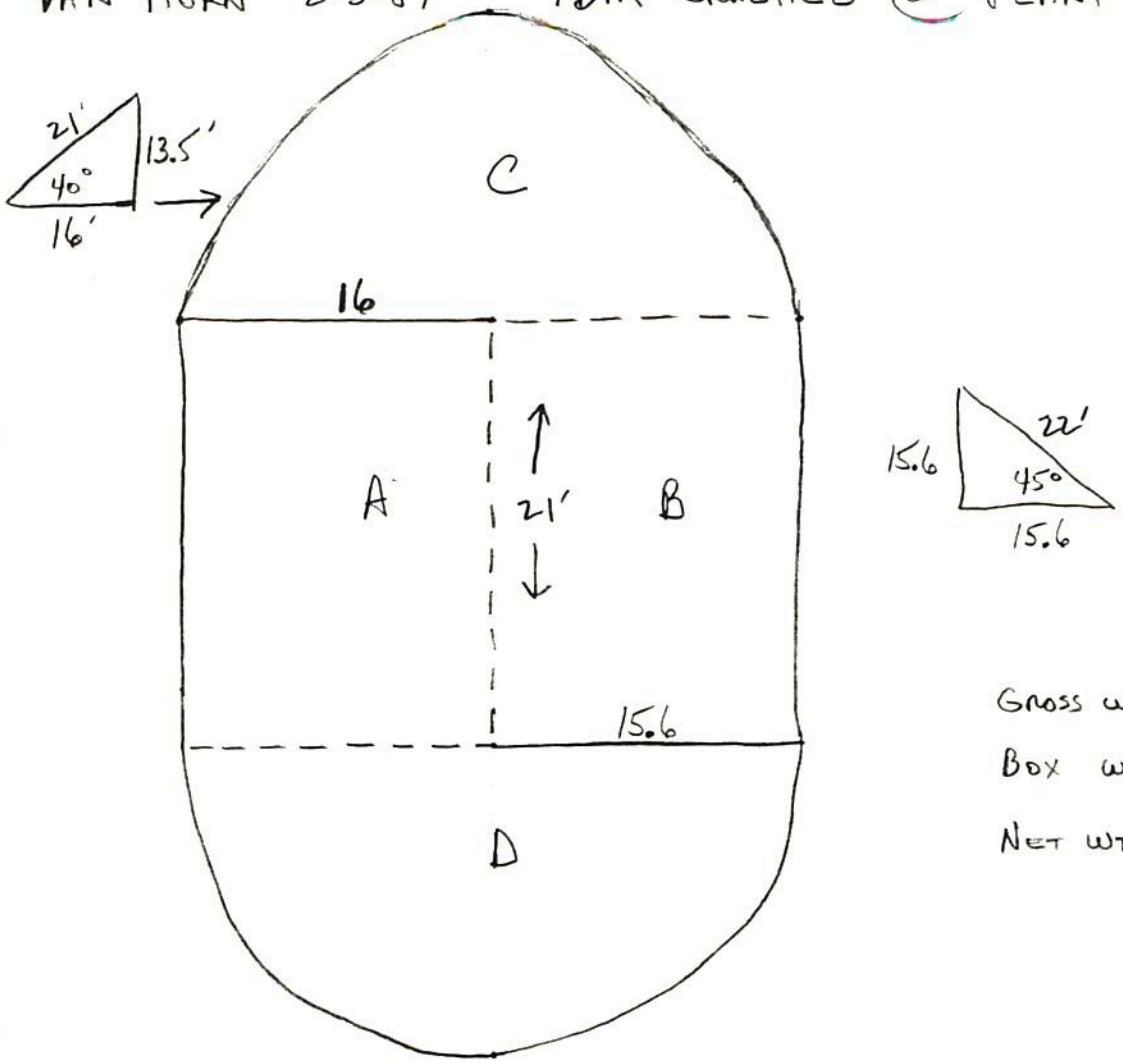
D= 7 × 9 × 10.7 ÷ 2 × 96 ÷ 2000 = 16.18

E= 7 × 9 × 10.7 ÷ 2 × 96 ÷ 2000 = 16.18

F= 10.7^2 × π × 9 ÷ 3 × 96 ÷ 2000 = 51.79

260.02

VAN HORN 2-3-87 TDM CRUSHED @ PLANT



GROSS WT 153

BOX WT <30>

NET WT. 123 #/ft³

A = 21 × 13.5 × 16 ÷ 2 × 123 #/ft³ ÷ 2000 = 139.48

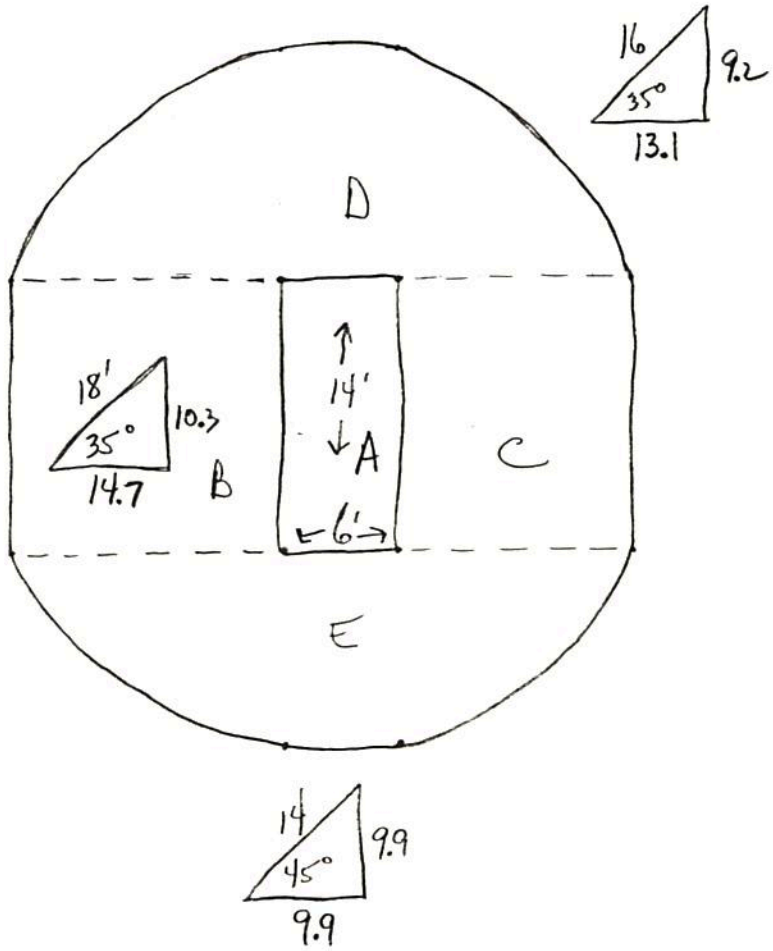
B = 21 × 15.6 × 15.6 ÷ 2 × 123 ÷ 2000 = 157.15

C = 16² × π × 13.5 ÷ 3 ÷ 2 × 123 ÷ 2000 = 111.29

D = 15.6² × π × 15.6 ÷ 3 ÷ 2 × 123 ÷ 2000 = 122.25

530.17

VAN HORN 2-3-87 TDM CRUSHED @ PLANT



GROSS WT 153

BOX WT <30>

NET WT. 123 #/ft³

A = 14 × 6 × 9.75 AVG H. × 123 #/ft³ ÷ 2000 = 50.37

B = 14 × 10.3 × 14.7 ÷ 2 × 123 ÷ 2000 = 65.18

C = 14 × 9.6 × 11.5 ÷ 2 × 123 ÷ 2000 = 47.53

D = 13.1² × π × 9.2 ÷ 3 ÷ 2 × 123 ÷ 2000 = 50.84

E = 9.9² × π × 9.9 ÷ 3 ÷ 2 × 123 ÷ 2000 = 31.24

245.16

+ 530.17

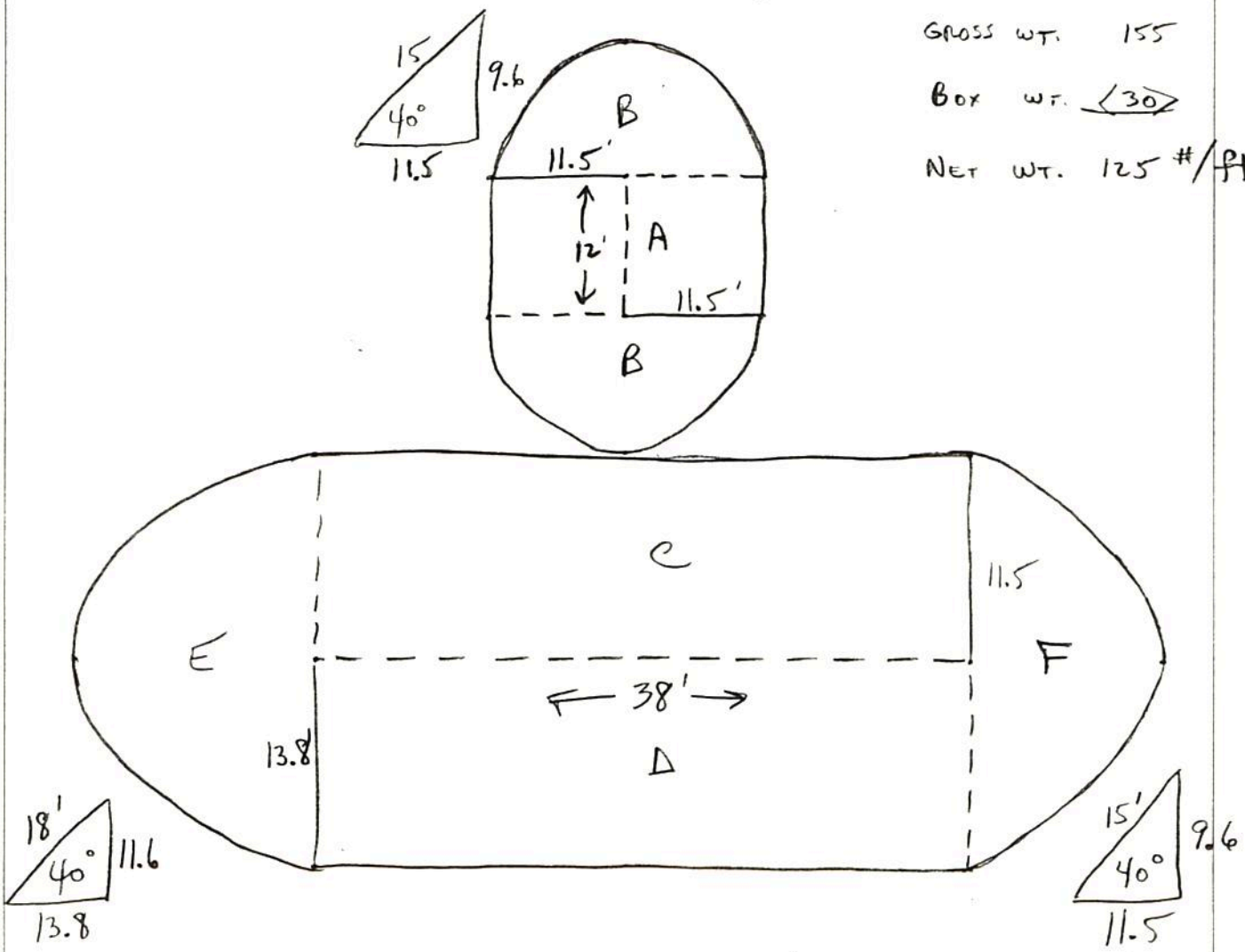
TOTAL TDM CRUSHED = 775.33

VAN HORN 2-3-87 TOM FINES @ PLANT
(MILL FEED)

GROSS WT. 155

BOX WT. <30>

NET WT. 125 #/ft3



A = 12 × 9.6 × 23 ÷ 2 × 125 #/ft³ ÷ 2000 = 82.80

B = 11.5² × π × 9.6 ÷ 3 × 125 ÷ 2000 = 83.10

C = 38 × 9.6 × 11.5 ÷ 2 × 125 ÷ 2000 = 131.10

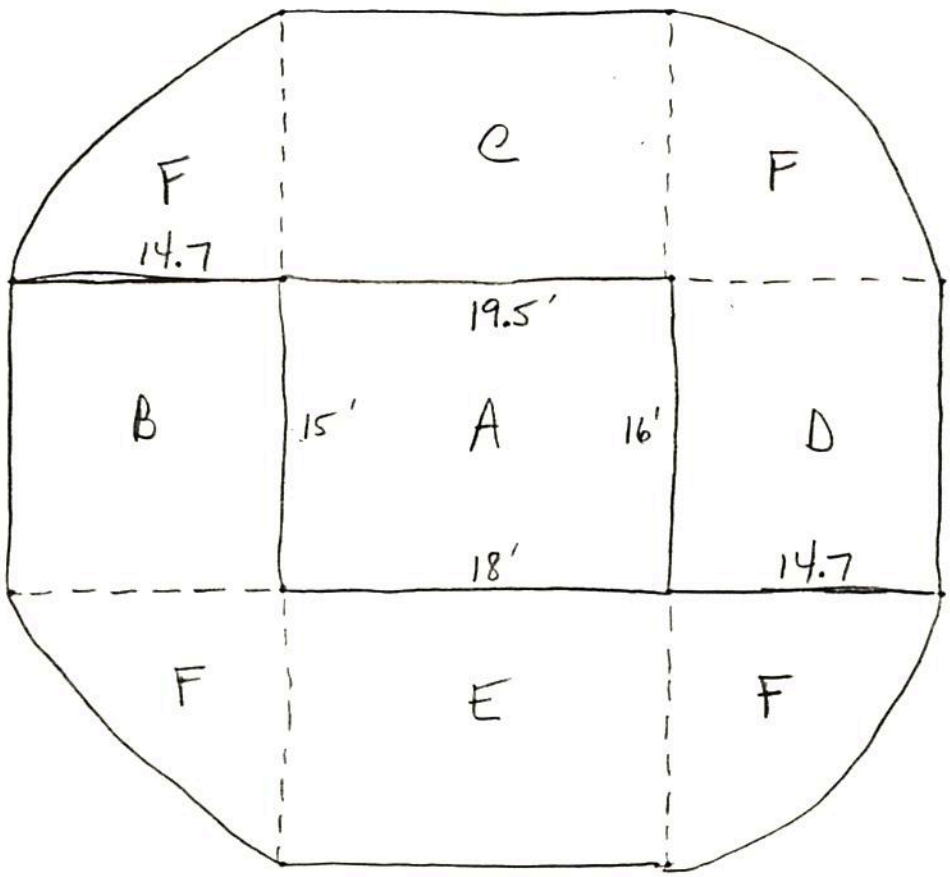
D = 38 × 11.6 × 13.8 ÷ 2 × 125 ÷ 2000 = 190.10

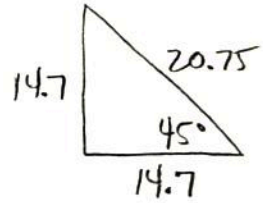
E = 13.8² × π × 11.6 ÷ 3 ÷ 2 × 125 ÷ 2000 = 72.29

F = 11.5² × π × 9.6 ÷ 3 ÷ 2 × 125 ÷ 2000 = 41.55

600.94

VAN HORN 2-3-87 CALCINED TOM @ PLANT





GROSS WT. 124

BOX WT. <30>

NET WT 94 #/ft³

$A = \frac{18+19.5}{2} \times \frac{15+16}{2} \times 14.7 \times 94\ \#/ft^3 \div 2000 = 200.79$

$B = 15 \times 14.7 \times 14.7 \div 2 \times 94 \div 2000 = 76.17$

$C = 19.5 \times 14.7 \times 14.7 \div 2 \times 94 \div 2000 = 99.02$

$D = 16 \times 14.7 \times 14.7 \div 2 \times 94 \div 2000 = 81.25$

$E = 18 \times 14.7 \times 14.7 \div 2 \times 94 \div 2000 = 91.41$

$F = 14.7^2 \times \pi \times 14.7 \div 3 \times 94 \div 2000 = 156.34$

704.98