Message

From: SWMM-USERS [SWMM-USERS@LISTSERV.UOGUELPH.CA]
on behalf of Robert Dickinson Ex. 6 Personal Privacy (PP)
Sent: 3/1/2020 2:38:03 AM
To: SWMM-USERS@LISTSERV.UOGUELPH.CA
Subject: [SWMM-USERS] Groundwater results interpretation

Hello Belen,

The EPA SWMM 5 GUI (written in Delphi and a clear, easy to understand and robust view of the inp and out files of SWMM 5) has the following menu structure at the top.
1. File
2. View
3, Edit
4. Project/Summary/Details
5. Report/Status/Summary/Graph/Table/Statistics
6. Tools
7. Windows
8. Help

You need to view the Report/Status menu to see the Status report. The Report/Summary shows you the Runoff, LID, GW and other summary tables. If you use Matlab, PySWMM, run the SWMM5 console program or other non UX tools for SWMM5 you can find the status report and summary tables in the text RPT file for your model.

Regards,
Robert Dickinson
Innovyze Inc.

From: SWMM-USERS On Behalf Of Belen Aguirre
Sent: Sunday, March 01, 2020 02:00 AM [UTC]
Subject: Groundwater results interpretation

Thank you so much, Mitch, for all your suggestions. I have re-run the model with 30 min rainfall resolution and routed to pervious. I am working on the simplification and the errors that I get.

The study area has a Mediterranean climate, high temperatures and high evaporation registers. Also, sandy soils that generate high infiltration on pervious areas. In this case, initial pervious abstraction should be around 8 mm right?

I cannot find through the EPA GUI to review the status report, can you give me a hint on this?

Thank you again for your help and time!
Belen.

From: SWMM-USERS On Behalf Of Robert Dickinson
Sent: Saturday, February 29, 2020 11:42 AM [UTC]
Subject: Groundwater results interpretation

In addition to Mitch's great comments I have the following based on what I could find in your large posting:
1. In 99 percent of your Subcatchments the evaporation is 100 times greater than the infiltration in the table,
2. The output of Subcarchment S18_4 seems to have #IND so please look at the Subcatchment GW data
3. Subcatchment S43 has 99 percent of your overall infiltration in the model or 1618 mm
4. Please looks the Subcatchment and GW summary tables - you will catch the errors
5. You have very little GW flow and a few Subcatchment have large Runon volumes but you probably intended that to happen

Use Mitch suggestion and try to make a smaller model for testing the problem Subcatchments.

From: SWMM-USERS On Behalf Of Mitchell Heineman
Sent: Friday, February 28, 2020 07:59 PM [UTC]
Subject: Groundwater results interpretation

First, a few broad suggestions:

1. Simplify, simplify, simplify when debugging and building understanding. E.g. if the problem is in hydrology, just run the hydrologic component of the model: set IGNORE_ROUTING to YES in the [Options] section
2. Almost never use SWMM with daily precipitation data. If the best thing you have is daily, test with an hourly or better dataset from somewhere with similar climate, or synthetically disaggregate the data (e.g. using Transform | Short Duration Disaggregation in my NetSTORM software).
3. Please don't paste large files into SWMM-USERS messages
4. Unless you have very detailed hydrologic data, it is not worth differentiating runoff surface Manning's N and initial abstraction by subcatchment. Use the same values system-wide (e.g. 0.02 and 0.08 for impervious/pervious N, 1 mm initial impervious abstraction, 2 mm pervious abstraction)
5. For typical urban subcatchments, use the PERVIOUS routing option (not the OUTLET option) and estimate percent routed using the Sutherland method described in the SWMM hydrology manual.
6. Examine the status report! A good model should have few or no warnings. If you're put off by the size of the report, turn off the input summary if you had it turned on. Use the EPA GUI to review the status report contents - it does a nice job of presenting the main summary in one place and each summary table on its own.

I ran your model by inserting my own precipitation and temperature datasets. The model performs acceptably, and some groundwater flow is generated. Most subcatchments generate no groundwater flow though because there's minimal infiltration from the surface and because evaporation greatly exceeds infiltration. This is evident in the Continuity tables. In my run of your model, I simulated 1187 mm of rainfall over a year, but only 41 mm of that infiltrated. In the subsurface, there was 300 mm of evaporation.

```
  **************************        Volume         Depth
  Runoff Quantity Continuity     hectare-m            mm
  **************************     ---------       -------
  Initial LID Storage ......         0.142         3.136
  Total Precipitation ......        53.692      1187.704
  Evaporation Loss .........        14.265       315.562
  Infiltration Loss ........         1.870        41.357
  Surface Runoff ...........        37.983       840.208
  Final Storage ............         0.142         3.136
  Continuity Error (%) .....        -0.791


  **************************        Volume         Depth
  Groundwater Continuity         hectare-m            mm
  **************************     ---------       -------
  Initial Storage ..........       218.151      5950.635
  Infiltration .............         1.864        50.848
  Upper Zone ET ............        10.975       299.381
  Lower Zone ET ............         0.000         0.008
  Deep Percolation .........         0.537        14.639
  Groundwater Flow .........         1.570        42.834
  Final Storage ............       206.208      5624.846
  Continuity Error (%) .....         0.330
```

From: SWMM-USERS On Behalf Of Robert Dickinson
Sent: Friday, February 28, 2020 07:03 PM [UTC]
Subject: Groundwater results interpretation

Thanks for sharing, Belen, but most of your data is not usable as the time series data is external to the inp file or if it is in the inp file there are too many lines. Your model (from the sections I can see) is very complex and to replicate the odd results you probably need to put the model, model inputs on Google Drive (or some other location) and then you can share it with the SWMM List Server groups. Your model network data is too large to post here.

From: SWMM-USERS On Behalf Of Belen Aguirre
Sent: Friday, February 28, 2020 02:28 PM [UTC]
Subject: Groundwater results interpretation

Thank you very much for your reply!

I send the details for:

A. My ground components model setting

```
[OPTIONS]
;;Options            Value
;;------------------ ------------
FLOW_UNITS           CMS
```

```
INFILTRATION         MODIFIED_HORTON
FLOW_ROUTING         DYNWAVE
LINK_OFFSETS         ELEVATION
MIN_SLOPE            0
ALLOW_PONDING        NO
SKIP_STEADY_STATE    NO
START_DATE           01/01/2014
START_TIME           00:00:00
REPORT_START_DATE    01/01/2014
REPORT_START_TIME    00:00:00
END_DATE             12/31/2014
END_TIME             00:00:00
SWEEP_START          01/01
SWEEP_END            12/31
DRY_DAYS             0
REPORT_STEP          00:01:00
WET_STEP             00:05:00
DRY_STEP             00:05:00
ROUTING_STEP         5
RULE_STEP            00:00:00
INERTIAL_DAMPING     PARTIAL
NORMAL_FLOW_LIMITED  BOTH
FORCE_MAIN_EQUATION  H-W
VARIABLE_STEP        0.75
LENGTHENING_STEP     0
MIN_SURFAREA         0
MAX_TRIALS           8
HEAD_TOLERANCE       0.0015
SYS_FLOW_TOL         5
LAT_FLOW_TOL         5
MINIMUM_STEP         0.5
THREADS              4<!-- Standard PRE tag rules -->

[EVAPORATION]
;;Type          Parameters
;;------------- ----------
TIMESERIES   DailyEvaporation
DRY_ONLY     YES<!-- Standard PRE tag rules -->

[TEMPERATURE]
TIMESERIES   MeanTemperature
WINDSPEED    MONTHLY    19.7 19.05 17.35 14.7 12.85 13.2 13.45 14.5 15.85 19.4 19.65 16.45
SNOWMELT               34 0.5 0.6 0.0 50.0 0.0
ADC          IMPERVIOUS 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
ADC          PERVIOUS   1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0<!-- Standard PRE tag rules -->

[RAINGAGES]
;;                       Rain      Time   Snow   Data
;;Name                   Type      Intrvl Catch  Source
;;---------------------- --------- ------ ------ ----------
Chicago_3h               INTENSITY 0:05   1.0    TIMESERIES Chicago_3h
DailyRainfall_Canning    VOLUME    24:00  1.0    TIMESERIES DailyRainfall_Canning
Florida_Type_II_1mm      INTENSITY 0:30   1.0    TIMESERIES Florida_Type_II_1mm
NOAA_Type_A_1mm          INTENSITY 0:06   1.0    TIMESERIES NOAA_Type_A_1mm
Precipitation_Net15012018 INTENSITY 0:30   1.0    TIMESERIES Precipitation_Net15012018
RainEvent_19072009       INTENSITY 0:30   1.0    TIMESERIES RainEvent_19072009<!-- Standard PRE tag
rules -->

[SUBCATCHMENTS]
;;                                                Total    Pcnt.             Pcnt.    Curb     Snow
;;Name           Raingage         Outlet           Area     Imperv   Width    Slope    Length   Pack
;;-------------- ---------------- ---------------- -------- -------- -------- -------- -------- --------
S1               DailyRainfall_Canning J80         0.3717   52.136   37.17    0.5      0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
220-
03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177528809&amp;sdata=QC209AZWAViFbuuknvvDWQLjq5BmyYoVnn1QjhGjUvY%3D&amp;rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S10              DailyRainfall_Canning S43_7       0.1883   100      47.075   0.05     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177528809&sdata=QC209AZWAViFbuuknvvDWQLjq5BmyYoVnn1QjhGjUvY%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S11 DailyRainfall_Canning J80 0.1631 100 40.775 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177528809&sdata=QC209AZWAViFbuuknvvDWQLjq5BmyYoVnn1QjhGjUvY%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S12 DailyRainfall_Canning J9 0.328 85.661 68.95 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177528809&sdata=QC209AZWAViFbuuknvvDWQLjq5BmyYoVnn1QjhGjUvY%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S13 DailyRainfall_Canning S23_4 0.0623 48.572 70 0.5 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177528809&sdata=QC209AZWAViFbuuknvvDWQLjq5BmyYoVnn1QjhGjUvY%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S14 DailyRainfall_Canning J9 0.1929 53.816 167.216 3.2 0
S15_1 DailyRainfall_Canning S15_10 0.0772 38.009 12.254 3.828 0
S15_10 DailyRainfall_Canning J24 0.093 37.412 28.822 3.828 0
S15_12 DailyRainfall_Canning J2312 0.1353 64.066 30.75 3.828 0
S15_2 DailyRainfall_Canning J20 0.7757 65.844 58.647 3.828 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S15_3 DailyRainfall_Canning J11 0.1895 100 48.55 0.05 0
S15_4 DailyRainfall_Canning J17 0.1955 56.802 27.153 3.828 0
S15_5 DailyRainfall_Canning J18 0.6841 67.95 51.721 3.828 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177528809&sdata=QC209AZWAViFbuuknvvDWQLjq5BmyYoVnn1QjhGjUvY%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S15_6 DailyRainfall_Canning S29_1 0.1401 100 35.025 0.05 0
S15_7 DailyRainfall_Canning J2181 1.5126 66.6 114.36 3.828 0
S15_8 DailyRainfall_Canning J26 0.0604 37.965 14.732 3.828 0
S15_9 DailyRainfall_Canning J23 0.3905 26.281 41.543 3.828 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S16 DailyRainfall_Canning J13 0.0564 100 14.1 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S17 DailyRainfall_Canning J2918 0.1816 100 45.4 0.05 0
S18_2 DailyRainfall_Canning J32 0.6703 98.672 67.03 0.05 0
S18_3 DailyRainfall_Canning J30 0.203 100 20.3 0.05 0
S18_4 DailyRainfall_Canning J30 0.2343 100 41.839 0.5 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S19 DailyRainfall_Canning J28 0.2406 100 60.15 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S2 DailyRainfall_Canning J79 1.169 98.794 276.274 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S20 DailyRainfall_Canning J3 0.0728 100 18.2 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S21 DailyRainfall_Canning J26 0.1829 100 45.725 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
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reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S22 DailyRainfall_Canning J7 0.0773 100 152.165 2.218 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S23 DailyRainfall_Canning J25 0.1345 58.387 59.999 0.5 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0

;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S23_1 DailyRainfall_Canning J4 0.9466 65.317 167.211 3.2 0
S23_3 DailyRainfall_Canning J12 0.5648 60.553 54.499 3.2 0
S23_4 DailyRainfall_Canning J6 1.1682 56.237 112.723 3.2 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S24 DailyRainfall_Canning S15_9 0.0596 100 14.9 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S25 DailyRainfall_Canning J57 0.1097 100 27.425 0.05 0
S26_1 DailyRainfall_Canning J2787 0.141 56.387 23.016 3.235 0
S26_3 DailyRainfall_Canning J2909 0.958 60.166 156.378 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S29_1 DailyRainfall_Canning J9 0.4583 45.588 200.894 3.24 0
S29_10 DailyRainfall_Canning J2931 1.8356 55.854 130.724 2.945 0
S29_11 DailyRainfall_Canning J2931 0.0383 93.738 2.728 2.945 0
S29_12 DailyRainfall_Canning J40 0.627 55.88 44.652 2.945 0
S29_13 DailyRainfall_Canning J35 0.6475 56.911 46.112 2.945 0
S29_14 DailyRainfall_Canning J48 0.7997 54.491 56.951 2.945 0
S29_15 DailyRainfall_Canning J29_14 0.4343 60.746 101 0.05 0
S29_17 DailyRainfall_Canning S29_14 0.0994 100 23.116 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S29_2 DailyRainfall_Canning J2754 0.3117 98.902 261.449 3.24 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S29_3 DailyRainfall_Canning J11 0.827 59.354 200.894 3.24 0
S29_5 DailyRainfall_Canning J79 0.2214 57.605 15.767 2.945 0
S29_7 DailyRainfall_Canning J63 0.2047 64.043 14.578 2.945 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S29_8 DailyRainfall_Canning J13 0.6318 65.957 200.89 3.24 0
S29_9 DailyRainfall_Canning J83 0.1842 47.154 13.118 2.945 0

S3 DailyRainfall_Canning S46_5 0.4046 38.659 279.671 3.38 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S30 DailyRainfall_Canning J355 0.1272 93.347 29.475 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S31 DailyRainfall_Canning J2712 0.0559 90.128 11.125 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S32 DailyRainfall_Canning J2717 0.131 100 32.75 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S33 DailyRainfall_Canning J2717 0.2423 100 60.575 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S34 DailyRainfall_Canning J2722 0.3585 100 89.625 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S35 DailyRainfall_Canning J2692 0.3274 100 81.85 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S36 DailyRainfall_Canning J46 0.0404 100 10.1 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177538768&sdata=iPhy0qM0Bo1Iol0sKm2C7X%2B3EL9%2FXbLi00mTjgBDzks%3D&
reserved=0

;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S37 DailyRainfall_Canning S46_5 0.0681 72.125 40.059 3.38 0
S37_1 DailyRainfall_Canning J7 0.4128 62.153 50.924 2.218 0
S37_10 DailyRainfall_Canning J22 0.048 13.973 16.552 2.218 0
S37_11 DailyRainfall_Canning J2510 0.2028 45.489 25.018 2.218 0
S37_12 DailyRainfall_Canning J2510 0.0768 29.908 9.474 2.218 0
S37_2 DailyRainfall_Canning J4 0.2283 57.225 94.452 2.218 0
S37_3 DailyRainfall_Canning J4 0.1395 46.874 57.714 2.218 0
S37_4 DailyRainfall_Canning J16 0.3603 76.393 44.447 2.218 0
S37_8 DailyRainfall_Canning J1 0.1327 22.603 16.37 2.218 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S38 DailyRainfall_Canning S43_7 0.1879 100 46.975 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S39 DailyRainfall_Canning S63_9 0.4715 72.469 74.725 0.05 0
S4 DailyRainfall_Canning J2722 0.3988 100 87.381 0.064 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S40 DailyRainfall_Canning S63_9 0.1823 98.986 46.075 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S41 DailyRainfall_Canning J2931 0.2732 100 68.3 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S42 DailyRainfall_Canning J1040 0.4108 100 102.7 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S43 DailyRainfall_Canning J1969 1.6677 22.429 236.175 4.358 0
S43_2 DailyRainfall_Canning J56 0.5507 25.345 28.644 5.22 0
S43_4 DailyRainfall_Canning J46 0.3177 18.768 16.525 5.22 0
S43_5 DailyRainfall_Canning S43_7 0.9576 42.96 49.808 5.22 0
S43_6 DailyRainfall_Canning S43 0.5222 27.26 27.162 5.22 0
S43_7 DailyRainfall_Canning J46 0.5973 56.609 31.068 5.22 0

S43_9 DailyRainfall_Canning S43 0.8962 46.849 46.615 5.22 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S44 DailyRainfall_Canning S43 0.7133 100 178.325 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S45 DailyRainfall_Canning J2510 0.0497 100 12.425 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S46 DailyRainfall_Canning J7 0.0773 100 19.325 0.05 0
S46_1 DailyRainfall_Canning J2771 0.5576 54.56 68.572 3.38 0
S46_10 DailyRainfall_Canning S63_3 0.1148 66.117 35.104 3.38 0
S46_2 DailyRainfall_Canning J2594 0.3392 37.978 41.714 3.38 0
S46_3 DailyRainfall_Canning S63_14 0.3311 70.857 101.245 3.38 0
S46_4 DailyRainfall_Canning J16 0.5264 61.818 64.735 3.38 0
S46_5 DailyRainfall_Canning J2722 0.4568 50.359 35.969 3.38 0
S46_6 DailyRainfall_Canning J2678 0.2967 52.181 36.487 3.38 0
S46_7 DailyRainfall_Canning J2722 0.5254 67.845 64.612 3.38 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S47 DailyRainfall_Canning J2839 0.2228 100 55.7 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S48 DailyRainfall_Canning J2847 0.1209 100 30.225 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S49 DailyRainfall_Canning J5 0.1499 100 37.475 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.

S5 DailyRainfall_Canning J63 0.2259 100 56.475 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S50 DailyRainfall_Canning J5 0.1966 100 49.15 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S51 DailyRainfall_Canning J3 0.1831 100 45.775 0.05 0
S52_1 DailyRainfall_Canning S43 0.9201 31.473 59.154 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S52_2 DailyRainfall_Canning S43 0.8425 48.211 304.437 2.945 0
S52_3 DailyRainfall_Canning J2909 0.2611 61.555 16.786 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S52_4 DailyRainfall_Canning J70 0.3919 57.11 304.436 2.945 0
S52_6 DailyRainfall_Canning J2838 0.8612 73.374 55.367 3.235 0
S52_7 DailyRainfall_Canning J2860 0.7479 50.071 48.083 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S53 DailyRainfall_Canning J4 0.2626 100 65.65 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S54 DailyRainfall_Canning S15_7 0.1028 100 25.7 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S55 DailyRainfall_Canning S15_7 0.0122 100 3.05 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S56 DailyRainfall_Canning S15_7 0.0722 100 18.05 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177548723&sdata=hPhT%2ByKXM0L2UMQ22oU2OxMP9OxPN6cIEZf3p7ndMXw%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S57 DailyRainfall_Canning J13 0.056391 100 200.894 3.24 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177558678&sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S59 DailyRainfall_Canning J13 0.1094 97.656 36.326 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177558678&sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_1 DailyRainfall_Canning J355 0.6135 38.355 180.24 4.534 0
S63_11 DailyRainfall_Canning J2728 0.2498 61.02 35.183 4.534 0
S63_12 DailyRainfall_Canning J2822 0.131 56.273 32.75 4.534 0
S63_13 DailyRainfall_Canning J2794 0.4345 48.85 52.988 4.534 0
S63_14 DailyRainfall_Canning J2757 0.1862 59.93 46.55 4.534 0
S63_15 DailyRainfall_Canning J2709 0.2832 50.726 28.32 4.534 0
S63_2 DailyRainfall_Canning J2855 1.2038 26.59 75.703 4.534 0
S63_3 DailyRainfall_Canning J2719 0.2036 65.386 30.848 4.534 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177558678&sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_4 DailyRainfall_Canning S63_9 0.112 89.578 11.2 4.534 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177558678&sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_5 DailyRainfall_Canning S63_1 0.0042 90.878 5.886 4.534 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177558678&sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_6 DailyRainfall_Canning J2785 0.2827 52.709 180.236 4.534 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_7            DailyRainfall_Canning J1969       0.0761   35.47    180.246  4.534    0
S63_8            DailyRainfall_Canning J2730       0.1497   54.886   49.9     4.534    0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177558678&amp;sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&amp;re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_9            DailyRainfall_Canning J2785       0.2791   36.183   34.037   4.534    0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177558678&amp;sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&amp;re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S7               DailyRainfall_Canning J2757       0.123    100      30.75    0.05     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177558678&amp;sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&amp;re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S8               DailyRainfall_Canning J2755       0.1461   100      36.525   0.05     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177558678&amp;sdata=KmEGql90OI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&amp;re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S9               DailyRainfall_Canning S43_7       0.1578   100      39.45    0.05     0<!-- Standard PRE
tag rules -->

[SUBAREAS]
;;Subcatchment   N-Imperv   N-Perv     S-Imperv   S-Perv     PctZero    RouteTo    PctRouted
;;-------------- ---------- ---------- ---------- ---------- ---------- ---------- ----------
S1               0.03       0.089      1.033      5.103      25         OUTLET
S10              0.014      0          1.25       0          0          OUTLET
S11              0.014      0          1.25       0.001      0          OUTLET
S12              0.021      0          1.051      1.275      0          OUTLET
S13              0.03       0.016      0.882      2.879      25         OUTLET
S14              0.038      0          0.611      4.103      25         OUTLET
S15_1            0.045      0.009      0.473      5.435      25         OUTLET
S15_10           0.046      0          0.381      5.563      25         OUTLET
S15_12           0.02       0.142      1.34       5.112      25         OUTLET
S15_2            0.015      0.177      1.618      5          25         OUTLET
S15_3            0.014      0          1.25       0          0          OUTLET
S15_4            0.023      0.136      1.408      4.803      25         OUTLET
S15_5            0.014      0.174      1.578      5          25         OUTLET
S15_6            0.014      0          1.25       0          0          OUTLET
S15_7            0.019      0.144      1.303      5.173      25         OUTLET
S15_8            0.046      0          0.388      5.514      25         OUTLET
S15_9            0.051      0.004      0.27       6.514      25         OUTLET
S16              0.014      0          1.25       0          0          OUTLET
S17              0.014      0          1.25       0          0          OUTLET
S18_2            0.016      0.006      1.227      0.49       0          OUTLET
S18_3            0.015      0          1.221      0.187      0          OUTLET
S18_4            0.027      0.084      0.97       4.923      25         OUTLET
S19              0.014      0          1.25       0          0          OUTLET
S2               0.015      0          1.233      0.107      0          OUTLET
S20              0.014      0          1.25       0          0          OUTLET
S21              0.014      0          1.25       0          0          OUTLET
```

S22	0.014	0	1.25	0	25	OUTLET	
S23	0.032	0.022	0.891	3.503	25	OUTLET	
S23_1	0.022	0.118	1.221	4.796	25	OUTLET	
S23_3	0.031	0.033	0.846	3.855	25	OUTLET	
S23_4	0.027	0.105	1.154	4.847	25	OUTLET	
S24	0.014	0	1.25	0	0	OUTLET	
S25	0.014	0	1.25	0	0	OUTLET	
S26_1	0.025	0.116	1.409	4.073	25	OUTLET	
S26_3	0.028	0.075	1.005	4.45	25	OUTLET	
S29_1	0.038	0.05	0.803	4.778	25	OUTLET	
S29_10	0.031	0.063	0.936	4.521	25	OUTLET	
S29_11	0.017	0	1.163	0.557	25	OUTLET	
S29_12	0.032	0.06	0.95	4.496	25	OUTLET	
S29_13	0.033	0.04	0.747	4.659	25	OUTLET	
S29_14	0.033	0.048	0.782	4.756	25	OUTLET	
S29_15	0.016	0.005	1.237	0.354	0	OUTLET	
S29_17	0.016	0	1.183	0.429	0	OUTLET	
S29_2	0.014	0	1.249	0.008	25	OUTLET	
S29_3	0.027	0.092	1.099	4.544	25	OUTLET	
S29_5	0.031	0.055	0.787	4.927	25	OUTLET	
S29_7	0.023	0.105	1.199	4.44	25	OUTLET	
S29_8	0.03	0.015	0.901	2.911	25	OUTLET	
S29_9	0.036	0.065	0.661	6.012	25	OUTLET	
S3	0.043	0.044	0.606	5.679	25	PERVIOUS	50
S30	0.016	0.011	1.251	0.504	0	OUTLET	
S31	0.019	0	1.113	0.877	0	OUTLET	
S32	0.014	0	1.25	0	0	OUTLET	
S33	0.014	0	1.25	0	0	OUTLET	
S34	0.014	0	1.25	0	0	OUTLET	
S35	0.014	0	1.25	0	0	OUTLET	
S36	0.014	0	1.25	0	0	OUTLET	
S37	0.027	0.027	1.022	2.31	25	OUTLET	
S37_1	0.033	0.003	0.742	3.346	25	OUTLET	
S37_10	0.055	0	0.135	7.135	25	OUTLET	
S37_11	0.042	0	0.493	4.845	25	OUTLET	
S37_12	0.052	0	0.224	6.565	25	OUTLET	
S37_2	0.027	0.103	1.097	5.128	25	OUTLET	
S37_3	0.037	0.065	0.861	4.739	25	OUTLET	
S37_4	0.026	0.005	0.942	2.129	25	OUTLET	
S37_8	0.052	0.022	0.294	6.902	25	OUTLET	
S38	0.014	0	1.25	0	0	OUTLET	
S39	0.028	0.003	0.893	2.425	0	OUTLET	
S4	0.014	0	1.25	0	0.103	OUTLET	
S40	0.015	0	1.236	0.09	0	OUTLET	
S41	0.014	0	1.25	0	0	OUTLET	
S42	0.014	0	1.25	0	0	OUTLET	
S43	0.034	0.32	2.368	4.705	25	OUTLET	
S43_2	0.052	0.001	0.221	6.628	25	PERVIOUS	50
S43_4	0.042	0.331	2.088	5.155	25	OUTLET	
S43_5	0.033	0.123	1.367	4.362	25	PERVIOUS	50
S43_6	0.044	0.166	1.264	5.406	25	PERVIOUS	50
S43_7	0.035	0.016	0.758	3.747	25	PERVIOUS	50
S43_9	0.041	0.005	0.55	4.687	25	PERVIOUS	50
S44	0.014	0	1.25	0	0	OUTLET	
S45	0.014	0	1.25	0	0	OUTLET	
S46	0.014	0	1.25	0	0	OUTLET	
S46_1	0.029	0.089	1.098	4.622	25	OUTLET	
S46_10	0.031	0	0.779	3.012	25	OUTLET	
S46_2	0.045	0.013	0.494	5.423	25	OUTLET	
S46_3	0.028	0.005	0.891	2.549	25	OUTLET	
S46_4	0.026	0.102	1.104	4.722	25	OUTLET	
S46_5	0.039	0.004	0.597	4.38	25	OUTLET	
S46_6	0.031	0.102	0.938	5.562	25	OUTLET	
S46_7	0.03	0.007	0.874	2.795	25	OUTLET	
S47	0.014	0	1.25	0	0	OUTLET	
S48	0.014	0	1.25	0	0	OUTLET	
S49	0.014	0	1.25	0	0	OUTLET	
S5	0.014	0	1.25	0	0	OUTLET	
S50	0.014	0	1.25	0	0	OUTLET	
S51	0.014	0	1.25	0	0	OUTLET	
S52_1	0.034	0.238	1.779	5.387	25	OUTLET	
S52_2	0.035	0.092	1.131	4.028	25	OUTLET	
S52_3	0.023	0.107	1.34	4.059	25	OUTLET	
S52_4	0.031	0.057	0.85	4.746	25	OUTLET	
S52_6	0.023	0.048	1.143	2.732	25	OUTLET	
S52_7	0.035	0.039	0.834	4.523	25	OUTLET	
S53	0.014	0	1.25	0	0	OUTLET	
S54	0.014	0	1.25	0	0	OUTLET	

```
S55              0.014      0          1.25       0          0          OUTLET
S56              0.014      0          1.25       0          0          OUTLET
S57              0.014      0          1.25       0          25         OUTLET
S59              0.014      0          1.249      0.008      0          OUTLET
S63_1            0.042      0.08       0.908      5.056      25         OUTLET
S63_11           0.029      0.055      0.901      4.342      25         OUTLET
S63_12           0.032      0.036      0.962      3.593      25         OUTLET
S63_13           0.038      0.023      0.663      4.684      25         OUTLET
S63_14           0.034      0.013      0.788      3.47       25         OUTLET
S63_15           0.037      0.014      0.706      4.254      25         OUTLET
S63_2            0.044      0.115      1.019      5.739      25         OUTLET
S63_3            0.025      0.071      1.112      3.856      25         OUTLET
S63_4            0.018      0.012      1.201      0.835      25         OUTLET
S63_5            0.018      0.01       1.197      0.739      25         OUTLET
S63_6            0.035      0.025      0.825      3.993      25         OUTLET
S63_7            0.044      0.049      0.694      5.399      25         OUTLET
S63_8            0.031      0.082      0.818      5.704      25         OUTLET
S63_9            0.047      0          0.364      5.673      25         OUTLET
S7               0.014      0          1.25       0          0          OUTLET
S8               0.014      0          1.25       0          0          OUTLET
S9               0.014      0          1.25       0          0          OUTLET<!-- Standard PRE tag rules
-->

[INFILTRATION]
;;Subcatchment   MaxRate    MinRate    Decay      DryTime    MaxInfil
;;-------------- ---------- ---------- ---------- ---------- ----------
S1               127        120        4          2          157.8
S10              127        120        4          2          157.8
S11              127        120        4          2          157.8
S12              127        120        4          2          157.8
S13              127        120        4          2          157.8
S14              127        120        4          2          157.8
S15_1            127        120        4          2          157.8
S15_10           127        120        4          2          157.8
S15_12           127        120        4          2          157.8
S15_2            127        120        4          2          157.8
S15_3            127        120        4          2          157.8
S15_4            127        120        4          2          157.8
S15_5            127        120        4          2          157.8
S15_6            127        120        4          2          157.8
S15_7            127        120        4          2          157.8
S15_8            127        120        4          2          157.8
S15_9            127        120        4          2          157.8
S16              127        120        4          2          157.8
S17              127        120        4          2          157.8
S18_2            76.2       70         4          2          157.8
S18_3            76.2       70         4          2          157.8
S18_4            76.2       70         4          2          157.8
S19              127        120        4          2          157.8
S2               127        120        4          2          157.8
S20              127        120        4          2          157.8
S21              127        120        4          2          157.8
S22              127        120        4          2          157.8
S23              127        120        4          2          157.8
S23_1            127        120        4          2          157.8
S23_3            127        120        4          2          157.8
S23_4            127        120        4          2          157.8
S24              127        120        4          2          157.8
S25              127        120        4          2          157.8
S26_1            127        120        4          2          157.8
S26_3            127        120        4          2          157.8
S29_1            127        120        4          2          157.8
S29_10           127        120        4          2          157.8
S29_11           127        120        4          2          157.8
S29_12           127        120        4          2          157.8
S29_13           127        120        4          2          157.8
S29_14           127        120        4          2          157.8
S29_15           127        120        4          2          157.8
S29_17           127        120        4          2          157.8
S29_2            127        120        4          2          157.8
S29_3            127        120        4          2          157.8
S29_5            127        120        4          2          157.8
S29_7            127        120        4          2          157.8
S29_8            127        120        4          2          157.8
S29_9            127        120        4          2          157.8
S3               127        120        4          2          157.8
S30              127        120        4          2          157.8
S31              127        120        4          2          157.8
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S32              127        120        4          2          157.8
S33              127        120        4          2          157.8
S34              127        120        4          2          157.8
S35              127        120        4          2          157.8
S36              127        120        4          2          157.8
S37              127        120        4          2          157.8
S37_1            127        120        4          2          157.8
S37_10           127        120        4          2          157.8
S37_11           127        120        4          2          157.8
S37_12           127        120        4          2          157.8
S37_2            127        120        4          2          157.8
S37_3            127        120        4          2          157.8
S37_4            127        120        4          2          157.8
S37_8            127        120        4          2          157.8
S38              127        120        4          2          157.8
S39              127        120        4          2          157.8
S4               127        120        4          2          157.8
S40              127        120        4          2          157.8
S41              127        120        4          2          157.8
S42              127        120        4          2          157.8
S43              76.2       10.92      4          2          157.8
S43_2            127        120        4          2          157.8
S43_4            127        120        4          2          157.8
S43_5            127        120        4          2          157.8
S43_6            127        120        4          2          157.8
S43_7            127        120        4          2          157.8
S43_9            127        120        4          2          157.8
S44              127        120        4          2          157.8
S45              127        120        4          2          157.8
S46              127        120        4          2          157.8
S46_1            127        120        4          2          157.8
S46_10           127        120        4          2          157.8
S46_2            127        120        4          2          157.8
S46_3            127        120        4          2          157.8
S46_4            127        120        4          2          157.8
S46_5            127        120        4          2          157.8
S46_6            127        120        4          2          157.8
S46_7            127        120        4          2          157.8
S47              127        120        4          2          157.8
S48              127        120        4          2          157.8
S49              127        120        4          2          157.8
S5               127        120        4          2          157.8
S50              127        120        4          2          157.8
S51              127        120        4          2          157.8
S52_1            127        120        4          2          157.8
S52_2            127        120        4          2          157.8
S52_3            127        120        4          2          157.8
S52_4            127        120        4          2          157.8
S52_6            127        120        4          2          157.8
S52_7            127        120        4          2          157.8
S53              127        120        4          2          157.8
S54              127        120        4          2          157.8
S55              127        120        4          2          157.8
S56              127        120        4          2          157.8
S57              127        120        4          2          157.8
S59              127        120        4          2          157.8
S63_1            127        120        4          2          157.8
S63_11           127        120        4          2          157.8
S63_12           127        120        4          2          157.8
S63_13           127        120        4          2          157.8
S63_14           127        120        4          2          157.8
S63_15           127        120        4          2          157.8
S63_2            127        120        4          2          157.8
S63_3            127        120        4          2          157.8
S63_4            127        120        4          2          157.8
S63_5            127        120        4          2          157.8
S63_6            127        120        4          2          157.8
S63_7            127        120        4          2          157.8
S63_8            127        120        4          2          157.8
S63_9            127        120        4          2          157.8
S7               127        120        4          2          157.8
S8               127        120        4          2          157.8
S9               127        120        4          2          157.8<!-- Standard PRE tag rules -->

[LID_CONTROLS]
;;               Type/Layer Parameters
;;-------------- ---------- ----------
BioSwale         BC
```

```
BioSwale         SURFACE    300        0.01       0          0          5
BioSwale         SOIL       1000       0.4        0.19       0.085      120        10.0       110
BioSwale         STORAGE    1000       0.67       6          0
BioSwale         DRAIN      0.09       0.5        500        6          0          0<!-- Standard PRE tag
rules -->
EnhancedSwale    BC
EnhancedSwale    SURFACE    100        0.01       0          0          5
EnhancedSwale    SOIL       200        0.25       0.19       0.085      200        10.0       100
EnhancedSwale    STORAGE    800        0.33       6          0
EnhancedSwale    DRAIN      0.0011     0.5        300        6          0          0<!-- Multi line
multiple consecutive spaces -->

[LID_USAGE]
;;Subcatchment   LID Process      Number  Area       Width      InitSatur  FromImprv  ToPerv     Report
File                Drain to          FromPerv
;;-------------- ---------------- ------- ---------- ---------- ---------- ---------- ---------- --------
------------------ ---------------- ----------------
S43              BioSwale         1       16677      0          0          0          0          *
*                0<!-- Standard PRE tag rules -->

[AQUIFERS]
;;               Por-   Wilt   Field  Hyd    Cond   Tens   Upper  Lower  Lower  Bottom Water  Upper
Upper
;;Name           osity  Point  Capac  Cond   Slope  Slope  Evap   Evap   Loss   Elev   Table  Moist  Evap
Pat
;;-------------- ------ ------ ------ ------ ------ ------ ------ ------ ------ ------ ------ ------ ----
--------
Aquifer1         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      11.96  0.3
Aquifer1_11.96   0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      11.96  0.413
Aquifer2         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      11.35  0.3
Aquifer2_11.35   0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      11.35  0.413
Aquifer3         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      11     0.3
Aquifer3_11      0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      11     0.413
Aquifer4         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      10.6   0.3
Aquifer4_10.6    0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      10.6   0.413
Aquifer5         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      10     0.3
Aquifer5_10      0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      10     0.413
S10AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.7    9.7    0.3
S11AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.826 11.826 0.3
S12AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  16.367 16.367 0.3
S13AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.311 13.311 0.3
S14AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  16.367 16.367 0.3
S15_10AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.548 11.548 0.3
S15_12AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.58  11.58  0.3
S15_1AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.548 11.548 0.3
S15_2AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.779 13.779 0.3
S15_3AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.022 13.022 0.3
S15_4AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.641 13.641 0.3
S15_5AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.807 13.807 0.3
S15_6AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  16.367 16.367 0.3
S15_7AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.91  11.91  0.3
S15_8AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.364 13.364 0.3
S15_9AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.496 11.496 0.3
S16AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.72  14.72  0.3
S17AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.563 13.563 0.3
S18_2AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.593 12.593 0.3
S18_3AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.343 12.343 0.3
S18_4AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.343 12.343 0.3
S19AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.286 13.286 0.3
S1AQ             0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.826 11.826 0.3
S20AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.591 13.591 0.3
S21AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.364 13.364 0.3
S22AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.34  13.34  0.3
S23_1AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.794 13.794 0.3
S23_3AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  17.492 17.492 0.3
S23_4AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.311 13.311 0.3
S23AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.355 12.355 0.3
S24AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.496 11.496 0.3
S25AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.2   13.2   0.3
S26_1AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.938 14.938 0.3
S26_3AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.478 13.478 0.3
S29_10AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.871 11.871 0.3
S29_11AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.871 11.871 0.3
S29_12AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.987 11.987 0.3
S29_13AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      9.7    0.3
S29_14AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.508 11.508 0.3
S29_15AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12     12     0.3
S29_17AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.508 11.508 0.3
```

S29_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	16.367	16.367	0.3
S29_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.562	14.562	0.3
S29_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.022	13.022	0.3
S29_5AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.188	12.188	0.3
S29_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.238	12.238	0.3
S29_8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.72	14.72	0.3
S29_9AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.696	11.696	0.3
S2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.188	12.188	0.3
S30AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	8.33	8.33	0.3
S31AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.4	15.4	0.3
S32AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.975	15.975	0.3
S33AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.975	15.975	0.3
S34AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S35AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	10.61	10.61	0.3
S36AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S37_10AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.5	11.5	0.3
S37_11AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S37_12AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S37_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.34	13.34	0.3
S37_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.794	13.794	0.3
S37_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.794	13.794	0.3
S37_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.307	12.307	0.3
S37_8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.397	13.397	0.3
S37AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S38AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S39AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.5	15.5	0.3
S3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S40AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.5	15.5	0.3
S41AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.871	11.871	0.3
S42AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.07	9.07	0.3
S43_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.194	13.194	0.3
S43_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S43_5AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S43_6AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S43_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S43_9AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S43AQ	0.5	0.15	0.3	5	10	15	0.35	1	0.002	9.1	9.1	0.3
S44AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S45AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S46_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.9	9.9	0.3
S46_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.02	11.02	0.3
S46_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S46_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.307	12.307	0.3
S46_6AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	10.5	10.5	0.3
S46_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S46_8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.307	12.307	0.3
S46AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.34	13.34	0.3
S47AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.094	14.094	0.3
S48AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.578	13.578	0.3
S49AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.987	13.987	0.3
S4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S50AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.987	13.987	0.3
S51AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.591	13.591	0.3
S52_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S52_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S52_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.478	13.478	0.3
S52_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.668	12.668	0.3
S52_6AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.291	12.291	0.3
S52_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.49	12.49	0.3
S53AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.794	13.794	0.3
S54AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.91	11.91	0.3
S55AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.91	11.91	0.3
S56AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.91	11.91	0.3
S57AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.72	14.72	0.3
S59AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.72	14.72	0.3
S5AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.238	12.238	0.3
S63_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	8.33	8.33	0.3
S63_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.01	9.01	0.3
S63_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14	14	0.3
S63_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S63_5AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	8.33	8.33	0.3
S63_6AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.126	14.126	0.3
S63_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S63_9AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.5	15.5	0.3
S7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.322	15.322	0.3
S8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.084	14.084	0.3
S9AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3<!--

Standard PRE tag rules -->

```
[GROUNDWATER]
;;Subcatchment   Aquifer          Node             Elev   A1     B1     A2     B2     A3     Depth  Elev
Ebot   Wgr   Umc
;;-------------- ---------------- ---------------- ------ ------ ------ ------ ------ ------ ------ -----
- ------ ------ ------
S1               S1AQ             J80              11.826 0.1    1      0.1    1      0      0      *
0      10     *
S12              S12AQ            J9               16.367 0.1    1      0.1    1      0      0      *
0      12     *
S13              S13AQ            J6               13.311 0.1    1      0.1    1      0      0      *
0      11.35  *
S14              S14AQ            J9               16.367 0.1    1      0.1    1      0      0      *
0      12     *
S15_1            S15_1AQ          J24              12.983 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_10           S15_10AQ         J24              12.983 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_12           S15_12AQ         J2312            13.002 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_2            S15_2AQ          J20              13.779 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_4            S15_4AQ          J17              13.641 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_5            S15_5AQ          J18              13.807 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_7            S15_7AQ          J2181            11.96  0.1    1      0.1    1      0      0      *
0      11.35  *
S15_8            S15_8AQ          J26              13.364 0.1    1      0.1    1      0      0      *
0      11.35  *
S15_9            S15_9AQ          J23              12.996 0.1    1      0.1    1      0      0      *
0      11.35  *
S2               S2AQ             J79              12.188 0.1    1      0.1    1      0      0      *
0      10.6   *
S23              S23AQ            J25              15     0.1    1      0.1    1      0      0      *
0      11.35  *
S23_1            S23_1AQ          J4               13.794 0.1    1      0.1    1      0      0      *
0      12     *
S23_3            S23_3AQ          J12              17.492 0.1    1      0.1    1      0      0      *
0      12     *
S23_4            S23_4AQ          J6               13.311 0.1    1      0.1    1      0      0      *
0      12     *
S26_1            S26_1AQ          J2787            14.938 0.1    1      0.1    1      0      0      *
0      11.35  *
S26_3            S26_3AQ          J2909            13.478 0.1    1      0.1    1      0      0      *
0      11.35  *
S29_1            S29_1AQ          J9               16.367 0.1    1      0.1    1      0      0      *
0      12     *
S29_10           S29_10AQ         J2931            11.871 0.1    1      0.1    1      0      0      *
0      10.6   *
S29_11           S29_11AQ         J2931            11.871 0.1    1      0.1    1      0      0      *
0      9.7    *
S29_12           S29_12AQ         J40              11.987 0.1    1      0.1    1      0      0      *
0      10     *
S29_13           S29_13AQ         J35              11.7   0.1    1      0.1    1      0      0      *
0      10.6   *
S29_14           S29_14AQ         J48              11.508 0.1    1      0.1    1      0      0      *
0      10     *
S29_2            S29_2AQ          J2754            14.562 0.1    1      0.1    1      0      0      *
0      11.35  *
S29_3            S29_3AQ          J11              13.022 0.1    1      0.1    1      0      0      *
0      11.35  *
S29_5            S29_5AQ          J79              12.188 0.1    1      0.1    1      0      0      *
0      10.6   *
S29_7            S29_7AQ          J63              12.238 0.1    1      0.1    1      0      0      *
0      10.6   *
S29_8            S29_8AQ          J13              14.72  0.1    1      0.1    1      0      0      *
0      12     *
S29_9            S29_9AQ          J83              12.896 0.1    1      0.1    1      0      0      *
0      10.6   *
S3               S3AQ             J2510            12.804 0.1    1      0.1    1      0      0      *
0      11     *
S30              S30AQ            J355             10     0.1    1      0.1    1      0      0      *
0      9.7    *
S31              S31AQ            J2712            15.668 0.1    1      0.1    1      0      0      *
0      10     *
S37              S37AQ            J2722            14.544 0.1    1      0.1    1      0      0      *
0      10.6   *
```

S37_1	S37_1AQ	J7	13.34	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_10	S37_10AQ	J22	15	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_11	S37_11AQ	J2510	12.804	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_12	S37_12AQ	J2510	12.804	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_2	S37_2AQ	J4	13.794	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_3	S37_3AQ	J4	13.794	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_4	S37_4AQ	J16	13.307	0.1	1	0.1	1	0	0	*	0	11.35	*
S37_8	S37_8AQ	J1	13.397	0.1	1	0.1	1	0	0	*	0	11.35	*
S39	S39AQ	J2709	15.7	0.1	1	0.1	1	0	0	*	0	10	*
S40	S40AQ	J2709	15.7	0.1	1	0.1	1	0	0	*	0	10	*
S43	S43AQ	J1969	10.206	0.1	1	0.1	1	0	0	*	0	9.7	*
S43_2	S43_2AQ	J56	13.194	0.1	1	0.1	1	0	0	*	0	11	*
S43_4	S43_4AQ	J46	11.099	0.1	1	0.1	1	0	0	*	0	9.7	*
S43_5	S43_5AQ	J46	11.099	0.1	1	0.1	1	0	0	*	0	11	*
S43_6	S43_6AQ	J1969	10.206	0.1	1	0.1	1	0	0	*	0	9.7	*
S43_7	S43_7AQ	J46	11.099	0.1	1	0.1	1	0	0	*	0	11	*
S43_9	S43_9AQ	J1969	10.206	0.1	1	0.1	1	0	0	*	0	9.7	*
S46_1	S46_1AQ	J2771	11.738	0.1	1	0.1	1	0	0	*	0	11	*
S46_10	S46_3AQ	J2722	14.544	0.1	1	0.1	1	0	0	*	0	10.6	*
S46_2	S46_2AQ	J2594	12.819	0.1	1	0.1	1	0	0	*	0	11.35	*
S46_3	S46_3AQ	J2722	14.544	0.1	1	0.1	1	0	0	*	0	10.6	*
S46_4	S46_4AQ	J16	13.307	0.1	1	0.1	1	0	0	*	0	11.35	*
S46_5	S46_3AQ	J2722	14.544	0.1	1	0.1	1	0	0	*	0	11	*
S46_6	S46_6AQ	J2678	12.647	0.1	1	0.1	1	0	0	*	0	11.35	*
S46_7	S46_7AQ	J2722	14.544	0.1	1	0.1	1	0	0	*	0	11	*
S52_1	S52_1AQ	J1969	10.206	0.1	1	0.1	1	0	0	*	0	9.7	*
S52_2	S52_2AQ	J1969	10.206	0.1	1	0.1	1	0	0	*	0	9.7	*
S52_3	S52_3AQ	J2909	13.478	0.1	1	0.1	1	0	0	*	0	9.7	*
S52_4	S52_4AQ	J70	12.668	0.1	1	0.1	1	0	0	*	0	10.6	*
S52_6	S52_6AQ	J2838	12.291	0.1	1	0.1	1	0	0	*	0	11	*
S52_7	S52_7AQ	J2860	12.49	0.1	1	0.1	1	0	0	*	0	11.35	*
S59	S59AQ	J13	14.72	0.1	1	0.1	1	0	0	*	0	11.35	*
S63_1	S63_1AQ	J355	10	0.1	1	0.1	1	0	0	*	0	9.7	*
S63_11	S63_3AQ	J2794	14.366	0.1	1	0.1	1	0	0	*	0	10	*
S63_12	S63_3AQ	J2794	14.366	0.1	1	0.1	1	0	0	*	0	9.7	*
S63_13	S63_3AQ	J2794	14.366	0.1	1	0.1	1	0	0	*	0	9.7	*
S63_14	S63_3AQ	J2794	14.366	0.1	1	0.1	1	0	0	*	0	10.6	*
S63_15	S63_3AQ	J2794	14.366	0.1	1	0.1	1	0	0	*	0	10	*
S63_2	S63_2AQ	J2855	11.297	0.1	1	0.1	1	0	0	*	0	9.7	*

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S63_3            S63_3AQ          J2794            14.366 0.1    1      0.1    1      0      0      *
0      10.6   *
S63_4            S63_4AQ          J1969            10.206 0.1    1      0.1    1      0      0      *
0      10     *
S63_5            S63_5AQ          J355             10     0.1    1      0.1    1      0      0      *
0      9.7    *
S63_6            S63_6AQ          J2785            14.126 0.1    1      0.1    1      0      0      *
0      10     *
S63_7            S63_7AQ          J1969            10.206 0.1    1      0.1    1      0      0      *
0      10     *
S63_8            S63_3AQ          J2794            14.366 0.1    1      0.1    1      0      0      *
0      10.6   *
S63_9            S63_9AQ          J2709            15.7   0.1    1      0.1    1      0      0      *
0      10     *<!-- Standard PRE tag rules -->

[JUNCTIONS]
;;               Invert     Max.       Init.      Surcharge  Ponded
;;Name           Elev.      Depth      Depth      Depth      Area
;;-------------- ---------- ---------- ---------- ---------- ----------
J1               13.397     0          0          0          0
J10              13.307     0          0          0          0
J1040            9.07       2.211      0          0          0
J11              13.022     0          0          0          0
J12              17.492     0          0          0          0
J13              14.72      0          0          0          0
J14              13.165     0          0          0          0
J1415            9.712      2.03       0          0          0
J15              13.771     0          0          0          0
J16              12.307     1          0          0          0
J17              13.641     0          0          0          0
J1701            14.3       0.045      0          0          0
;Wetland outfall
J1788            9.08       1.679      0          0          0
J18              13.807     0          0          0          0
J19              12.482     0          0          0          0
J1969            9.1        1.106      0          0          0
J2               13.175     0          0          0          0
J20              13.779     0          0          0          0
J21              11         2.351      0          0          0
J2181            11.91      0.05       0          0          0
J22              11.5       3.5        0          0          0
J2293            11.6       1.396      0          0          0
J23              11.496     1.5        0          0          0
J2312            11.58      1.422      0          0          0
J24              11.548     1.435      0          0          0
J25              12.355     2.645      0          0          0
J2510            11.21      1.594      0          0          0
J2594            11.02      1.799      0          0          0
J26              13.364     0          0          0          0
J2678            10.5       2.147      0          0          0
J2692            10.61      1.866      0          0          0
J27              12.482     0          0          0          0
J2709            15.5       0.2        0          0          0
J2712            15.4       0.268      0          0          0
J2717            15.975     0          0          0          0
J2719            15.875     0          0          0          0
J2722            14.544     0          0          0          0
J2728            15.283     0          0          0          0
J2730            15.255     0          0          0          0
J2749            15.158     0          0          0          0
J2754            14.562     0          0          0          0
J2755            14.084     0          0          0          0
J2757            15.322     0          0          0          0
J2764            14.47      0          0          0          0
J2771            9.9        1.838      0          0          0
J2779            14.324     0          0          0          0
J2785            14.126     0          0          0          0
J2786            15.063     0          0          0          0
J2787            14.938     0          0          0          0
J2794            14         0.366      0          0          0
J2797            13.274     0          0          0          0
J28              13.286     0          0          0          0
J2813            12.422     0          0          0          0
J2816            12.292     0          0          0          0
J2822            12.933     0          0          0          0
J2831            12.636     0          0          0          0
J2838            12.291     0          0          0          0
J2839            14.094     0          0          0          0
```

```
J2845            12.619     0          0          0          0
J2847            13.578     0          0          0          0
J2855            9.01       2.287      0          0          0
J2857            9.64       2.06       0          0          0
J2860            12.49      0          0          0          0
J2868            12.78      0          0          0          0
J2870            12.8       0.01       0          0          0
J2887            9.57       2.046      0          0          0
J2890            12.9       0.1        0          0          0
J2891            10         0.379      0          0          0
J29              12.674     0          0          0          0
J29_14           12         0          0          0          0
J2909            13.478     0          0          0          0
J2915            9.2        2.4        0          0          0
J2918            13.563     0.9        0          0          0
J2921            11.284     0          0          0          0
J2931            11.871     0          0          0          0
J2938            14.358     0.795      0          0          0
J3               13.591     0          0          0          0
J30              12.343     0          0          0          0
J31              12.665     0          0          0          0
J32              12.593     0          0          0          0
J33              12.308     0          0          0          0
J34              12.132     0          0          0          0
J35              11.496     0.204      0          0          0
J36              11.727     0          0          0          0
J37              12.207     0          0          0          0
J38              12.299     0          0          0          0
J39              12.123     0          0          0          0
J4               13.794     0          0          0          0
J40              11.987     0          0          0          0
J41              12         0          0          0          0
J42              12.238     0          0          0          0
J43              12.872     0          0          0          0
J44              12.872     0          0          0          0
J45              9.3        1.534      0          0          0
J46              9.7        1.399      0          0          0
J47              11.647     0          0          0          0
J48              11.508     0          0          0          0
J49              9.09       1.828      0          0          0
J5               13.987     0          0          0          0
J50              12.202     0          0          0          0
J52              11.508     0.2        0          0          0
J53              11.509     0.2        0          0          0
J55              9.69       1.316      0          0          0
J56              13.194     0          0          0          0
J57              13.2       0          0          0          0
J59              12.499     0          0          0          0
J6               13.311     0          0          0          0
J63              12.238     0          0          0          0
J64              12.805     0          0          0          0
J65              11.793     0          0          0          0
J66              11.582     0          0          0          0
J67              11.916     0          0          0          0
J68              12         0          0          0          0
J69              11.759     0          0          0          0
J7               13.34      0          0          0          0
J70              12.668     0          0          0          0
J72              11.596     0.1        0          0          0
J73              12.86      0          0          0          0
J78              12.4       0          0          0          0
J79              12.188     0          0          0          0
J8               11.34      1.65       0          0          0
J80              11.826     0          0          0          0
J83              11.696     1.2        0          0          0
J9               16.367     0          0          0          0<!-- Standard PRE tag rules -->

[OUTFALLS]
;;               Invert     Outfall      Stage/Table      Tide
;;Name           Elev.      Type         Time Series      Gate Route To
;;-------------- ---------- ------------ ---------------- ---- ----------------
J355             8.33       FREE                          NO<!-- Standard PRE tag rules -->

[STORAGE]
;;               Invert   Max.     Init.    Storage    Curve                              Evap.
;;Name           Elev.    Depth    Depth    Curve      Params                             Frac.
Infiltration parameters
```

```
;;-------------- -------- -------- -------- ---------- -------- -------- -------- -------- -------- -----
------------------
J54              8.8      2.169    0        TABULAR    SedimentationPond          0       0<!-- Standard
PRE tag rules -->

[CONDUITS]
;;               Inlet            Outlet                      Manning    Inlet      Outlet     Init.
Max.
;;Name            Node             Node             Length     N          Offset     Offset     Flow
Flow
;;-------------- ---------------- ---------------- ---------- ---------- ---------- ---------- ----------
----------
;B- branch
206110366        J2510            J2594            68.079     0.012      11.21      11.02      0
0
;B- branch
206110379_1      J2312            J24              23.888     0.012      11.58      11.54      0
0
;B- branch
206110379_2      J8               J2510            51.399     0.012      11.34      11.21      0
0
;B- branch
206110379_4      J23              J8               67.866     0.012      11.496     11.34      0
0
;B- branch
206110379_5      J24              J23              39.622     0.012      11.54      11.496     0
0
;B- branch
22803188_2       J45              J2915            159.449    0.027      9.3        9.2        0
0
;B- branch
22803188_3       J54              J45              89.837     0.027      9.45       9.3        0
0
;B- branch
22803188_4       J46              J55              61.407     0.027      9.7        9.69       0
0
;B- branch
22803188_5       J55              J54              24.469     0.01       9.69       8.8        0
0
;B- branch
22926618_1       J2915            J1969            23.772     0.027      9.2        9.1        0
0
;B- branch
22926618_2       J1969            J49              64.7       0.027      9.1        9.09       0
0
;B- branch
22926618_3       J1040            J2855            33.579     0.027      9.07       9.01       0
0
;B- branch
22926618_4       J1788            J1040            50.452     0.027      9.08       9.07       0
0
;B- branch
22926629         J2887            J2915            19.716     0.027      9.57       9.2        0
0
;B- branch
23116769         J2594            J2678            67.769     0.012      10.5       10.842     0
0
;B- branch
23116814         J1415            J2857            21.548     0.012      9.71       9.64       0
0
;B- branch
23116826         J2857            J2887            27.164     0.012      9.64       9.57       0
0
;B- branch
23405543         J2293            J2312            8.129      0.012      11.6       11.58      0
0
;B- branch
23405563         J2181            J2293            111.419    0.012      11.91      11.6       0
0
;B- branch
57466689_1       J2771            J1415            34.821     0.012      9.9        9.71       0
0
;B- branch
57466741         J2692            J2771            111.323    0.012      10.61      9.9        0
0
;B- branch
57466813         J2678            J2692            18.756     0.012      10.841     10.649     0
0
```

C1	J10	J2	4.637	0.012	13.307	13.175	0
0							
C1_1	J2	J14	9.039	0.012	13.175	13.165	0
0							
C1_2	J14	J1	58.507	0.012	13.165	13.397	0
0							
C10	J9	J5	67.889	0.012	16.367	13.987	0
0							
C108	J2921	J1969	21.276	0.012	11.284	9.1	0
0							
C109	J2831	J2845	40.393	0.012	12.636	12.619	0
0							
C11	J11	J14	10.311	0.012	13.022	13.165	0
0							
C110	J2794	J1040	48.667	0.012	14.366	9.9	0
0							
C111	J2785	J2794	97.324	0.012	14.126	14.366	0
0							
C112	J2717	J2719	2.496	0.012	15.975	15.875	0
0							
C113	J2918	J2909	49.617	0.012	13.582	13.178	0
0							
C12	J1	J7	51.477	0.012	13.397	13.34	0
0							
C126	J2890	J2870	8.515	0.012	12.9	12.8	0
0							
C127	J2816	J2813	8.596	0.012	12.292	12.422	0
0							
C128	J2722	J2797	104.347	0.012	14.544	13.274	0
0							
C129_1	J2764	J1701	7.023	0.012	14.47	14.3	0
0							
C129_2	J1701	J2847	42.939	0.012	14.3	13.578	0
0							
C13	J12	J9	67.473	0.012	17.492	16.367	0
0							
C130	J2787	J2764	47.719	0.012	14.938	14.47	0
0							
C131	J2870	J2868	1.688	0.012	12.8	12.78	0
0							
C141	J2931	J2921	12.998	0.012	11.871	11.284	0
0							
C142	J2822	J2831	53.415	0.012	12.933	12.636	0
0							
C143	J2712	J2785	77.216	0.012	15.668	14.126	0
0							
C144	J2786	J2794	10.768	0.012	15.063	14	0
0							
C145	J2839	J2847	7.54	0.012	14.094	13.578	0
0							
C146	J2779	J1701	4.365	0.012	14.324	0	0
0							
C147	J2730	J2749	16.81	0.012	15.255	15.158	0
0							
C148	J2719	J2730	33.014	0.012	15.875	15.255	0
0							
C158	J2860	J2838	85.236	0.012	12.49	12.291	0
0							
C159	J2797	J2822	5.744	0.012	13.274	12.933	0
0							
C16	J13	J2	107.922	0.012	14.72	13.175	0
0							
C160	J2845	J2857	10.336	0.012	12.619	9.64	0
0							
C161	J2728	J2730	5.612	0.012	15.283	15.255	0
0							
C167_2	J47	J2931	62.151	0.012	11.647	11.871	0
0							
C169	J2838	J1415	29.473	0.012	12.291	9.71	0
0							
C17	J17	J15	17.34	0.012	13.641	13.771	0
0							
C170	J2813	J1415	17.522	0.012	12.422	9.71	0
0							
C176	J2855	J355	189.997	0.012	9.01	8.33	0
0							
C18	J18	J2293	9.374	0.012	13.807	11.6	0
0							

C182	J2757	J2786	23.114	0.012	15.322	15.063	0
0							
C185	J2868	J2860	37.359	0.012	12.78	12.49	0
0							
C186	J2909	J2868	76.26	0.012	13.178	12.78	0
0							
C19	J20	J17	8.543	0.012	13.779	13.641	0
0							
C193	J2709	J2712	5.018	0.012	15.5	15.4	0
0							
C194	J2749	J2786	40.681	0.012	15.158	15.063	0
0							
C195	J2754	J2764	7.405	0.012	14.562	14.47	0
0							
C196	J2891	J1788	3.836	0.012	10	9.8	0
0							
C20	J22	J8	29.309	0.012	11.5	11.34	0
0							
C21	J25	J8	3.458	0.012	12.407	11.34	0
0							
C22	J26	J23	3.504	0.012	13.364	11.496	0
0							
C23	J28	J24	5.29	0.012	13.286	11.548	0
0							
C24	J16	J21	12.672	0.012	12.307	11	0
0							
C25	J21	J2678	29.87	0.012	11	10.5	0
0							
C26	J27	J19	1.36	0.012	12.482	12.482	0
0							
C27	J30	J29	9.258	0.012	12.343	12.674	0
0							
C28	J32	J31	3.951	0.012	12.593	12.665	0
0							
C29	J34	J33	1.846	0.012	12.132	12.308	0
0							
C3	J4	J3	40.802	0.012	13.794	13.591	0
0							
C30	J36	J35	38.306	0.012	11.727	11.496	0
0							
C31	J38	J37	32.41	0.012	12.299	12.207	0
0							
C32	J40	J39	20.545	0.012	11.987	12.123	0
0							
C33	J41	J40	2.028	0.012	12	11.987	0
0							
C34	J42	J33	24.628	0.012	12.238	12.308	0
0							
C35	J44	J43	2.945	0.012	12.872	12.872	0
0							
C37	J35	J47	13.225	0.012	11.496	11.647	0
0							
C38	J52	J48	3.314	0.012	11.508	11.508	0
0							
C39	J37	J50	31.398	0.012	12.207	12.202	0
0							
C4	J5	J6	79.213	0.012	13.987	13.311	0
0							
C40	J39	J38	19.101	0.012	12.123	12.299	0
0							
C41	J29_14	J40	5.115	0.012	12	11.987	0
0							
C42	J53	J52	1.209	0.012	11.509	11.508	0
0							
C44	J57	J56	17.729	0.012	13.2	13.194	0
0							
C45	J59	J19	11.134	0.012	12.499	12.482	0
0							
C46	J33	J47	69.917	0.012	12.308	11.647	0
0							
C47	J63	J42	4.441	0.012	12.238	12.238	0
0							
C49	J19	J33	65.276	0.012	12.482	12.308	0
0							
C5	J7	J2510	44.939	0.012	13.34	11.804	0
0							
C50	J56	J19	66.196	0.012	13.194	12.482	0
0							

```
C51             J64             J63             9.046     0.012     12.805    12.238    0
0
C52             J65             J52             9.715     0.012     11.793    11.508    0
0
C53             J66             J48             18.477    0.012     11.582    11.508    0
0
C54             J67             J66             36.208    0.012     11.916    11.582    0
0
C55             J68             J40             16.677    0.012     12        11.987    0
0
C56             J69             J65             1.909     0.012     11.759    11.793    0
0
C57             J78             J70             2.562     0.012     12.4      12.668    0
0
C58             J72             J35             1.316     0.012     11.596    11.496    0
0
C59             J50             J67             19.402    0.012     12.202    11.916    0
0
C6              J15             J2312           20.221    0.012     13.771    11.58     0
0
C60             J43             J70             73.615    0.012     12.872    12.668    0
0
C61             J31             J43             47.818    0.012     12.665    12.872    0
0
C62             J73             J44             2.889     0.012     12.86     12.872    0
0
C63             J48             J36             58.382    0.012     11.508    11.727    0
0
C65             J70             J42             64.446    0.012     12.668    12.238    0
0
C66             J29             J31             3.655     0.012     12.674    12.665    0
0
C67             J79             J78             9.05      0.012     12.188    12.4      0
0
C68             J80             J67             12.636    0.012     11.826    11.916    0
0
C7              J6              J1              17.512    0.012     13.311    13.397    0
0
C70             J83             J72             2.461     0.012     11.696    11.596    0
0
C8              J3              J6              59.949    0.012     13.591    13.311    0
0
C95             J2755           J2860           73.223    0.012     14.084    12.49     0
0
C96             J2847           J2909           51.011    0.012     13.578    13.178    0
0
C97             J2938           J2918           68.42     0.012     14.358    13.582    0
0<!-- Standard PRE tag rules -->

[WEIRS]
;;              Inlet           Outlet          Weir        Crest     Disch.    Flap End     End
;;Name          Node            Node            Type        Height    Coeff.    Gate Con.
Coeff.     Surcharge  RoadWidth  RoadSurf   Coeff. Curve
;;-------------- ---------------- ---------------- ------------ ---------- ---------- ---- -------- -----
----- ---------- ---------- ---------- ----------------
;B- branch
;{22405761@student.uwa.edu.au - 2019.12.30} The discharge coefficient has been taken from the mean
average of the 2012-2017 flow data
22926618_6      J49             J1788           TRANSVERSE  9.09      3.33      NO   0       0
YES<!-- Standard PRE tag rules -->

[XSECTIONS]
;;Link           Shape        Geom1            Geom2      Geom3      Geom4      Barrels
;;-------------- ------------ ---------------- ---------- ---------- ---------- ----------
206110366       CIRCULAR     1.35             0          0          0          1
206110379_1     CIRCULAR     1.35             0          0          0          1
206110379_2     CIRCULAR     1.35             0          0          0          1
206110379_4     CIRCULAR     1.35             0          0          0          1
206110379_5     CIRCULAR     1.35             0          0          0          1
22803188_2      IRREGULAR    AnvilTransect    0          0          0          1
22803188_3      IRREGULAR    AnvilTransect    0          0          0          1
22803188_4      IRREGULAR    AnvilTransect    0          0          0          1
22803188_5      IRREGULAR    AnvilTransect    0          0          0          1
22926618_1      IRREGULAR    AnvilTransect    0          0          0          1
22926618_2      IRREGULAR    AnvilTransect    0          0          0          1
22926618_3      IRREGULAR    Anvil_Transect2  0          0          0          1
22926618_4      IRREGULAR    Anvil_Transect2  0          0          0          1
22926629        PARABOLIC    1.35             2          0          0          1
```

23116769	CIRCULAR	1.35	0	0	0	1
23116814	CIRCULAR	1.35	0	0	0	1
23116826	CIRCULAR	1.35	0	0	0	1
23405543	CIRCULAR	1.35	0	0	0	1
23405563	CIRCULAR	1.35	0	0	0	1
57466689_1	CIRCULAR	1.35	0	0	0	1
57466741	CIRCULAR	1.35	0	0	0	1
57466813	CIRCULAR	1.35	0	0	0	1
C1	CIRCULAR	1	0	0	0	1
C1_1	CIRCULAR	1	0	0	0	1
C1_2	CIRCULAR	1	0	0	0	1
C10	CIRCULAR	1	0	0	0	1
C108	CIRCULAR	1	0	0	0	1
C109	CIRCULAR	0.75	0	0	0	1
C11	CIRCULAR	1	0	0	0	1
C110	CIRCULAR	0.75	0	0	0	1
C111	CIRCULAR	0.45	0	0	0	1
C112	CIRCULAR	0.45	0	0	0	1
C113	CIRCULAR	0.75	0	0	0	1
C12	CIRCULAR	1	0	0	0	1
C126	CIRCULAR	1	0	0	0	1
C127	CIRCULAR	1	0	0	0	1
C128	CIRCULAR	0.45	0	0	0	1
C129_1	CIRCULAR	1	0	0	0	1
C129_2	CIRCULAR	1	0	0	0	1
C13	CIRCULAR	1	0	0	0	1
C130	CIRCULAR	1	0	0	0	1
C131	CIRCULAR	1	0	0	0	1
C141	CIRCULAR	1	0	0	0	1
C142	CIRCULAR	0.75	0	0	0	1
C143	CIRCULAR	0.45	0	0	0	1
C144	CIRCULAR	0.45	0	0	0	1
C145	CIRCULAR	1	0	0	0	1
C146	CIRCULAR	1	0	0	0	1
C147	CIRCULAR	0.45	0	0	0	1
C148	CIRCULAR	0.45	0	0	0	1
C158	CIRCULAR	0.75	0	0	0	1
C159	CIRCULAR	0.75	0	0	0	1
C16	CIRCULAR	1	0	0	0	1
C160	CIRCULAR	0.75	0	0	0	1
C161	CIRCULAR	0.45	0	0	0	1
C167_2	CIRCULAR	1	0	0	0	1
C169	CIRCULAR	0.75	0	0	0	1
C17	CIRCULAR	1	0	0	0	1
C170	CIRCULAR	1	0	0	0	1
C176	IRREGULAR	Anvil_Transect2	0	0	0	1
C18	CIRCULAR	1	0	0	0	1
C182	CIRCULAR	0.45	0	0	0	1
C185	CIRCULAR	1	0	0	0	1
C186	CIRCULAR	1	0	0	0	1
C19	CIRCULAR	1	0	0	0	1
C193	CIRCULAR	0.45	0	0	0	1
C194	CIRCULAR	0.45	0	0	0	1
C195	CIRCULAR	1	0	0	0	1
C196	CIRCULAR	1	0	0	0	1
C20	CIRCULAR	1.65	0	0	0	1
C21	CIRCULAR	1	0	0	0	1
C22	CIRCULAR	1	0	0	0	1
C23	CIRCULAR	1	0	0	0	1
C24	CIRCULAR	1	0	0	0	1
C25	CIRCULAR	1	0	0	0	1
C26	CIRCULAR	1	0	0	0	1
C27	CIRCULAR	1	0	0	0	1
C28	CIRCULAR	1	0	0	0	1
C29	CIRCULAR	1	0	0	0	1
C3	CIRCULAR	1	0	0	0	1
C30	CIRCULAR	1	0	0	0	1
C31	CIRCULAR	1	0	0	0	1
C32	CIRCULAR	1	0	0	0	1
C33	CIRCULAR	1	0	0	0	1
C34	CIRCULAR	1	0	0	0	1
C35	CIRCULAR	1	0	0	0	1
C37	CIRCULAR	1	0	0	0	1
C38	CIRCULAR	1	0	0	0	1
C39	CIRCULAR	1	0	0	0	1
C4	CIRCULAR	1	0	0	0	1
C40	CIRCULAR	1	0	0	0	1
C41	CIRCULAR	1	0	0	0	1

```
C42              CIRCULAR     1                0          0          0          1
C44              CIRCULAR     1                0          0          0          1
C45              CIRCULAR     1                0          0          0          1
C46              CIRCULAR     1                0          0          0          1
C47              CIRCULAR     1                0          0          0          1
C49              CIRCULAR     1                0          0          0          1
C5               CIRCULAR     1                0          0          0          1
C50              CIRCULAR     1                0          0          0          1
C51              CIRCULAR     1                0          0          0          1
C52              CIRCULAR     1                0          0          0          1
C53              CIRCULAR     1                0          0          0          1
C54              CIRCULAR     1                0          0          0          1
C55              CIRCULAR     1                0          0          0          1
C56              CIRCULAR     1                0          0          0          1
C57              CIRCULAR     1                0          0          0          1
C58              CIRCULAR     1                0          0          0          1
C59              CIRCULAR     1                0          0          0          1
C6               CIRCULAR     1                0          0          0          1
C60              CIRCULAR     1                0          0          0          1
C61              CIRCULAR     1                0          0          0          1
C62              CIRCULAR     1                0          0          0          1
C63              CIRCULAR     1                0          0          0          1
C65              CIRCULAR     1                0          0          0          1
C66              CIRCULAR     1                0          0          0          1
C67              CIRCULAR     1                0          0          0          1
C68              CIRCULAR     1                0          0          0          1
C7               CIRCULAR     1                0          0          0          1
C70              CIRCULAR     1                0          0          0          1
C8               CIRCULAR     1                0          0          0          1
C95              CIRCULAR     1                0          0          0          1
C96              CIRCULAR     1                0          0          0          1
C97              CIRCULAR     0.75             0          0          0          1
22926618_6       RECT_OPEN    0.7              0.6        0          0<!-- Standard PRE tag rules -->

[TRANSECTS]
;Half street, width = 5m, curb = 0.15m , cross-slope = 0.02m/m, bank-slope = 0.02m/m, bank-height =
0.23m.
NC 0.02     0.02     0.014
X1 Anvil_Transect2  4        0.0      5        0.0       0.0       0.0      0.0      0.0
GR 1.3      0        0        3        0        6        1.3      9<!-- Standard PRE tag rules -->
NC 0.01     0.01     0.01
X1 AnvilTransect    4        0.0      0.0      0.0       0.0       0.0      0.0      0.0
GR 0.65     0        0        3        0        8.5      0.65     11.5<!-- Multi line multiple
consecutive spaces -->

[LOSSES]
;;Link           Inlet      Outlet     Average    Flap Gate  SeepageRate
;;-------------- ---------- ---------- ---------- ---------- ----------<!-- Standard PRE tag rules -->

[INFLOWS]
;;                                                Param    Units    Scale    Baseline Baseline
;;Node           Parameter        Time Series      Type     Factor   Factor   Value    Pattern
;;-------------- ---------------- ---------------- -------- -------- -------- -------- --------
J2887            FLOW             ""               FLOW     1.0      1        0.001
J46              FLOW             InflowWetland    FLOW     1.0      1        0
J355             FLOW             ""               FLOW     1.0      1        0.047<!-- Standard PRE tag
rules -->

[CURVES]
;;Name           Type       X-Value    Y-Value
;;-------------- ---------- ---------- ----------
;The inlet structure has a rock drop structure, with an assigned curve that I take as a beehave curve
Beehivegate      Rating     0          0
Beehivegate                 0.06096    42.4752699
Beehivegate                 0.12192    84.9505398
Beehivegate                 0.18288    104.7723324
Beehivegate                 0.24384    121.7624404
Beehivegate                 0.3048     135.9208637
Beehivegate                 0.36576    150.079287
Beehivegate                 0.42672    161.4060256
Beehivegate                 0.48768    172.7327643
Beehivegate                 0.54864    184.0595029
Beehivegate                 0.6096     192.5545569
Beehivegate                 0.67056    201.0496109
Beehivegate                 0.73152    212.3763495
Beehivegate                 0.79248    220.8714035<!-- Standard PRE tag rules -->
;In the inlet of the wetland there is a sedimentation pond to trap particular material
SedimentationPond Storage    0          0
```

```
SedimentationPond            0.65       1308
SedimentationPond            0.95       1808<!-- Standard PRE tag rules -->

[TIMESERIES]
DailyEvaporation 01/01/2009 0:00       11.2
DailyEvaporation 01/02/2009 0:00       11
DailyEvaporation 01/03/2009 0:00       11
DailyEvaporation 01/04/2009 0:00       10.4
DailyEvaporation 01/05/2009 0:00       11.4
DailyEvaporation 01/06/2009 0:00       11.2
DailyEvaporation 01/07/2009 0:00       10.4
DailyEvaporation 01/08/2009 0:00       12
DailyEvaporation 01/09/2009 0:00       10.4
DailyEvaporation 01/10/2009 0:00       10.8
DailyEvaporation 01/11/2009 0:00       10.8<!-- Standard PRE tag rules -->

......
Too many data points (3751 in total).


DailyRainfall_Canning 01/02/2009 0:00       0
DailyRainfall_Canning 01/03/2009 0:00       0
DailyRainfall_Canning 01/04/2009 0:00       0
DailyRainfall_Canning 01/05/2009 0:00       0
DailyRainfall_Canning 01/06/2009 0:00       0
DailyRainfall_Canning 01/07/2009 0:00       0
DailyRainfall_Canning 01/08/2009 0:00       0
DailyRainfall_Canning 01/09/2009 0:00       0
DailyRainfall_Canning 01/10/2009 0:00       0
DailyRainfall_Canning 01/11/2009 0:00       0
DailyRainfall_Canning 01/12/2009 0:00       0<!-- Multi line missing multiple consecutive spaces but
tabular format data -->

......
Too many data points (3750 in total).


;UpInflow Flow (m^3/s)
InflowWetland    07/18/2012 15:30      0.016
InflowWetland    07/18/2012 15:35      0.016
InflowWetland    07/18/2012 15:40      0.015
InflowWetland    07/18/2012 15:45      0.014
InflowWetland    07/18/2012 15:50      0.014
InflowWetland    07/18/2012 15:55      0.014
InflowWetland    07/18/2012 16:00      0.014
InflowWetland    07/18/2012 16:05      0.014
InflowWetland    07/18/2012 16:10      0.013
InflowWetland    07/18/2012 16:15      0.012
InflowWetland    07/18/2012 16:20      0.012<!-- Standard PRE tag rules -->

......
Too many data points (570306 in total).


MeanTemperature  FILE "D:\RESEARCH PROJECT\7. STRUCTURED DATA\Anvil\Climatology\MeanTemp_Canning.dat"

;Anvil precipitation for calibration
Precipitation_Net10112010 10/11/2010 5:00:00    0
Precipitation_Net10112010 10/11/2010 5:30:00    0
Precipitation_Net10112010 10/11/2010 6:00:00    0
Precipitation_Net10112010 10/11/2010 6:30:00    0
Precipitation_Net10112010 10/11/2010 7:00:00    0
Precipitation_Net10112010 10/11/2010 7:30:00    0
Precipitation_Net10112010 10/11/2010 8:00:00    0
Precipitation_Net10112010 10/11/2010 8:30:00    0
Precipitation_Net10112010 10/11/2010 9:00:00    0
Precipitation_Net10112010 10/11/2010 9:30:00    0
Precipitation_Net10112010 10/11/2010 10:00:00   0
Precipitation_Net10112010 10/11/2010 10:30:00   0
Precipitation_Net10112010 10/11/2010 11:00:00   0
Precipitation_Net10112010 10/11/2010 11:30:00   0
Precipitation_Net10112010 10/11/2010 12:00:00   0
Precipitation_Net10112010 10/11/2010 12:30:00   0
Precipitation_Net10112010 10/11/2010 13:00:00   0
Precipitation_Net10112010 10/11/2010 13:30:00   0
Precipitation_Net10112010 10/11/2010 14:00:00   0
Precipitation_Net10112010 10/11/2010 14:30:00   0.2
Precipitation_Net10112010 10/11/2010 15:00:00   0.8
```

```
Precipitation_Net10112010 10/11/2010 15:30:00   0.2
Precipitation_Net10112010 10/11/2010 16:00:00   1.6
Precipitation_Net10112010 10/11/2010 16:30:00   1.8
Precipitation_Net10112010 10/11/2010 17:00:00   1
Precipitation_Net10112010 10/11/2010 17:30:00   0.4
Precipitation_Net10112010 10/11/2010 18:00:00   0.2
Precipitation_Net10112010 10/11/2010 18:30:00   0
Precipitation_Net10112010 10/11/2010 19:00:00   0.2
Precipitation_Net10112010 10/11/2010 19:30:00   0
Precipitation_Net10112010 10/11/2010 20:00:00   0
Precipitation_Net10112010 10/11/2010 20:30:00   0
Precipitation_Net10112010 10/11/2010 21:00:00   0
Precipitation_Net10112010 10/11/2010 21:30:00   0
Precipitation_Net10112010 10/11/2010 22:00:00   0
Precipitation_Net10112010 10/11/2010 22:30:00   0
Precipitation_Net10112010 10/11/2010 23:00:00   0
Precipitation_Net10112010 10/11/2010 23:30:00   0
Precipitation_Net10112010 11/11/2010 0:00:00    0
Precipitation_Net10112010 11/11/2010 0:30:00    0
Precipitation_Net10112010 11/11/2010 1:00:00    0
Precipitation_Net10112010 11/11/2010 1:30:00    0
Precipitation_Net10112010 11/11/2010 2:00:00    0
Precipitation_Net10112010 11/11/2010 2:30:00    0
Precipitation_Net10112010 11/11/2010 3:00:00    0
Precipitation_Net10112010 11/11/2010 3:30:00    0
Precipitation_Net10112010 11/11/2010 4:00:00    0
Precipitation_Net10112010 11/11/2010 4:30:00    0
Precipitation_Net10112010 11/11/2010 5:00:00    0
Precipitation_Net10112010 11/11/2010 5:30:00    0
Precipitation_Net10112010 11/11/2010 6:00:00    0
Precipitation_Net10112010 11/11/2010 6:30:00    0
Precipitation_Net10112010 11/11/2010 7:00:00    0
Precipitation_Net10112010 11/11/2010 7:30:00    0
Precipitation_Net10112010 11/11/2010 8:00:00    0
Precipitation_Net10112010 11/11/2010 8:30:00    0.4
Precipitation_Net10112010 11/11/2010 9:00:00    0.2<!-- Standard PRE tag rules -->
;Rainfall (mm)
Precipitation_Net15012018 01/15/2018 5:00:00    0.4
Precipitation_Net15012018 01/15/2018 5:30:00    0.2
Precipitation_Net15012018 01/15/2018 6:00:00    2.2
Precipitation_Net15012018 01/15/2018 6:30:00    2.4
Precipitation_Net15012018 01/15/2018 7:00:00    4.4
Precipitation_Net15012018 01/15/2018 7:30:00    4.8
Precipitation_Net15012018 01/15/2018 8:00:00    2.6
Precipitation_Net15012018 01/15/2018 8:30:00    1.4
Precipitation_Net15012018 01/15/2018 9:00:00    0.4
Precipitation_Net15012018 01/15/2018 9:30:00    2
Precipitation_Net15012018 01/15/2018 10:00:00   3
Precipitation_Net15012018 01/15/2018 10:30:00   4.2
Precipitation_Net15012018 01/15/2018 11:00:00   2.6
Precipitation_Net15012018 01/15/2018 11:30:00   0.4
Precipitation_Net15012018 01/15/2018 12:00:00   1
Precipitation_Net15012018 01/15/2018 12:30:00   1
Precipitation_Net15012018 01/15/2018 13:00:00   0.8
Precipitation_Net15012018 01/15/2018 13:30:00   3.2
Precipitation_Net15012018 01/15/2018 14:00:00   1.8
Precipitation_Net15012018 01/15/2018 14:30:00   2.8
Precipitation_Net15012018 01/15/2018 15:00:00   0.4
Precipitation_Net15012018 01/15/2018 15:30:00   2.4
Precipitation_Net15012018 01/15/2018 16:00:00   2.4
Precipitation_Net15012018 01/15/2018 16:30:00   1.4
Precipitation_Net15012018 01/15/2018 17:00:00   1
Precipitation_Net15012018 01/15/2018 17:30:00   1.4
Precipitation_Net15012018 01/15/2018 18:00:00   0.2
Precipitation_Net15012018 01/15/2018 18:30:00   1.8
Precipitation_Net15012018 01/15/2018 19:00:00   0.8
Precipitation_Net15012018 01/15/2018 19:30:00   2.8
Precipitation_Net15012018 01/15/2018 20:00:00   3.6
Precipitation_Net15012018 01/15/2018 20:30:00   2
Precipitation_Net15012018 01/15/2018 21:00:00   0.2
Precipitation_Net15012018 01/15/2018 21:30:00   2
Precipitation_Net15012018 01/15/2018 22:00:00   0.2
Precipitation_Net15012018 01/15/2018 22:30:00   1.4
Precipitation_Net15012018 01/15/2018 23:00:00   0.4
Precipitation_Net15012018 01/15/2018 23:30:00   0.6
Precipitation_Net15012018 01/16/2018 0:00:00    0.4
Precipitation_Net15012018 01/16/2018 0:30:00    2
Precipitation_Net15012018 01/16/2018 1:00:00    1
```

```
Precipitation_Net15012018 01/16/2018 1:30:00    3
Precipitation_Net15012018 01/16/2018 2:00:00    0.2
Precipitation_Net15012018 01/16/2018 2:30:00    0
Precipitation_Net15012018 01/16/2018 3:00:00    1.4
Precipitation_Net15012018 01/16/2018 3:30:00    0
Precipitation_Net15012018 01/16/2018 4:00:00    0.4
Precipitation_Net15012018 01/16/2018 4:30:00    0.2<!-- Standard PRE tag rules -->
RainEvent_19072009 07/19/2009 0:00:00    1.2
RainEvent_19072009 07/19/2009 0:30:00    0
RainEvent_19072009 07/19/2009 1:00:00    1.4
RainEvent_19072009 07/19/2009 1:30:00    0.8
RainEvent_19072009 07/19/2009 2:00:00    1.4
RainEvent_19072009 07/19/2009 2:30:00    0.2
RainEvent_19072009 07/19/2009 3:00:00    0
RainEvent_19072009 07/19/2009 3:30:00    0.2
RainEvent_19072009 07/19/2009 4:00:00    0.2
RainEvent_19072009 07/19/2009 4:30:00    1.6
RainEvent_19072009 07/19/2009 5:00:00    1.4
RainEvent_19072009 07/19/2009 5:30:00    1.4
RainEvent_19072009 07/19/2009 6:00:00    0.6
RainEvent_19072009 07/19/2009 6:30:00    0.6
RainEvent_19072009 07/19/2009 7:00:00    0.6
RainEvent_19072009 07/19/2009 7:30:00    0.4
RainEvent_19072009 07/19/2009 8:00:00    0
RainEvent_19072009 07/19/2009 8:30:00    0.8
RainEvent_19072009 07/19/2009 9:00:00    0
RainEvent_19072009 07/19/2009 9:30:00    0
RainEvent_19072009 07/19/2009 10:00:00   0
RainEvent_19072009 07/19/2009 10:30:00   0.2
RainEvent_19072009 07/19/2009 11:00:00   0
RainEvent_19072009 07/19/2009 11:30:00   0
RainEvent_19072009 07/19/2009 12:00:00   0.2
RainEvent_19072009 07/19/2009 12:30:00   0
RainEvent_19072009 07/19/2009 13:00:00   0
RainEvent_19072009 07/19/2009 13:30:00   0
RainEvent_19072009 07/19/2009 14:00:00   2
RainEvent_19072009 07/19/2009 14:30:00   0.4
RainEvent_19072009 07/19/2009 15:00:00   0.2
RainEvent_19072009 07/19/2009 15:30:00   0
RainEvent_19072009 07/19/2009 16:00:00   0
RainEvent_19072009 07/19/2009 16:30:00   0
RainEvent_19072009 07/19/2009 17:00:00   0.2
RainEvent_19072009 07/19/2009 17:30:00   1.2
RainEvent_19072009 07/19/2009 18:00:00   0
RainEvent_19072009 07/19/2009 18:30:00   0.2
RainEvent_19072009 07/19/2009 19:00:00   0
RainEvent_19072009 07/19/2009 19:30:00   0
RainEvent_19072009 07/19/2009 20:00:00   0.2
RainEvent_19072009 07/19/2009 20:30:00   1.8
RainEvent_19072009 07/19/2009 21:00:00   1.4
RainEvent_19072009 07/19/2009 21:30:00   0.2
RainEvent_19072009 07/19/2009 22:00:00   0.8
RainEvent_19072009 07/19/2009 22:30:00   1.6
RainEvent_19072009 07/19/2009 23:00:00   3.4
RainEvent_19072009 07/19/2009 23:30:00   1
RainEvent_19072009 07/20/2009 0:00:00    0.8
RainEvent_19072009 07/20/2009 0:30:00    0.4
RainEvent_19072009 07/20/2009 1:00:00    0.8
RainEvent_19072009 07/20/2009 1:30:00    0.4
RainEvent_19072009 07/20/2009 2:00:00    0
RainEvent_19072009 07/20/2009 2:30:00    0
RainEvent_19072009 07/20/2009 3:00:00    0
RainEvent_19072009 07/20/2009 3:30:00    0.2
RainEvent_19072009 07/20/2009 4:00:00    0.2
RainEvent_19072009 07/20/2009 4:30:00    0
RainEvent_19072009 07/20/2009 5:00:00    0
RainEvent_19072009 07/20/2009 5:30:00    0
RainEvent_19072009 07/20/2009 6:00:00    0
RainEvent_19072009 07/20/2009 6:30:00    0.8
RainEvent_19072009 07/20/2009 7:00:00    0
RainEvent_19072009 07/20/2009 7:30:00    0
RainEvent_19072009 07/20/2009 8:00:00    1.6
RainEvent_19072009 07/20/2009 8:30:00    0.4
RainEvent_19072009 07/20/2009 9:00:00    22.8
RainEvent_19072009 07/20/2009 9:30:00    0.2
RainEvent_19072009 07/20/2009 10:00:00   0
RainEvent_19072009 07/20/2009 10:30:00   0
RainEvent_19072009 07/20/2009 11:00:00   0.2
```

```
RainEvent_19072009 07/20/2009 11:30:00   0.2
RainEvent_19072009 07/20/2009 12:00:00   1
RainEvent_19072009 07/20/2009 12:30:00   0.2
RainEvent_19072009 07/20/2009 13:00:00   1.2
RainEvent_19072009 07/20/2009 13:30:00   0
RainEvent_19072009 07/20/2009 14:00:00   0.2
RainEvent_19072009 07/20/2009 14:30:00   0
RainEvent_19072009 07/20/2009 15:00:00   0.4
RainEvent_19072009 07/20/2009 15:30:00   0
RainEvent_19072009 07/20/2009 16:00:00   0
RainEvent_19072009 07/20/2009 16:30:00   0
RainEvent_19072009 07/20/2009 17:00:00   0
RainEvent_19072009 07/20/2009 17:30:00   0
RainEvent_19072009 07/20/2009 18:00:00   0.2
RainEvent_19072009 07/20/2009 18:30:00   0.2
RainEvent_19072009 07/20/2009 19:00:00   0
RainEvent_19072009 07/20/2009 19:30:00   0.8
RainEvent_19072009 07/20/2009 20:00:00   0.2
RainEvent_19072009 07/20/2009 20:30:00   0.2
RainEvent_19072009 07/20/2009 21:00:00   0
RainEvent_19072009 07/20/2009 21:30:00   0.6
RainEvent_19072009 07/20/2009 22:00:00   0
RainEvent_19072009 07/20/2009 22:30:00   0.2
RainEvent_19072009 07/20/2009 23:00:00   0
RainEvent_19072009 07/20/2009 23:30:00   0.4<!-- Multi line missing multiple consecutive spaces but
tabular format data -->
;Outflow (m^3/s)
System           01/02/2009 00:01:00   0.047
System           01/02/2009 00:02:00   0.047
System           01/02/2009 00:03:00   0.047
System           01/02/2009 00:04:00   0.047
System           01/02/2009 00:05:00   0.047
System           01/02/2009 00:06:00   0.047
System           01/02/2009 00:07:00   0.047
System           01/02/2009 00:08:00   0.047
System           01/02/2009 00:09:00   0.047
System           01/02/2009 00:10:00   0.047
System           01/02/2009 00:11:00   0.047<!-- Standard PRE tag rules -->

......
Too many data points (921600 in total).


Temperature19072009 07/19/2009 9:00:00    13.25
Temperature19072009 07/20/2009 9:00:00    11<!-- Multi line missing multiple consecutive spaces but
tabular format data -->

[REPORT]
INPUT      YES
CONTROLS   NO
AVERAGES   YES
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL<!-- Standard PRE tag rules -->

[TAGS]
Subcatch   S10              BUILDING
Subcatch   S11              BUILDING
Subcatch   S12              BUILDING
Subcatch   S13              Extract
Subcatch   S14              WDT
Subcatch   S15_1            WDT
Subcatch   S15_10           WDT
Subcatch   S15_12           WDT
Subcatch   S15_2            WDT
Subcatch   S15_3            BUILDING
Subcatch   S15_4            WDT
Subcatch   S15_5            WDT
Subcatch   S15_6            BUILDING
Subcatch   S15_7            WDT
Subcatch   S15_8            WDT
Subcatch   S15_9            WDT
Subcatch   S16              BUILDING
Subcatch   S17              BUILDING
Subcatch   S18_2            BUILDING
Subcatch   S18_3            BUILDING
Subcatch   S19              BUILDING
Subcatch   S2               BUILDING
```

Subcatch	S20	BUILDING
Subcatch	S21	BUILDING
Subcatch	S22	BUILDING
Subcatch	S23_1	WDT
Subcatch	S23_3	WDT
Subcatch	S23_4	WDT
Subcatch	S24	BUILDING
Subcatch	S25	BUILDING
Subcatch	S26_1	WDT_SA1
Subcatch	S26_3	WDT_SA1
Subcatch	S29_1	WDT
Subcatch	S29_10	WDT_SA1
Subcatch	S29_11	WDT_SA1
Subcatch	S29_12	WDT_SA1
Subcatch	S29_13	WDT_SA1
Subcatch	S29_14	WDT_SA1
Subcatch	S29_15	BUILDING
Subcatch	S29_17	BUILDING
Subcatch	S29_2	BUILDING
Subcatch	S29_3	WDT
Subcatch	S29_5	WDT_SA1
Subcatch	S29_7	WDT_SA1
Subcatch	S29_8	WDT
Subcatch	S29_9	WDT_SA1
Subcatch	S3	WDT_SA1
Subcatch	S30	BUILDING
Subcatch	S31	BUILDING
Subcatch	S32	BUILDING
Subcatch	S33	BUILDING
Subcatch	S34	BUILDING
Subcatch	S35	BUILDING
Subcatch	S36	BUILDING
Subcatch	S37	WDT_SA1
Subcatch	S37_1	WDT
Subcatch	S37_10	WDT
Subcatch	S37_11	WDT
Subcatch	S37_12	WDT
Subcatch	S37_2	WDT
Subcatch	S37_3	WDT
Subcatch	S37_4	WDT
Subcatch	S37_8	WDT
Subcatch	S38	BUILDING
Subcatch	S39	BUILDING
Subcatch	S4	BUILDING
Subcatch	S40	BUILDING
Subcatch	S41	BUILDING
Subcatch	S42	BUILDING
Subcatch	S43	Wetland
Subcatch	S43_2	WDT_SA1
Subcatch	S43_4	WDT_SA1
Subcatch	S43_5	WDT_SA1
Subcatch	S43_6	WDT_SA1
Subcatch	S43_7	WDT_SA1
Subcatch	S43_9	WDT_SA1
Subcatch	S44	BUILDING
Subcatch	S45	BUILDING
Subcatch	S46	BUILDING
Subcatch	S46_1	WDT_SA1
Subcatch	S46_10	WDT_SA1
Subcatch	S46_2	WDT_SA1
Subcatch	S46_3	WDT_SA1
Subcatch	S46_4	WDT_SA1
Subcatch	S46_5	WDT_SA1
Subcatch	S46_6	WDT_SA1
Subcatch	S46_7	WDT_SA1
Subcatch	S47	BUILDING
Subcatch	S48	BUILDING
Subcatch	S49	BUILDING
Subcatch	S5	BUILDING
Subcatch	S50	BUILDING
Subcatch	S51	BUILDING
Subcatch	S52_1	WDT_SA1
Subcatch	S52_2	WDT_SA1
Subcatch	S52_3	WDT_SA1
Subcatch	S52_4	WDT_SA1
Subcatch	S52_6	WDT_SA1
Subcatch	S52_7	WDT_SA1
Subcatch	S53	BUILDING

Subcatch	S54	BUILDING
Subcatch	S55	BUILDING
Subcatch	S56	BUILDING
Subcatch	S57	BUILDING
Subcatch	S59	BUILDING
Subcatch	S63_1	WDT_SA1
Subcatch	S63_11	WDT_SA1
Subcatch	S63_12	WDT_SA1
Subcatch	S63_13	WDT_SA1
Subcatch	S63_14	WDT_SA1
Subcatch	S63_15	WDT_SA1
Subcatch	S63_2	WDT_SA1
Subcatch	S63_3	WDT_SA1
Subcatch	S63_4	WDT_SA1
Subcatch	S63_5	WDT_SA1
Subcatch	S63_6	WDT_SA1
Subcatch	S63_7	WDT_SA1
Subcatch	S63_8	WDT_SA1
Subcatch	S63_9	WDT_SA1
Subcatch	S7	BUILDING
Subcatch	S8	BUILDING
Subcatch	S9	BUILDING
Node	J1788	SITE6162796
Node	J2887	SITE6162962
Link	206110366	MainPipe
Link	206110379_1	MainPipe
Link	206110379_2	MainPipe
Link	206110379_4	MainPipe
Link	206110379_5	MainPipe
Link	22803188_2	OpenChannel
Link	22803188_3	OpenChannel
Link	22803188_4	OpenChannel
Link	22803188_5	OpenChannel
Link	22926618_1	OpenChannel
Link	22926618_2	OpenChannel
Link	22926618_3	OpenChannel
Link	22926618_4	OpenChannel
Link	22926629	OpenChannel
Link	23116769	MainPipe
Link	23116814	MainPipe
Link	23116826	MainPipe
Link	23405543	MainPipe
Link	23405563	MainPipe
Link	57466689_1	MainPipe
Link	57466741	MainPipe
Link	57466813	MainPipe
Link	C1	Secondary
Link	C1_1	Secondary
Link	C1_2	Secondary
Link	C10	Secondary
Link	C108	Secondary
Link	C109	Secondary
Link	C11	Secondary
Link	C110	Secondary
Link	C111	Secondary
Link	C112	Secondary
Link	C113	Secondary
Link	C12	Secondary
Link	C126	Secondary
Link	C127	Secondary
Link	C128	Secondary
Link	C129_1	Secondary
Link	C129_2	Secondary
Link	C13	Secondary
Link	C130	Secondary
Link	C131	Secondary
Link	C141	Secondary
Link	C142	Secondary
Link	C143	Secondary
Link	C144	Secondary
Link	C145	Secondary
Link	C146	Secondary
Link	C147	Secondary
Link	C148	Secondary
Link	C158	Secondary
Link	C159	Secondary
Link	C16	Secondary
Link	C160	Secondary

```
Link       C161            Secondary
Link       C167_2          Secondary
Link       C169            Secondary
Link       C17             Secondary
Link       C170            Secondary
Link       C176            OpenChannel
Link       C18             Secondary
Link       C182            Secondary
Link       C185            Secondary
Link       C186            Secondary
Link       C19             Secondary
Link       C193            Secondary
Link       C194            Secondary
Link       C195            Secondary
Link       C196            Secondary
Link       C20             Secondary
Link       C21             Secondary
Link       C22             Secondary
Link       C23             Secondary
Link       C24             Secondary
Link       C25             Secondary
Link       C26             Secondary
Link       C27             Secondary
Link       C28             Secondary
Link       C29             Secondary
Link       C3              Secondary
Link       C30             Secondary
Link       C31             Secondary
Link       C32             Secondary
Link       C33             Secondary
Link       C34             Secondary
Link       C35             Secondary
Link       C37             Secondary
Link       C38             Secondary
Link       C39             Secondary
Link       C4              Secondary
Link       C40             Secondary
Link       C41             Secondary
Link       C42             Secondary
Link       C44             Secondary
Link       C45             Secondary
Link       C46             Secondary
Link       C47             Secondary
Link       C49             Secondary
Link       C5              Secondary
Link       C50             Secondary
Link       C51             Secondary
Link       C52             Secondary
Link       C53             Secondary
Link       C54             Secondary
Link       C55             Secondary
Link       C56             Secondary
Link       C57             Secondary
Link       C58             Secondary
Link       C59             Secondary
Link       C6              Secondary
Link       C60             Secondary
Link       C61             Secondary
Link       C62             Secondary
Link       C63             Secondary
Link       C65             Secondary
Link       C66             Secondary
Link       C67             Secondary
Link       C68             Secondary
Link       C7              Secondary
Link       C70             Secondary
Link       C8              Secondary
Link       C95             Secondary
Link       C96             Secondary
Link       C97             Secondary
Link       22926618_6      OpenChannel<!-- Standard PRE tag rules -->

[MAP]
DIMENSIONS       398805.4205      6459555.4531     399946.9235      6460565.1849
UNITS            Meters<!-- Standard PRE tag rules -->

[COORDINATES]
;;Node           X-Coord          Y-Coord
```

```
;;-------------- ---------------- ----------------
J1               399197.305       6460229.757
J10              399260.054       6460206.219
J1040            399469.516       6459823.245
J11              399256.887       6460222.68
J12              399302.225       6460422.998
J13              399320.993       6460300.764
J14              399253.344       6460213
J1415            399431.896       6460000.328
J15              398978.916       6460194.465
J16              399281.445       6460128.954
J17              398982.456       6460211.435
J1701            399403.636       6460246.674
J1788            399476.978       6459873.079
J18              398983.792       6460179.049
J19              399658.215       6459991.701
J1969            399491.903       6459957.783
J2               399262.005       6460210.425
J20              398975.813       6460216.802
J21              399281.864       6460116.293
J2181            398881.963       6460218.562
J22              399117.121       6460122.566
J2293            398988.781       6460186.982
J23              399058.4         6460170.453
J2312            398996.538       6460184.559
J24              399019.976       6460179.966
J25              399124.364       6460154.51
J2510            399172.717       6460136.572
J2594            399236.254       6460113.123
J26              399058.921       6460173.916
J2678            399301.08        6460093.436
J2692            399319.153       6460088.442
J27              399659.522       6459992.075
J2709            399334.483       6459745.528
J2712            399335.071       6459750.51
J2717            399340.338       6459827.346
J2719            399342.126       6459825.604
J2722            399348.75        6459967.199
J2728            399360.633       6459799.18
J2730            399365.374       6459802.178
J2749            399382.112       6459800.666
J2754            399389.557       6460249.812
J2755            399390.164       6460131.861
J2757            399393.141       6459845.119
J2764            399396.777       6460248.179
J2771            399398.609       6460010.513
J2779            399402.467       6460242.47
J2785            399410.01        6459731.986
J2786            399410.463       6459829.825
J2787            399411.625       6460293.515
J2794            399421.163       6459828.642
J2797            399422.825       6459893.748
J28              399020.934       6460185.167
J2813            399425.724       6460016.721
J2816            399425.84        6460025.315
J2822            399428.045       6459896.141
J2831            399433.805       6459949.231
J2838            399439.055       6460028.91
J2839            399440.815       6460231.622
J2845            399444.015       6459988.3
J2847            399445.566       6460237.476
J2855            399451.861       6459795.752
J2857            399452.527       6459994.151
J2860            399460.446       6460111.393
J2868            399469.988       6460147.503
J2870            399471.599       6460146.992
J2887            399478.548       6459986.383
J2890            399479.577       6460144.021
J2891            399480.813       6459873.117
J29              399768.438       6459801.465
J29_14           399684.862       6459729.111
J2909            399493.486       6460220.03
J2915            399497.491       6459980.942
J2918            399509.12        6460267.105
J2921            399510.228       6459948.071
J2931            399519.353       6459938.821
J2938            399529.643       6460332.355
J3               399132.494       6460262.847
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J30             399774.88       6459808.11
J31             399764.791      6459801.234
J32             399764.014      6459797.361
J33             399612.149      6459945.478
J34             399613.992      6459945.468
J35             399574.325      6459887.471
J36             399557.54       6459853.05
J37             399621.798      6459745.98
J38             399653.377      6459753.232
J39             399671.7        6459747.856
J4              399093.302      6460274.155
J40             399686.74       6459733.868
J41             399688.706      6459733.375
J42             399632.737      6459931.975
J43             399730.874      6459834.923
J44             399728.958      6459832.687
J45             399578.456      6460030.91
J46             399550.314      6460173.841
J47             399563.596      6459895.196
J48             399551.272      6459795.022
J49             399479.158      6459894.527
J5              399212.806      6460321.425
J50             399590.445      6459744.48
J52             399549.065      6459792.548
J53             399548.935      6459791.34
J55             399533.544      6460114.773
J56             399704.756      6460038.748
J57             399719.649      6460029.139
J59             399667.533      6459985.613
J6              399189.897      6460245.62
J63             399637.08       6459931.047
J64             399643.418      6459937.498
J65             399539.483      6459794.13
J66             399549.433      6459776.642
J67             399571.34       6459747.826
J68             399699.902      6459744.101
J69             399538.697      6459792.389
J7              399183.374      6460180.216
J70             399678.638      6459886.764
J72             399574.147      6459888.772
J73             399726.959      6459830.603
J78             399680.977      6459887.813
J79             399687.446      6459894.139
J8              399123.452      6460151.175
J80             399580.657      6459756.357
J83             399575.164      6459891.013
J9              399257.655      6460372.366
J355            399430.348      6459607.009
J54             399545.068      6460094.129<!-- Standard PRE tag rules -->

[VERTICES]
;;Link           X-Coord         Y-Coord
;;-------------- --------------- ---------------
206110366       399212.17       6460125.045
206110366       399218.344      6460123.001
206110379_1     399003.086      6460183.252
206110379_1     399007.337      6460182.425
206110379_2     399125.257      6460150.633
206110379_4     399060.669      6460169.78
206110379_5     399023.913      6460179.2
206110379_5     399042.987      6460175.016
22803188_2      399543.06       6460045.188
22803188_2      399530.668      6460035.563
22803188_2      399557.402      6460005.857
22803188_2      399550.122      6459999.207
22803188_2      399512.061      6459985.675
22803188_3      399547.014      6460091.237
22803188_3      399566.246      6460077.538
22803188_3      399587.731      6460058.744
22803188_3      399591.547      6460044.182
22803188_3      399579.925      6460030.911
22803188_4      399546.274      6460159.78
22803188_5      399532.851      6460112.309
22926618_2      399481.02       6459912.84
22926618_3      399468.184      6459816.094
22926618_3      399466.896      6459813.389
22926618_3      399452.65       6459797.701
22926618_4      399474.788      6459851.53
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23116814          399434.053       6459999.654
23116814          399434.053       6459999.66
57466741          399325.345       6460082.355
C108              399507.973       6459950.301
C108              399505.977       6459951.57
C108              399504.019       6459952.452
C108              399502.747       6459953.34
C108              399501.145       6459954.155
C108              399498.831       6459955.172
C108              399497.016       6459956.069
C108              399495.687       6459956.748
C108              399494.735       6459957.473
C108              399493.644       6459957.906
C108              399492.496       6459958.075
C176              399443.574       6459723.038<!-- Standard PRE tag rules -->

[POLYGONS]
;;Subcatchment   X-Coord          Y-Coord
;;-------------- ---------------- ----------------
S1                399599.959       6459771
S1                399602.191       6459771
S1                399625.527       6459773.554
S1                399626           6459786
S1                399626           6459791
S1                399627.856       6459791
S1                399628.251       6459793.958
S1                399664.158       6459790.143
S1                399653.453       6459758.802
S1                399627.666       6459749.232
S1                399617.944       6459729.957
S1                399579.926       6459732.323
S1                399542.893       6459733.533
S1                399598.979       6459781.461
S1                399599.959       6459771
S10               399696.029       6460162.171
S10               399710.028       6460211.482
S10               399731.394       6460208.873
S10               399734.343       6460210.485
S10               399740.046       6460219.117
S10               399745.481       6460219.923
S10               399748.16        6460218.327
S10               399747.396       6460216
S10               399746           6460216
S10               399746           6460211.746
S10               399739.19        6460191
S10               399736           6460191
S10               399736           6460186
S10               399737.549       6460186
S10               399729.344       6460161
S10               399726           6460161
S10               399726           6460153.172
S10               399696.029       6460162.171
S11               399595.745       6459816
S11               399594.808       6459826
S11               399596           6459826
S11               399596           6459836
S11               399606           6459836
S11               399606           6459841
S11               399613.536       6459841
S11               399613.225       6459833.214
S11               399623.95        6459804.668
S11               399625.056       6459795.162
S11               399628.251       6459793.958
S11               399627.856       6459791
S11               399626           6459791
S11               399626           6459786
S11               399627.189       6459786
S11               399625.527       6459773.554
S11               399602.191       6459771
S11               399599.959       6459771
S11               399596           6459813.274
S11               399596           6459816
S11               399595.745       6459816
S12               399236           6460374.834
S12               399171.009       6460434.606
S12               399171           6460434.607
S12               399171.006       6460434.608
S12               399176.324       6460435.345
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S12	399181	6460435.993
S12	399201.788	6460461.719
S12	399216	6460446
S12	399216	6460443.818
S12	399216	6460441
S12	399219.336	6460441
S12	399231	6460431.148
S12	399231	6460426
S12	399236	6460426
S12	399236.899	6460426
S12	399246	6460417.263
S12	399246	6460416
S12	399247.315	6460416
S12	399251	6460412.463
S12	399251	6460411
S12	399252.524	6460411
S12	399261	6460402.863
S12	399261	6460398.572
S12	399259.328	6460396
S12	399256	6460396
S12	399256	6460391
S12	399251	6460391
S12	399251	6460383.183
S12	399250.86	6460382.968
S12	399248.162	6460381
S12	399246	6460381
S12	399246	6460379.423
S12	399241.308	6460376
S12	399236	6460376
S12	399236	6460374.834
S13	399304.73	6460276.227
S13	399299.309	6460267.792
S13	399235.903	6460288.461
S13	399239.861	6460296.45
S13	399304.73	6460276.227
S14	399171.588	6460405.244
S14	399159.302	6460419.22
S14	399171	6460434.614
S14	399236	6460375.993
S14	399208.299	6460363.455
S14	399184.103	6460391
S14	399181	6460391
S14	399181	6460394.532
S14	399171.588	6460405.244
S15_1	399051	6460179.467
S15_1	399031.18	6460188.671
S15_1	399041	6460204.593
S15_1	399041	6460206
S15_1	399041.868	6460206
S15_1	399046	6460212.699
S15_1	399046	6460216
S15_1	399048.036	6460216
S15_1	399051.12	6460221
S15_1	399051	6460221
S15_1	399051	6460223.648
S15_1	399051	6460226
S15_1	399053.033	6460226
S15_1	399054.203	6460226
S15_1	399057.118	6460230.726
S15_1	399057.287	6460231
S15_1	399056	6460231
S15_1	399056	6460238.386
S15_1	399056	6460238.53
S15_1	399044.996	6460245.428
S15_1	399060.637	6460245.197
S15_1	399066.289	6460242.416
S15_1	399066	6460241.738
S15_1	399066	6460241
S15_1	399066	6460236
S15_1	399063.553	6460236
S15_1	399051	6460206.572
S15_1	399051	6460206
S15_1	399056	6460206
S15_1	399056	6460201
S15_1	399061	6460201
S15_1	399061	6460196
S15_1	399056	6460196
S15_1	399056	6460191

S15_1	399051	6460191
S15_1	399051	6460181
S15_1	399051	6460179.467
S15_10	398992.048	6460167.842
S15_10	399001.106	6460195.798
S15_10	399021.114	6460189.073
S15_10	399029.657	6460186.202
S15_10	399031.18	6460188.671
S15_10	399034.305	6460187.219
S15_10	399018.663	6460154.438
S15_10	399012.029	6460162.135
S15_10	399006.169	6460166.276
S15_10	399001.824	6460166.758
S15_10	398992.048	6460167.842
S15_12	399001.106	6460195.798
S15_12	398992.048	6460167.842
S15_12	398988.166	6460168.273
S15_12	398981.172	6460169.776
S15_12	398955.701	6460175.25
S15_12	398949.246	6460174.928
S15_12	398948.066	6460173.875
S15_12	398955.18	6460203.721
S15_12	398993.52	6460199.306
S15_12	398993.068	6460198.5
S15_12	398998.79	6460196.577
S15_12	399001.106	6460195.798
S15_2	398981.855	6460283.995
S15_2	399067.808	6460357.575
S15_2	399065.369	6460334.352
S15_2	399054.46	6460315.26
S15_2	399052.307	6460307.413
S15_2	399043.332	6460291.388
S15_2	399025.105	6460274.616
S15_2	399022.693	6460267.145
S15_2	399022.952	6460264.408
S15_2	398958.999	6460219.745
S15_2	398948.066	6460173.875
S15_2	398944.246	6460170.465
S15_2	398943.661	6460169.427
S15_2	398885.712	6460173.577
S15_2	398981.855	6460283.995
S15_3	399235.903	6460288.468
S15_3	399299.309	6460267.798
S15_3	399281	6460246
S15_3	399281	6460241
S15_3	399282.068	6460241
S15_3	399281.629	6460240.317
S15_3	399223.088	6460262.604
S15_3	399235.903	6460288.468
S15_4	398993.52	6460199.306
S15_4	398955.18	6460203.721
S15_4	398958.999	6460219.745
S15_4	399022.952	6460264.408
S15_4	399023.503	6460258.6
S15_4	399027.267	6460254.746
S15_4	399023.253	6460252.296
S15_4	399006	6460221.548
S15_4	399006	6460216
S15_4	399002.887	6460216
S15_4	398996	6460203.726
S15_4	398996	6460201
S15_4	398994.47	6460201
S15_4	398993.52	6460199.306
S15_5	398884.393	6460173.671
S15_5	398943.661	6460169.427
S15_5	398940.647	6460164.074
S15_5	398930.691	6460144.03
S15_5	398919.192	6460115.529
S15_5	398908.166	6460076.554
S15_5	398907.307	6460057.413
S15_5	398907.307	6460052.413
S15_5	398900.955	6460043.766
S15_5	398891.394	6460038.326
S15_5	398857.307	6460037.413
S15_5	398858.166	6460071.554
S15_5	398868.113	6460116.608
S15_5	398881.453	6460158.268
S15_5	398884.393	6460173.671

S15_6	399255.986	6460291
S15_6	399239.861	6460296.457
S15_6	399242.112	6460301
S15_6	399246	6460301
S15_6	399246	6460306
S15_6	399246	6460308.846
S15_6	399247.067	6460311
S15_6	399251	6460311
S15_6	399251	6460315.402
S15_6	399261	6460312.474
S15_6	399261	6460311
S15_6	399266.032	6460311
S15_6	399276	6460308.081
S15_6	399276	6460306
S15_6	399281	6460306
S15_6	399281	6460306.616
S15_6	399286.285	6460305.068
S15_6	399291	6460302.636
S15_6	399291	6460301
S15_6	399294.171	6460301
S15_6	399314.059	6460290.739
S15_6	399304.73	6460276.234
S15_6	399291	6460280.329
S15_6	399291	6460281
S15_6	399288.751	6460281
S15_6	399276	6460284.803
S15_6	399276	6460286
S15_6	399271.986	6460286
S15_6	399261.668	6460289.077
S15_6	399256	6460290.995
S15_6	399256	6460291
S15_6	399255.986	6460291
S15_7	398981.855	6460283.995
S15_7	398885.712	6460173.577
S15_7	398884.393	6460173.671
S15_7	398886.174	6460182.999
S15_7	398883.909	6460194.025
S15_7	398873.22	6460213.326
S15_7	398872.307	6460227.413
S15_7	398893.274	6460225.216
S15_7	398898.328	6460226.94
S15_7	398941.282	6460283.439
S15_7	398963.279	6460306.442
S15_7	398970.32	6460324.401
S15_7	398981.98	6460332.741
S15_7	398986.448	6460343.273
S15_7	398988.166	6460352.926
S15_7	399006.77	6460372.159
S15_7	399001.653	6460376.919
S15_7	399003.305	6460380.416
S15_7	399010.73	6460373.788
S15_7	399011	6460374.071
S15_7	399011	6460376
S15_7	399012.831	6460376
S15_7	399026	6460389.867
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S63_12	399400.526	6459900.742
S63_12	399400.378	6459901.168
S63_12	399409.465	6459920.255
S63_12	399417.307	6459927.413
S63_12	399433.274	6459925.216
S63_12	399438.328	6459926.94
S63_12	399439.519	6459928.827
S63_12	399433.822	6459872.568
S63_13	399382.015	6459819.563
S63_13	399433.117	6459865.606
S63_13	399420.567	6459741.65
S63_13	399371.033	6459781.335
S63_13	399370.981	6459781.286
S63_13	399360.53	6459801.807
S63_13	399382.555	6459818.702
S63_13	399382.015	6459819.563
S63_14	399400.526	6459900.742
S63_14	399433.822	6459872.568
S63_14	399433.117	6459865.606
S63_14	399382.015	6459819.563
S63_14	399363.856	6459848.535
S63_14	399388.788	6459861.68
S63_14	399398.564	6459852.318
S63_14	399410.32	6459863.548
S63_14	399403.722	6459870.924
S63_14	399406.116	6459873.595
S63_14	399406.97	6459882.194
S63_14	399400.526	6459900.742
S63_15	399291.693	6459782.755
S63_15	399332.618	6459757.177
S63_15	399327.384	6459752.731
S63_15	399332.923	6459745.245
S63_15	399257.818	6459671.209
S63_15	399254.028	6459674.668
S63_15	399259.499	6459675.758

S63_15	399261.706	6459682.477
S63_15	399259.519	6459693.971
S63_15	399260.383	6459699.884
S63_15	399268.972	6459705.201
S63_15	399284.133	6459706.134
S63_15	399289.456	6459710.167
S63_15	399290.896	6459713.278
S63_15	399290.31	6459720.534
S63_15	399287.248	6459727.355
S63_15	399275.383	6459741.613
S63_15	399283.166	6459761.554
S63_15	399291.169	6459773.541
S63_15	399291.916	6459782.14
S63_15	399291.693	6459782.755
S63_2	399420.567	6459741.65
S63_2	399439.519	6459928.827
S63_2	399443.918	6459935.802
S63_2	399450.745	6459953.966
S63_2	399454.836	6459959.337
S63_2	399457.585	6459960.416
S63_2	399470.702	6459958.95
S63_2	399479.883	6459924.977
S63_2	399490.618	6459916
S63_2	399489.949	6459916
S63_2	399486.666	6459875.07
S63_2	399499.569	6459871
S63_2	399501	6459871
S63_2	399501	6459870.549
S63_2	399514.448	6459866.307
S63_2	399513.855	6459865.856
S63_2	399501.879	6459862.354
S63_2	399485.819	6459864.506
S63_2	399477.218	6459757.282
S63_2	399476.575	6459749.262
S63_2	399475.27	6459732.994
S63_2	399473.498	6459731.222
S63_2	399468.775	6459702.448
S63_2	399458.686	6459711.11
S63_2	399420.567	6459741.65
S63_3	399357.107	6459831.548
S63_3	399303.752	6459798.689
S63_3	399279.492	6459796.872
S63_3	399278.494	6459798.6
S63_3	399276.174	6459821.281
S63_3	399272.307	6459827.413
S63_3	399277.366	6459842.355
S63_3	399281.506	6459848.214
S63_3	399282.174	6459848.697
S63_3	399316	6459819.698
S63_3	399316	6459821
S63_3	399320.155	6459821
S63_3	399326	6459825.769
S63_3	399326	6459826
S63_3	399326.283	6459826
S63_3	399331	6459829.849
S63_3	399331	6459831
S63_3	399332.41	6459831
S63_3	399338.538	6459836
S63_3	399336	6459836
S63_3	399336	6459840.229
S63_3	399334.607	6459841.341
S63_3	399337.133	6459843.366
S63_3	399339.346	6459841
S63_3	399341	6459841
S63_3	399341	6459839.232
S63_3	399344.023	6459836
S63_3	399346.598	6459836
S63_3	399354.7	6459843.284
S63_3	399357.107	6459831.548
S63_4	399367.99	6459715.993
S63_4	399374.345	6459715.993
S63_4	399308.587	6459645.202
S63_4	399323.883	6459634.499
S63_4	399317.413	6459631.098
S63_4	399297.878	6459634.645
S63_4	399257.818	6459671.209
S63_4	399259.499	6459675.751
S63_4	399296	6459643.626

S63_4	399367.99	6459715.993
S63_5	399383.847	6459624.977
S63_5	399382.95	6459626.438
S63_5	399403.229	6459650.147
S63_5	399402.994	6459648.169
S63_5	399383.847	6459624.977
S63_6	399390.707	6459675.87
S63_6	399344.193	6459626.236
S63_6	399317.413	6459631.098
S63_6	399392.237	6459707.479
S63_6	399416.763	6459743.441
S63_6	399406.77	6459674.292
S63_6	399390.707	6459675.87
S63_7	399383.847	6459624.977
S63_7	399402.994	6459648.169
S63_7	399398.402	6459616.393
S63_7	399344.193	6459626.236
S63_7	399360.173	6459643.287
S63_7	399383.847	6459624.977
S63_8	399382.555	6459818.702
S63_8	399360.53	6459801.807
S63_8	399359.974	6459802.899
S63_8	399303.752	6459798.689
S63_8	399357.107	6459831.548
S63_8	399354.7	6459843.284
S63_8	399357.733	6459846.011
S63_8	399359.192	6459846.076
S63_8	399363.856	6459848.535
S63_8	399382.555	6459818.702
S63_9	399369.752	6459748.01
S63_9	399388.472	6459767.362
S63_9	399416.926	6459744.566
S63_9	399416.763	6459743.441
S63_9	399392.237	6459707.479
S63_9	399390.09	6459705.288
S63_9	399367.99	6459715.993
S63_9	399356	6459730.993
S63_9	399332.923	6459745.251
S63_9	399327.384	6459752.738
S63_9	399333.059	6459755.315
S63_9	399342.772	6459765.81
S63_9	399369.752	6459748.01
S7	399410.32	6459863.548
S7	399398.564	6459852.318
S7	399351.687	6459897.212
S7	399366.287	6459912.772
S7	399410.32	6459863.548
S8	399391	6460145.784
S8	399387.468	6460141
S8	399371	6460141
S8	399371	6460146
S8	399356	6460146
S8	399356	6460151
S8	399355.598	6460151
S8	399376.563	6460185.662
S8	399381	6460184.431
S8	399381	6460181
S8	399393.366	6460181
S8	399406	6460177.495
S8	399406	6460176
S8	399411.388	6460176
S8	399412.982	6460175.558
S8	399394.851	6460151
S8	399391	6460151
S8	399391	6460145.784
S9	399636	6460186.296
S9	399643.445	6460212.861
S9	399654.465	6460204.572
S9	399675.95	6460200.49
S9	399680.198	6460204.62
S9	399684.47	6460213.532
S9	399686.609	6460214.342
S9	399690.735	6460213.838
S9	399677.744	6460171
S9	399676	6460171
S9	399676	6460165.25
S9	399675.003	6460161.964
S9	399671	6460163.907

```
S9                399671           6460166
S9                399666.689       6460166
S9                399641           6460178.469
S9                399641           6460181
S9                399635.786       6460181
S9                399634.668       6460181.543
S9                399635.917       6460186
S9                399636           6460186
S9                399636           6460186.296<!-- Standard PRE tag rules -->

[SYMBOLS]
;;Gage           X-Coord          Y-Coord
;;-------------- ---------------- ----------------<!-- Standard PRE tag rules -->
```

B. My without-groundwater components model

```
[OPTIONS]
;;Options             Value
;;------------------ ------------
FLOW_UNITS            CMS
INFILTRATION          MODIFIED_HORTON
FLOW_ROUTING          DYNWAVE
LINK_OFFSETS          ELEVATION
MIN_SLOPE             0
ALLOW_PONDING         NO
SKIP_STEADY_STATE     NO
START_DATE            01/01/2014
START_TIME            00:00:00
REPORT_START_DATE     01/01/2014
REPORT_START_TIME     00:00:00
END_DATE              12/31/2014
END_TIME              00:00:00
SWEEP_START           01/01
SWEEP_END             12/31
DRY_DAYS              0
REPORT_STEP           00:01:00
WET_STEP              00:05:00
DRY_STEP              00:05:00
ROUTING_STEP          5
RULE_STEP             00:00:00
INERTIAL_DAMPING      PARTIAL
NORMAL_FLOW_LIMITED   BOTH
FORCE_MAIN_EQUATION   H-W
VARIABLE_STEP         0.75
LENGTHENING_STEP      0
MIN_SURFAREA          0
MAX_TRIALS            8
HEAD_TOLERANCE        0.0015
SYS_FLOW_TOL          5
LAT_FLOW_TOL          5
MINIMUM_STEP          0.5
THREADS               4<!-- Standard PRE tag rules -->

[EVAPORATION]
;;Type          Parameters
;;------------- ----------
TIMESERIES   DailyEvaporation
DRY_ONLY     YES<!-- Standard PRE tag rules -->

[TEMPERATURE]
TIMESERIES   MeanTemperature
WINDSPEED    MONTHLY    19.7 19.05 17.35 14.7 12.85 13.2 13.45 14.5 15.85 19.4 19.65 16.45
SNOWMELT               34 0.5 0.6 0.0 50.0 0.0
ADC          IMPERVIOUS 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
ADC          PERVIOUS   1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0<!-- Standard PRE tag rules -->

[RAINGAGES]
;;                       Rain      Time   Snow   Data
;;Name                   Type      Intrvl Catch  Source
;;---------------------- --------- ------ ------ ----------
Chicago_3h               INTENSITY 0:05   1.0    TIMESERIES Chicago_3h
DailyRainfall_Canning    VOLUME    24:00  1.0    TIMESERIES DailyRainfall_Canning
Florida_Type_II_1mm      INTENSITY 0:30   1.0    TIMESERIES Florida_Type_II_1mm
NOAA_Type_A_1mm          INTENSITY 0:06   1.0    TIMESERIES NOAA_Type_A_1mm
Precipitation_Net15012018 INTENSITY 0:30   1.0    TIMESERIES Precipitation_Net15012018
RainEvent_19072009       INTENSITY 0:30   1.0    TIMESERIES RainEvent_19072009<!-- Standard PRE tag
rules -->
```

```
[SUBCATCHMENTS]
;;                                                Total     Pcnt.              Pcnt.     Curb      Snow
;;Name           Raingage         Outlet           Area      Imperv    Width    Slope     Length    Pack
;;-------------- ---------------- ---------------- -------- -------- -------- -------- -------- --------
S1               DailyRainfall_Canning J80         0.3717   52.136   37.17    0.5       0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
220-
03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177558678&amp;sdata=KmEGql9OOI0yyU1Vj%2BKdXSBjRTldmPOpDxfG18qGgas%3D&amp;re
served=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S10              DailyRainfall_Canning S43_7       0.1883   100      47.075   0.05      0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&amp;sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&amp;rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S11              DailyRainfall_Canning J80         0.1631   100      40.775   0.05      0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&amp;sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&amp;rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S12              DailyRainfall_Canning J9          0.328    85.661   68.95    0.05      0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&amp;sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&amp;rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S13              DailyRainfall_Canning S23_4       0.0623   48.572   70       0.5       0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
220-
03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&amp;sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&amp;rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S14              DailyRainfall_Canning J9          0.1929   53.816   167.216  3.2       0
S15_1            DailyRainfall_Canning S15_10      0.0772   38.009   12.254   3.828     0
S15_10           DailyRainfall_Canning J24         0.093    37.412   28.822   3.828     0
S15_12           DailyRainfall_Canning J2312       0.1353   64.066   30.75    3.828     0
S15_2            DailyRainfall_Canning J20         0.7757   65.844   58.647   3.828     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&amp;sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&amp;rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S15_3            DailyRainfall_Canning J11         0.1895   100      48.55    0.05      0
S15_4            DailyRainfall_Canning J17         0.1955   56.802   27.153   3.828     0
S15_5            DailyRainfall_Canning J18         0.6841   67.95    51.721   3.828     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
220-
03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&amp;sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&amp;rese
rved=0
```

;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S15_6 DailyRainfall_Canning S29_1 0.1401 100 35.025 0.05 0
S15_7 DailyRainfall_Canning J2181 1.5126 66.6 114.36 3.828 0
S15_8 DailyRainfall_Canning J26 0.0604 37.965 14.732 3.828 0
S15_9 DailyRainfall_Canning J23 0.3905 26.281 41.543 3.828 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S16 DailyRainfall_Canning J13 0.0564 100 14.1 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S17 DailyRainfall_Canning J2918 0.1816 100 45.4 0.05 0
S18_2 DailyRainfall_Canning J32 0.6703 98.672 67.03 0.05 0
S18_3 DailyRainfall_Canning J30 0.203 100 20.3 0.05 0
S18_4 DailyRainfall_Canning J30 0.2343 100 41.839 0.5 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S19 DailyRainfall_Canning J28 0.2406 100 60.15 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S2 DailyRainfall_Canning J79 1.169 98.794 276.274 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S20 DailyRainfall_Canning J3 0.0728 100 18.2 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S21 DailyRainfall_Canning J26 0.1829 100 45.725 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-
03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0

;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S22 DailyRainfall_Canning J7 0.0773 100 152.165 2.218 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S23 DailyRainfall_Canning J25 0.1345 58.387 59.999 0.5 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S23_1 DailyRainfall_Canning J4 0.9466 65.317 167.211 3.2 0
S23_3 DailyRainfall_Canning J12 0.5648 60.553 54.499 3.2 0
S23_4 DailyRainfall_Canning J6 1.1682 56.237 112.723 3.2 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S24 DailyRainfall_Canning S15_9 0.0596 100 14.9 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S25 DailyRainfall_Canning J57 0.1097 100 27.425 0.05 0
S26_1 DailyRainfall_Canning J2787 0.141 56.387 23.016 3.235 0
S26_3 DailyRainfall_Canning J2909 0.958 60.166 156.378 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S29_1 DailyRainfall_Canning J9 0.4583 45.588 200.894 3.24 0
S29_10 DailyRainfall_Canning J2931 1.8356 55.854 130.724 2.945 0
S29_11 DailyRainfall_Canning J2931 0.0383 93.738 2.728 2.945 0
S29_12 DailyRainfall_Canning J40 0.627 55.88 44.652 2.945 0
S29_13 DailyRainfall_Canning J35 0.6475 56.911 46.112 2.945 0
S29_14 DailyRainfall_Canning J48 0.7997 54.491 56.951 2.945 0
S29_15 DailyRainfall_Canning J29_14 0.4343 60.746 101 0.05 0
S29_17 DailyRainfall_Canning S29_14 0.0994 100 23.116 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S29_2 DailyRainfall_Canning J2754 0.3117 98.902 261.449 3.24 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-

03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S29_3 DailyRainfall_Canning J11 0.827 59.354 200.894 3.24 0
S29_5 DailyRainfall_Canning J79 0.2214 57.605 15.767 2.945 0
S29_7 DailyRainfall_Canning J63 0.2047 64.043 14.578 2.945 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S29_8 DailyRainfall_Canning J13 0.6318 65.957 200.89 3.24 0
S29_9 DailyRainfall_Canning J83 0.1842 47.154 13.118 2.945 0
S3 DailyRainfall_Canning S46_5 0.4046 38.659 279.671 3.38 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S30 DailyRainfall_Canning J355 0.1272 93.347 29.475 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177568637&sdata=zCA7GqVCdZlptHKOMojolIgAo2wwRkUv0NBpbslciX0%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S31 DailyRainfall_Canning J2712 0.0559 90.128 11.125 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S32 DailyRainfall_Canning J2717 0.131 100 32.75 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S33 DailyRainfall_Canning J2717 0.2423 100 60.575 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S34 DailyRainfall_Canning J2722 0.3585 100 89.625 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0

;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S35 DailyRainfall_Canning J2692 0.3274 100 81.85 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S36 DailyRainfall_Canning J46 0.0404 100 10.1 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S37 DailyRainfall_Canning S46_5 0.0681 72.125 40.059 3.38 0
S37_1 DailyRainfall_Canning J7 0.4128 62.153 50.924 2.218 0
S37_10 DailyRainfall_Canning J22 0.048 13.973 16.552 2.218 0
S37_11 DailyRainfall_Canning J2510 0.2028 45.489 25.018 2.218 0
S37_12 DailyRainfall_Canning J2510 0.0768 29.908 9.474 2.218 0
S37_2 DailyRainfall_Canning J4 0.2283 57.225 94.452 2.218 0
S37_3 DailyRainfall_Canning J4 0.1395 46.874 57.714 2.218 0
S37_4 DailyRainfall_Canning J16 0.3603 76.393 44.447 2.218 0
S37_8 DailyRainfall_Canning J1 0.1327 22.603 16.37 2.218 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
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;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S38 DailyRainfall_Canning S43_7 0.1879 100 46.975 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S39 DailyRainfall_Canning S63_9 0.4715 72.469 74.725 0.05 0
S4 DailyRainfall_Canning J2722 0.3988 100 87.381 0.064 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S40 DailyRainfall_Canning S63_9 0.1823 98.986 46.075 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S41 DailyRainfall_Canning J2931 0.2732 100 68.3 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976

aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S42 DailyRainfall_Canning J1040 0.4108 100 102.7 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S43 DailyRainfall_Canning J1969 1.6677 22.429 236.175 4.358 0
S43_2 DailyRainfall_Canning J56 0.5507 25.345 28.644 5.22 0
S43_4 DailyRainfall_Canning J46 0.3177 18.768 16.525 5.22 0
S43_5 DailyRainfall_Canning S43_7 0.9576 42.96 49.808 5.22 0
S43_6 DailyRainfall_Canning S43 0.5222 27.26 27.162 5.22 0
S43_7 DailyRainfall_Canning J46 0.5973 56.609 31.068 5.22 0
S43_9 DailyRainfall_Canning S43 0.8962 46.849 46.615 5.22 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S44 DailyRainfall_Canning S43 0.7133 100 178.325 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S45 DailyRainfall_Canning J2510 0.0497 100 12.425 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S46 DailyRainfall_Canning J7 0.0773 100 19.325 0.05 0
S46_1 DailyRainfall_Canning J2771 0.5576 54.56 68.572 3.38 0
S46_10 DailyRainfall_Canning S63_3 0.1148 66.117 35.104 3.38 0
S46_2 DailyRainfall_Canning J2594 0.3392 37.978 41.714 3.38 0
S46_3 DailyRainfall_Canning S63_14 0.3311 70.857 101.245 3.38 0
S46_4 DailyRainfall_Canning J16 0.5264 61.818 64.735 3.38 0
S46_5 DailyRainfall_Canning J2722 0.4568 50.359 35.969 3.38 0
S46_6 DailyRainfall_Canning J2678 0.2967 52.181 36.487 3.38 0
S46_7 DailyRainfall_Canning J2722 0.5254 67.845 64.612 3.38 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S47 DailyRainfall_Canning J2839 0.2228 100 55.7 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&rese
rved=0

;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S48 DailyRainfall_Canning J2847 0.1209 100 30.225 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S49 DailyRainfall_Canning J5 0.1499 100 37.475 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S5 DailyRainfall_Canning J63 0.2259 100 56.475 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S50 DailyRainfall_Canning J5 0.1966 100 49.15 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S51 DailyRainfall_Canning J3 0.1831 100 45.775 0.05 0
S52_1 DailyRainfall_Canning S43 0.9201 31.473 59.154 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S52_2 DailyRainfall_Canning S43 0.8425 48.211 304.437 2.945 0
S52_3 DailyRainfall_Canning J2909 0.2611 61.555 16.786 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S52_4 DailyRainfall_Canning J70 0.3919 57.11 304.436 2.945 0
S52_6 DailyRainfall_Canning J2838 0.8612 73.374 55.367 3.235 0
S52_7 DailyRainfall_Canning J2860 0.7479 50.071 48.083 3.235 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR220-03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976aacbeca6a7%7C0%7C0%7C637186271177578591&sdata=GJHsTF8pHChJoza43uRCmb4sirXYrAqdxVAGuGfOELo%3D&reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S53 DailyRainfall_Canning J4 0.2626 100 65.65 0.05 0

;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S54 DailyRainfall_Canning S15_7 0.1028 100 25.7 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S55 DailyRainfall_Canning S15_7 0.0122 100 3.05 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S56 DailyRainfall_Canning S15_7 0.0722 100 18.05 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S57 DailyRainfall_Canning J13 0.056391 100 200.894 3.24 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S59 DailyRainfall_Canning J13 0.1094 97.656 36.326 0.05 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S63_1 DailyRainfall_Canning J355 0.6135 38.355 180.24 4.534 0
S63_11 DailyRainfall_Canning J2728 0.2498 61.02 35.183 4.534 0
S63_12 DailyRainfall_Canning J2822 0.131 56.273 32.75 4.534 0
S63_13 DailyRainfall_Canning J2794 0.4345 48.85 52.988 4.534 0
S63_14 DailyRainfall_Canning J2757 0.1862 59.93 46.55 4.534 0
S63_15 DailyRainfall_Canning J2709 0.2832 50.726 28.32 4.534 0
S63_2 DailyRainfall_Canning J2855 1.2038 26.59 75.703 4.534 0
S63_3 DailyRainfall_Canning J2719 0.2036 65.386 30.848 4.534 0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the infiltration capacity is reduced.
S63_4 DailyRainfall_Canning S63_9 0.112 89.578 11.2 4.534 0

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;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_5            DailyRainfall_Canning S63_1       0.0042   90.878   5.886    4.534    0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_6            DailyRainfall_Canning J2785       0.2827   52.709   180.236  4.534    0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_7            DailyRainfall_Canning J1969       0.0761   35.47    180.246  4.534    0
S63_8            DailyRainfall_Canning J2730       0.1497   54.886   49.9     4.534    0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S63_9            DailyRainfall_Canning J2785       0.2791   36.183   34.037   4.534    0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
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03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S7               DailyRainfall_Canning J2757       0.123    100      30.75    0.05     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
220-
03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S8               DailyRainfall_Canning J2755       0.1461   100      36.525   0.05     0
;{22405761@student.uwa.edu.au - 2019.12.13} I am considering Horton method for infiltration of group A.
https://gcc01.safelinks.protection.outlook.com/?url=https%3A%2F%2Fwww.chijournal.org%2FJournals%2FPDF%2FR
220-
03&amp;data=02%7C01%7CTryby.Michael%40epa.gov%7Cc187adfbc35e4cc2347908d7bd89a11f%7C88b378b367484867acf976
aacbeca6a7%7C0%7C0%7C637186271177588547&amp;sdata=%2F1YZB0qXybiCKnswKRevt91Af2U9dUAQnFa%2FL%2FyIEWA%3D&am
p;reserved=0
;Low runoff potential because it is sandy soils and I am taking an average field capacity (infililtration
capacity) that could be decresed in wet period and increased in dry periods. Also if the GW is high, the
infiltration capacity is reduced.
S9               DailyRainfall_Canning S43_7       0.1578   100      39.45    0.05     0<!-- Standard PRE
tag rules -->

[SUBAREAS]
;;Subcatchment   N-Imperv   N-Perv     S-Imperv   S-Perv     PctZero    RouteTo    PctRouted
;;-------------- ---------- ---------- ---------- ---------- ---------- ---------- ----------
S1               0.03       0.089      1.033      5.103      25         OUTLET
S10              0.014      0          1.25       0          0          OUTLET
```

S11	0.014	0	1.25	0.001	0	OUTLET	
S12	0.021	0	1.051	1.275	0	OUTLET	
S13	0.03	0.016	0.882	2.879	25	OUTLET	
S14	0.038	0	0.611	4.103	25	OUTLET	
S15_1	0.045	0.009	0.473	5.435	25	OUTLET	
S15_10	0.046	0	0.381	5.563	25	OUTLET	
S15_12	0.02	0.142	1.34	5.112	25	OUTLET	
S15_2	0.015	0.177	1.618	5	25	OUTLET	
S15_3	0.014	0	1.25	0	0	OUTLET	
S15_4	0.023	0.136	1.408	4.803	25	OUTLET	
S15_5	0.014	0.174	1.578	5	25	OUTLET	
S15_6	0.014	0	1.25	0	0	OUTLET	
S15_7	0.019	0.144	1.303	5.173	25	OUTLET	
S15_8	0.046	0	0.388	5.514	25	OUTLET	
S15_9	0.051	0.004	0.27	6.514	25	OUTLET	
S16	0.014	0	1.25	0	0	OUTLET	
S17	0.014	0	1.25	0	0	OUTLET	
S18_2	0.016	0.006	1.227	0.49	0	OUTLET	
S18_3	0.015	0	1.221	0.187	0	OUTLET	
S18_4	0.027	0.084	0.97	4.923	25	OUTLET	
S19	0.014	0	1.25	0	0	OUTLET	
S2	0.015	0	1.233	0.107	0	OUTLET	
S20	0.014	0	1.25	0	0	OUTLET	
S21	0.014	0	1.25	0	0	OUTLET	
S22	0.014	0	1.25	0	25	OUTLET	
S23	0.032	0.022	0.891	3.503	25	OUTLET	
S23_1	0.022	0.118	1.221	4.796	25	OUTLET	
S23_3	0.031	0.033	0.846	3.855	25	OUTLET	
S23_4	0.027	0.105	1.154	4.847	25	OUTLET	
S24	0.014	0	1.25	0	0	OUTLET	
S25	0.014	0	1.25	0	0	OUTLET	
S26_1	0.025	0.116	1.409	4.073	25	OUTLET	
S26_3	0.028	0.075	1.005	4.45	25	OUTLET	
S29_1	0.038	0.05	0.803	4.778	25	OUTLET	
S29_10	0.031	0.063	0.936	4.521	25	OUTLET	
S29_11	0.017	0	1.163	0.557	25	OUTLET	
S29_12	0.032	0.06	0.95	4.496	25	OUTLET	
S29_13	0.033	0.04	0.747	4.659	25	OUTLET	
S29_14	0.033	0.048	0.782	4.756	25	OUTLET	
S29_15	0.016	0.005	1.237	0.354	0	OUTLET	
S29_17	0.016	0	1.183	0.429	0	OUTLET	
S29_2	0.014	0	1.249	0.008	25	OUTLET	
S29_3	0.027	0.092	1.099	4.544	25	OUTLET	
S29_5	0.031	0.055	0.787	4.927	25	OUTLET	
S29_7	0.023	0.105	1.199	4.44	25	OUTLET	
S29_8	0.03	0.015	0.901	2.911	25	OUTLET	
S29_9	0.036	0.065	0.661	6.012	25	OUTLET	
S3	0.043	0.044	0.606	5.679	25	PERVIOUS	50
S30	0.016	0.011	1.251	0.504	0	OUTLET	
S31	0.019	0	1.113	0.877	0	OUTLET	
S32	0.014	0	1.25	0	0	OUTLET	
S33	0.014	0	1.25	0	0	OUTLET	
S34	0.014	0	1.25	0	0	OUTLET	
S35	0.014	0	1.25	0	0	OUTLET	
S36	0.014	0	1.25	0	0	OUTLET	
S37	0.027	0.027	1.022	2.31	25	OUTLET	
S37_1	0.033	0.003	0.742	3.346	25	OUTLET	
S37_10	0.055	0	0.135	7.135	25	OUTLET	
S37_11	0.042	0	0.493	4.845	25	OUTLET	
S37_12	0.052	0	0.224	6.565	25	OUTLET	
S37_2	0.027	0.103	1.097	5.128	25	OUTLET	
S37_3	0.037	0.065	0.861	4.739	25	OUTLET	
S37_4	0.026	0.005	0.942	2.129	25	OUTLET	
S37_8	0.052	0.022	0.294	6.902	25	OUTLET	
S38	0.014	0	1.25	0	0	OUTLET	
S39	0.028	0.003	0.893	2.425	0	OUTLET	
S4	0.014	0	1.25	0	0.103	OUTLET	
S40	0.015	0	1.236	0.09	0	OUTLET	
S41	0.014	0	1.25	0	0	OUTLET	
S42	0.014	0	1.25	0	0	OUTLET	
S43	0.034	0.32	2.368	4.705	25	OUTLET	
S43_2	0.052	0.001	0.221	6.628	25	PERVIOUS	50
S43_4	0.042	0.331	2.088	5.155	25	OUTLET	
S43_5	0.033	0.123	1.367	4.362	25	PERVIOUS	50
S43_6	0.044	0.166	1.264	5.406	25	PERVIOUS	50
S43_7	0.035	0.016	0.758	3.747	25	PERVIOUS	50
S43_9	0.041	0.005	0.55	4.687	25	PERVIOUS	50
S44	0.014	0	1.25	0	0	OUTLET	

```
S45             0.014     0         1.25      0         0         OUTLET
S46             0.014     0         1.25      0         0         OUTLET
S46_1           0.029     0.089     1.098     4.622     25        OUTLET
S46_10          0.031     0         0.779     3.012     25        OUTLET
S46_2           0.045     0.013     0.494     5.423     25        OUTLET
S46_3           0.028     0.005     0.891     2.549     25        OUTLET
S46_4           0.026     0.102     1.104     4.722     25        OUTLET
S46_5           0.039     0.004     0.597     4.38      25        OUTLET
S46_6           0.031     0.102     0.938     5.562     25        OUTLET
S46_7           0.03      0.007     0.874     2.795     25        OUTLET
S47             0.014     0         1.25      0         0         OUTLET
S48             0.014     0         1.25      0         0         OUTLET
S49             0.014     0         1.25      0         0         OUTLET
S5              0.014     0         1.25      0         0         OUTLET
S50             0.014     0         1.25      0         0         OUTLET
S51             0.014     0         1.25      0         0         OUTLET
S52_1           0.034     0.238     1.779     5.387     25        OUTLET
S52_2           0.035     0.092     1.131     4.028     25        OUTLET
S52_3           0.023     0.107     1.34      4.059     25        OUTLET
S52_4           0.031     0.057     0.85      4.746     25        OUTLET
S52_6           0.023     0.048     1.143     2.732     25        OUTLET
S52_7           0.035     0.039     0.834     4.523     25        OUTLET
S53             0.014     0         1.25      0         0         OUTLET
S54             0.014     0         1.25      0         0         OUTLET
S55             0.014     0         1.25      0         0         OUTLET
S56             0.014     0         1.25      0         0         OUTLET
S57             0.014     0         1.25      0         25        OUTLET
S59             0.014     0         1.249     0.008     0         OUTLET
S63_1           0.042     0.08      0.908     5.056     25        OUTLET
S63_11          0.029     0.055     0.901     4.342     25        OUTLET
S63_12          0.032     0.036     0.962     3.593     25        OUTLET
S63_13          0.038     0.023     0.663     4.684     25        OUTLET
S63_14          0.034     0.013     0.788     3.47      25        OUTLET
S63_15          0.037     0.014     0.706     4.254     25        OUTLET
S63_2           0.044     0.115     1.019     5.739     25        OUTLET
S63_3           0.025     0.071     1.112     3.856     25        OUTLET
S63_4           0.018     0.012     1.201     0.835     25        OUTLET
S63_5           0.018     0.01      1.197     0.739     25        OUTLET
S63_6           0.035     0.025     0.825     3.993     25        OUTLET
S63_7           0.044     0.049     0.694     5.399     25        OUTLET
S63_8           0.031     0.082     0.818     5.704     25        OUTLET
S63_9           0.047     0         0.364     5.673     25        OUTLET
S7              0.014     0         1.25      0         0         OUTLET
S8              0.014     0         1.25      0         0         OUTLET
S9              0.014     0         1.25      0         0         OUTLET<!-- Standard PRE tag rules
-->

[INFILTRATION]
;;Subcatchment   MaxRate    MinRate    Decay      DryTime    MaxInfil
;;-------------- ---------- ---------- ---------- ---------- ----------
S1              127        120        4          2          157.8
S10             127        120        4          2          157.8
S11             127        120        4          2          157.8
S12             127        120        4          2          157.8
S13             127        120        4          2          157.8
S14             127        120        4          2          157.8
S15_1           127        120        4          2          157.8
S15_10          127        120        4          2          157.8
S15_12          127        120        4          2          157.8
S15_2           127        120        4          2          157.8
S15_3           127        120        4          2          157.8
S15_4           127        120        4          2          157.8
S15_5           127        120        4          2          157.8
S15_6           127        120        4          2          157.8
S15_7           127        120        4          2          157.8
S15_8           127        120        4          2          157.8
S15_9           127        120        4          2          157.8
S16             127        120        4          2          157.8
S17             127        120        4          2          157.8
S18_2           76.2       70         4          2          157.8
S18_3           76.2       70         4          2          157.8
S18_4           76.2       70         4          2          157.8
S19             127        120        4          2          157.8
S2              127        120        4          2          157.8
S20             127        120        4          2          157.8
S21             127        120        4          2          157.8
S22             127        120        4          2          157.8
S23             127        120        4          2          157.8
```

S23_1	127	120	4	2	157.8
S23_3	127	120	4	2	157.8
S23_4	127	120	4	2	157.8
S24	127	120	4	2	157.8
S25	127	120	4	2	157.8
S26_1	127	120	4	2	157.8
S26_3	127	120	4	2	157.8
S29_1	127	120	4	2	157.8
S29_10	127	120	4	2	157.8
S29_11	127	120	4	2	157.8
S29_12	127	120	4	2	157.8
S29_13	127	120	4	2	157.8
S29_14	127	120	4	2	157.8
S29_15	127	120	4	2	157.8
S29_17	127	120	4	2	157.8
S29_2	127	120	4	2	157.8
S29_3	127	120	4	2	157.8
S29_5	127	120	4	2	157.8
S29_7	127	120	4	2	157.8
S29_8	127	120	4	2	157.8
S29_9	127	120	4	2	157.8
S3	127	120	4	2	157.8
S30	127	120	4	2	157.8
S31	127	120	4	2	157.8
S32	127	120	4	2	157.8
S33	127	120	4	2	157.8
S34	127	120	4	2	157.8
S35	127	120	4	2	157.8
S36	127	120	4	2	157.8
S37	127	120	4	2	157.8
S37_1	127	120	4	2	157.8
S37_10	127	120	4	2	157.8
S37_11	127	120	4	2	157.8
S37_12	127	120	4	2	157.8
S37_2	127	120	4	2	157.8
S37_3	127	120	4	2	157.8
S37_4	127	120	4	2	157.8
S37_8	127	120	4	2	157.8
S38	127	120	4	2	157.8
S39	127	120	4	2	157.8
S4	127	120	4	2	157.8
S40	127	120	4	2	157.8
S41	127	120	4	2	157.8
S42	127	120	4	2	157.8
S43	76.2	10.92	4	2	157.8
S43_2	127	120	4	2	157.8
S43_4	127	120	4	2	157.8
S43_5	127	120	4	2	157.8
S43_6	127	120	4	2	157.8
S43_7	127	120	4	2	157.8
S43_9	127	120	4	2	157.8
S44	127	120	4	2	157.8
S45	127	120	4	2	157.8
S46	127	120	4	2	157.8
S46_1	127	120	4	2	157.8
S46_10	127	120	4	2	157.8
S46_2	127	120	4	2	157.8
S46_3	127	120	4	2	157.8
S46_4	127	120	4	2	157.8
S46_5	127	120	4	2	157.8
S46_6	127	120	4	2	157.8
S46_7	127	120	4	2	157.8
S47	127	120	4	2	157.8
S48	127	120	4	2	157.8
S49	127	120	4	2	157.8
S5	127	120	4	2	157.8
S50	127	120	4	2	157.8
S51	127	120	4	2	157.8
S52_1	127	120	4	2	157.8
S52_2	127	120	4	2	157.8
S52_3	127	120	4	2	157.8
S52_4	127	120	4	2	157.8
S52_6	127	120	4	2	157.8
S52_7	127	120	4	2	157.8
S53	127	120	4	2	157.8
S54	127	120	4	2	157.8
S55	127	120	4	2	157.8
S56	127	120	4	2	157.8

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S57             127        120        4          2          157.8
S59             127        120        4          2          157.8
S63_1           127        120        4          2          157.8
S63_11          127        120        4          2          157.8
S63_12          127        120        4          2          157.8
S63_13          127        120        4          2          157.8
S63_14          127        120        4          2          157.8
S63_15          127        120        4          2          157.8
S63_2           127        120        4          2          157.8
S63_3           127        120        4          2          157.8
S63_4           127        120        4          2          157.8
S63_5           127        120        4          2          157.8
S63_6           127        120        4          2          157.8
S63_7           127        120        4          2          157.8
S63_8           127        120        4          2          157.8
S63_9           127        120        4          2          157.8
S7              127        120        4          2          157.8
S8              127        120        4          2          157.8
S9              127        120        4          2          157.8<!-- Standard PRE tag rules -->

[LID_CONTROLS]
;;              Type/Layer Parameters
;;-------------- ---------- ----------
BioSwale        BC
BioSwale        SURFACE    300        0.01       0          0          5
BioSwale        SOIL       1000       0.4        0.19       0.085      120        10.0       110
BioSwale        STORAGE    1000       0.67       6          0
BioSwale        DRAIN      0.09       0.5        500        6          0          0<!-- Standard PRE tag
rules -->
EnhancedSwale   BC
EnhancedSwale   SURFACE    100        0.01       0          0          5
EnhancedSwale   SOIL       200        0.25       0.19       0.085      200        10.0       100
EnhancedSwale   STORAGE    800        0.33       6          0
EnhancedSwale   DRAIN      0.0011     0.5        300        6          0          0<!-- Multi line
multiple consecutive spaces -->

[LID_USAGE]
;;Subcatchment   LID Process      Number  Area       Width      InitSatur  FromImprv  ToPerv     Report
File                Drain to          FromPerv
;;-------------- ---------------- ------- ---------- ---------- ---------- ---------- ---------- --------
------------------- ---------------- ----------------
S43             BioSwale         1       16677      0          0          0          0          *
*               0<!-- Standard PRE tag rules -->

[AQUIFERS]
;;              Por-   Wilt   Field  Hyd    Cond   Tens   Upper  Lower  Lower  Bottom Water  Upper
Upper
;;Name          osity  Point  Capac  Cond   Slope  Slope  Evap   Evap   Loss   Elev   Table  Moist  Evap
Pat
;;-------------- ------ ------ ------ ------ ------ ------ ------ ------ ------ ------ ------ ------ ----
--------
Aquifer1        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      11.96  0.3
Aquifer1_11.96  0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      11.96  0.413
Aquifer2        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      11.35  0.3
Aquifer2_11.35  0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      11.35  0.413
Aquifer3        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      11     0.3
Aquifer3_11     0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      11     0.413
Aquifer4        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      10.6   0.3
Aquifer4_10.6   0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      10.6   0.413
Aquifer5        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  0      10     0.3
Aquifer5_10     0.437  0.024  0.062  120.34 5      49.02  0.35   0.4    0.002  0      10     0.413
S10AQ           0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.7    9.7    0.3
S11AQ           0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.826 11.826 0.3
S12AQ           0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  16.367 16.367 0.3
S13AQ           0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.311 13.311 0.3
S14AQ           0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  16.367 16.367 0.3
S15_10AQ        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.548 11.548 0.3
S15_12AQ        0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.58  11.58  0.3
S15_1AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.548 11.548 0.3
S15_2AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.779 13.779 0.3
S15_3AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.022 13.022 0.3
S15_4AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.641 13.641 0.3
S15_5AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.807 13.807 0.3
S15_6AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  16.367 16.367 0.3
S15_7AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.91  11.91  0.3
S15_8AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.364 13.364 0.3
S15_9AQ         0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.496 11.496 0.3
S16AQ           0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.72  14.72  0.3
```

S17AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.563	13.563	0.3
S18_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.593	12.593	0.3
S18_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.343	12.343	0.3
S18_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.343	12.343	0.3
S19AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.286	13.286	0.3
S1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.826	11.826	0.3
S20AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.591	13.591	0.3
S21AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.364	13.364	0.3
S22AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.34	13.34	0.3
S23_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.794	13.794	0.3
S23_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	17.492	17.492	0.3
S23_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.311	13.311	0.3
S23AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.355	12.355	0.3
S24AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.496	11.496	0.3
S25AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.2	13.2	0.3
S26_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.938	14.938	0.3
S26_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.478	13.478	0.3
S29_10AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.871	11.871	0.3
S29_11AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.871	11.871	0.3
S29_12AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.987	11.987	0.3
S29_13AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	0	9.7	0.3
S29_14AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.508	11.508	0.3
S29_15AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12	12	0.3
S29_17AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.508	11.508	0.3
S29_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	16.367	16.367	0.3
S29_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.562	14.562	0.3
S29_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.022	13.022	0.3
S29_5AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.188	12.188	0.3
S29_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.238	12.238	0.3
S29_8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.72	14.72	0.3
S29_9AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.696	11.696	0.3
S2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.188	12.188	0.3
S30AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	8.33	8.33	0.3
S31AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.4	15.4	0.3
S32AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.975	15.975	0.3
S33AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.975	15.975	0.3
S34AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S35AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	10.61	10.61	0.3
S36AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S37_10AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.5	11.5	0.3
S37_11AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S37_12AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S37_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.34	13.34	0.3
S37_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.794	13.794	0.3
S37_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.794	13.794	0.3
S37_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.307	12.307	0.3
S37_8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.397	13.397	0.3
S37AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S38AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S39AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.5	15.5	0.3
S3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S40AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	15.5	15.5	0.3
S41AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.871	11.871	0.3
S42AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.07	9.07	0.3
S43_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.194	13.194	0.3
S43_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S43_5AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S43_6AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S43_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.7	9.7	0.3
S43_9AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S43AQ	0.5	0.15	0.3	5	10	15	0.35	1	0.002	9.1	9.1	0.3
S44AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3
S45AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.21	11.21	0.3
S46_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.9	9.9	0.3
S46_2AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	11.02	11.02	0.3
S46_3AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S46_4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.307	12.307	0.3
S46_6AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	10.5	10.5	0.3
S46_7AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S46_8AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	12.307	12.307	0.3
S46AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.34	13.34	0.3
S47AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.094	14.094	0.3
S48AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.578	13.578	0.3
S49AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.987	13.987	0.3
S4AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	14.544	14.544	0.3
S50AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.987	13.987	0.3
S51AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	13.591	13.591	0.3
S52_1AQ	0.5	0.15	0.3	5	10	15	0.35	0.4	0.002	9.1	9.1	0.3

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S52_2AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.1    9.1    0.3
S52_3AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.478 13.478 0.3
S52_4AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.668 12.668 0.3
S52_6AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.291 12.291 0.3
S52_7AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.49  12.49  0.3
S53AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  13.794 13.794 0.3
S54AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.91  11.91  0.3
S55AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.91  11.91  0.3
S56AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  11.91  11.91  0.3
S57AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.72  14.72  0.3
S59AQ            0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.72  14.72  0.3
S5AQ             0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  12.238 12.238 0.3
S63_1AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  8.33   8.33   0.3
S63_2AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.01   9.01   0.3
S63_3AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14     14     0.3
S63_4AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.1    9.1    0.3
S63_5AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  8.33   8.33   0.3
S63_6AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.126 14.126 0.3
S63_7AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.1    9.1    0.3
S63_9AQ          0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  15.5   15.5   0.3
S7AQ             0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  15.322 15.322 0.3
S8AQ             0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  14.084 14.084 0.3
S9AQ             0.5    0.15   0.3    5      10     15     0.35   0.4    0.002  9.7    9.7    0.3<!--
Standard PRE tag rules -->

[GROUNDWATER]
;;Subcatchment   Aquifer          Node             Elev   A1     B1     A2     B2     A3     Depth  Elev
Ebot   Wgr   Umc
;;-------------- ---------------- ---------------- ------ ------ ------ ------ ------ ------ ------ -----
- ------ ------ ------<!-- Standard PRE tag rules -->

[JUNCTIONS]
;;               Invert     Max.       Init.      Surcharge  Ponded
;;Name           Elev.      Depth      Depth      Depth      Area
;;-------------- ---------- ---------- ---------- ---------- ----------
J1               13.397     0          0          0          0
J10              13.307     0          0          0          0
J1040            9.07       2.211      0          0          0
J11              13.022     0          0          0          0
J12              17.492     0          0          0          0
J13              14.72      0          0          0          0
J14              13.165     0          0          0          0
J1415            9.712      2.03       0          0          0
J15              13.771     0          0          0          0
J16              12.307     1          0          0          0
J17              13.641     0          0          0          0
J1701            14.3       0.045      0          0          0
;Wetland outfall
J1788            9.08       1.679      0          0          0
J18              13.807     0          0          0          0
J19              12.482     0          0          0          0
J1969            9.1        1.106      0          0          0
J2               13.175     0          0          0          0
J20              13.779     0          0          0          0
J21              11         2.351      0          0          0
J2181            11.91      0.05       0          0          0
J22              11.5       3.5        0          0          0
J2293            11.6       1.396      0          0          0
J23              11.496     1.5        0          0          0
J2312            11.58      1.422      0          0          0
J24              11.548     1.435      0          0          0
J25              12.355     2.645      0          0          0
J2510            11.21      1.594      0          0          0
J2594            11.02      1.799      0          0          0
J26              13.364     0          0          0          0
J2678            10.5       2.147      0          0          0
J2692            10.61      1.866      0          0          0
J27              12.482     0          0          0          0
J2709            15.5       0.2        0          0          0
J2712            15.4       0.268      0          0          0
J2717            15.975     0          0          0          0
J2719            15.875     0          0          0          0
J2722            14.544     0          0          0          0
J2728            15.283     0          0          0          0
J2730            15.255     0          0          0          0
J2749            15.158     0          0          0          0
J2754            14.562     0          0          0          0
J2755            14.084     0          0          0          0
```

J2757	15.322	0	0	0	0
J2764	14.47	0	0	0	0
J2771	9.9	1.838	0	0	0
J2779	14.324	0	0	0	0
J2785	14.126	0	0	0	0
J2786	15.063	0	0	0	0
J2787	14.938	0	0	0	0
J2794	14	0.366	0	0	0
J2797	13.274	0	0	0	0
J28	13.286	0	0	0	0
J2813	12.422	0	0	0	0
J2816	12.292	0	0	0	0
J2822	12.933	0	0	0	0
J2831	12.636	0	0	0	0
J2838	12.291	0	0	0	0
J2839	14.094	0	0	0	0
J2845	12.619	0	0	0	0
J2847	13.578	0	0	0	0
J2855	9.01	2.287	0	0	0
J2857	9.64	2.06	0	0	0
J2860	12.49	0	0	0	0
J2868	12.78	0	0	0	0
J2870	12.8	0.01	0	0	0
J2887	9.57	2.046	0	0	0
J2890	12.9	0.1	0	0	0
J2891	10	0.379	0	0	0
J29	12.674	0	0	0	0
J29_14	12	0	0	0	0
J2909	13.478	0	0	0	0
J2915	9.2	2.4	0	0	0
J2918	13.563	0.9	0	0	0
J2921	11.284	0	0	0	0
J2931	11.871	0	0	0	0
J2938	14.358	0.795	0	0	0
J3	13.591	0	0	0	0
J30	12.343	0	0	0	0
J31	12.665	0	0	0	0
J32	12.593	0	0	0	0
J33	12.308	0	0	0	0
J34	12.132	0	0	0	0
J35	11.496	0.204	0	0	0
J36	11.727	0	0	0	0
J37	12.207	0	0	0	0
J38	12.299	0	0	0	0
J39	12.123	0	0	0	0
J4	13.794	0	0	0	0
J40	11.987	0	0	0	0
J41	12	0	0	0	0
J42	12.238	0	0	0	0
J43	12.872	0	0	0	0
J44	12.872	0	0	0	0
J45	9.3	1.534	0	0	0
J46	9.7	1.399	0	0	0
J47	11.647	0	0	0	0
J48	11.508	0	0	0	0
J49	9.09	1.828	0	0	0
J5	13.987	0	0	0	0
J50	12.202	0	0	0	0
J52	11.508	0.2	0	0	0
J53	11.509	0.2	0	0	0
J55	9.69	1.316	0	0	0
J56	13.194	0	0	0	0
J57	13.2	0	0	0	0
J59	12.499	0	0	0	0
J6	13.311	0	0	0	0
J63	12.238	0	0	0	0
J64	12.805	0	0	0	0
J65	11.793	0	0	0	0
J66	11.582	0	0	0	0
J67	11.916	0	0	0	0
J68	12	0	0	0	0
J69	11.759	0	0	0	0
J7	13.34	0	0	0	0
J70	12.668	0	0	0	0
J72	11.596	0.1	0	0	0
J73	12.86	0	0	0	0
J78	12.4	0	0	0	0
J79	12.188	0	0	0	0

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J8                11.34      1.65       0          0          0
J80               11.826     0          0          0          0
J83               11.696     1.2        0          0          0
J9                16.367     0          0          0          0<!-- Standard PRE tag rules -->

[OUTFALLS]
;;                Invert     Outfall      Stage/Table      Tide
;;Name            Elev.      Type         Time Series      Gate Route To
;;-------------- ---------- ------------ ---------------- ---- ---------------
J355              8.33       FREE                          NO<!-- Standard PRE tag rules -->

[STORAGE]
;;                Invert   Max.     Init.    Storage    Curve                                Evap.
;;Name            Elev.    Depth    Depth    Curve      Params                               Frac.
Infiltration parameters
;;-------------- -------- -------- -------- ---------- -------- -------- -------- -------- -------- -----
------------------
J54               8.8      2.169    0        TABULAR    SedimentationPond           0       0<!-- Standard
PRE tag rules -->

[CONDUITS]
;;                Inlet            Outlet                       Manning    Inlet      Outlet     Init.
Max.
;;Name            Node             Node             Length      N          Offset     Offset     Flow
Flow
;;-------------- ---------------- ---------------- ---------- ---------- ---------- ---------- ----------
----------
;B- branch
206110366         J2510            J2594            68.079      0.012      11.21      11.02      0
0
;B- branch
206110379_1       J2312            J24              23.888      0.012      11.58      11.54      0
0
;B- branch
206110379_2       J8               J2510            51.399      0.012      11.34      11.21      0
0
;B- branch
206110379_4       J23              J8               67.866      0.012      11.496     11.34      0
0
;B- branch
206110379_5       J24              J23              39.622      0.012      11.54      11.496     0
0
;B- branch
22803188_2        J45              J2915            159.449     0.027      9.3        9.2        0
0
;B- branch
22803188_3        J54              J45              89.837      0.027      9.45       9.3        0
0
;B- branch
22803188_4        J46              J55              61.407      0.027      9.7        9.69       0
0
;B- branch
22803188_5        J55              J54              24.469      0.01       9.69       8.8        0
0
;B- branch
22926618_1        J2915            J1969            23.772      0.027      9.2        9.1        0
0
;B- branch
22926618_2        J1969            J49              64.7        0.027      9.1        9.09       0
0
;B- branch
22926618_3        J1040            J2855            33.579      0.027      9.07       9.01       0
0
;B- branch
22926618_4        J1788            J1040            50.452      0.027      9.08       9.07       0
0
;B- branch
22926629          J2887            J2915            19.716      0.027      9.57       9.2        0
0
;B- branch
23116769          J2594            J2678            67.769      0.012      10.5       10.842     0
0
;B- branch
23116814          J1415            J2857            21.548      0.012      9.71       9.64       0
0
;B- branch
23116826          J2857            J2887            27.164      0.012      9.64       9.57       0
0
```

;B- branch
23405543 J2293 J2312 8.129 0.012 11.6 11.58 0
0
;B- branch
23405563 J2181 J2293 111.419 0.012 11.91 11.6 0
0
;B- branch
57466689_1 J2771 J1415 34.821 0.012 9.9 9.71 0
0
;B- branch
57466741 J2692 J2771 111.323 0.012 10.61 9.9 0
0
;B- branch
57466813 J2678 J2692 18.756 0.012 10.841 10.649 0
0
C1 J10 J2 4.637 0.012 13.307 13.175 0
0
C1_1 J2 J14 9.039 0.012 13.175 13.165 0
0
C1_2 J14 J1 58.507 0.012 13.165 13.397 0
0
C10 J9 J5 67.889 0.012 16.367 13.987 0
0
C108 J2921 J1969 21.276 0.012 11.284 9.1 0
0
C109 J2831 J2845 40.393 0.012 12.636 12.619 0
0
C11 J11 J14 10.311 0.012 13.022 13.165 0
0
C110 J2794 J1040 48.667 0.012 14.366 9.9 0
0
C111 J2785 J2794 97.324 0.012 14.126 14.366 0
0
C112 J2717 J2719 2.496 0.012 15.975 15.875 0
0
C113 J2918 J2909 49.617 0.012 13.582 13.178 0
0
C12 J1 J7 51.477 0.012 13.397 13.34 0
0
C126 J2890 J2870 8.515 0.012 12.9 12.8 0
0
C127 J2816 J2813 8.596 0.012 12.292 12.422 0
0
C128 J2722 J2797 104.347 0.012 14.544 13.274 0
0
C129_1 J2764 J1701 7.023 0.012 14.47 14.3 0
0
C129_2 J1701 J2847 42.939 0.012 14.3 13.578 0
0
C13 J12 J9 67.473 0.012 17.492 16.367 0
0
C130 J2787 J2764 47.719 0.012 14.938 14.47 0
0
C131 J2870 J2868 1.688 0.012 12.8 12.78 0
0
C141 J2931 J2921 12.998 0.012 11.871 11.284 0
0
C142 J2822 J2831 53.415 0.012 12.933 12.636 0
0
C143 J2712 J2785 77.216 0.012 15.668 14.126 0
0
C144 J2786 J2794 10.768 0.012 15.063 14 0
0
C145 J2839 J2847 7.54 0.012 14.094 13.578 0
0
C146 J2779 J1701 4.365 0.012 14.324 0 0
0
C147 J2730 J2749 16.81 0.012 15.255 15.158 0
0
C148 J2719 J2730 33.014 0.012 15.875 15.255 0
0
C158 J2860 J2838 85.236 0.012 12.49 12.291 0
0
C159 J2797 J2822 5.744 0.012 13.274 12.933 0
0
C16 J13 J2 107.922 0.012 14.72 13.175 0
0

C160	J2845	J2857	10.336	0.012	12.619	9.64	0
0							
C161	J2728	J2730	5.612	0.012	15.283	15.255	0
0							
C167_2	J47	J2931	62.151	0.012	11.647	11.871	0
0							
C169	J2838	J1415	29.473	0.012	12.291	9.71	0
0							
C17	J17	J15	17.34	0.012	13.641	13.771	0
0							
C170	J2813	J1415	17.522	0.012	12.422	9.71	0
0							
C176	J2855	J355	189.997	0.012	9.01	8.33	0
0							
C18	J18	J2293	9.374	0.012	13.807	11.6	0
0							
C182	J2757	J2786	23.114	0.012	15.322	15.063	0
0							
C185	J2868	J2860	37.359	0.012	12.78	12.49	0
0							
C186	J2909	J2868	76.26	0.012	13.178	12.78	0
0							
C19	J20	J17	8.543	0.012	13.779	13.641	0
0							
C193	J2709	J2712	5.018	0.012	15.5	15.4	0
0							
C194	J2749	J2786	40.681	0.012	15.158	15.063	0
0							
C195	J2754	J2764	7.405	0.012	14.562	14.47	0
0							
C196	J2891	J1788	3.836	0.012	10	9.8	0
0							
C20	J22	J8	29.309	0.012	11.5	11.34	0
0							
C21	J25	J8	3.458	0.012	12.407	11.34	0
0							
C22	J26	J23	3.504	0.012	13.364	11.496	0
0							
C23	J28	J24	5.29	0.012	13.286	11.548	0
0							
C24	J16	J21	12.672	0.012	12.307	11	0
0							
C25	J21	J2678	29.87	0.012	11	10.5	0
0							
C26	J27	J19	1.36	0.012	12.482	12.482	0
0							
C27	J30	J29	9.258	0.012	12.343	12.674	0
0							
C28	J32	J31	3.951	0.012	12.593	12.665	0
0							
C29	J34	J33	1.846	0.012	12.132	12.308	0
0							
C3	J4	J3	40.802	0.012	13.794	13.591	0
0							
C30	J36	J35	38.306	0.012	11.727	11.496	0
0							
C31	J38	J37	32.41	0.012	12.299	12.207	0
0							
C32	J40	J39	20.545	0.012	11.987	12.123	0
0							
C33	J41	J40	2.028	0.012	12	11.987	0
0							
C34	J42	J33	24.628	0.012	12.238	12.308	0
0							
C35	J44	J43	2.945	0.012	12.872	12.872	0
0							
C37	J35	J47	13.225	0.012	11.496	11.647	0
0							
C38	J52	J48	3.314	0.012	11.508	11.508	0
0							
C39	J37	J50	31.398	0.012	12.207	12.202	0
0							
C4	J5	J6	79.213	0.012	13.987	13.311	0
0							
C40	J39	J38	19.101	0.012	12.123	12.299	0
0							
C41	J29_14	J40	5.115	0.012	12	11.987	0
0							

```
C42             J53             J52             1.209     0.012     11.509    11.508    0
0
C44             J57             J56             17.729    0.012     13.2      13.194    0
0
C45             J59             J19             11.134    0.012     12.499    12.482    0
0
C46             J33             J47             69.917    0.012     12.308    11.647    0
0
C47             J63             J42             4.441     0.012     12.238    12.238    0
0
C49             J19             J33             65.276    0.012     12.482    12.308    0
0
C5              J7              J2510           44.939    0.012     13.34     11.804    0
0
C50             J56             J19             66.196    0.012     13.194    12.482    0
0
C51             J64             J63             9.046     0.012     12.805    12.238    0
0
C52             J65             J52             9.715     0.012     11.793    11.508    0
0
C53             J66             J48             18.477    0.012     11.582    11.508    0
0
C54             J67             J66             36.208    0.012     11.916    11.582    0
0
C55             J68             J40             16.677    0.012     12        11.987    0
0
C56             J69             J65             1.909     0.012     11.759    11.793    0
0
C57             J78             J70             2.562     0.012     12.4      12.668    0
0
C58             J72             J35             1.316     0.012     11.596    11.496    0
0
C59             J50             J67             19.402    0.012     12.202    11.916    0
0
C6              J15             J2312           20.221    0.012     13.771    11.58     0
0
C60             J43             J70             73.615    0.012     12.872    12.668    0
0
C61             J31             J43             47.818    0.012     12.665    12.872    0
0
C62             J73             J44             2.889     0.012     12.86     12.872    0
0
C63             J48             J36             58.382    0.012     11.508    11.727    0
0
C65             J70             J42             64.446    0.012     12.668    12.238    0
0
C66             J29             J31             3.655     0.012     12.674    12.665    0
0
C67             J79             J78             9.05      0.012     12.188    12.4      0
0
C68             J80             J67             12.636    0.012     11.826    11.916    0
0
C7              J6              J1              17.512    0.012     13.311    13.397    0
0
C70             J83             J72             2.461     0.012     11.696    11.596    0
0
C8              J3              J6              59.949    0.012     13.591    13.311    0
0
C95             J2755           J2860           73.223    0.012     14.084    12.49     0
0
C96             J2847           J2909           51.011    0.012     13.578    13.178    0
0
C97             J2938           J2918           68.42     0.012     14.358    13.582    0
0<!-- Standard PRE tag rules -->

[WEIRS]
;;              Inlet           Outlet          Weir        Crest     Disch.    Flap End     End
;;Name          Node            Node            Type        Height    Coeff.    Gate Con.
Coeff.     Surcharge  RoadWidth  RoadSurf   Coeff. Curve
;;-------------- ---------------- ---------------- ------------ ---------- ---------- ---- -------- -----
----- ---------- ---------- ---------- ----------------
;B- branch
;{22405761@student.uwa.edu.au - 2019.12.30} The discharge coefficient has been taken from the mean
average of the 2012-2017 flow data
22926618_6      J49             J1788           TRANSVERSE  9.09      3.33      NO   0        0
YES<!-- Standard PRE tag rules -->

[XSECTIONS]
```

;;Link	Shape	Geom1	Geom2	Geom3	Geom4	Barrels
206110366	CIRCULAR	1.35	0	0	0	1
206110379_1	CIRCULAR	1.35	0	0	0	1
206110379_2	CIRCULAR	1.35	0	0	0	1
206110379_4	CIRCULAR	1.35	0	0	0	1
206110379_5	CIRCULAR	1.35	0	0	0	1
22803188_2	IRREGULAR	AnvilTransect	0	0	0	1
22803188_3	IRREGULAR	AnvilTransect	0	0	0	1
22803188_4	IRREGULAR	AnvilTransect	0	0	0	1
22803188_5	IRREGULAR	AnvilTransect	0	0	0	1
22926618_1	IRREGULAR	AnvilTransect	0	0	0	1
22926618_2	IRREGULAR	AnvilTransect	0	0	0	1
22926618_3	IRREGULAR	Anvil_Transect2	0	0	0	1
22926618_4	IRREGULAR	Anvil_Transect2	0	0	0	1
22926629	PARABOLIC	1.35	2	0	0	1
23116769	CIRCULAR	1.35	0	0	0	1
23116814	CIRCULAR	1.35	0	0	0	1
23116826	CIRCULAR	1.35	0	0	0	1
23405543	CIRCULAR	1.35	0	0	0	1
23405563	CIRCULAR	1.35	0	0	0	1
57466689_1	CIRCULAR	1.35	0	0	0	1
57466741	CIRCULAR	1.35	0	0	0	1
57466813	CIRCULAR	1.35	0	0	0	1
C1	CIRCULAR	1	0	0	0	1
C1_1	CIRCULAR	1	0	0	0	1
C1_2	CIRCULAR	1	0	0	0	1
C10	CIRCULAR	1	0	0	0	1
C108	CIRCULAR	1	0	0	0	1
C109	CIRCULAR	0.75	0	0	0	1
C11	CIRCULAR	1	0	0	0	1
C110	CIRCULAR	0.75	0	0	0	1
C111	CIRCULAR	0.45	0	0	0	1
C112	CIRCULAR	0.45	0	0	0	1
C113	CIRCULAR	0.75	0	0	0	1
C12	CIRCULAR	1	0	0	0	1
C126	CIRCULAR	1	0	0	0	1
C127	CIRCULAR	1	0	0	0	1
C128	CIRCULAR	0.45	0	0	0	1
C129_1	CIRCULAR	1	0	0	0	1
C129_2	CIRCULAR	1	0	0	0	1
C13	CIRCULAR	1	0	0	0	1
C130	CIRCULAR	1	0	0	0	1
C131	CIRCULAR	1	0	0	0	1
C141	CIRCULAR	1	0	0	0	1
C142	CIRCULAR	0.75	0	0	0	1
C143	CIRCULAR	0.45	0	0	0	1
C144	CIRCULAR	0.45	0	0	0	1
C145	CIRCULAR	1	0	0	0	1
C146	CIRCULAR	1	0	0	0	1
C147	CIRCULAR	0.45	0	0	0	1
C148	CIRCULAR	0.45	0	0	0	1
C158	CIRCULAR	0.75	0	0	0	1
C159	CIRCULAR	0.75	0	0	0	1
C16	CIRCULAR	1	0	0	0	1
C160	CIRCULAR	0.75	0	0	0	1
C161	CIRCULAR	0.45	0	0	0	1
C167_2	CIRCULAR	1	0	0	0	1
C169	CIRCULAR	0.75	0	0	0	1
C17	CIRCULAR	1	0	0	0	1
C170	CIRCULAR	1	0	0	0	1
C176	IRREGULAR	Anvil_Transect2	0	0	0	1
C18	CIRCULAR	1	0	0	0	1
C182	CIRCULAR	0.45	0	0	0	1
C185	CIRCULAR	1	0	0	0	1
C186	CIRCULAR	1	0	0	0	1
C19	CIRCULAR	1	0	0	0	1
C193	CIRCULAR	0.45	0	0	0	1
C194	CIRCULAR	0.45	0	0	0	1
C195	CIRCULAR	1	0	0	0	1
C196	CIRCULAR	1	0	0	0	1
C20	CIRCULAR	1.65	0	0	0	1
C21	CIRCULAR	1	0	0	0	1
C22	CIRCULAR	1	0	0	0	1
C23	CIRCULAR	1	0	0	0	1
C24	CIRCULAR	1	0	0	0	1
C25	CIRCULAR	1	0	0	0	1
C26	CIRCULAR	1	0	0	0	1

```
C27              CIRCULAR     1                0          0          0          1
C28              CIRCULAR     1                0          0          0          1
C29              CIRCULAR     1                0          0          0          1
C3               CIRCULAR     1                0          0          0          1
C30              CIRCULAR     1                0          0          0          1
C31              CIRCULAR     1                0          0          0          1
C32              CIRCULAR     1                0          0          0          1
C33              CIRCULAR     1                0          0          0          1
C34              CIRCULAR     1                0          0          0          1
C35              CIRCULAR     1                0          0          0          1
C37              CIRCULAR     1                0          0          0          1
C38              CIRCULAR     1                0          0          0          1
C39              CIRCULAR     1                0          0          0          1
C4               CIRCULAR     1                0          0          0          1
C40              CIRCULAR     1                0          0          0          1
C41              CIRCULAR     1                0          0          0          1
C42              CIRCULAR     1                0          0          0          1
C44              CIRCULAR     1                0          0          0          1
C45              CIRCULAR     1                0          0          0          1
C46              CIRCULAR     1                0          0          0          1
C47              CIRCULAR     1                0          0          0          1
C49              CIRCULAR     1                0          0          0          1
C5               CIRCULAR     1                0          0          0          1
C50              CIRCULAR     1                0          0          0          1
C51              CIRCULAR     1                0          0          0          1
C52              CIRCULAR     1                0          0          0          1
C53              CIRCULAR     1                0          0          0          1
C54              CIRCULAR     1                0          0          0          1
C55              CIRCULAR     1                0          0          0          1
C56              CIRCULAR     1                0          0          0          1
C57              CIRCULAR     1                0          0          0          1
C58              CIRCULAR     1                0          0          0          1
C59              CIRCULAR     1                0          0          0          1
C6               CIRCULAR     1                0          0          0          1
C60              CIRCULAR     1                0          0          0          1
C61              CIRCULAR     1                0          0          0          1
C62              CIRCULAR     1                0          0          0          1
C63              CIRCULAR     1                0          0          0          1
C65              CIRCULAR     1                0          0          0          1
C66              CIRCULAR     1                0          0          0          1
C67              CIRCULAR     1                0          0          0          1
C68              CIRCULAR     1                0          0          0          1
C7               CIRCULAR     1                0          0          0          1
C70              CIRCULAR     1                0          0          0          1
C8               CIRCULAR     1                0          0          0          1
C95              CIRCULAR     1                0          0          0          1
C96              CIRCULAR     1                0          0          0          1
C97              CIRCULAR     0.75             0          0          0          1
22926618_6       RECT_OPEN    0.7              0.6        0          0<!-- Standard PRE tag rules -->

[TRANSECTS]
;Half street, width = 5m, curb = 0.15m , cross-slope = 0.02m/m, bank-slope = 0.02m/m, bank-height =
0.23m.
NC 0.02     0.02     0.014
X1 Anvil_Transect2  4        0.0      5        0.0       0.0       0.0      0.0      0.0
GR 1.3      0        0        3        0        6        1.3      9<!-- Standard PRE tag rules -->
NC 0.01     0.01     0.01
X1 AnvilTransect    4        0.0      0.0      0.0       0.0       0.0      0.0      0.0
GR 0.65     0        0        3        0        8.5      0.65     11.5<!-- Multi line multiple
consecutive spaces -->

[LOSSES]
;;Link           Inlet      Outlet     Average    Flap Gate  SeepageRate
;;-------------- ---------- ---------- ---------- ---------- ----------<!-- Standard PRE tag rules -->

[INFLOWS]
;;                                                Param    Units    Scale    Baseline Baseline
;;Node           Parameter        Time Series      Type     Factor   Factor   Value    Pattern
;;-------------- ---------------- ---------------- -------- -------- -------- -------- --------
J2887            FLOW             ""               FLOW     1.0      1        0.001
J46              FLOW             InflowWetland    FLOW     1.0      1        0
J355             FLOW             ""               FLOW     1.0      1        0.047<!-- Standard PRE tag
rules -->

[CURVES]
;;Name           Type       X-Value    Y-Value
;;-------------- ---------- ---------- ----------
;The inlet structure has a rock drop structure, with an assigned curve that I take as a beehave curve
```

```
Beehivegate      Rating     0          0
Beehivegate                 0.06096    42.4752699
Beehivegate                 0.12192    84.9505398
Beehivegate                 0.18288    104.7723324
Beehivegate                 0.24384    121.7624404
Beehivegate                 0.3048     135.9208637
Beehivegate                 0.36576    150.079287
Beehivegate                 0.42672    161.4060256
Beehivegate                 0.48768    172.7327643
Beehivegate                 0.54864    184.0595029
Beehivegate                 0.6096     192.5545569
Beehivegate                 0.67056    201.0496109
Beehivegate                 0.73152    212.3763495
Beehivegate                 0.79248    220.8714035<!-- Standard PRE tag rules -->
;In the inlet of the wetland there is a sedimentation pond to trap particular material
SedimentationPond Storage    0          0
SedimentationPond            0.65       1308
SedimentationPond            0.95       1808<!-- Standard PRE tag rules -->

[TIMESERIES]
DailyRainfall_Canning 01/02/2009 0:00       0
DailyRainfall_Canning 01/03/2009 0:00       0
DailyRainfall_Canning 01/04/2009 0:00       0
DailyRainfall_Canning 01/05/2009 0:00       0
DailyRainfall_Canning 01/06/2009 0:00       0
DailyRainfall_Canning 01/07/2009 0:00       0
DailyRainfall_Canning 01/08/2009 0:00       0
DailyRainfall_Canning 01/09/2009 0:00       0
DailyRainfall_Canning 01/10/2009 0:00       0
DailyRainfall_Canning 01/11/2009 0:00       0
DailyRainfall_Canning 01/12/2009 0:00       0<!-- Standard PRE tag rules -->

......
Too many data points (3750 in total).


;UpInflow Flow (m^3/s)
InflowWetland    07/18/2012 15:30      0.016
InflowWetland    07/18/2012 15:35      0.016
InflowWetland    07/18/2012 15:40      0.015
InflowWetland    07/18/2012 15:45      0.014
InflowWetland    07/18/2012 15:50      0.014
InflowWetland    07/18/2012 15:55      0.014
InflowWetland    07/18/2012 16:00      0.014
InflowWetland    07/18/2012 16:05      0.014
InflowWetland    07/18/2012 16:10      0.013
InflowWetland    07/18/2012 16:15      0.012
InflowWetland    07/18/2012 16:20      0.012<!-- Standard PRE tag rules -->

......
Too many data points (570306 in total).


;Lateral inflow (m^3/s)
J355             01/02/2009 00:01:00   0.047
J355             01/02/2009 00:02:00   0.047
J355             01/02/2009 00:03:00   0.047
J355             01/02/2009 00:04:00   0.047
J355             01/02/2009 00:05:00   0.047
J355             01/02/2009 00:06:00   0.047
J355             01/02/2009 00:07:00   0.047
J355             01/02/2009 00:08:00   0.047
J355             01/02/2009 00:09:00   0.047
J355             01/02/2009 00:10:00   0.047
J355             01/02/2009 00:11:00   0.047<!-- Standard PRE tag rules -->

......
Too many data points (921600 in total).


LateralInflow    02/25/2012 8:45       0.012
LateralInflow    02/25/2012 8:50       0.012
LateralInflow    02/25/2012 8:55       0.012
LateralInflow    02/25/2012 9:00       0.012
LateralInflow    02/25/2012 9:05       0.012
LateralInflow    02/25/2012 9:10       0.012
LateralInflow    02/25/2012 9:15       0.012
LateralInflow    02/25/2012 9:20       0.012
```

```
LateralInflow    02/25/2012 9:25       0.012
LateralInflow    02/25/2012 9:30       0.011
LateralInflow    02/25/2012 9:35       0.011<!-- Multi line multiple consecutive spaces -->

......
Too many data points (611859 in total).


MeanTemperature  FILE "D:\RESEARCH PROJECT\7. STRUCTURED DATA\Anvil\Climatology\MeanTemp_Canning.dat"

;Rainfall (mm)
Precipitation    01/15/2018 08:00:00   0
Precipitation    01/15/2018 08:30:00   0.2
Precipitation    01/15/2018 08:49:00   0.2
Precipitation    01/15/2018 09:00:00   0.2
Precipitation    01/15/2018 09:21:00   0
Precipitation    01/15/2018 09:30:00   0
Precipitation    01/15/2018 10:00:00   0
Precipitation    01/15/2018 10:01:00   0
Precipitation    01/15/2018 10:30:00   0
Precipitation    01/15/2018 10:53:00   0.4
Precipitation    01/15/2018 11:00:00   0.2
Precipitation    01/15/2018 11:30:00   0.4
Precipitation    01/15/2018 11:47:00   0
Precipitation    01/15/2018 12:00:00   0.4
Precipitation    01/15/2018 12:02:00   0.2
Precipitation    01/15/2018 12:22:00   2.2
Precipitation    01/15/2018 12:30:00   2.4
Precipitation    01/15/2018 13:00:00   4.4
Precipitation    01/15/2018 13:30:00   4.8
Precipitation    01/15/2018 14:00:00   2.6
Precipitation    01/15/2018 14:22:00   1.4
Precipitation    01/15/2018 14:30:00   0.4
Precipitation    01/15/2018 15:00:00   2
Precipitation    01/15/2018 15:30:00   3
Precipitation    01/15/2018 16:00:00   4.2
Precipitation    01/15/2018 16:30:00   2.6
Precipitation    01/15/2018 16:40:00   0.4
Precipitation    01/15/2018 16:51:00   1
Precipitation    01/15/2018 17:00:00   1
Precipitation    01/15/2018 17:08:00   0.8
Precipitation    01/15/2018 17:30:00   3.2
Precipitation    01/15/2018 17:40:00   1.8
Precipitation    01/15/2018 18:00:00   2.8
Precipitation    01/15/2018 18:03:00   0.4
Precipitation    01/15/2018 18:30:00   2.4
Precipitation    01/15/2018 19:00:00   2.4
Precipitation    01/15/2018 19:13:00   1.4
Precipitation    01/15/2018 19:30:00   1
Precipitation    01/15/2018 20:00:00   1.4
Precipitation    01/15/2018 20:02:00   0.2
Precipitation    01/15/2018 20:30:00   1.8
Precipitation    01/15/2018 20:41:00   0.8
Precipitation    01/15/2018 21:00:00   2.8
Precipitation    01/15/2018 21:30:00   3.6
Precipitation    01/15/2018 21:55:00   2
Precipitation    01/15/2018 22:00:00   0.2
Precipitation    01/15/2018 22:30:00   2
Precipitation    01/15/2018 22:31:00   0.2
Precipitation    01/15/2018 22:52:00   1.4
Precipitation    01/15/2018 23:00:00   0.4
Precipitation    01/15/2018 23:30:00   0.6
Precipitation    01/15/2018 23:36:00   0.4
Precipitation    01/15/2018 23:54:00   2
Precipitation    01/16/2018 00:00:00   1
Precipitation    01/16/2018 00:30:00   3
Precipitation    01/16/2018 00:31:00   0.2
Precipitation    01/16/2018 00:33:00   0
Precipitation    01/16/2018 01:00:00   1.4
Precipitation    01/16/2018 01:03:00   0
Precipitation    01/16/2018 01:11:00   0.4
Precipitation    01/16/2018 01:30:00   0.2
Precipitation    01/16/2018 02:00:00   0.4
Precipitation    01/16/2018 02:17:00   0.2
Precipitation    01/16/2018 02:30:00   0.2
Precipitation    01/16/2018 02:34:00   0<!-- Standard PRE tag rules -->
;Outflow (m^3/s)
System           01/02/2009 00:01:00   0.047
```

```
System           01/02/2009 00:02:00   0.047
System           01/02/2009 00:03:00   0.047
System           01/02/2009 00:04:00   0.047
System           01/02/2009 00:05:00   0.047
System           01/02/2009 00:06:00   0.047
System           01/02/2009 00:07:00   0.047
System           01/02/2009 00:08:00   0.047
System           01/02/2009 00:09:00   0.047
System           01/02/2009 00:10:00   0.047
System           01/02/2009 00:11:00   0.047<!-- Standard PRE tag rules -->

......
Too many data points (921600 in total).


Temperature19072009 07/19/2009 9:00:00    13.25
Temperature19072009 07/20/2009 9:00:00    11<!-- Multi line missing multiple consecutive spaces but
tabular format data -->

[REPORT]
INPUT      YES
CONTROLS   NO
AVERAGES   YES
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL<!-- Standard PRE tag rules -->

[TAGS]
Subcatch   S10              BUILDING
Subcatch   S11              BUILDING
Subcatch   S12              BUILDING
Subcatch   S13              Extract
Subcatch   S14              WDT
Subcatch   S15_1            WDT
Subcatch   S15_10           WDT
Subcatch   S15_12           WDT
Subcatch   S15_2            WDT
Subcatch   S15_3            BUILDING
Subcatch   S15_4            WDT
Subcatch   S15_5            WDT
Subcatch   S15_6            BUILDING
Subcatch   S15_7            WDT
Subcatch   S15_8            WDT
Subcatch   S15_9            WDT
Subcatch   S16              BUILDING
Subcatch   S17              BUILDING
Subcatch   S18_2            BUILDING
Subcatch   S18_3            BUILDING
Subcatch   S19              BUILDING
Subcatch   S2               BUILDING
Subcatch   S20              BUILDING
Subcatch   S21              BUILDING
Subcatch   S22              BUILDING
Subcatch   S23_1            WDT
Subcatch   S23_3            WDT
Subcatch   S23_4            WDT
Subcatch   S24              BUILDING
Subcatch   S25              BUILDING
Subcatch   S26_1            WDT_SA1
Subcatch   S26_3            WDT_SA1
Subcatch   S29_1            WDT
Subcatch   S29_10           WDT_SA1
Subcatch   S29_11           WDT_SA1
Subcatch   S29_12           WDT_SA1
Subcatch   S29_13           WDT_SA1
Subcatch   S29_14           WDT_SA1
Subcatch   S29_15           BUILDING
Subcatch   S29_17           BUILDING
Subcatch   S29_2            BUILDING
Subcatch   S29_3            WDT
Subcatch   S29_5            WDT_SA1
Subcatch   S29_7            WDT_SA1
Subcatch   S29_8            WDT
Subcatch   S29_9            WDT_SA1
Subcatch   S3               WDT_SA1
Subcatch   S30              BUILDING
Subcatch   S31              BUILDING
Subcatch   S32              BUILDING
```

Subcatch	S33	BUILDING
Subcatch	S34	BUILDING
Subcatch	S35	BUILDING
Subcatch	S36	BUILDING
Subcatch	S37	WDT_SA1
Subcatch	S37_1	WDT
Subcatch	S37_10	WDT
Subcatch	S37_11	WDT
Subcatch	S37_12	WDT
Subcatch	S37_2	WDT
Subcatch	S37_3	WDT
Subcatch	S37_4	WDT
Subcatch	S37_8	WDT
Subcatch	S38	BUILDING
Subcatch	S39	BUILDING
Subcatch	S4	BUILDING
Subcatch	S40	BUILDING
Subcatch	S41	BUILDING
Subcatch	S42	BUILDING
Subcatch	S43	Wetland
Subcatch	S43_2	WDT_SA1
Subcatch	S43_4	WDT_SA1
Subcatch	S43_5	WDT_SA1
Subcatch	S43_6	WDT_SA1
Subcatch	S43_7	WDT_SA1
Subcatch	S43_9	WDT_SA1
Subcatch	S44	BUILDING
Subcatch	S45	BUILDING
Subcatch	S46	BUILDING
Subcatch	S46_1	WDT_SA1
Subcatch	S46_10	WDT_SA1
Subcatch	S46_2	WDT_SA1
Subcatch	S46_3	WDT_SA1
Subcatch	S46_4	WDT_SA1
Subcatch	S46_5	WDT_SA1
Subcatch	S46_6	WDT_SA1
Subcatch	S46_7	WDT_SA1
Subcatch	S47	BUILDING
Subcatch	S48	BUILDING
Subcatch	S49	BUILDING
Subcatch	S5	BUILDING
Subcatch	S50	BUILDING
Subcatch	S51	BUILDING
Subcatch	S52_1	WDT_SA1
Subcatch	S52_2	WDT_SA1
Subcatch	S52_3	WDT_SA1
Subcatch	S52_4	WDT_SA1
Subcatch	S52_6	WDT_SA1
Subcatch	S52_7	WDT_SA1
Subcatch	S53	BUILDING
Subcatch	S54	BUILDING
Subcatch	S55	BUILDING
Subcatch	S56	BUILDING
Subcatch	S57	BUILDING
Subcatch	S59	BUILDING
Subcatch	S63_1	WDT_SA1
Subcatch	S63_11	WDT_SA1
Subcatch	S63_12	WDT_SA1
Subcatch	S63_13	WDT_SA1
Subcatch	S63_14	WDT_SA1
Subcatch	S63_15	WDT_SA1
Subcatch	S63_2	WDT_SA1
Subcatch	S63_3	WDT_SA1
Subcatch	S63_4	WDT_SA1
Subcatch	S63_5	WDT_SA1
Subcatch	S63_6	WDT_SA1
Subcatch	S63_7	WDT_SA1
Subcatch	S63_8	WDT_SA1
Subcatch	S63_9	WDT_SA1
Subcatch	S7	BUILDING
Subcatch	S8	BUILDING
Subcatch	S9	BUILDING
Node	J1788	SITE6162796
Node	J2887	SITE6162962
Link	206110366	MainPipe
Link	206110379_1	MainPipe
Link	206110379_2	MainPipe
Link	206110379_4	MainPipe

Link	206110379_5	MainPipe
Link	22803188_2	OpenChannel
Link	22803188_3	OpenChannel
Link	22803188_4	OpenChannel
Link	22803188_5	OpenChannel
Link	22926618_1	OpenChannel
Link	22926618_2	OpenChannel
Link	22926618_3	OpenChannel
Link	22926618_4	OpenChannel
Link	22926629	OpenChannel
Link	23116769	MainPipe
Link	23116814	MainPipe
Link	23116826	MainPipe
Link	23405543	MainPipe
Link	23405563	MainPipe
Link	57466689_1	MainPipe
Link	57466741	MainPipe
Link	57466813	MainPipe
Link	C1	Secondary
Link	C1_1	Secondary
Link	C1_2	Secondary
Link	C10	Secondary
Link	C108	Secondary
Link	C109	Secondary
Link	C11	Secondary
Link	C110	Secondary
Link	C111	Secondary
Link	C112	Secondary
Link	C113	Secondary
Link	C12	Secondary
Link	C126	Secondary
Link	C127	Secondary
Link	C128	Secondary
Link	C129_1	Secondary
Link	C129_2	Secondary
Link	C13	Secondary
Link	C130	Secondary
Link	C131	Secondary
Link	C141	Secondary
Link	C142	Secondary
Link	C143	Secondary
Link	C144	Secondary
Link	C145	Secondary
Link	C146	Secondary
Link	C147	Secondary
Link	C148	Secondary
Link	C158	Secondary
Link	C159	Secondary
Link	C16	Secondary
Link	C160	Secondary
Link	C161	Secondary
Link	C167_2	Secondary
Link	C169	Secondary
Link	C17	Secondary
Link	C170	Secondary
Link	C176	OpenChannel
Link	C18	Secondary
Link	C182	Secondary
Link	C185	Secondary
Link	C186	Secondary
Link	C19	Secondary
Link	C193	Secondary
Link	C194	Secondary
Link	C195	Secondary
Link	C196	Secondary
Link	C20	Secondary
Link	C21	Secondary
Link	C22	Secondary
Link	C23	Secondary
Link	C24	Secondary
Link	C25	Secondary
Link	C26	Secondary
Link	C27	Secondary
Link	C28	Secondary
Link	C29	Secondary
Link	C3	Secondary
Link	C30	Secondary
Link	C31	Secondary

```
Link       C32              Secondary
Link       C33              Secondary
Link       C34              Secondary
Link       C35              Secondary
Link       C37              Secondary
Link       C38              Secondary
Link       C39              Secondary
Link       C4               Secondary
Link       C40              Secondary
Link       C41              Secondary
Link       C42              Secondary
Link       C44              Secondary
Link       C45              Secondary
Link       C46              Secondary
Link       C47              Secondary
Link       C49              Secondary
Link       C5               Secondary
Link       C50              Secondary
Link       C51              Secondary
Link       C52              Secondary
Link       C53              Secondary
Link       C54              Secondary
Link       C55              Secondary
Link       C56              Secondary
Link       C57              Secondary
Link       C58              Secondary
Link       C59              Secondary
Link       C6               Secondary
Link       C60              Secondary
Link       C61              Secondary
Link       C62              Secondary
Link       C63              Secondary
Link       C65              Secondary
Link       C66              Secondary
Link       C67              Secondary
Link       C68              Secondary
Link       C7               Secondary
Link       C70              Secondary
Link       C8               Secondary
Link       C95              Secondary
Link       C96              Secondary
Link       C97              Secondary
Link       22926618_6       OpenChannel<!-- Standard PRE tag rules -->

[MAP]
DIMENSIONS       398805.4205      6459555.4531     399946.9235      6460565.1849
UNITS            Meters<!-- Standard PRE tag rules -->

[COORDINATES]
;;Node           X-Coord          Y-Coord
;;-------------- ---------------- ----------------
J1               399197.305       6460229.757
J10              399260.054       6460206.219
J1040            399469.516       6459823.245
J11              399256.887       6460222.68
J12              399302.225       6460422.998
J13              399320.993       6460300.764
J14              399253.344       6460213
J1415            399431.896       6460000.328
J15              398978.916       6460194.465
J16              399281.445       6460128.954
J17              398982.456       6460211.435
J1701            399403.636       6460246.674
J1788            399476.978       6459873.079
J18              398983.792       6460179.049
J19              399658.215       6459991.701
J1969            399491.903       6459957.783
J2               399262.005       6460210.425
J20              398975.813       6460216.802
J21              399281.864       6460116.293
J2181            398881.963       6460218.562
J22              399117.121       6460122.566
J2293            398988.781       6460186.982
J23              399058.4         6460170.453
J2312            398996.538       6460184.559
J24              399019.976       6460179.966
J25              399124.364       6460154.51
J2510            399172.717       6460136.572
```

J2594	399236.254	6460113.123
J26	399058.921	6460173.916
J2678	399301.08	6460093.436
J2692	399319.153	6460088.442
J27	399659.522	6459992.075
J2709	399334.483	6459745.528
J2712	399335.071	6459750.51
J2717	399340.338	6459827.346
J2719	399342.126	6459825.604
J2722	399348.75	6459967.199
J2728	399360.633	6459799.18
J2730	399365.374	6459802.178
J2749	399382.112	6459800.666
J2754	399389.557	6460249.812
J2755	399390.164	6460131.861
J2757	399393.141	6459845.119
J2764	399396.777	6460248.179
J2771	399398.609	6460010.513
J2779	399402.467	6460242.47
J2785	399410.01	6459731.986
J2786	399410.463	6459829.825
J2787	399411.625	6460293.515
J2794	399421.163	6459828.642
J2797	399422.825	6459893.748
J28	399020.934	6460185.167
J2813	399425.724	6460016.721
J2816	399425.84	6460025.315
J2822	399428.045	6459896.141
J2831	399433.805	6459949.231
J2838	399439.055	6460028.91
J2839	399440.815	6460231.622
J2845	399444.015	6459988.3
J2847	399445.566	6460237.476
J2855	399451.861	6459795.752
J2857	399452.527	6459994.151
J2860	399460.446	6460111.393
J2868	399469.988	6460147.503
J2870	399471.599	6460146.992
J2887	399478.548	6459986.383
J2890	399479.577	6460144.021
J2891	399480.813	6459873.117
J29	399768.438	6459801.465
J29_14	399684.862	6459729.111
J2909	399493.486	6460220.03
J2915	399497.491	6459980.942
J2918	399509.12	6460267.105
J2921	399510.228	6459948.071
J2931	399519.353	6459938.821
J2938	399529.643	6460332.355
J3	399132.494	6460262.847
J30	399774.88	6459808.11
J31	399764.791	6459801.234
J32	399764.014	6459797.361
J33	399612.149	6459945.478
J34	399613.992	6459945.468
J35	399574.325	6459887.471
J36	399557.54	6459853.05
J37	399621.798	6459745.98
J38	399653.377	6459753.232
J39	399671.7	6459747.856
J4	399093.302	6460274.155
J40	399686.74	6459733.868
J41	399688.706	6459733.375
J42	399632.737	6459931.975
J43	399730.874	6459834.923
J44	399728.958	6459832.687
J45	399578.456	6460030.91
J46	399550.314	6460173.841
J47	399563.596	6459895.196
J48	399551.272	6459795.022
J49	399479.158	6459894.527
J5	399212.806	6460321.425
J50	399590.445	6459744.48
J52	399549.065	6459792.548
J53	399548.935	6459791.34
J55	399533.544	6460114.773
J56	399704.756	6460038.748
J57	399719.649	6460029.139

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J59              399667.533       6459985.613
J6               399189.897       6460245.62
J63              399637.08        6459931.047
J64              399643.418       6459937.498
J65              399539.483       6459794.13
J66              399549.433       6459776.642
J67              399571.34        6459747.826
J68              399699.902       6459744.101
J69              399538.697       6459792.389
J7               399183.374       6460180.216
J70              399678.638       6459886.764
J72              399574.147       6459888.772
J73              399726.959       6459830.603
J78              399680.977       6459887.813
J79              399687.446       6459894.139
J8               399123.452       6460151.175
J80              399580.657       6459756.357
J83              399575.164       6459891.013
J9               399257.655       6460372.366
J355             399430.348       6459607.009
J54              399545.068       6460094.129<!-- Standard PRE tag rules -->

[VERTICES]
;;Link           X-Coord          Y-Coord
;;-------------- ---------------- ----------------
206110366        399212.17        6460125.045
206110366        399218.344       6460123.001
206110379_1      399003.086       6460183.252
206110379_1      399007.337       6460182.425
206110379_2      399125.257       6460150.633
206110379_4      399060.669       6460169.78
206110379_5      399023.913       6460179.2
206110379_5      399042.987       6460175.016
22803188_2       399543.06        6460045.188
22803188_2       399530.668       6460035.563
22803188_2       399557.402       6460005.857
22803188_2       399550.122       6459999.207
22803188_2       399512.061       6459985.675
22803188_3       399547.014       6460091.237
22803188_3       399566.246       6460077.538
22803188_3       399587.731       6460058.744
22803188_3       399591.547       6460044.182
22803188_3       399579.925       6460030.911
22803188_4       399546.274       6460159.78
22803188_5       399532.851       6460112.309
22926618_2       399481.02        6459912.84
22926618_3       399468.184       6459816.094
22926618_3       399466.896       6459813.389
22926618_3       399452.65        6459797.701
22926618_4       399474.788       6459851.53
23116814         399434.053       6459999.654
23116814         399434.053       6459999.66
57466741         399325.345       6460082.355
C108             399507.973       6459950.301
C108             399505.977       6459951.57
C108             399504.019       6459952.452
C108             399502.747       6459953.34
C108             399501.145       6459954.155
C108             399498.831       6459955.172
C108             399497.016       6459956.069
C108             399495.687       6459956.748
C108             399494.735       6459957.473
C108             399493.644       6459957.906
C108             399492.496       6459958.075
C176             399443.574       6459723.038<!-- Standard PRE tag rules -->

[POLYGONS]
;;Subcatchment   X-Coord          Y-Coord
;;-------------- ---------------- ----------------
S1               399599.959       6459771
S1               399602.191       6459771
S1               399625.527       6459773.554
S1               399626           6459786
S1               399626           6459791
S1               399627.856       6459791
S1               399628.251       6459793.958
S1               399664.158       6459790.143
S1               399653.453       6459758.802
```

S1	399627.666	6459749.232
S1	399617.944	6459729.957
S1	399579.926	6459732.323
S1	399542.893	6459733.533
S1	399598.979	6459781.461
S1	399599.959	6459771
S10	399696.029	6460162.171
S10	399710.028	6460211.482
S10	399731.394	6460208.873
S10	399734.343	6460210.485
S10	399740.046	6460219.117
S10	399745.481	6460219.923
S10	399748.16	6460218.327
S10	399747.396	6460216
S10	399746	6460216
S10	399746	6460211.746
S10	399739.19	6460191
S10	399736	6460191
S10	399736	6460186
S10	399737.549	6460186
S10	399729.344	6460161
S10	399726	6460161
S10	399726	6460153.172
S10	399696.029	6460162.171
S11	399595.745	6459816
S11	399594.808	6459826
S11	399596	6459826
S11	399596	6459836
S11	399606	6459836
S11	399606	6459841
S11	399613.536	6459841
S11	399613.225	6459833.214
S11	399623.95	6459804.668
S11	399625.056	6459795.162
S11	399628.251	6459793.958
S11	399627.856	6459791
S11	399626	6459791
S11	399626	6459786
S11	399627.189	6459786
S11	399625.527	6459773.554
S11	399602.191	6459771
S11	399599.959	6459771
S11	399596	6459813.274
S11	399596	6459816
S11	399595.745	6459816
S12	399236	6460374.834
S12	399171.009	6460434.606
S12	399171	6460434.607
S12	399171.006	6460434.608
S12	399176.324	6460435.345
S12	399181	6460435.993
S12	399201.788	6460461.719
S12	399216	6460446
S12	399216	6460443.818
S12	399216	6460441
S12	399219.336	6460441
S12	399231	6460431.148
S12	399231	6460426
S12	399236	6460426
S12	399236.899	6460426
S12	399246	6460417.263
S12	399246	6460416
S12	399247.315	6460416
S12	399251	6460412.463
S12	399251	6460411
S12	399252.524	6460411
S12	399261	6460402.863
S12	399261	6460398.572
S12	399259.328	6460396
S12	399256	6460396
S12	399256	6460391
S12	399251	6460391
S12	399251	6460383.183
S12	399250.86	6460382.968
S12	399248.162	6460381
S12	399246	6460381
S12	399246	6460379.423
S12	399241.308	6460376

S12	399236	6460376
S12	399236	6460374.834
S13	399304.73	6460276.227
S13	399299.309	6460267.792
S13	399235.903	6460288.461
S13	399239.861	6460296.45
S13	399304.73	6460276.227
S14	399171.588	6460405.244
S14	399159.302	6460419.22
S14	399171	6460434.614
S14	399236	6460375.993
S14	399208.299	6460363.455
S14	399184.103	6460391
S14	399181	6460391
S14	399181	6460394.532
S14	399171.588	6460405.244
S15_1	399051	6460179.467
S15_1	399031.18	6460188.671
S15_1	399041	6460204.593
S15_1	399041	6460206
S15_1	399041.868	6460206
S15_1	399046	6460212.699
S15_1	399046	6460216
S15_1	399048.036	6460216
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S52_4	399709.241	6459829.357
S52_4	399699.192	6459834.298
S52_4	399681.282	6459846.388
S52_4	399660.422	6459865.529
S52_4	399659.527	6459866.11
S52_4	399657.682	6459868.124
S52_6	399353.713	6460138.079
S52_6	399469.455	6460102.714
S52_6	399445.201	6460017.766
S52_6	399427.087	6460012.741
S52_6	399418.166	6460013.283
S52_6	399407.307	6460017.413
S52_6	399398.606	6460023.712
S52_6	399389.416	6460034.523
S52_6	399380.271	6460053.659
S52_6	399379.343	6460061.168
S52_6	399363.494	6460088.053
S52_6	399366.389	6460103.214
S52_6	399366.116	6460111.329
S52_6	399354.524	6460124.62
S52_6	399353.22	6460136.608
S52_6	399353.713	6460138.079
S52_7	399472.534	6460216.766
S52_7	399498.963	6460206.06
S52_7	399469.455	6460102.714
S52_7	399353.713	6460138.079
S52_7	399356.366	6460146
S52_7	399371	6460146
S52_7	399371	6460141
S52_7	399387.468	6460141
S52_7	399391	6460145.784
S52_7	399391	6460151
S52_7	399394.851	6460151
S52_7	399408.491	6460169.475
S52_7	399412.982	6460175.558
S52_7	399411.388	6460176
S52_7	399406	6460176
S52_7	399406	6460177.495
S52_7	399393.366	6460181
S52_7	399401.166	6460196
S52_7	399408.107	6460192.711
S52_7	399416	6460191
S52_7	399455.312	6460178.122
S52_7	399472.534	6460216.766
S52_7	399453.844	6460173.476
S52_7	399458.678	6460185.618
S52_7	399455.312	6460178.122
S52_7	399453.844	6460173.476
S53	399111	6460302.578
S53	399109.469	6460301.069
S53	399106	6460303.827
S53	399106	6460306
S53	399103.266	6460306
S53	399101	6460307.801
S53	399101	6460311
S53	399096.976	6460311
S53	399096	6460311.776
S53	399096	6460316
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S53	399086	6460319.726
S53	399086	6460322.197
S53	399124.362	6460360.414
S53	399173.564	6460318.698
S53	399171.347	6460311
S53	399171	6460311
S53	399171	6460309.795
S53	399169.804	6460305.641
S53	399166	6460306.306
S53	399123.281	6460314.677
S53	399122.137	6460313.55
S53	399122.37	6460315.565
S53	399118.731	6460311
S53	399116	6460311
S53	399116	6460307.575
S53	399115.736	6460307.243

S53	399114.474	6460306
S53	399111	6460306
S53	399111	6460302.578
S54	399039.705	6460424.383
S54	399009.195	6460394.375
S54	399008.005	6460398.659
S54	398997.307	6460412.413
S54	399004.514	6460415.206
S54	399021.335	6460433.385
S54	399044.289	6460440.431
S54	399050.051	6460449.669
S54	399052.169	6460451
S54	399056	6460451
S54	399056	6460446
S54	399059.907	6460446
S54	399038.835	6460425.097
S54	399039.705	6460424.383
S55	399001.653	6460376.919
S55	399006.77	6460372.159
S55	398988.166	6460352.926
S55	398989.47	6460360.25
S55	399000.417	6460374.303
S55	399001.653	6460376.919
S56	399035.638	6460420.383
S56	399046	6460412.18
S56	399046	6460410.927
S56	399041.321	6460406
S56	399041	6460406
S56	399041	6460405.662
S56	399036.573	6460401
S56	399036	6460401
S56	399036	6460400.397
S56	399031.825	6460396
S56	399031	6460396
S56	399031	6460395.132
S56	399027.076	6460391
S56	399026	6460391
S56	399026	6460389.867
S56	399012.831	6460376
S56	399011	6460376
S56	399011	6460374.071
S56	399010.73	6460373.788
S56	399003.305	6460380.416
S56	399009.456	6460393.439
S56	399009.195	6460394.375
S56	399035.638	6460420.383
S57	399302.829	6460346.96
S57	399311	6460359.743
S57	399311	6460356
S57	399316	6460356
S57	399316	6460359.883
S57	399336	6460342.144
S57	399336	6460341
S57	399337.29	6460341
S57	399337.54	6460340.779
S57	399324.153	6460326.626
S57	399302.829	6460346.96
S59	399305.999	6460271.192
S59	399306	6460271.193
S59	399306	6460271.193
S59	399306.001	6460271.195
S59	399304.73	6460276.234
S59	399314.059	6460290.739
S59	399329.053	6460282.229
S59	399301.417	6460233.233
S59	399281	6460241
S59	399281	6460246
S59	399305.999	6460271.192
S59	399305.999	6460271.192
S59	399306	6460271.193
S59	399306	6460271.193
S59	399305.999	6460271.192
S63_1	399397.43	6459606.842
S63_1	399416.926	6459744.566
S63_1	399458.686	6459711.11
S63_1	399468.775	6459702.448
S63_1	399466.448	6459688.273
S63_1	399454.246	6459660.475

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S63_1	399443.118	6459621.603
S63_1	399439.349	6459601.35
S63_1	399397.43	6459606.842
S63_11	399332.618	6459757.177
S63_11	399291.693	6459782.755
S63_11	399289.289	6459789.396
S63_11	399280.325	6459795.431
S63_11	399279.492	6459796.872
S63_11	399359.974	6459802.899
S63_11	399370.981	6459781.286
S63_11	399349.319	6459760.765
S63_11	399342.772	6459765.804
S63_11	399332.618	6459757.177
S63_12	399433.822	6459872.568
S63_12	399400.526	6459900.742
S63_12	399400.378	6459901.168
S63_12	399409.465	6459920.255
S63_12	399417.307	6459927.413
S63_12	399433.274	6459925.216
S63_12	399438.328	6459926.94
S63_12	399439.519	6459928.827
S63_12	399433.822	6459872.568
S63_13	399382.015	6459819.563
S63_13	399433.117	6459865.606
S63_13	399420.567	6459741.65
S63_13	399371.033	6459781.335
S63_13	399370.981	6459781.286
S63_13	399360.53	6459801.807
S63_13	399382.555	6459818.702
S63_13	399382.015	6459819.563
S63_14	399400.526	6459900.742
S63_14	399433.822	6459872.568
S63_14	399433.117	6459865.606
S63_14	399382.015	6459819.563
S63_14	399363.856	6459848.535
S63_14	399388.788	6459861.68
S63_14	399398.564	6459852.318
S63_14	399410.32	6459863.548
S63_14	399403.722	6459870.924
S63_14	399406.116	6459873.595
S63_14	399406.97	6459882.194
S63_14	399400.526	6459900.742
S63_15	399291.693	6459782.755
S63_15	399332.618	6459757.177
S63_15	399327.384	6459752.731
S63_15	399332.923	6459745.245
S63_15	399257.818	6459671.209
S63_15	399254.028	6459674.668
S63_15	399259.499	6459675.758
S63_15	399261.706	6459682.477
S63_15	399259.519	6459693.971
S63_15	399260.383	6459699.884
S63_15	399268.972	6459705.201
S63_15	399284.133	6459706.134
S63_15	399289.456	6459710.167
S63_15	399290.896	6459713.278
S63_15	399290.31	6459720.534
S63_15	399287.248	6459727.355
S63_15	399275.383	6459741.613
S63_15	399283.166	6459761.554
S63_15	399291.169	6459773.541
S63_15	399291.916	6459782.14
S63_15	399291.693	6459782.755
S63_2	399420.567	6459741.65
S63_2	399439.519	6459928.827
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S63_2	399450.745	6459953.966
S63_2	399454.836	6459959.337
S63_2	399457.585	6459960.416
S63_2	399470.702	6459958.95
S63_2	399479.883	6459924.977
S63_2	399490.618	6459916
S63_2	399489.949	6459916
S63_2	399486.666	6459875.07
S63_2	399499.569	6459871
S63_2	399501	6459871
S63_2	399501	6459870.549

S63_2	399514.448	6459866.307
S63_2	399513.855	6459865.856
S63_2	399501.879	6459862.354
S63_2	399485.819	6459864.506
S63_2	399477.218	6459757.282
S63_2	399476.575	6459749.262
S63_2	399475.27	6459732.994
S63_2	399473.498	6459731.222
S63_2	399468.775	6459702.448
S63_2	399458.686	6459711.11
S63_2	399420.567	6459741.65
S63_3	399357.107	6459831.548
S63_3	399303.752	6459798.689
S63_3	399279.492	6459796.872
S63_3	399278.494	6459798.6
S63_3	399276.174	6459821.281
S63_3	399272.307	6459827.413
S63_3	399277.366	6459842.355
S63_3	399281.506	6459848.214
S63_3	399282.174	6459848.697
S63_3	399316	6459819.698
S63_3	399316	6459821
S63_3	399320.155	6459821
S63_3	399326	6459825.769
S63_3	399326	6459826
S63_3	399326.283	6459826
S63_3	399331	6459829.849
S63_3	399331	6459831
S63_3	399332.41	6459831
S63_3	399338.538	6459836
S63_3	399336	6459836
S63_3	399336	6459840.229
S63_3	399334.607	6459841.341
S63_3	399337.133	6459843.366
S63_3	399339.346	6459841
S63_3	399341	6459841
S63_3	399341	6459839.232
S63_3	399344.023	6459836
S63_3	399346.598	6459836
S63_3	399354.7	6459843.284
S63_3	399357.107	6459831.548
S63_4	399367.99	6459715.993
S63_4	399374.345	6459715.993
S63_4	399308.587	6459645.202
S63_4	399323.883	6459634.499
S63_4	399317.413	6459631.098
S63_4	399297.878	6459634.645
S63_4	399257.818	6459671.209
S63_4	399259.499	6459675.751
S63_4	399296	6459643.626
S63_4	399367.99	6459715.993
S63_5	399383.847	6459624.977
S63_5	399382.95	6459626.438
S63_5	399403.229	6459650.147
S63_5	399402.994	6459648.169
S63_5	399383.847	6459624.977
S63_6	399390.707	6459675.87
S63_6	399344.193	6459626.236
S63_6	399317.413	6459631.098
S63_6	399392.237	6459707.479
S63_6	399416.763	6459743.441
S63_6	399406.77	6459674.292
S63_6	399390.707	6459675.87
S63_7	399383.847	6459624.977
S63_7	399402.994	6459648.169
S63_7	399398.402	6459616.393
S63_7	399344.193	6459626.236
S63_7	399360.173	6459643.287
S63_7	399383.847	6459624.977
S63_8	399382.555	6459818.702
S63_8	399360.53	6459801.807
S63_8	399359.974	6459802.899
S63_8	399303.752	6459798.689
S63_8	399357.107	6459831.548
S63_8	399354.7	6459843.284
S63_8	399357.733	6459846.011
S63_8	399359.192	6459846.076
S63_8	399363.856	6459848.535

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S63_8            399382.555       6459818.702
S63_9            399369.752       6459748.01
S63_9            399388.472       6459767.362
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S63_9            399416.763       6459743.441
S63_9            399392.237       6459707.479
S63_9            399390.09        6459705.288
S63_9            399367.99        6459715.993
S63_9            399356           6459730.993
S63_9            399332.923       6459745.251
S63_9            399327.384       6459752.738
S63_9            399333.059       6459755.315
S63_9            399342.772       6459765.81
S63_9            399369.752       6459748.01
S7               399410.32        6459863.548
S7               399398.564       6459852.318
S7               399351.687       6459897.212
S7               399366.287       6459912.772
S7               399410.32        6459863.548
S8               399391           6460145.784
S8               399387.468       6460141
S8               399371           6460141
S8               399371           6460146
S8               399356           6460146
S8               399356           6460151
S8               399355.598       6460151
S8               399376.563       6460185.662
S8               399381           6460184.431
S8               399381           6460181
S8               399393.366       6460181
S8               399406           6460177.495
S8               399406           6460176
S8               399411.388       6460176
S8               399412.982       6460175.558
S8               399394.851       6460151
S8               399391           6460151
S8               399391           6460145.784
S9               399636           6460186.296
S9               399643.445       6460212.861
S9               399654.465       6460204.572
S9               399675.95        6460200.49
S9               399680.198       6460204.62
S9               399684.47        6460213.532
S9               399686.609       6460214.342
S9               399690.735       6460213.838
S9               399677.744       6460171
S9               399676           6460171
S9               399676           6460165.25
S9               399675.003       6460161.964
S9               399671           6460163.907
S9               399671           6460166
S9               399666.689       6460166
S9               399641           6460178.469
S9               399641           6460181
S9               399635.786       6460181
S9               399634.668       6460181.543
S9               399635.917       6460186
S9               399636           6460186
S9               399636           6460186.296<!-- Standard PRE tag rules -->

[SYMBOLS]
;;Gage           X-Coord          Y-Coord
;;-------------- ---------------- ----------------<!-- Standard PRE tag rules -->
```

C. The results for my groundwater model

```
  Element Count
  *************
  Number of rain gages ...... 6
  Number of subcatchments ... 125
  Number of nodes ........... 126
  Number of links ........... 125
  Number of pollutants ...... 0
  Number of land uses ....... 0


  ****************
```

Raingage Summary
****

Name	Data Source	Data Type	Recording Interval
Chicago_3h	Chicago_3h	INTENSITY	5 min.
DailyRainfall_Canning	DailyRainfall_Canning	VOLUME	1440 min.
Florida_Type_II_1mm	Florida_Type_II_1mm	INTENSITY	30 min.
NOAA_Type_A_1mm	NOAA_Type_A_1mm	INTENSITY	6 min.
Precipitation_Net15012018	Precipitation_Net15012018	INTENSITY	30 min.
RainEvent_19072009	RainEvent_19072009	INTENSITY	30 min.

****
Subcatchment Summary
****

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	0.37	37.17	52.14	0.5000	DailyRainfall_Canning	J80
S10	0.19	47.08	100.00	0.0500	DailyRainfall_Canning	S43_7
S11	0.16	40.77	100.00	0.0500	DailyRainfall_Canning	J80
S12	0.33	68.95	85.66	0.0500	DailyRainfall_Canning	J9
S13	0.06	70.00	48.57	0.5000	DailyRainfall_Canning	S23_4
S14	0.19	167.22	53.82	3.2000	DailyRainfall_Canning	J9
S15_1	0.08	12.25	38.01	3.8280	DailyRainfall_Canning	S15_10
S15_10	0.09	28.82	37.41	3.8280	DailyRainfall_Canning	J24
S15_12	0.14	30.75	64.07	3.8280	DailyRainfall_Canning	J2312
S15_2	0.78	58.65	65.84	3.8280	DailyRainfall_Canning	J20
S15_3	0.19	48.55	100.00	0.0500	DailyRainfall_Canning	J11
S15_4	0.20	27.15	56.80	3.8280	DailyRainfall_Canning	J17
S15_5	0.68	51.72	67.95	3.8280	DailyRainfall_Canning	J18
S15_6	0.14	35.02	100.00	0.0500	DailyRainfall_Canning	S29_1
S15_7	1.51	114.36	66.60	3.8280	DailyRainfall_Canning	J2181
S15_8	0.06	14.73	37.97	3.8280	DailyRainfall_Canning	J26
S15_9	0.39	41.54	26.28	3.8280	DailyRainfall_Canning	J23
S16	0.06	14.10	100.00	0.0500	DailyRainfall_Canning	J13
S17	0.18	45.40	100.00	0.0500	DailyRainfall_Canning	J2918
S18_2	0.67	67.03	98.67	0.0500	DailyRainfall_Canning	J32
S18_3	0.20	20.30	100.00	0.0500	DailyRainfall_Canning	J30
S18_4	0.23	41.84	100.00	0.5000	DailyRainfall_Canning	J30
S19	0.24	60.15	100.00	0.0500	DailyRainfall_Canning	J28
S2	1.17	276.27	98.79	0.0500	DailyRainfall_Canning	J79
S20	0.07	18.20	100.00	0.0500	DailyRainfall_Canning	J3
S21	0.18	45.73	100.00	0.0500	DailyRainfall_Canning	J26
S22	0.08	152.16	100.00	2.2180	DailyRainfall_Canning	J7
S23	0.13	60.00	58.39	0.5000	DailyRainfall_Canning	J25
S23_1	0.95	167.21	65.32	3.2000	DailyRainfall_Canning	J4
S23_3	0.56	54.50	60.55	3.2000	DailyRainfall_Canning	J12
S23_4	1.17	112.72	56.24	3.2000	DailyRainfall_Canning	J6
S24	0.06	14.90	100.00	0.0500	DailyRainfall_Canning	S15_9
S25	0.11	27.42	100.00	0.0500	DailyRainfall_Canning	J57
S26_1	0.14	23.02	56.39	3.2350	DailyRainfall_Canning	J2787
S26_3	0.96	156.38	60.17	3.2350	DailyRainfall_Canning	J2909
S29_1	0.46	200.89	45.59	3.2400	DailyRainfall_Canning	J9
S29_10	1.84	130.72	55.85	2.9450	DailyRainfall_Canning	J2931
S29_11	0.04	2.73	93.74	2.9450	DailyRainfall_Canning	J2931
S29_12	0.63	44.65	55.88	2.9450	DailyRainfall_Canning	J40
S29_13	0.65	46.11	56.91	2.9450	DailyRainfall_Canning	J35
S29_14	0.80	56.95	54.49	2.9450	DailyRainfall_Canning	J48
S29_15	0.43	101.00	60.75	0.0500	DailyRainfall_Canning	J29_14
S29_17	0.10	23.12	0.00	0.0500	DailyRainfall_Canning	S29_14
S29_2	0.31	261.45	98.90	3.2400	DailyRainfall_Canning	J2754
S29_3	0.83	200.89	59.35	3.2400	DailyRainfall_Canning	J11
S29_5	0.22	15.77	57.60	2.9450	DailyRainfall_Canning	J79
S29_7	0.20	14.58	64.04	2.9450	DailyRainfall_Canning	J63
S29_8	0.63	200.89	65.96	3.2400	DailyRainfall_Canning	J13
S29_9	0.18	13.12	47.15	2.9450	DailyRainfall_Canning	J83
S3	0.40	279.67	38.66	3.3800	DailyRainfall_Canning	S46_5
S30	0.13	29.48	93.35	0.0500	DailyRainfall_Canning	J355
S31	0.06	11.13	90.13	0.0500	DailyRainfall_Canning	J2712
S32	0.13	32.75	100.00	0.0500	DailyRainfall_Canning	J2717
S33	0.24	60.58	100.00	0.0500	DailyRainfall_Canning	J2717
S34	0.36	89.63	100.00	0.0500	DailyRainfall_Canning	J2722
S35	0.33	81.85	100.00	0.0500	DailyRainfall_Canning	J2692
S36	0.04	10.10	100.00	0.0500	DailyRainfall_Canning	J46
S37	0.07	40.06	72.13	3.3800	DailyRainfall_Canning	S46_5
S37_1	0.41	50.92	62.15	2.2180	DailyRainfall_Canning	J7

S37_10	0.05	16.55	13.97	2.2180	DailyRainfall_Canning	J22
S37_11	0.20	25.02	45.49	2.2180	DailyRainfall_Canning	J2510
S37_12	0.08	9.47	29.91	2.2180	DailyRainfall_Canning	J2510
S37_2	0.23	94.45	57.23	2.2180	DailyRainfall_Canning	J4
S37_3	0.14	57.71	46.87	2.2180	DailyRainfall_Canning	J4
S37_4	0.36	44.45	76.39	2.2180	DailyRainfall_Canning	J16
S37_8	0.13	16.37	22.60	2.2180	DailyRainfall_Canning	J1
S38	0.19	46.98	100.00	0.0500	DailyRainfall_Canning	S43_7
S39	0.47	74.72	72.47	0.0500	DailyRainfall_Canning	S63_9
S4	0.40	87.38	100.00	0.0640	DailyRainfall_Canning	J2722
S40	0.18	46.08	98.99	0.0500	DailyRainfall_Canning	S63_9
S41	0.27	68.30	100.00	0.0500	DailyRainfall_Canning	J2931
S42	0.41	102.70	100.00	0.0500	DailyRainfall_Canning	J1040
S43	1.67	236.18	22.43	4.3580	DailyRainfall_Canning	J1969
S43_2	0.55	28.64	25.35	5.2200	DailyRainfall_Canning	J56
S43_4	0.32	16.52	18.77	5.2200	DailyRainfall_Canning	J46
S43_5	0.96	49.81	42.96	5.2200	DailyRainfall_Canning	S43_7
S43_6	0.52	27.16	27.26	5.2200	DailyRainfall_Canning	S43
S43_7	0.60	31.07	56.61	5.2200	DailyRainfall_Canning	J46
S43_9	0.90	46.61	46.85	5.2200	DailyRainfall_Canning	S43
S44	0.71	178.32	100.00	0.0500	DailyRainfall_Canning	S43
S45	0.05	12.43	100.00	0.0500	DailyRainfall_Canning	J2510
S46	0.08	19.32	100.00	0.0500	DailyRainfall_Canning	J7
S46_1	0.56	68.57	54.56	3.3800	DailyRainfall_Canning	J2771
S46_10	0.11	35.10	66.12	3.3800	DailyRainfall_Canning	S63_3
S46_2	0.34	41.71	37.98	3.3800	DailyRainfall_Canning	J2594
S46_3	0.33	101.25	70.86	3.3800	DailyRainfall_Canning	S63_14
S46_4	0.53	64.73	61.82	3.3800	DailyRainfall_Canning	J16
S46_5	0.46	35.97	50.36	3.3800	DailyRainfall_Canning	J2722
S46_6	0.30	36.49	52.18	3.3800	DailyRainfall_Canning	J2678
S46_7	0.53	64.61	67.84	3.3800	DailyRainfall_Canning	J2722
S47	0.22	55.70	100.00	0.0500	DailyRainfall_Canning	J2839
S48	0.12	30.23	100.00	0.0500	DailyRainfall_Canning	J2847
S49	0.15	37.48	100.00	0.0500	DailyRainfall_Canning	J5
S5	0.23	56.48	100.00	0.0500	DailyRainfall_Canning	J63
S50	0.20	49.15	100.00	0.0500	DailyRainfall_Canning	J5
S51	0.18	45.77	100.00	0.0500	DailyRainfall_Canning	J3
S52_1	0.92	59.15	31.47	3.2350	DailyRainfall_Canning	S43
S52_2	0.84	304.44	48.21	2.9450	DailyRainfall_Canning	S43
S52_3	0.26	16.79	61.56	3.2350	DailyRainfall_Canning	J2909
S52_4	0.39	304.44	57.11	2.9450	DailyRainfall_Canning	J70
S52_6	0.86	55.37	73.37	3.2350	DailyRainfall_Canning	J2838
S52_7	0.75	48.08	50.07	3.2350	DailyRainfall_Canning	J2860
S53	0.26	65.65	100.00	0.0500	DailyRainfall_Canning	J4
S54	0.10	25.70	100.00	0.0500	DailyRainfall_Canning	S15_7
S55	0.01	3.05	100.00	0.0500	DailyRainfall_Canning	S15_7
S56	0.07	18.05	100.00	0.0500	DailyRainfall_Canning	S15_7
S57	0.06	200.89	100.00	3.2400	DailyRainfall_Canning	J13
S59	0.11	36.33	97.66	0.0500	DailyRainfall_Canning	J13
S63_1	0.61	180.24	38.35	4.5340	DailyRainfall_Canning	J355
S63_11	0.25	35.18	61.02	4.5340	DailyRainfall_Canning	J2728
S63_12	0.13	32.75	56.27	4.5340	DailyRainfall_Canning	J2822
S63_13	0.43	52.99	48.85	4.5340	DailyRainfall_Canning	J2794
S63_14	0.19	46.55	59.93	4.5340	DailyRainfall_Canning	J2757
S63_15	0.28	28.32	50.73	4.5340	DailyRainfall_Canning	J2709
S63_2	1.20	75.70	26.59	4.5340	DailyRainfall_Canning	J2855
S63_3	0.20	30.85	65.39	4.5340	DailyRainfall_Canning	J2719
S63_4	0.11	11.20	89.58	4.5340	DailyRainfall_Canning	S63_9
S63_5	0.00	5.89	90.88	4.5340	DailyRainfall_Canning	S63_1
S63_6	0.28	180.24	52.71	4.5340	DailyRainfall_Canning	J2785
S63_7	0.08	180.25	35.47	4.5340	DailyRainfall_Canning	J1969
S63_8	0.15	49.90	54.89	4.5340	DailyRainfall_Canning	J2730
S63_9	0.28	34.04	36.18	4.5340	DailyRainfall_Canning	J2785
S7	0.12	30.75	100.00	0.0500	DailyRainfall_Canning	J2757
S8	0.15	36.52	100.00	0.0500	DailyRainfall_Canning	J2755
S9	0.16	39.45	100.00	0.0500	DailyRainfall_Canning	S43_7

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LID Control Summary
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Subcatchment	LID Control	No. of Units	Unit Area	Unit Width	% Area Covered	% Imperv Treated	% Perv Treated
S43	BioSwale	1	16677.00	0.00	100.00	0.00	0.00

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Node Summary
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Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
J1	JUNCTION	13.40	1.00	0.0	
J10	JUNCTION	13.31	1.00	0.0	
J1040	JUNCTION	9.07	2.21	0.0	
J11	JUNCTION	13.02	1.00	0.0	
J12	JUNCTION	17.49	1.00	0.0	
J13	JUNCTION	14.72	1.00	0.0	
J14	JUNCTION	13.16	1.00	0.0	
J1415	JUNCTION	9.71	2.03	0.0	
J15	JUNCTION	13.77	1.00	0.0	
J16	JUNCTION	12.31	1.00	0.0	
J17	JUNCTION	13.64	1.00	0.0	
J1701	JUNCTION	14.30	1.00	0.0	
J1788	JUNCTION	9.08	1.72	0.0	
J18	JUNCTION	13.81	1.00	0.0	
J19	JUNCTION	12.48	1.00	0.0	
J1969	JUNCTION	9.10	1.11	0.0	
J2	JUNCTION	13.18	1.00	0.0	
J20	JUNCTION	13.78	1.00	0.0	
J21	JUNCTION	11.00	2.35	0.0	
J2181	JUNCTION	11.91	1.35	0.0	
J22	JUNCTION	11.50	3.50	0.0	
J2293	JUNCTION	11.60	1.40	0.0	
J23	JUNCTION	11.50	1.50	0.0	
J2312	JUNCTION	11.58	1.42	0.0	
J24	JUNCTION	11.55	1.44	0.0	
J25	JUNCTION	12.36	2.64	0.0	
J2510	JUNCTION	11.21	1.59	0.0	
J2594	JUNCTION	11.02	1.80	0.0	
J26	JUNCTION	13.36	1.00	0.0	
J2678	JUNCTION	10.50	2.15	0.0	
J2692	JUNCTION	10.61	1.87	0.0	
J27	JUNCTION	12.48	1.00	0.0	
J2709	JUNCTION	15.50	0.45	0.0	
J2712	JUNCTION	15.40	0.72	0.0	
J2717	JUNCTION	15.97	0.45	0.0	
J2719	JUNCTION	15.88	0.45	0.0	
J2722	JUNCTION	14.54	0.45	0.0	
J2728	JUNCTION	15.28	0.45	0.0	
J2730	JUNCTION	15.25	0.45	0.0	
J2749	JUNCTION	15.16	0.45	0.0	
J2754	JUNCTION	14.56	1.00	0.0	
J2755	JUNCTION	14.08	1.00	0.0	
J2757	JUNCTION	15.32	0.45	0.0	
J2764	JUNCTION	14.47	1.00	0.0	
J2771	JUNCTION	9.90	1.84	0.0	
J2779	JUNCTION	14.32	1.00	0.0	
J2785	JUNCTION	14.13	0.45	0.0	
J2786	JUNCTION	15.06	0.45	0.0	
J2787	JUNCTION	14.94	1.00	0.0	
J2794	JUNCTION	14.00	1.12	0.0	
J2797	JUNCTION	13.27	0.75	0.0	
J28	JUNCTION	13.29	1.00	0.0	
J2813	JUNCTION	12.42	1.00	0.0	
J2816	JUNCTION	12.29	1.00	0.0	
J2822	JUNCTION	12.93	0.75	0.0	
J2831	JUNCTION	12.64	0.75	0.0	
J2838	JUNCTION	12.29	0.75	0.0	
J2839	JUNCTION	14.09	1.00	0.0	
J2845	JUNCTION	12.62	0.75	0.0	
J2847	JUNCTION	13.58	1.00	0.0	
J2855	JUNCTION	9.01	2.29	0.0	
J2857	JUNCTION	9.64	2.06	0.0	
J2860	JUNCTION	12.49	1.00	0.0	
J2868	JUNCTION	12.78	1.00	0.0	
J2870	JUNCTION	12.80	1.00	0.0	
J2887	JUNCTION	9.57	2.05	0.0	Yes
J2890	JUNCTION	12.90	1.00	0.0	
J2891	JUNCTION	10.00	1.00	0.0	
J29	JUNCTION	12.67	1.00	0.0	
J29_14	JUNCTION	12.00	1.00	0.0	
J2909	JUNCTION	13.48	1.00	0.0	
J2915	JUNCTION	9.20	2.40	0.0	
J2918	JUNCTION	13.56	0.90	0.0	

J2921	JUNCTION	11.28	1.00	0.0	
J2931	JUNCTION	11.87	1.00	0.0	
J2938	JUNCTION	14.36	0.79	0.0	
J3	JUNCTION	13.59	1.00	0.0	
J30	JUNCTION	12.34	1.00	0.0	
J31	JUNCTION	12.66	1.00	0.0	
J32	JUNCTION	12.59	1.00	0.0	
J33	JUNCTION	12.31	1.00	0.0	
J34	JUNCTION	12.13	1.00	0.0	
J35	JUNCTION	11.50	1.00	0.0	
J36	JUNCTION	11.73	1.00	0.0	
J37	JUNCTION	12.21	1.00	0.0	
J38	JUNCTION	12.30	1.00	0.0	
J39	JUNCTION	12.12	1.00	0.0	
J4	JUNCTION	13.79	1.00	0.0	
J40	JUNCTION	11.99	1.00	0.0	
J41	JUNCTION	12.00	1.00	0.0	
J42	JUNCTION	12.24	1.00	0.0	
J43	JUNCTION	12.87	1.00	0.0	
J44	JUNCTION	12.87	1.00	0.0	
J45	JUNCTION	9.30	1.53	0.0	
J46	JUNCTION	9.70	1.40	0.0	Yes
J47	JUNCTION	11.65	1.00	0.0	
J48	JUNCTION	11.51	1.00	0.0	
J49	JUNCTION	9.09	1.83	0.0	
J5	JUNCTION	13.99	1.00	0.0	
J50	JUNCTION	12.20	1.00	0.0	
J52	JUNCTION	11.51	1.00	0.0	
J53	JUNCTION	11.51	1.00	0.0	
J55	JUNCTION	9.69	1.32	0.0	
J56	JUNCTION	13.19	1.00	0.0	
J57	JUNCTION	13.20	1.00	0.0	
J59	JUNCTION	12.50	1.00	0.0	
J6	JUNCTION	13.31	1.00	0.0	
J63	JUNCTION	12.24	1.00	0.0	
J64	JUNCTION	12.80	1.00	0.0	
J65	JUNCTION	11.79	1.00	0.0	
J66	JUNCTION	11.58	1.00	0.0	
J67	JUNCTION	11.92	1.00	0.0	
J68	JUNCTION	12.00	1.00	0.0	
J69	JUNCTION	11.76	1.00	0.0	
J7	JUNCTION	13.34	1.00	0.0	
J70	JUNCTION	12.67	1.00	0.0	
J72	JUNCTION	11.60	1.00	0.0	
J73	JUNCTION	12.86	1.00	0.0	
J78	JUNCTION	12.40	1.00	0.0	
J79	JUNCTION	12.19	1.00	0.0	
J8	JUNCTION	11.34	1.65	0.0	
J80	JUNCTION	11.83	1.00	0.0	
J83	JUNCTION	11.70	1.20	0.0	
J9	JUNCTION	16.37	1.00	0.0	
J355	OUTFALL	8.33	1.30	0.0	Yes
J54	STORAGE	8.80	2.17	0.0	

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Link Summary
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Name	From Node	To Node	Type	Length	%Slope	Roughness
206110366	J2510	J2594	CONDUIT	68.1	0.2791	0.0120
206110379_1	J2312	J24	CONDUIT	23.9	0.1340	0.0120
206110379_2	J8	J2510	CONDUIT	51.4	0.2529	0.0120
206110379_4	J23	J8	CONDUIT	67.9	0.2299	0.0120
206110379_5	J24	J23	CONDUIT	39.6	0.1312	0.0120
22803188_2	J45	J2915	CONDUIT	159.4	0.0627	0.0100
22803188_3	J54	J45	CONDUIT	89.8	0.1670	0.0100
22803188_4	J46	J55	CONDUIT	61.4	0.0163	0.0100
22803188_5	J55	J54	CONDUIT	24.5	3.6397	0.0100
22926618_1	J2915	J1969	CONDUIT	23.8	0.4207	0.0100
22926618_2	J1969	J49	CONDUIT	64.7	0.0155	0.0100
22926618_3	J1040	J2855	CONDUIT	33.6	0.1787	0.0140
22926618_4	J1788	J1040	CONDUIT	50.5	0.0198	0.0140
22926629	J2887	J2915	CONDUIT	19.7	1.8770	0.0270
23116769	J2594	J2678	CONDUIT	67.8	0.2627	0.0120
23116814	J1415	J2857	CONDUIT	21.5	0.3341	0.0120
23116826	J2857	J2887	CONDUIT	27.2	0.2577	0.0120
23405543	J2293	J2312	CONDUIT	8.1	0.2460	0.0120

23405563	J2181	J2293	CONDUIT	111.4	0.2782	0.0120
57466689_1	J2771	J1415	CONDUIT	34.8	0.5399	0.0120
57466741	J2692	J2771	CONDUIT	111.3	0.6378	0.0120
57466813	J2678	J2692	CONDUIT	18.8	1.0237	0.0120
C1	J10	J2	CONDUIT	4.6	2.8478	0.0120
C1_1	J2	J14	CONDUIT	9.0	0.1106	0.0120
C1_2	J14	J1	CONDUIT	58.5	-0.3965	0.0120
C10	J9	J5	CONDUIT	67.9	3.5079	0.0120
C108	J2921	J1969	CONDUIT	21.3	10.3196	0.0120
C109	J2831	J2845	CONDUIT	40.4	0.0421	0.0120
C11	J11	J14	CONDUIT	10.3	-1.3870	0.0120
C110	J2794	J1040	CONDUIT	48.7	9.2155	0.0120
C111	J2785	J2794	CONDUIT	97.3	-0.2466	0.0120
C112	J2717	J2719	CONDUIT	2.5	4.0096	0.0120
C113	J2918	J2909	CONDUIT	49.6	0.2096	0.0120
C12	J1	J7	CONDUIT	51.5	0.1107	0.0120
C126	J2890	J2870	CONDUIT	8.5	1.1745	0.0120
C127	J2816	J2813	CONDUIT	8.6	-1.5125	0.0120
C128	J2722	J2797	CONDUIT	104.3	1.2172	0.0120
C129_1	J2764	J1701	CONDUIT	7.0	2.4213	0.0120
C129_2	J1701	J2847	CONDUIT	42.9	1.6817	0.0120
C13	J12	J9	CONDUIT	67.5	1.6676	0.0120
C130	J2787	J2764	CONDUIT	47.7	0.9808	0.0120
C131	J2870	J2868	CONDUIT	1.7	1.1849	0.0120
C141	J2931	J2921	CONDUIT	13.0	4.5207	0.0120
C142	J2822	J2831	CONDUIT	53.4	0.5560	0.0120
C143	J2712	J2785	CONDUIT	77.2	1.9974	0.0120
C144	J2786	J2794	CONDUIT	10.8	9.9203	0.0120
C145	J2839	J2847	CONDUIT	7.5	6.8596	0.0120
C146	J2779	J1701	CONDUIT	4.4	0.5498	0.0120
C147	J2730	J2749	CONDUIT	16.8	0.5770	0.0120
C148	J2719	J2730	CONDUIT	33.0	1.8783	0.0120
C158	J2860	J2838	CONDUIT	85.2	0.2335	0.0120
C159	J2797	J2822	CONDUIT	5.7	5.9471	0.0120
C16	J13	J2	CONDUIT	107.9	1.4317	0.0120
C160	J2845	J2857	CONDUIT	10.3	30.0988	0.0120
C161	J2728	J2730	CONDUIT	5.6	0.4989	0.0120
C167_2	J47	J2931	CONDUIT	62.2	-0.3604	0.0120
C169	J2838	J1415	CONDUIT	29.5	8.7841	0.0120
C17	J17	J15	CONDUIT	17.3	-0.7497	0.0120
C170	J2813	J1415	CONDUIT	17.5	15.6546	0.0120
C176	J2855	J355	CONDUIT	190.0	0.3579	0.0140
C18	J18	J2293	CONDUIT	9.4	24.2248	0.0120
C182	J2757	J2786	CONDUIT	23.1	1.1206	0.0120
C185	J2868	J2860	CONDUIT	37.4	0.7763	0.0120
C186	J2909	J2868	CONDUIT	76.3	0.9153	0.0120
C19	J20	J17	CONDUIT	8.5	1.6156	0.0120
C193	J2709	J2712	CONDUIT	5.0	1.9932	0.0120
C194	J2749	J2786	CONDUIT	40.7	0.2335	0.0120
C195	J2754	J2764	CONDUIT	7.4	1.2425	0.0120
C196	J2891	J1788	CONDUIT	3.8	5.2209	0.0120
C20	J22	J8	CONDUIT	29.3	0.5459	0.0120
C21	J25	J8	CONDUIT	3.5	32.4388	0.0120
C22	J26	J23	CONDUIT	3.5	63.0111	0.0120
C23	J28	J24	CONDUIT	5.3	34.7854	0.0120
C24	J16	J21	CONDUIT	12.7	10.3694	0.0120
C25	J21	J2678	CONDUIT	29.9	1.6742	0.0120
C26	J27	J19	CONDUIT	1.4	0.0224	0.0120
C27	J30	J29	CONDUIT	9.3	-3.5776	0.0120
C28	J32	J31	CONDUIT	4.0	-1.8226	0.0120
C29	J34	J33	CONDUIT	1.8	-9.5778	0.0120
C3	J4	J3	CONDUIT	40.8	0.4975	0.0120
C30	J36	J35	CONDUIT	38.3	0.6030	0.0120
C31	J38	J37	CONDUIT	32.4	0.2839	0.0120
C32	J40	J39	CONDUIT	20.5	-0.6620	0.0120
C33	J41	J40	CONDUIT	2.0	0.6410	0.0120
C34	J42	J33	CONDUIT	24.6	-0.2842	0.0120
C35	J44	J43	CONDUIT	2.9	0.0103	0.0120
C37	J35	J47	CONDUIT	13.2	-1.1419	0.0120
C38	J52	J48	CONDUIT	3.3	0.0092	0.0120
C39	J37	J50	CONDUIT	31.4	0.0159	0.0120
C4	J5	J6	CONDUIT	79.2	0.8534	0.0120
C40	J39	J38	CONDUIT	19.1	-0.9215	0.0120
C41	J29_14	J40	CONDUIT	5.1	0.2542	0.0120
C42	J53	J52	CONDUIT	1.2	0.0827	0.0120
C44	J57	J56	CONDUIT	17.7	0.0338	0.0120
C45	J59	J19	CONDUIT	11.1	0.1527	0.0120
C46	J33	J47	CONDUIT	69.9	0.9454	0.0120

C47	J63	J42	CONDUIT	4.4	0.0069	0.0120
C49	J19	J33	CONDUIT	65.3	0.2666	0.0120
C5	J7	J2510	CONDUIT	44.9	3.4200	0.0120
C50	J56	J19	CONDUIT	66.2	1.0757	0.0120
C51	J64	J63	CONDUIT	9.0	6.2803	0.0120
C52	J65	J52	CONDUIT	9.7	2.9349	0.0120
C53	J66	J48	CONDUIT	18.5	0.4005	0.0120
C54	J67	J66	CONDUIT	36.2	0.9225	0.0120
C55	J68	J40	CONDUIT	16.7	0.0780	0.0120
C56	J69	J65	CONDUIT	1.9	-1.7813	0.0120
C57	J78	J70	CONDUIT	2.6	-10.5183	0.0120
C58	J72	J35	CONDUIT	1.3	7.6208	0.0120
C59	J50	J67	CONDUIT	19.4	1.4742	0.0120
C6	J15	J2312	CONDUIT	20.2	10.8994	0.0120
C60	J43	J70	CONDUIT	73.6	0.2771	0.0120
C61	J31	J43	CONDUIT	47.8	-0.4329	0.0120
C62	J73	J44	CONDUIT	2.9	-0.4154	0.0120
C63	J48	J36	CONDUIT	58.4	-0.3751	0.0120
C65	J70	J42	CONDUIT	64.4	0.6672	0.0120
C66	J29	J31	CONDUIT	3.7	0.2462	0.0120
C67	J79	J78	CONDUIT	9.1	-2.3432	0.0120
C68	J80	J67	CONDUIT	12.6	-0.7123	0.0120
C7	J6	J1	CONDUIT	17.5	-0.4911	0.0120
C70	J83	J72	CONDUIT	2.5	4.0667	0.0120
C8	J3	J6	CONDUIT	59.9	0.4671	0.0120
C95	J2755	J2860	CONDUIT	73.2	2.1774	0.0120
C96	J2847	J2909	CONDUIT	51.0	0.1960	0.0120
C97	J2938	J2918	CONDUIT	68.4	1.1342	0.0120
22926618_6	J49	J1788	WEIR			

****
Cross Section Summary
****

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
206110366	CIRCULAR	1.35	1.43	0.34	1.35	1	3.06
206110379_1	CIRCULAR	1.35	1.43	0.34	1.35	1	2.12
206110379_2	CIRCULAR	1.35	1.43	0.34	1.35	1	2.91
206110379_4	CIRCULAR	1.35	1.43	0.34	1.35	1	2.77
206110379_5	CIRCULAR	1.35	1.43	0.34	1.35	1	2.10
22803188_2	AnvilTransect	0.65	5.53	0.47	11.50	1	8.40
22803188_3	AnvilTransect	0.65	5.53	0.47	11.50	1	13.70
22803188_4	AnvilTransect	0.65	5.53	0.47	11.50	1	4.28
22803188_5	AnvilTransect	0.65	5.53	0.47	11.50	1	63.98
22926618_1	AnvilTransect	0.65	5.53	0.47	11.50	1	21.75
22926618_2	AnvilTransect	0.65	5.53	0.47	11.50	1	4.17
22926618_3	Anvil_Transect2	1.30	7.80	0.48	9.00	1	14.38
22926618_4	Anvil_Transect2	1.30	7.80	0.48	9.00	1	4.79
22926629	PARABOLIC	1.35	1.80	0.51	2.00	1	5.85
23116769	CIRCULAR	1.35	1.43	0.34	1.35	1	2.96
23116814	CIRCULAR	1.35	1.43	0.34	1.35	1	3.34
23116826	CIRCULAR	1.35	1.43	0.34	1.35	1	2.94
23405543	CIRCULAR	1.35	1.43	0.34	1.35	1	2.87
23405563	CIRCULAR	1.35	1.43	0.34	1.35	1	3.05
57466689_1	CIRCULAR	1.35	1.43	0.34	1.35	1	4.25
57466741	CIRCULAR	1.35	1.43	0.34	1.35	1	4.62
57466813	CIRCULAR	1.35	1.43	0.34	1.35	1	5.85
C1	CIRCULAR	1.00	0.79	0.25	1.00	1	4.38
C1_1	CIRCULAR	1.00	0.79	0.25	1.00	1	0.86
C1_2	CIRCULAR	1.00	0.79	0.25	1.00	1	1.64
C10	CIRCULAR	1.00	0.79	0.25	1.00	1	4.87
C108	CIRCULAR	1.00	0.79	0.25	1.00	1	8.35
C109	CIRCULAR	0.75	0.44	0.19	0.75	1	0.25
C11	CIRCULAR	1.00	0.79	0.25	1.00	1	3.06
C110	CIRCULAR	0.75	0.44	0.19	0.75	1	3.66
C111	CIRCULAR	0.45	0.16	0.11	0.45	1	0.15
C112	CIRCULAR	0.45	0.16	0.11	0.45	1	0.62
C113	CIRCULAR	0.75	0.44	0.19	0.75	1	0.55
C12	CIRCULAR	1.00	0.79	0.25	1.00	1	0.86
C126	CIRCULAR	1.00	0.79	0.25	1.00	1	2.82
C127	CIRCULAR	1.00	0.79	0.25	1.00	1	3.19
C128	CIRCULAR	0.45	0.16	0.11	0.45	1	0.34
C129_1	CIRCULAR	1.00	0.79	0.25	1.00	1	4.04
C129_2	CIRCULAR	1.00	0.79	0.25	1.00	1	3.37
C13	CIRCULAR	1.00	0.79	0.25	1.00	1	3.35
C130	CIRCULAR	1.00	0.79	0.25	1.00	1	2.57

C131	CIRCULAR	1.00	0.79	0.25	1.00	1	2.83
C141	CIRCULAR	1.00	0.79	0.25	1.00	1	5.52
C142	CIRCULAR	0.75	0.44	0.19	0.75	1	0.90
C143	CIRCULAR	0.45	0.16	0.11	0.45	1	0.44
C144	CIRCULAR	0.45	0.16	0.11	0.45	1	0.97
C145	CIRCULAR	1.00	0.79	0.25	1.00	1	6.80
C146	CIRCULAR	1.00	0.79	0.25	1.00	1	1.93
C147	CIRCULAR	0.45	0.16	0.11	0.45	1	0.23
C148	CIRCULAR	0.45	0.16	0.11	0.45	1	0.42
C158	CIRCULAR	0.75	0.44	0.19	0.75	1	0.58
C159	CIRCULAR	0.75	0.44	0.19	0.75	1	2.94
C16	CIRCULAR	1.00	0.79	0.25	1.00	1	3.11
C160	CIRCULAR	0.75	0.44	0.19	0.75	1	6.62
C161	CIRCULAR	0.45	0.16	0.11	0.45	1	0.22
C167_2	CIRCULAR	1.00	0.79	0.25	1.00	1	1.56
C169	CIRCULAR	0.75	0.44	0.19	0.75	1	3.58
C17	CIRCULAR	1.00	0.79	0.25	1.00	1	2.25
C170	CIRCULAR	1.00	0.79	0.25	1.00	1	10.28
C176	Anvil_Transect2	1.30	7.80	0.48	9.00	1	20.35
C18	CIRCULAR	1.00	0.79	0.25	1.00	1	12.79
C182	CIRCULAR	0.45	0.16	0.11	0.45	1	0.33
C185	CIRCULAR	1.00	0.79	0.25	1.00	1	2.29
C186	CIRCULAR	1.00	0.79	0.25	1.00	1	2.49
C19	CIRCULAR	1.00	0.79	0.25	1.00	1	3.30
C193	CIRCULAR	0.45	0.16	0.11	0.45	1	0.44
C194	CIRCULAR	0.45	0.16	0.11	0.45	1	0.15
C195	CIRCULAR	1.00	0.79	0.25	1.00	1	2.90
C196	CIRCULAR	1.00	0.79	0.25	1.00	1	5.94
C20	CIRCULAR	1.65	2.14	0.41	1.65	1	7.30
C21	CIRCULAR	1.00	0.79	0.25	1.00	1	14.80
C22	CIRCULAR	1.00	0.79	0.25	1.00	1	20.62
C23	CIRCULAR	1.00	0.79	0.25	1.00	1	15.32
C24	CIRCULAR	1.00	0.79	0.25	1.00	1	8.37
C25	CIRCULAR	1.00	0.79	0.25	1.00	1	3.36
C26	CIRCULAR	1.00	0.79	0.25	1.00	1	0.39
C27	CIRCULAR	1.00	0.79	0.25	1.00	1	4.91
C28	CIRCULAR	1.00	0.79	0.25	1.00	1	3.51
C29	CIRCULAR	1.00	0.79	0.25	1.00	1	8.04
C3	CIRCULAR	1.00	0.79	0.25	1.00	1	1.83
C30	CIRCULAR	1.00	0.79	0.25	1.00	1	2.02
C31	CIRCULAR	1.00	0.79	0.25	1.00	1	1.38
C32	CIRCULAR	1.00	0.79	0.25	1.00	1	2.11
C33	CIRCULAR	1.00	0.79	0.25	1.00	1	2.08
C34	CIRCULAR	1.00	0.79	0.25	1.00	1	1.38
C35	CIRCULAR	1.00	0.79	0.25	1.00	1	0.26
C37	CIRCULAR	1.00	0.79	0.25	1.00	1	2.78
C38	CIRCULAR	1.00	0.79	0.25	1.00	1	0.25
C39	CIRCULAR	1.00	0.79	0.25	1.00	1	0.33
C4	CIRCULAR	1.00	0.79	0.25	1.00	1	2.40
C40	CIRCULAR	1.00	0.79	0.25	1.00	1	2.49
C41	CIRCULAR	1.00	0.79	0.25	1.00	1	1.31
C42	CIRCULAR	1.00	0.79	0.25	1.00	1	0.75
C44	CIRCULAR	1.00	0.79	0.25	1.00	1	0.48
C45	CIRCULAR	1.00	0.79	0.25	1.00	1	1.02
C46	CIRCULAR	1.00	0.79	0.25	1.00	1	2.53
C47	CIRCULAR	1.00	0.79	0.25	1.00	1	0.22
C49	CIRCULAR	1.00	0.79	0.25	1.00	1	1.34
C5	CIRCULAR	1.00	0.79	0.25	1.00	1	4.80
C50	CIRCULAR	1.00	0.79	0.25	1.00	1	2.69
C51	CIRCULAR	1.00	0.79	0.25	1.00	1	6.51
C52	CIRCULAR	1.00	0.79	0.25	1.00	1	4.45
C53	CIRCULAR	1.00	0.79	0.25	1.00	1	1.64
C54	CIRCULAR	1.00	0.79	0.25	1.00	1	2.50
C55	CIRCULAR	1.00	0.79	0.25	1.00	1	0.73
C56	CIRCULAR	1.00	0.79	0.25	1.00	1	3.47
C57	CIRCULAR	1.00	0.79	0.25	1.00	1	8.43
C58	CIRCULAR	1.00	0.79	0.25	1.00	1	7.17
C59	CIRCULAR	1.00	0.79	0.25	1.00	1	3.15
C6	CIRCULAR	1.00	0.79	0.25	1.00	1	8.58
C60	CIRCULAR	1.00	0.79	0.25	1.00	1	1.37
C61	CIRCULAR	1.00	0.79	0.25	1.00	1	1.71
C62	CIRCULAR	1.00	0.79	0.25	1.00	1	1.67
C63	CIRCULAR	1.00	0.79	0.25	1.00	1	1.59
C65	CIRCULAR	1.00	0.79	0.25	1.00	1	2.12
C66	CIRCULAR	1.00	0.79	0.25	1.00	1	1.29
C67	CIRCULAR	1.00	0.79	0.25	1.00	1	3.98
C68	CIRCULAR	1.00	0.79	0.25	1.00	1	2.19
C7	CIRCULAR	1.00	0.79	0.25	1.00	1	1.82

C70	CIRCULAR	1.00	0.79	0.25	1.00	1	5.24
C8	CIRCULAR	1.00	0.79	0.25	1.00	1	1.78
C95	CIRCULAR	1.00	0.79	0.25	1.00	1	3.83
C96	CIRCULAR	1.00	0.79	0.25	1.00	1	1.15
C97	CIRCULAR	0.75	0.44	0.19	0.75	1	1.28

****
Transect Summary
****

Transect Anvil_Transect2
Area:

0.0102	0.0208	0.0318	0.0432	0.0550
0.0672	0.0798	0.0928	0.1062	0.1200
0.1342	0.1488	0.1638	0.1792	0.1950
0.2112	0.2278	0.2448	0.2622	0.2800
0.2982	0.3168	0.3358	0.3552	0.3750
0.3952	0.4158	0.4368	0.4582	0.4800
0.5022	0.5248	0.5478	0.5712	0.5950
0.6192	0.6438	0.6688	0.6942	0.7200
0.7462	0.7728	0.7998	0.8272	0.8550
0.8832	0.9118	0.9408	0.9702	1.0000

Hrad:

0.0311	0.0608	0.0894	0.1170	0.1436
0.1694	0.1944	0.2188	0.2425	0.2657
0.2884	0.3106	0.3324	0.3538	0.3749
0.3956	0.4160	0.4361	0.4560	0.4756
0.4950	0.5142	0.5332	0.5519	0.5706
0.5890	0.6073	0.6254	0.6435	0.6613
0.6791	0.6967	0.7143	0.7317	0.7490
0.7663	0.7834	0.8005	0.8175	0.8344
0.8512	0.8680	0.8847	0.9013	0.9179
0.9344	0.9509	0.9673	0.9837	1.0000

Width:

0.3467	0.3600	0.3733	0.3867	0.4000
0.4133	0.4267	0.4400	0.4533	0.4667
0.4800	0.4933	0.5067	0.5200	0.5333
0.5467	0.5600	0.5733	0.5867	0.6000
0.6133	0.6267	0.6400	0.6533	0.6667
0.6800	0.6933	0.7067	0.7200	0.7333
0.7467	0.7600	0.7733	0.7867	0.8000
0.8133	0.8267	0.8400	0.8533	0.8667
0.8800	0.8933	0.9067	0.9200	0.9333
0.9467	0.9600	0.9733	0.9867	1.0000

Transect AnvilTransect
Area:

0.0131	0.0264	0.0401	0.0540	0.0682
0.0827	0.0975	0.1126	0.1279	0.1435
0.1594	0.1756	0.1921	0.2088	0.2259
0.2432	0.2608	0.2787	0.2968	0.3153
0.3340	0.3530	0.3723	0.3919	0.4118
0.4319	0.4523	0.4730	0.4940	0.5153
0.5368	0.5587	0.5808	0.6032	0.6259
0.6488	0.6721	0.6956	0.7194	0.7435
0.7679	0.7926	0.8175	0.8427	0.8682
0.8940	0.9201	0.9464	0.9731	1.0000

Hrad:

0.0271	0.0536	0.0795	0.1050	0.1299
0.1544	0.1785	0.2021	0.2254	0.2483
0.2709	0.2931	0.3151	0.3367	0.3581
0.3792	0.4001	0.4207	0.4411	0.4613
0.4813	0.5010	0.5206	0.5400	0.5593
0.5783	0.5972	0.6160	0.6346	0.6531
0.6714	0.6896	0.7077	0.7257	0.7435
0.7613	0.7789	0.7964	0.8139	0.8312
0.8485	0.8656	0.8827	0.8997	0.9166
0.9334	0.9502	0.9668	0.9835	1.0000

Width:

0.4887	0.4991	0.5096	0.5200	0.5304
0.5409	0.5513	0.5617	0.5722	0.5826
0.5930	0.6035	0.6139	0.6243	0.6348
0.6452	0.6557	0.6661	0.6765	0.6870
0.6974	0.7078	0.7183	0.7287	0.7391
0.7496	0.7600	0.7704	0.7809	0.7913
0.8017	0.8122	0.8226	0.8330	0.8435

```
            0.8539     0.8643     0.8748     0.8852     0.8957
            0.9061     0.9165     0.9270     0.9374     0.9478
            0.9583     0.9687     0.9791     0.9896     1.0000

*********************************************************
NOTE: The summary statistics displayed in this report are
based on results found at every computational time step,
not just on results from each reporting time step.
*********************************************************

****************
Analysis Options
****************
Flow Units ............... CMS
Process Models:
  Rainfall/Runoff ........ YES
  RDII ................... NO
  Snowmelt ............... NO
  Groundwater ............ YES
  Flow Routing ........... YES
  Ponding Allowed ........ NO
  Water Quality .......... NO
Infiltration Method ...... MODIFIED_HORTON
Flow Routing Method ...... DYNWAVE
Surcharge Method ......... EXTRAN
Starting Date ............ 01/01/2014 00:00:00
Ending Date .............. 12/31/2014 00:00:00
Antecedent Dry Days ...... 0.0
Report Time Step ......... 00:01:00
Wet Time Step ............ 00:05:00
Dry Time Step ............ 00:05:00
Routing Time Step ........ 5.00 sec
Variable Time Step ....... YES
Maximum Trials ........... 8
Number of Threads ........ 4
Head Tolerance ........... 0.001500 m

**************************        Volume         Depth
Runoff Quantity Continuity     hectare-m            mm
**************************     ---------       -------
Initial LID Storage ......         0.142         3.136
Total Precipitation ......        30.207       668.200
Evaporation Loss .........         3.483        77.054
Infiltration Loss ........         2.712        60.000
Surface Runoff ...........        24.013       531.196
Final Storage ............         0.142         3.136
Continuity Error (%) .....        -0.008

**************************        Volume         Depth
Groundwater Continuity         hectare-m            mm
**************************     ---------       -------
Initial Storage ..........       219.516      5949.824
Infiltration .............         2.712        73.511
Upper Zone ET ............         8.162       221.221
Lower Zone ET ............         0.004         0.115
Deep Percolation .........         0.538        14.582
Groundwater Flow .........         3.733       101.179
Final Storage ............       209.775      5685.815
Continuity Error (%) .....         0.007

**************************        Volume        Volume
Flow Routing Continuity        hectare-m      10^6 ltr
**************************     ---------     ---------
Dry Weather Inflow .......         0.000         0.000
Wet Weather Inflow .......        24.013       240.137
Groundwater Inflow .......         3.733        37.327
RDII Inflow ..............         0.000         0.000
External Inflow ..........       263.125      2631.275
External Outflow .........       308.064      3080.675
Flooding Loss ............        17.360       173.601
Evaporation Loss .........         0.673         6.727
Exfiltration Loss ........         0.000         0.000
Initial Stored Volume ....         0.000         0.000
Final Stored Volume ......         0.068         0.678
```

Continuity Error (%) ..... -12.134

****
Highest Continuity Errors
****
Node J72 (-11.86%)
Node J35 (-8.74%)
Node J48 (1.15%)

****
Time-Step Critical Elements
****
Link C58 (51.58%)
Link C42 (26.95%)
Link C38 (6.66%)
Link C57 (4.69%)
Link C56 (3.10%)

****
Highest Flow Instability Indexes
****
Link C42 (35)
Link C58 (25)
Link C70 (24)
Link C56 (16)
Link C38 (16)

****
Routing Time Step Summary
****

Minimum Time Step	:	0.50 sec
Average Time Step	:	1.02 sec
Maximum Time Step	:	5.00 sec
Percent in Steady State	:	-0.00
Average Iterations per Step	:	2.52
Percent Not Converging	:	1.40

****
Subcatchment Runoff Summary
****

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10^6 ltr	Peak Runoff CMS	Runoff Coeff
S1	668.20	0.00	76.14	0.38	333.25	258.44	591.69	2.20	0.00	0.886
S10	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.18	0.00	0.934
S11	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.02	0.00	0.934
S12	668.20	0.00	39.50	0.12	538.88	89.78	628.65	2.06	0.00	0.941
S13	668.20	0.00	53.24	0.44	313.21	301.42	614.63	0.38	0.00	0.920
S14	668.20	0.00	57.78	0.39	350.37	259.97	610.34	1.18	0.00	0.913
S15_1	668.20	0.00	86.28	0.49	248.39	333.12	581.51	0.45	0.00	0.870
S15_10	668.20	482.72	91.00	0.49	425.99	633.88	1059.88	0.99	0.00	0.921
S15_12	668.20	0.00	66.47	0.29	406.67	194.83	601.50	0.81	0.00	0.900
S15_2	668.20	0.00	68.87	0.27	413.76	185.33	599.09	4.65	0.01	0.897
S15_3	668.20	0.00	43.91	0.00	624.31	0.00	624.31	1.18	0.00	0.934

S15_4	668.20	0.00	72.00	0.34	359.56	236.33	595.90	1.16	0.00	0.892
S15_5	668.20	0.00	66.47	0.26	427.57	173.95	601.51	4.11	0.00	0.900
S15_6	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.87	0.00	0.934
S15_7	668.20	77.26	65.46	0.27	474.07	205.70	679.77	10.28	0.01	0.912
S15_8	668.20	0.00	85.99	0.49	249.05	333.01	582.06	0.35	0.00	0.871
S15_9	668.20	95.28	113.17	0.56	198.08	451.77	649.85	2.54	0.00	0.851
S16	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.35	0.00	0.934
S17	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.13	0.00	0.934
S18_2	668.20	0.00	45.51	0.01	614.07	8.62	622.69	4.17	0.00	0.932
S18_3	668.20	0.00	45.54	0.00	622.67	0.00	622.67	1.26	0.00	0.932
S18_4	668.20	0.00	27.59	0.00	640.63	0.00	640.63	1.50	0.00	0.959
S19	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.50	0.00	0.934
S2	668.20	0.00	43.21	0.01	617.00	8.00	625.00	7.31	0.01	0.935
S20	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.45	0.00	0.934
S21	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.14	0.00	0.934
S22	668.20	0.00	31.05	0.00	637.33	0.00	637.33	0.49	0.00	0.954
S23	668.20	0.00	53.41	0.35	375.97	238.53	614.50	0.83	0.00	0.920
S23_1	668.20	0.00	61.93	0.28	416.06	189.98	606.04	5.74	0.01	0.907
S23_3	668.20	0.00	54.48	0.33	390.15	223.27	613.42	3.46	0.00	0.918
S23_4	668.20	32.78	70.46	0.35	377.10	253.10	630.20	7.36	0.01	0.899
S24	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.37	0.00	0.934
S25	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.68	0.00	0.934
S26_1	668.20	0.00	66.21	0.37	356.93	244.73	601.66	0.85	0.00	0.900
S26_3	668.20	0.00	61.08	0.34	385.95	220.87	606.82	5.81	0.01	0.908
S29_1	668.20	190.83	76.17	0.46	381.56	400.93	782.48	3.59	0.00	0.911
S29_10	668.20	0.00	65.44	0.37	358.59	243.82	602.41	11.06	0.01	0.902
S29_11	668.20	0.00	30.38	0.06	597.29	40.53	637.82	0.24	0.00	0.955
S29_12	668.20	0.00	65.38	0.37	358.56	243.91	602.47	3.78	0.00	0.902
S29_13	668.20	0.00	63.12	0.36	367.65	237.08	604.74	3.92	0.00	0.905
S29_14	668.20	80.96	67.89	0.39	395.65	285.27	680.92	5.45	0.01	0.909
S29_15	668.20	0.00	32.00	0.35	379.73	256.16	635.88	2.76	0.00	0.952
S29_17	668.20	0.00	16.28	0.90	0.00	651.34	651.34	0.65	0.00	0.975
S29_2	668.20	0.00	30.83	0.01	630.17	7.33	637.50	1.99	0.00	0.954
S29_3	668.20	0.00	63.49	0.34	379.72	224.70	604.42	5.00	0.01	0.905
S29_5	668.20	0.00	65.16	0.34	371.67	231.06	602.73	1.33	0.00	0.902
S29_7	668.20	0.00	61.29	0.30	407.64	198.99	606.63	1.24	0.00	0.908
S29_8	668.20	0.00	43.86	0.29	424.83	199.31	624.14	3.94	0.00	0.934
S29_9	668.20	0.00	84.51	0.41	305.59	277.71	583.30	1.07	0.00	0.873
S3	668.20	0.00	92.62	0.48	251.74	449.34	575.21	2.33	0.00	0.861

S30	668.20	0.00	42.59	0.06	582.46	43.11	625.57	0.80	0.00	0.936
S31	668.20	0.00	39.89	0.09	565.35	62.93	628.28	0.35	0.00	0.940
S32	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.82	0.00	0.934
S33	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.51	0.00	0.934
S34	668.20	0.00	43.95	0.00	624.27	0.00	624.27	2.24	0.00	0.934
S35	668.20	0.00	43.95	0.00	624.27	0.00	624.27	2.04	0.00	0.934
S36	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.25	0.00	0.934
S37	668.20	0.00	38.37	0.24	462.90	166.80	629.70	0.43	0.00	0.942
S37_1	668.20	0.00	47.81	0.32	401.85	218.30	620.14	2.56	0.00	0.928
S37_10	668.20	0.00	135.17	0.65	92.70	440.25	532.95	0.26	0.00	0.798
S37_11	668.20	0.00	72.12	0.44	296.75	299.13	595.88	1.21	0.00	0.892
S37_12	668.20	0.00	106.54	0.54	197.27	364.22	561.49	0.43	0.00	0.840
S37_2	668.20	0.00	69.73	0.34	366.25	231.95	598.20	1.37	0.00	0.895
S37_3	668.20	0.00	73.56	0.45	302.38	291.87	594.25	0.83	0.00	0.889
S37_4	668.20	0.00	35.17	0.20	490.61	142.28	632.89	2.28	0.00	0.947
S37_8	668.20	0.00	121.60	0.58	148.72	397.33	546.06	0.72	0.00	0.817
S38	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.17	0.00	0.934
S39	668.20	0.00	45.64	0.23	458.43	163.93	622.35	2.93	0.00	0.931
S4	668.20	0.00	43.93	0.00	624.29	0.00	624.29	2.49	0.00	0.934
S40	668.20	0.00	43.24	0.01	618.24	6.73	624.97	1.14	0.00	0.935
S41	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.71	0.00	0.934
S42	668.20	0.00	43.95	0.00	624.27	0.00	624.27	2.56	0.00	0.934
S43	668.20	1373.58	423.06	1618.71	0.00	0.00	0.00	0.00	0.00	0.000
S43_2	668.20	0.00	117.21	0.56	167.11	467.01	550.57	3.03	0.00	0.824
S43_4	668.20	0.00	117.33	0.64	116.22	434.02	550.24	1.75	0.00	0.823
S43_5	668.20	0.00	82.87	0.48	271.94	448.90	584.87	5.60	0.01	0.875
S43_6	668.20	0.00	108.69	0.57	173.20	472.35	558.95	2.92	0.00	0.837
S43_7	668.20	1495.78	62.65	0.37	1210.84	1495.62	2101.04	12.55	0.01	0.971
S43_9	668.20	0.00	74.45	0.45	304.71	441.02	593.37	5.32	0.01	0.888
S44	668.20	0.00	43.95	0.00	624.27	0.00	624.27	4.45	0.00	0.934
S45	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.31	0.00	0.934
S46	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.48	0.00	0.934
S46_1	668.20	0.00	68.83	0.38	348.79	250.23	599.02	3.34	0.00	0.896
S46_10	668.20	0.00	42.63	0.29	427.59	197.87	625.46	0.72	0.00	0.936
S46_2	668.20	0.00	86.63	0.49	247.88	333.25	581.13	1.97	0.00	0.870
S46_3	668.20	0.00	38.62	0.25	456.53	172.83	629.37	2.08	0.00	0.942
S46_4	668.20	0.00	63.26	0.32	395.10	209.55	604.65	3.18	0.00	0.905
S46_5	668.20	603.36	67.15	0.42	630.57	573.50	1204.07	5.50	0.01	0.947
S46_6	668.20	0.00	77.36	0.38	335.39	255.11	590.50	1.75	0.00	0.884

S46_7	668.20	0.00	42.10	0.27	436.86	189.03	625.89	3.29	0.00	0.937
S47	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.39	0.00	0.934
S48	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.75	0.00	0.934
S49	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.94	0.00	0.934
S5	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.41	0.00	0.934
S50	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.23	0.00	0.934
S51	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.14	0.00	0.934
S52_1	668.20	0.00	106.21	0.54	196.65	364.81	561.46	5.17	0.01	0.840
S52_2	668.20	0.00	68.22	0.44	308.18	291.42	599.60	5.05	0.01	0.897
S52_3	668.20	0.00	62.47	0.33	389.97	215.45	605.43	1.58	0.00	0.906
S52_4	668.20	0.00	63.40	0.36	368.75	235.79	604.54	2.37	0.00	0.905
S52_6	668.20	0.00	43.71	0.23	467.74	156.55	624.29	5.38	0.01	0.934
S52_7	668.20	0.00	69.36	0.42	322.53	275.92	598.44	4.48	0.00	0.896
S53	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.64	0.00	0.934
S54	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.64	0.00	0.934
S55	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.08	0.00	0.934
S56	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.45	0.00	0.934
S57	668.20	0.00	30.94	0.00	637.29	0.00	637.29	0.36	0.00	0.954
S59	668.20	0.00	42.42	0.02	610.15	15.64	625.79	0.68	0.00	0.937
S63_1	668.20	4.37	85.75	0.49	248.72	337.66	586.39	3.60	0.00	0.872
S63_11	668.20	0.00	58.08	0.33	392.79	217.04	609.83	1.52	0.00	0.913
S63_12	668.20	0.00	56.29	0.37	361.71	249.89	611.61	0.80	0.00	0.915
S63_13	668.20	0.00	69.27	0.43	316.94	281.61	598.55	2.60	0.00	0.896
S63_14	668.20	1119.14	54.81	0.34	1057.36	675.00	1732.36	3.23	0.00	0.969
S63_15	668.20	0.00	63.94	0.42	328.51	275.39	603.90	1.71	0.00	0.904
S63_2	668.20	0.00	109.14	0.58	170.38	388.12	558.51	6.72	0.01	0.836
S63_3	668.20	352.67	56.36	0.29	648.21	316.07	964.29	1.96	0.00	0.945
S63_4	668.20	0.00	31.06	0.09	570.59	66.51	637.10	0.71	0.00	0.953
S63_5	668.20	0.00	29.62	0.08	580.16	58.53	638.70	0.03	0.00	0.956
S63_6	668.20	0.00	60.46	0.40	340.61	266.85	607.46	1.72	0.00	0.909
S63_7	668.20	0.00	90.12	0.51	230.40	347.36	577.76	0.44	0.00	0.865
S63_8	668.20	0.00	73.18	0.36	354.62	240.11	594.73	0.89	0.00	0.890
S63_9	668.20	1715.25	102.56	0.50	857.26	1424.01	2281.27	6.37	0.01	0.957
S7	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.77	0.00	0.934
S8	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.91	0.00	0.934
S9	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.99	0.00	0.934

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LID Performance Summary
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Subcatchment	LID Control	Total Inflow mm	Evap Loss mm	Infil Loss mm	Surface Outflow mm	Drain Outflow mm	Initial Storage mm	Final Storage mm	Continuity Error %
S43	BioSwale	2041.78	423.06	1618.71	0.00	0.00	85.00	85.00	-0.00

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Groundwater Summary
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Subcatchment	Total Infil mm	Total Evap mm	Total Lower Seepage mm	Total Lateral Outflow mm	Maximum Lateral Outflow CMS	Average Upper Moist.	Average Water Table m	Final Upper Moist.	Final Water Table m
S1	0.38	277.55	14.73	0.00	0.00	0.21	9.97	0.15	9.95
S12	0.12	97.86	12.78	0.00	0.00	0.29	11.97	0.28	11.94
S13	0.44	297.81	14.86	0.00	0.00	0.21	11.32	0.15	11.30
S14	0.39	305.06	12.78	0.00	0.00	0.26	11.97	0.23	11.95
S15_1	0.49	247.17	15.24	0.00	0.00	0.18	11.32	0.15	11.30
S15_10	0.49	247.14	15.24	0.00	0.00	0.18	11.32	0.15	11.30
S15_12	0.29	234.80	15.21	0.00	0.00	0.22	11.32	0.16	11.29
S15_2	0.27	223.24	14.35	0.00	0.00	0.25	11.32	0.21	11.29
S15_4	0.34	283.01	14.50	0.00	0.00	0.23	11.32	0.18	11.29
S15_5	0.26	209.49	14.32	0.00	0.00	0.25	11.32	0.22	11.29
S15_7	0.27	92.85	16.54	0.00	0.00	0.17	11.32	0.15	11.30
S15_8	0.49	305.12	14.80	0.00	0.00	0.20	11.32	0.15	11.30
S15_9	0.56	248.72	15.23	0.00	0.00	0.17	11.32	0.15	11.30
S18_4	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
3153571065128955710362509467078816911962727800095975475139526902326298918526825682743572656381581645287519436234655060718842629630136188326954812831209994510663 68.00									
2885547982936050907108122638380376301024455318599573227268058958025955286807502646486599991106599290234878967106152740497093638220684091451762534031757218844981085628758378406848041334916206511776109830006450546414714 88.00									
S2	0.01	8.22	15.14	0.00	0.00	0.30	10.56	0.29	10.53
S23	0.35	276.43	13.19	0.00	0.00	0.26	11.32	0.22	11.29
S23_1	0.28	227.30	15.16	0.00	0.00	0.23	11.97	0.18	11.94
S23_3	0.33	261.05	11.96	0.00	0.00	0.27	11.97	0.25	11.95
S23_4	0.35	199.32	15.71	0.00	0.00	0.19	11.97	0.15	11.95
S26_1	0.37	287.88	13.24	0.00	0.00	0.26	11.32	0.22	11.30
S26_3	0.34	262.01	14.68	0.00	0.00	0.23	11.32	0.18	11.29
S29_1	0.46	356.27	12.78	0.00	0.00	0.26	11.97	0.22	11.95
S29_10	0.37	193.15	15.56	0.00	0.00	0.19	10.57	0.15	10.55
S29_11	0.06	42.77	14.23	0.00	0.00	0.29	9.67	0.28	9.63
S29_12	0.37	289.95	14.53	0.00	0.00	0.22	9.97	0.16	9.95
S29_13	0.36	167.05	15.79	0.00	0.00	0.18	10.57	0.15	10.55
S29_14	0.39	229.27	15.14	0.00	0.00	0.20	9.97	0.15	9.95
S29_2	0.01	7.50	13.58	0.00	0.00	0.30	11.32	0.30	11.28
S29_3	0.34	254.88	15.19	0.00	0.00	0.21	11.32	0.15	11.30
S29_5	0.34	241.81	15.15	0.00	0.00	0.21	10.57	0.15	10.55
S29_7	0.30	236.37	15.09	0.00	0.00	0.22	10.57	0.16	10.54
S29_8	0.29	227.60	14.21	0.00	0.00	0.26	11.97	0.22	11.94
S29_9	0.41	342.24	14.32	0.00	0.00	0.22	10.57	0.15	10.55
S3	0.48	273.22	14.97	0.00	0.00	0.19	10.97	0.15	10.95
S30	0.06	45.35	14.60	254.20	0.02	0.29	8.36	0.27	8.35
S31	0.09	67.41	11.12	0.00	0.00	0.29	9.97	0.29	9.95
S37	0.24	187.61	12.70	0.00	0.00	0.27	10.57	0.25	10.54
S37_1	0.32	251.88	14.83	0.00	0.00	0.23	11.32	0.18	11.29
S37_10	0.65	551.56	13.19	0.00	0.00	0.22	11.32	0.15	11.30
S37_11	0.44	241.50	15.26	27.68	0.00	0.19	11.18	0.15	11.16
S37_12	0.54	240.75	15.26	27.70	0.00	0.17	11.19	0.15	11.16
S37_2	0.34	279.51	14.34	0.00	0.00	0.24	11.32	0.19	11.29
S37_3	0.45	348.49	14.34	0.00	0.00	0.22	11.32	0.16	11.30
S37_4	0.20	159.25	14.86	0.00	0.00	0.26	11.32	0.22	11.29
S37_8	0.58	309.33	14.77	0.00	0.00	0.18	11.32	0.15	11.30
S39	0.23	185.02	11.10	0.00	0.00	0.28	9.97	0.27	9.95
S40	0.01	6.91	11.10	0.00	0.00	0.30	9.97	0.30	9.94
S43	1618.71	332.79	15.72	1523.64	0.10	0.25	9.19	0.16	9.15
S43_2	0.56	331.74	14.53	0.00	0.00	0.19	10.97	0.15	10.95
S43_4	0.64	211.40	15.23	0.00	0.00	0.17	9.68	0.15	9.65

S43_5	0.48	205.58	15.33	238.27	0.12	0.17	9.74	0.15	9.73
S43_6	0.57	161.24	15.72	89.72	0.03	0.16	9.18	0.15	9.15
S43_7	0.37	205.07	15.33	238.68	0.08	0.19	9.74	0.15	9.73
S43_9	0.45	161.26	15.72	89.48	0.05	0.17	9.18	0.15	9.15
S46_1	0.38	279.00	14.70	218.35	0.06	0.21	9.87	0.15	9.85
S46_10	0.29	226.32	12.70	0.00	0.00	0.27	10.57	0.24	10.54
S46_2	0.49	272.10	14.99	65.38	0.01	0.19	11.00	0.15	10.97
S46_3	0.25	195.63	12.70	0.00	0.00	0.27	10.57	0.25	10.54
S46_4	0.32	250.39	14.86	0.00	0.00	0.23	11.32	0.17	11.29
S46_5	0.42	326.06	13.18	0.00	0.00	0.25	10.97	0.21	10.95
S46_6	0.38	270.71	14.99	87.72	0.02	0.21	10.85	0.15	10.84
S46_7	0.27	215.24	13.18	0.00	0.00	0.27	10.97	0.24	10.94
S52_1	0.54	161.25	15.72	89.55	0.05	0.16	9.18	0.15	9.15
S52_2	0.44	161.19	15.72	89.55	0.05	0.17	9.18	0.15	9.15
S52_3	0.33	253.67	12.54	0.00	0.00	0.26	9.67	0.23	9.65
S52_4	0.36	281.39	14.58	0.00	0.00	0.23	10.57	0.17	10.55
S52_6	0.23	178.25	15.59	0.00	0.00	0.23	10.97	0.17	10.94
S52_7	0.42	172.79	15.84	0.00	0.00	0.17	11.32	0.15	11.30
S59	0.02	15.98	13.43	0.00	0.00	0.30	11.32	0.30	11.28
S63_1	0.49	247.71	14.60	254.83	0.08	0.18	8.36	0.15	8.35
S63_11	0.33	256.70	12.13	0.00	0.00	0.27	9.97	0.24	9.95
S63_12	0.37	290.21	11.77	0.00	0.00	0.27	9.67	0.24	9.65
S63_13	0.43	335.73	11.77	0.00	0.00	0.26	9.67	0.23	9.65
S63_14	0.34	265.07	12.86	0.00	0.00	0.26	10.57	0.23	10.55
S63_15	0.42	324.85	12.13	0.00	0.00	0.26	9.97	0.23	9.95
S63_2	0.58	338.12	14.01	116.58	0.08	0.19	9.06	0.15	9.04
S63_3	0.29	228.40	12.86	0.00	0.00	0.27	10.57	0.24	10.54
S63_4	0.09	71.17	15.72	153.22	0.01	0.26	9.18	0.23	9.15
S63_5	0.08	62.32	14.60	254.25	0.00	0.28	8.36	0.26	8.35
S63_6	0.40	312.66	12.34	0.00	0.00	0.26	9.97	0.22	9.95
S63_7	0.51	160.89	15.72	150.12	0.01	0.16	9.18	0.15	9.15
S63_8	0.36	293.21	12.86	0.00	0.00	0.26	10.57	0.22	10.55
S63_9	0.50	410.92	11.10	0.00	0.00	0.26	9.98	0.23	9.95

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Node Depth Summary
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Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
J1	JUNCTION	0.01	0.14	13.54	168 12:37	0.14
J10	JUNCTION	0.10	0.24	13.54	168 13:27	0.24
J1040	JUNCTION	0.05	0.28	9.35	241 03:25	0.28
J11	JUNCTION	0.37	0.52	13.54	168 19:53	0.52
J12	JUNCTION	0.00	0.03	17.52	168 07:28	0.03
J13	JUNCTION	0.00	0.03	14.75	168 07:12	0.03
J14	JUNCTION	0.23	0.38	13.54	168 12:36	0.38
J1415	JUNCTION	0.01	0.19	9.90	169 00:00	0.19
J15	JUNCTION	0.00	0.02	13.79	168 22:56	0.02
J16	JUNCTION	0.00	0.02	12.33	168 11:49	0.02
J17	JUNCTION	0.13	0.16	13.80	168 19:42	0.16
J1701	JUNCTION	0.00	0.02	14.32	168 16:15	0.02
J1788	JUNCTION	0.07	0.36	9.44	241 03:24	0.36
J18	JUNCTION	0.00	0.01	13.82	168 18:41	0.01
J19	JUNCTION	0.00	0.04	12.52	168 23:43	0.04
J1969	JUNCTION	0.08	0.76	9.86	241 03:47	0.76
J2	JUNCTION	0.22	0.37	13.54	168 13:27	0.37
J20	JUNCTION	0.00	0.03	13.81	168 17:43	0.03
J21	JUNCTION	0.00	0.03	11.03	168 11:41	0.03
J2181	JUNCTION	0.00	0.06	11.97	168 13:53	0.06
J22	JUNCTION	0.00	0.01	11.51	168 03:50	0.01
J2293	JUNCTION	0.00	0.08	11.68	168 18:37	0.08
J23	JUNCTION	0.01	0.10	11.60	168 18:42	0.10
J2312	JUNCTION	0.01	0.10	11.68	168 22:22	0.10
J24	JUNCTION	0.01	0.11	11.65	168 18:38	0.11
J25	JUNCTION	0.05	0.06	12.41	168 06:19	0.06
J2510	JUNCTION	0.01	0.15	11.36	168 19:08	0.15
J2594	JUNCTION	0.01	0.16	11.18	168 17:59	0.16
J26	JUNCTION	0.00	0.01	13.37	168 17:27	0.01
J2678	JUNCTION	0.35	0.46	10.96	169 00:00	0.46
J2692	JUNCTION	0.01	0.14	10.75	169 00:00	0.14
J27	JUNCTION	0.00	0.04	12.52	168 22:16	0.04
J2709	JUNCTION	0.16	0.19	15.69	168 13:25	0.19
J2712	JUNCTION	0.26	0.29	15.69	168 13:56	0.29

J2717	JUNCTION	0.00	0.02	16.00	168	14:53	0.02
J2719	JUNCTION	0.00	0.03	15.91	168	17:51	0.03
J2722	JUNCTION	0.00	0.07	14.61	168	11:32	0.07
J2728	JUNCTION	0.00	0.03	15.31	168	11:04	0.03
J2730	JUNCTION	0.00	0.05	15.31	168	15:02	0.05
J2749	JUNCTION	0.00	0.07	15.23	168	07:00	0.07
J2754	JUNCTION	0.00	0.02	14.58	168	00:50	0.02
J2755	JUNCTION	0.00	0.01	14.10	168	11:44	0.01
J2757	JUNCTION	0.00	0.04	15.36	168	01:57	0.04
J2764	JUNCTION	0.00	0.02	14.49	168	19:39	0.02
J2771	JUNCTION	0.01	0.14	10.04	169	00:00	0.14
J2779	JUNCTION	0.00	0.00	14.32	0	00:00	0.00
J2785	JUNCTION	0.23	0.32	14.45	168	17:30	0.32
J2786	JUNCTION	0.00	0.03	15.10	168	07:11	0.03
J2787	JUNCTION	0.00	0.01	14.95	168	11:18	0.01
J2794	JUNCTION	0.35	0.41	14.41	168	12:11	0.41
J2797	JUNCTION	0.00	0.04	13.31	168	12:30	0.04
J28	JUNCTION	0.00	0.01	13.29	168	12:49	0.01
J2813	JUNCTION	0.00	0.00	12.42	0	00:00	0.00
J2816	JUNCTION	0.00	0.00	12.29	0	00:00	0.00
J2822	JUNCTION	0.00	0.07	13.00	168	16:56	0.07
J2831	JUNCTION	0.01	0.10	12.74	168	11:14	0.10
J2838	JUNCTION	0.00	0.05	12.34	168	23:01	0.05
J2839	JUNCTION	0.00	0.01	14.11	168	21:13	0.01
J2845	JUNCTION	0.00	0.03	12.65	168	12:36	0.03
J2847	JUNCTION	0.00	0.05	13.63	168	14:05	0.05
J2855	JUNCTION	0.05	0.25	9.26	241	03:25	0.25
J2857	JUNCTION	0.01	0.20	9.84	169	00:00	0.20
J2860	JUNCTION	0.01	0.10	12.59	168	15:21	0.10
J2868	JUNCTION	0.00	0.06	12.84	168	23:02	0.06
J2870	JUNCTION	0.00	0.04	12.84	168	23:02	0.04
J2887	JUNCTION	0.03	0.21	9.78	169	00:00	0.21
J2890	JUNCTION	0.00	0.00	12.90	0	00:00	0.00
J2891	JUNCTION	0.00	0.00	10.00	0	00:00	0.00
J29	JUNCTION	0.19	0.25	12.93	168	18:25	0.25
J29_14	JUNCTION	0.29	0.35	12.35	168	06:30	0.35
J2909	JUNCTION	0.00	0.05	13.53	168	15:52	0.05
J2915	JUNCTION	0.02	0.57	9.77	241	03:23	0.57
J2918	JUNCTION	0.02	0.04	13.61	168	11:21	0.04
J2921	JUNCTION	0.02	0.11	11.40	180	18:33	0.10
J2931	JUNCTION	0.03	0.13	12.00	180	18:33	0.13
J2938	JUNCTION	0.00	0.00	14.36	0	00:00	0.00
J3	JUNCTION	0.00	0.06	13.65	168	11:19	0.06
J30	JUNCTION	0.51	0.58	12.93	168	18:25	0.58
J31	JUNCTION	0.20	0.26	12.93	168	18:25	0.26
J32	JUNCTION	0.27	0.33	12.93	168	18:25	0.33
J33	JUNCTION	0.00	0.07	12.38	168	13:20	0.07
J34	JUNCTION	0.17	0.25	12.38	168	15:01	0.25
J35	JUNCTION	0.40	1.00	12.50	89	07:17	1.00
J36	JUNCTION	0.18	0.48	12.21	180	18:33	0.46
J37	JUNCTION	0.01	0.08	12.29	168	11:16	0.08
J38	JUNCTION	0.00	0.05	12.35	168	06:28	0.05
J39	JUNCTION	0.17	0.23	12.35	168	06:29	0.23
J4	JUNCTION	0.00	0.05	13.85	168	11:36	0.05
J40	JUNCTION	0.30	0.37	12.35	168	06:30	0.37
J41	JUNCTION	0.29	0.54	12.54	136	07:34	0.53
J42	JUNCTION	0.07	0.18	12.41	168	22:25	0.18
J43	JUNCTION	0.00	0.05	12.92	168	23:29	0.05
J44	JUNCTION	0.00	0.05	12.92	168	22:01	0.05
J45	JUNCTION	0.03	0.42	9.72	241	03:26	0.42
J46	JUNCTION	0.03	0.16	9.86	174	16:30	0.16
J47	JUNCTION	0.25	0.62	12.26	361	22:33	0.59
J48	JUNCTION	0.39	0.58	12.09	110	07:06	0.56
J49	JUNCTION	0.09	0.69	9.78	241	03:19	0.69
J5	JUNCTION	0.00	0.05	14.04	168	14:53	0.05
J50	JUNCTION	0.00	0.03	12.24	168	11:17	0.03
J52	JUNCTION	0.39	1.00	12.51	89	00:55	1.00
J53	JUNCTION	0.39	1.00	12.51	88	08:05	1.00
J55	JUNCTION	0.01	0.06	9.75	174	16:30	0.06
J56	JUNCTION	0.00	0.03	13.22	168	14:42	0.03
J57	JUNCTION	0.00	0.03	13.23	168	15:34	0.03
J59	JUNCTION	0.00	0.02	12.52	168	10:53	0.02
J6	JUNCTION	0.09	0.24	13.55	168	19:07	0.24
J63	JUNCTION	0.07	0.18	12.41	168	22:25	0.18
J64	JUNCTION	0.00	0.00	12.80	0	00:00	0.00
J65	JUNCTION	0.12	0.78	12.57	361	22:43	0.63
J66	JUNCTION	0.32	0.49	12.07	212	16:04	0.48
J67	JUNCTION	0.02	0.20	12.12	212	16:05	0.20

J68	JUNCTION	0.29	0.35	12.35	168	06:31	0.35
J69	JUNCTION	0.15	1.00	12.76	238	21:58	0.68
J7	JUNCTION	0.00	0.07	13.41	168	12:37	0.07
J70	JUNCTION	0.00	0.07	12.74	168	20:23	0.07
J72	JUNCTION	0.30	1.00	12.60	88	07:36	1.00
J73	JUNCTION	0.01	0.06	12.92	168	15:38	0.06
J78	JUNCTION	0.26	0.34	12.74	168	20:23	0.34
J79	JUNCTION	0.46	0.55	12.74	168	21:53	0.55
J8	JUNCTION	0.01	0.10	11.44	168	17:15	0.10
J80	JUNCTION	0.10	0.35	12.17	184	12:26	0.35
J83	JUNCTION	0.21	1.20	12.90	88	23:49	1.20
J9	JUNCTION	0.00	0.04	16.40	168	16:36	0.04
J355	OUTFALL	0.03	0.19	8.52	241	03:25	0.19
J54	STORAGE	0.67	0.92	9.72	241	03:24	0.92

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Node Inflow Summary
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Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days	hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent	
J1	JUNCTION	0.001	0.047	168	12:36	0.725	43.3	0.000	
J10	JUNCTION	0.000	0.000	168	00:41	0	0.11	0.114	
J1040	JUNCTION	0.003	0.920	241	03:23	2.56	1.59e+03	0.006	
J11	JUNCTION	0.007	0.007	168	12:20	6.18	6.28	0.020	
J12	JUNCTION	0.004	0.004	168	07:45	3.46	3.46	0.001	
J13	JUNCTION	0.006	0.006	168	07:10	5.34	5.34	-0.007	
J14	JUNCTION	0.000	0.012	168	12:37	0	12.2	0.041	
J1415	JUNCTION	0.000	0.126	169	00:00	0	118	0.000	
J15	JUNCTION	0.000	0.006	168	19:29	0	5.81	-0.000	
J16	JUNCTION	0.006	0.006	168	11:25	5.46	5.46	0.004	
J17	JUNCTION	0.001	0.006	168	21:05	1.16	5.81	0.011	
J1701	JUNCTION	0.000	0.003	168	09:41	0	2.84	-0.005	
J1788	JUNCTION	0.000	0.968	241	03:19	0	1.56e+03	-0.003	
J18	JUNCTION	0.005	0.005	168	17:10	4.11	4.11	0.003	
J19	JUNCTION	0.000	0.004	168	23:42	0	3.73	-0.004	
J1969	JUNCTION	0.303	6.106	168	02:09	29	2.44e+03	0.140	
J2	JUNCTION	0.000	0.006	168	23:34	0	5.99	0.121	
J20	JUNCTION	0.005	0.005	168	17:56	4.65	4.65	0.000	
J21	JUNCTION	0.000	0.006	168	10:08	0	5.46	-0.005	
J2181	JUNCTION	0.011	0.011	168	15:15	10.3	10.3	-0.001	
J22	JUNCTION	0.000	0.000	168	03:10	0.256	0.256	0.013	
J2293	JUNCTION	0.000	0.016	168	16:28	0	14.4	0.000	
J23	JUNCTION	0.003	0.030	168	18:02	2.54	27.5	-0.002	
J2312	JUNCTION	0.001	0.023	168	22:22	0.814	21	-0.000	
J24	JUNCTION	0.001	0.026	168	18:38	0.986	23.5	-0.000	
J25	JUNCTION	0.001	0.001	168	05:45	0.827	0.827	0.040	
J2510	JUNCTION	0.004	0.085	168	12:37	2.03	77.4	0.000	
J2594	JUNCTION	0.011	0.087	168	19:08	2.19	79.6	0.000	
J26	JUNCTION	0.002	0.002	168	12:28	1.49	1.49	0.017	
J2678	JUNCTION	0.025	0.094	169	00:00	2.01	87.7	0.004	
J2692	JUNCTION	0.002	0.097	169	00:00	2.04	89.1	0.000	
J27	JUNCTION	0.000	0.000	168	02:35	0	0.0138	0.010	
J2709	JUNCTION	0.002	0.002	168	07:00	1.71	1.91	0.014	
J2712	JUNCTION	0.000	0.002	168	13:25	0.351	2.26	-0.114	
J2717	JUNCTION	0.002	0.002	168	12:30	2.33	2.33	-0.000	
J2719	JUNCTION	0.002	0.005	168	12:00	1.96	4.29	0.000	
J2722	JUNCTION	0.015	0.015	168	12:40	13.5	13.5	-0.000	
J2728	JUNCTION	0.002	0.002	168	07:30	1.52	1.52	-0.000	
J2730	JUNCTION	0.001	0.007	168	11:11	0.89	6.71	-0.000	
J2749	JUNCTION	0.000	0.007	168	11:19	0	6.71	0.000	
J2754	JUNCTION	0.002	0.002	168	02:20	1.99	1.99	0.000	
J2755	JUNCTION	0.001	0.001	168	12:31	0.912	0.912	0.007	
J2757	JUNCTION	0.004	0.004	168	07:10	3.99	3.99	0.001	
J2764	JUNCTION	0.000	0.003	168	10:09	0	2.84	-0.002	
J2771	JUNCTION	0.060	0.100	169	00:00	4.56	93.7	-0.003	
J2779	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2785	JUNCTION	0.009	0.011	168	20:05	8.08	10.2	0.041	
J2786	JUNCTION	0.000	0.011	168	07:10	0	10.7	-0.000	
J2787	JUNCTION	0.001	0.001	168	11:40	0.848	0.848	0.006	
J2794	JUNCTION	0.003	0.025	168	12:11	2.6	23.4	0.008	
J2797	JUNCTION	0.000	0.015	168	15:54	0	13.5	0.000	
J28	JUNCTION	0.002	0.002	168	12:30	1.5	1.5	0.002	

J2813	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2816	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2822	JUNCTION	0.001	0.016	168	12:00	0.801	14.3	-0.001	
J2831	JUNCTION	0.000	0.016	168	11:03	0	14.3	-0.005	
J2838	JUNCTION	0.006	0.026	168	23:01	5.38	24.3	-0.001	
J2839	JUNCTION	0.001	0.001	168	12:30	1.39	1.39	0.000	
J2845	JUNCTION	0.000	0.016	168	12:55	0	14.3	0.007	
J2847	JUNCTION	0.001	0.005	168	16:13	0.755	4.98	0.002	
J2855	JUNCTION	0.082	0.879	241	03:25	8.13	1.61e+03	0.001	
J2857	JUNCTION	0.000	0.142	169	00:00	0	132	0.001	
J2860	JUNCTION	0.005	0.020	168	23:02	4.48	18.9	0.001	
J2868	JUNCTION	0.000	0.015	168	15:22	0	13.5	-0.000	
J2870	JUNCTION	0.000	0.000	142	00:10	0	0.00519	0.012	
J2887	JUNCTION	0.001	0.143	169	00:00	31.4	164	0.007	
J2890	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2891	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J29	JUNCTION	0.000	0.003	168	21:54	0	3.29	0.026	
J29_14	JUNCTION	0.003	0.021	158	09:02	2.76	3.23	0.007	
J2909	JUNCTION	0.008	0.015	168	15:54	7.39	13.5	-0.002	
J2915	JUNCTION	0.000	4.318	241	04:07	0	1.91e+03	0.022	
J2918	JUNCTION	0.001	0.001	168	12:30	1.13	1.13	0.017	
J2921	JUNCTION	0.000	0.184	180	18:33	0	244	0.023	
J2931	JUNCTION	0.014	0.209	180	18:33	13	246	0.487	
J2938	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J3	JUNCTION	0.002	0.012	168	12:29	1.6	11.2	-0.002	
J30	JUNCTION	0.003	0.003	168	22:10	2.77	2.97	0.059	
J31	JUNCTION	0.000	0.007	168	21:54	0	7.54	0.039	
J32	JUNCTION	0.004	0.004	168	22:50	4.17	4.45	0.008	
J33	JUNCTION	0.000	0.026	168	12:57	0	24.4	0.001	
J34	JUNCTION	0.000	0.000	303	06:48	0	0.0576	0.314	
J35	JUNCTION	0.004	8.525	107	09:56	3.92	1.12e+03	-8.041	
J36	JUNCTION	0.000	0.902	260	23:09	0	424	0.160	
J37	JUNCTION	0.000	0.007	168	06:28	0	6.53	0.001	
J38	JUNCTION	0.000	0.007	168	06:29	0	6.53	-0.001	
J39	JUNCTION	0.000	0.007	168	06:28	0	7.35	0.025	
J4	JUNCTION	0.010	0.010	168	12:30	9.57	9.57	-0.001	
J40	JUNCTION	0.004	0.307	122	16:01	3.78	9.81	0.022	
J41	JUNCTION	0.000	0.262	178	12:04	0	0.926	0.295	
J42	JUNCTION	0.000	0.022	168	22:01	0	20.7	0.005	
J43	JUNCTION	0.000	0.007	168	22:00	0	6.96	0.006	
J44	JUNCTION	0.000	0.000	127	23:30	0	0.0402	0.004	
J45	JUNCTION	0.000	0.931	127	00:32	0	1.14e+03	-0.016	
J46	JUNCTION	0.923	0.923	174	16:30	1.14e+03	1.14e+03	0.000	
J47	JUNCTION	0.000	1.555	361	22:33	0	765	0.143	
J48	JUNCTION	0.006	2.528	238	21:58	5.45	487	1.159	
J49	JUNCTION	0.000	2.767	241	04:00	0	1.74e+03	0.198	
J5	JUNCTION	0.002	0.013	168	14:25	2.16	12.5	-0.002	
J50	JUNCTION	0.000	0.007	168	11:17	0	6.53	0.001	
J52	JUNCTION	0.000	8.502	158	07:19	0	347	-0.795	
J53	JUNCTION	0.000	3.757	110	07:06	0	95.5	-8.379	
J55	JUNCTION	0.000	0.922	174	16:30	0	1.14e+03	0.000	
J56	JUNCTION	0.004	0.004	168	12:23	3.03	3.72	-0.004	
J57	JUNCTION	0.001	0.001	168	12:30	0.685	0.685	0.001	
J59	JUNCTION	0.000	0.000	142	00:08	0	0.00294	0.028	
J6	JUNCTION	0.008	0.034	168	14:50	7.36	31	0.009	
J63	JUNCTION	0.003	0.003	168	15:16	2.65	2.78	0.006	
J64	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J65	JUNCTION	0.000	1.111	238	21:58	0	80.9	0.568	
J66	JUNCTION	0.000	0.183	148	15:50	0	139	-0.178	
J67	JUNCTION	0.000	0.105	184	12:26	0	38.7	0.563	
J68	JUNCTION	0.000	0.006	158	09:02	0	1.06	0.147	
J69	JUNCTION	0.000	0.855	238	21:58	0	26.2	0.664	
J7	JUNCTION	0.004	0.051	168	12:37	3.54	46.7	0.000	
J70	JUNCTION	0.003	0.019	168	23:29	2.37	18	-0.002	
J72	JUNCTION	0.000	9.844	236	12:16	0	580	-10.599	
J73	JUNCTION	0.000	0.000	88	11:53	0	0.0191	0.076	
J78	JUNCTION	0.000	0.009	168	22:01	0	8.78	0.005	
J79	JUNCTION	0.009	0.009	168	13:20	8.64	8.77	0.024	
J8	JUNCTION	0.000	0.032	168	17:15	0	28.6	-0.001	
J80	JUNCTION	0.004	0.053	324	14:53	3.22	10.8	0.520	
J83	JUNCTION	0.001	3.426	338	23:38	1.07	172	-52.693	
J9	JUNCTION	0.007	0.011	168	15:50	6.83	10.3	-0.001	
J355	OUTFALL	0.148	0.899	241	03:28	1.48e+03	3.08e+03	0.000	
J54	STORAGE	0.000	0.922	174	16:30	0	1.14e+03	0.005	

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Node Surcharge Summary

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Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
J35	JUNCTION	1.15	0.000	0.000
J52	JUNCTION	0.11	0.000	0.000
J53	JUNCTION	5.67	0.000	0.000
J69	JUNCTION	0.01	0.000	0.000
J72	JUNCTION	23.28	0.000	0.000
J83	JUNCTION	10.35	0.200	0.000

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Node Flooding Summary
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Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CMS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 ltr	Maximum Ponded Depth Meters
J35	1.15	4.259	197 17:55	8.101	0.000
J52	0.11	4.922	158 07:19	1.397	0.000
J53	5.67	2.997	110 07:06	9.868	0.000
J69	0.01	0.559	238 21:58	0.000	0.000
J72	23.28	5.992	106 01:34	185.381	0.000
J83	2.69	1.713	338 23:38	8.940	0.000

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Storage Volume Summary
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Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
J54	0.447	10	0	0	0.844	19	241 03:24	0.931

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Outfall Loading Summary
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Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
J355	100.00	0.094	0.899	3080.661
System	100.00	0.094	0.899	3080.661

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Link Flow Summary
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Link	Type	Maximum |Flow| CMS	Time of Max Occurrence days hr:min	Maximum |Veloc| m/sec	Max/ Full Flow	Max/ Full Depth
206110366	CONDUIT	0.085	168 19:08	0.91	0.03	0.12
206110379_1	CONDUIT	0.023	168 18:38	0.46	0.01	0.08
206110379_2	CONDUIT	0.032	168 15:56	0.46	0.01	0.09
206110379_4	CONDUIT	0.030	168 17:15	0.64	0.01	0.07
206110379_5	CONDUIT	0.026	168 21:32	0.52	0.01	0.08
22803188_2	CHANNEL	1.094	127 00:08	0.90	0.13	0.76
22803188_3	CHANNEL	0.931	127 00:32	0.87	0.07	0.54
22803188_4	CHANNEL	0.922	174 16:30	1.42	0.22	0.17

22803188_5	CHANNEL	0.922	174	16:30	0.64	0.01	0.54
22926618_1	CHANNEL	5.047	241	04:01	1.16	0.23	0.90
22926618_2	CHANNEL	2.767	241	04:00	0.55	0.66	0.99
22926618_3	CHANNEL	0.879	241	03:25	0.92	0.06	0.20
22926618_4	CHANNEL	0.901	241	03:23	0.75	0.19	0.25
22926629	CONDUIT	0.143	169	00:00	1.86	0.02	0.28
23116769	CONDUIT	0.087	168	17:59	0.96	0.03	0.11
23116814	CONDUIT	0.126	169	00:00	0.99	0.04	0.14
23116826	CONDUIT	0.142	169	00:00	1.00	0.05	0.16
23405543	CONDUIT	0.016	168	18:38	0.37	0.01	0.07
23405563	CONDUIT	0.011	168	13:59	0.38	0.00	0.05
57466689_1	CONDUIT	0.100	169	00:00	1.07	0.02	0.12
57466741	CONDUIT	0.097	169	00:00	1.24	0.02	0.10
57466813	CONDUIT	0.094	169	00:00	1.52	0.02	0.09
C1	CONDUIT	0.000	168	00:41	0.00	0.00	0.30
C1_1	CONDUIT	0.006	169	00:04	0.03	0.01	0.37
C1_2	CONDUIT	0.012	168	13:24	0.08	0.01	0.26
C10	CONDUIT	0.011	168	14:25	0.90	0.00	0.04
C108	CONDUIT	0.186	180	18:33	5.45	0.02	0.40
C109	CONDUIT	0.016	168	12:55	0.86	0.06	0.08
C11	CONDUIT	0.007	168	16:13	0.02	0.00	0.45
C110	CONDUIT	0.025	168	12:11	2.38	0.01	0.06
C111	CONDUIT	0.011	168	18:27	0.17	0.07	0.44
C112	CONDUIT	0.002	168	12:00	0.64	0.00	0.06
C113	CONDUIT	0.001	168	11:21	0.14	0.00	0.05
C12	CONDUIT	0.047	168	12:37	1.02	0.05	0.11
C126	CONDUIT	0.000	0	00:00	0.00	0.00	0.02
C127	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
C128	CONDUIT	0.015	168	15:54	1.37	0.04	0.12
C129_1	CONDUIT	0.003	168	09:41	0.70	0.00	0.02
C129_2	CONDUIT	0.003	168	15:54	0.40	0.00	0.04
C13	CONDUIT	0.004	168	07:00	0.53	0.00	0.03
C130	CONDUIT	0.001	168	14:11	0.31	0.00	0.02
C131	CONDUIT	0.000	169	00:05	0.03	0.00	0.05
C141	CONDUIT	0.184	180	18:33	3.49	0.03	0.12
C142	CONDUIT	0.016	168	11:03	0.57	0.02	0.11
C143	CONDUIT	0.002	168	13:30	0.04	0.01	0.38
C144	CONDUIT	0.011	168	07:11	0.15	0.01	0.49
C145	CONDUIT	0.001	168	11:16	0.22	0.00	0.03
C146	CONDUIT	0.000	0	00:00	0.00	0.00	0.01
C147	CONDUIT	0.007	168	11:19	0.55	0.03	0.14
C148	CONDUIT	0.005	168	11:04	0.61	0.01	0.10
C158	CONDUIT	0.020	168	23:01	0.91	0.04	0.10
C159	CONDUIT	0.015	168	12:00	1.05	0.00	0.07
C16	CONDUIT	0.006	168	07:12	0.05	0.00	0.20
C160	CONDUIT	0.016	168	10:51	0.56	0.00	0.15
C161	CONDUIT	0.002	168	07:15	0.23	0.01	0.09
C167_2	CONDUIT	0.209	180	18:33	0.89	0.13	0.35
C169	CONDUIT	0.026	168	23:01	0.64	0.01	0.15
C17	CONDUIT	0.006	168	19:29	0.18	0.00	0.09
C170	CONDUIT	0.000	0	00:00	0.00	0.00	0.09
C176	CHANNEL	0.854	241	03:25	1.10	0.04	0.17
C18	CONDUIT	0.005	168	16:16	0.37	0.00	0.05
C182	CONDUIT	0.004	168	07:10	0.77	0.01	0.08
C185	CONDUIT	0.015	168	23:02	0.50	0.01	0.08
C186	CONDUIT	0.015	168	14:35	0.84	0.01	0.06
C19	CONDUIT	0.005	168	21:05	0.13	0.00	0.10
C193	CONDUIT	0.002	168	10:39	0.02	0.00	0.54
C194	CONDUIT	0.007	168	09:35	0.71	0.05	0.11
C195	CONDUIT	0.002	168	02:00	0.56	0.00	0.02
C196	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
C20	CONDUIT	0.000	168	03:43	0.06	0.00	0.03
C21	CONDUIT	0.001	168	05:16	0.16	0.00	0.05
C22	CONDUIT	0.002	168	10:57	0.16	0.00	0.05
C23	CONDUIT	0.002	168	12:03	0.11	0.00	0.06
C24	CONDUIT	0.006	168	10:08	1.07	0.00	0.03
C25	CONDUIT	0.006	168	10:02	0.04	0.00	0.25
C26	CONDUIT	0.000	168	02:35	0.07	0.00	0.04
C27	CONDUIT	0.003	168	21:54	0.01	0.00	0.42
C28	CONDUIT	0.004	168	23:29	0.02	0.00	0.30
C29	CONDUIT	0.000	303	06:48	0.01	0.00	0.16
C3	CONDUIT	0.010	168	10:50	0.59	0.01	0.06
C30	CONDUIT	0.902	260	23:09	4.00	0.45	0.65
C31	CONDUIT	0.007	168	06:28	0.31	0.01	0.07
C32	CONDUIT	0.007	168	06:28	0.04	0.00	0.30
C33	CONDUIT	0.300	122	16:01	1.63	0.14	0.43
C34	CONDUIT	0.022	168	22:26	0.39	0.02	0.12
C35	CONDUIT	0.000	169	00:15	0.09	0.00	0.05

C37	CONDUIT	1.555	361	22:33	4.62	0.56	0.71
C38	CONDUIT	2.517	238	21:58	3.96	10.10	0.78
C39	CONDUIT	0.007	168	11:17	0.38	0.02	0.06
C4	CONDUIT	0.013	168	13:46	0.20	0.01	0.15
C40	CONDUIT	0.007	168	06:29	0.10	0.00	0.14
C41	CONDUIT	0.024	158	09:02	0.12	0.02	0.36
C42	CONDUIT	7.795	158	07:19	19.49	10.43	0.99
C44	CONDUIT	0.001	168	02:32	0.16	0.00	0.03
C45	CONDUIT	0.000	142	00:08	0.03	0.00	0.03
C46	CONDUIT	0.026	168	13:20	0.22	0.01	0.31
C47	CONDUIT	0.003	168	18:56	0.03	0.01	0.18
C49	CONDUIT	0.004	168	23:43	0.30	0.00	0.06
C5	CONDUIT	0.051	168	12:37	1.99	0.01	0.07
C50	CONDUIT	0.004	168	11:24	0.51	0.00	0.04
C51	CONDUIT	0.000	0	00:00	0.00	0.00	0.09
C52	CONDUIT	0.970	361	22:43	5.50	0.22	0.70
C53	CONDUIT	0.183	148	15:50	0.57	0.11	0.52
C54	CONDUIT	0.118	184	12:27	0.64	0.05	0.34
C55	CONDUIT	0.006	158	09:02	0.03	0.01	0.36
C56	CONDUIT	0.855	238	21:58	5.03	0.25	0.83
C57	CONDUIT	0.009	168	21:53	0.08	0.00	0.20
C58	CONDUIT	8.525	107	09:56	13.86	1.19	0.98
C59	CONDUIT	0.007	168	11:17	0.58	0.00	0.10
C6	CONDUIT	0.006	168	16:48	0.33	0.00	0.06
C60	CONDUIT	0.007	168	22:00	0.39	0.01	0.06
C61	CONDUIT	0.007	168	23:29	0.09	0.00	0.16
C62	CONDUIT	0.000	168	22:01	0.07	0.00	0.06
C63	CONDUIT	0.288	263	04:51	1.01	0.18	0.46
C65	CONDUIT	0.019	168	20:23	0.35	0.01	0.12
C66	CONDUIT	0.003	168	21:54	0.11	0.00	0.26
C67	CONDUIT	0.009	168	22:01	0.03	0.00	0.44
C68	CONDUIT	0.053	324	14:53	0.55	0.02	0.26
C7	CONDUIT	0.034	168	14:06	0.32	0.02	0.19
C70	CONDUIT	8.109	234	15:08	>50.00	1.55	1.00
C8	CONDUIT	0.012	168	11:03	0.16	0.01	0.15
C95	CONDUIT	0.001	168	11:09	0.06	0.00	0.06
C96	CONDUIT	0.005	168	11:57	0.35	0.00	0.05
C97	CONDUIT	0.000	0	00:00	0.00	0.00	0.02
22926618_6	WEIR	0.968	241	03:19			0.98

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Flow Classification Summary
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Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class: Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
206110366	1.00	0.00	0.36	0.00	0.64	0.00	0.00	0.00	0.93	0.00
206110379_1	1.00	0.04	0.02	0.00	0.94	0.00	0.00	0.00	0.79	0.00
206110379_2	1.00	0.36	0.28	0.00	0.36	0.00	0.00	0.00	0.80	0.00
206110379_4	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.49	0.00
206110379_5	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.46	0.00
22803188_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.07	0.00
22803188_3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
22803188_4	1.00	0.00	0.00	0.00	0.97	0.03	0.00	0.00	0.00	0.00
22803188_5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
22926618_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.85	0.00
22926618_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
22926618_3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.80	0.00
22926618_4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
22926629	1.00	0.00	0.00	0.00	0.08	0.92	0.00	0.00	0.09	0.00
23116769	1.00	0.00	0.00	0.00	0.46	0.00	0.00	0.54	0.13	0.00
23116814	1.00	0.01	0.00	0.00	0.99	0.00	0.00	0.00	0.59	0.00
23116826	1.00	0.00	0.31	0.00	0.69	0.00	0.00	0.00	0.97	0.00
23405543	1.00	0.06	0.55	0.00	0.39	0.00	0.00	0.00	0.68	0.00
23405563	1.00	0.09	0.00	0.00	0.91	0.00	0.00	0.00	0.78	0.00
57466689_1	1.00	0.01	0.05	0.00	0.94	0.00	0.00	0.00	0.99	0.00
57466741	1.00	0.04	0.00	0.00	0.83	0.12	0.00	0.00	0.85	0.00
57466813	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
C1	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C1_1	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C1_2	1.00	0.04	0.27	0.00	0.69	0.00	0.00	0.00	0.19	0.00
C10	1.00	0.38	0.00	0.00	0.45	0.16	0.00	0.00	0.73	0.00
C108	1.00	0.00	0.05	0.00	0.42	0.53	0.00	0.00	0.80	0.00
C109	1.00	0.04	0.00	0.00	0.94	0.02	0.00	0.00	0.02	0.00

C11	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C110	1.00	0.05	0.00	0.00	0.00	0.00	0.00	0.95	0.00	0.00
C111	1.00	0.04	0.01	0.00	0.85	0.00	0.10	0.00	0.07	0.00
C112	1.00	0.06	0.06	0.00	0.71	0.16	0.00	0.00	0.76	0.00
C113	1.00	0.04	0.23	0.00	0.73	0.00	0.00	0.00	0.67	0.00
C12	1.00	0.04	0.32	0.00	0.62	0.02	0.00	0.00	0.32	0.00
C126	1.00	0.96	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C127	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C128	1.00	0.04	0.00	0.00	0.64	0.32	0.00	0.00	0.01	0.00
C129_1	1.00	0.04	0.00	0.00	0.77	0.19	0.00	0.00	0.46	0.00
C129_2	1.00	0.17	0.41	0.00	0.43	0.00	0.00	0.00	0.80	0.00
C13	1.00	0.30	0.12	0.00	0.55	0.03	0.00	0.00	0.70	0.00
C130	1.00	0.04	0.02	0.00	0.95	0.00	0.00	0.00	0.80	0.00
C131	1.00	0.64	0.31	0.00	0.04	0.00	0.00	0.00	0.59	0.00
C141	1.00	0.04	0.00	0.00	0.01	0.95	0.00	0.00	0.05	0.00
C142	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C143	1.00	0.04	0.17	0.00	0.79	0.00	0.00	0.00	0.76	0.00
C144	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C145	1.00	0.05	0.24	0.00	0.71	0.00	0.00	0.00	0.75	0.00
C146	1.00	0.57	0.43	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C147	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C148	1.00	0.16	0.00	0.00	0.83	0.02	0.00	0.00	0.79	0.00
C158	1.00	0.04	0.00	0.00	0.86	0.10	0.00	0.00	0.03	0.00
C159	1.00	0.55	0.00	0.00	0.24	0.21	0.00	0.00	0.77	0.00
C16	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C160	1.00	0.31	0.33	0.00	0.36	0.00	0.00	0.00	0.78	0.00
C161	1.00	0.45	0.00	0.00	0.55	0.00	0.00	0.00	0.80	0.00
C167_2	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.05	0.00
C169	1.00	0.00	0.63	0.00	0.36	0.01	0.00	0.00	0.80	0.00
C17	1.00	0.04	0.56	0.00	0.40	0.00	0.00	0.00	0.30	0.00
C170	1.00	0.01	0.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C176	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C18	1.00	0.15	0.03	0.00	0.82	0.00	0.00	0.00	0.80	0.00
C182	1.00	0.30	0.00	0.00	0.53	0.16	0.00	0.00	0.49	0.00
C185	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C186	1.00	0.04	0.00	0.00	0.85	0.11	0.00	0.00	0.66	0.00
C19	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C193	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C194	1.00	0.04	0.00	0.00	0.93	0.03	0.00	0.00	0.00	0.00
C195	1.00	0.04	0.43	0.00	0.47	0.06	0.00	0.00	0.69	0.00
C196	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C20	1.00	0.64	0.09	0.00	0.27	0.00	0.00	0.00	0.80	0.00
C21	1.00	0.64	0.07	0.00	0.29	0.00	0.00	0.00	0.80	0.00
C22	1.00	0.04	0.66	0.00	0.30	0.00	0.00	0.00	0.80	0.00
C23	1.00	0.04	0.70	0.00	0.26	0.00	0.00	0.00	0.76	0.00
C24	1.00	0.22	0.00	0.00	0.44	0.33	0.00	0.00	0.73	0.00
C25	1.00	0.00	0.64	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C26	1.00	0.07	0.00	0.00	0.93	0.00	0.00	0.00	0.00	0.00
C27	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C28	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C29	1.00	0.04	0.57	0.00	0.39	0.00	0.00	0.00	0.45	0.00
C3	1.00	0.61	0.00	0.00	0.39	0.00	0.00	0.00	0.78	0.00
C30	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C31	1.00	0.05	0.53	0.00	0.41	0.00	0.00	0.00	0.69	0.00
C32	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C33	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C34	1.00	0.04	0.53	0.00	0.43	0.00	0.00	0.00	0.34	0.00
C35	1.00	0.06	0.00	0.00	0.94	0.00	0.00	0.00	0.00	0.00
C37	1.00	0.04	0.00	0.00	0.95	0.01	0.00	0.00	0.02	0.00
C38	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C39	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.01	0.00
C4	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C40	1.00	0.05	0.50	0.00	0.45	0.00	0.00	0.00	0.33	0.00
C41	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C42	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.01	0.00
C44	1.00	0.05	0.22	0.00	0.73	0.00	0.00	0.00	0.52	0.00
C45	1.00	0.62	0.35	0.00	0.03	0.00	0.00	0.00	0.62	0.00
C46	1.00	0.04	0.57	0.00	0.39	0.00	0.00	0.00	0.79	0.00
C47	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C49	1.00	0.59	0.04	0.00	0.38	0.00	0.00	0.00	0.75	0.00
C5	1.00	0.04	0.00	0.00	0.00	0.00	0.00	0.96	0.00	0.00
C50	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.38	0.00
C51	1.00	0.04	0.96	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C52	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C53	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.02	0.00
C54	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.65	0.00
C55	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C56	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00

C57	1.00	0.04	0.40	0.00	0.55	0.00	0.00	0.00	0.33	0.00
C58	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C59	1.00	0.05	0.53	0.00	0.38	0.04	0.00	0.00	0.76	0.00
C6	1.00	0.05	0.57	0.00	0.38	0.00	0.00	0.00	0.80	0.00
C60	1.00	0.06	0.00	0.00	0.93	0.00	0.00	0.00	0.32	0.00
C61	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.28	0.00
C62	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C63	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C65	1.00	0.04	0.57	0.00	0.39	0.00	0.00	0.00	0.80	0.00
C66	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C67	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C68	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.08	0.00
C7	1.00	0.04	0.18	0.00	0.78	0.00	0.00	0.00	0.11	0.00
C70	1.00	0.04	0.01	0.00	0.94	0.01	0.00	0.00	0.05	0.00
C8	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C95	1.00	0.04	0.72	0.00	0.24	0.00	0.00	0.00	0.76	0.00
C96	1.00	0.04	0.13	0.00	0.83	0.00	0.00	0.00	0.71	0.00
C97	1.00	0.27	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00

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Conduit Surcharge Summary
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Conduit	Hours Full Both Ends	Hours Full Upstream	Hours Full Dnstream	Hours Above Full Normal Flow	Hours Capacity Limited
22803188_5	0.01	0.01	8735.19	0.01	0.01
22926618_1	0.01	0.01	13.73	0.01	0.01
22926618_2	0.01	13.73	4.56	0.01	0.01
C30	0.01	0.01	1.11	0.01	0.01
C37	0.01	0.01	1.11	0.01	0.01
C38	0.01	0.29	0.01	2.94	0.01
C42	0.01	7.61	0.30	5.39	0.01
C52	0.01	0.01	0.29	0.01	0.01
C56	0.01	0.01	0.01	0.01	0.01
C58	0.01	23.31	1.11	0.17	0.01
C70	0.01	6.57	30.74	7.05	0.01

D. Results for the non-groundwater component model

Element Count
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Number of rain gages 6
Number of subcatchments ... 125
Number of nodes 126
Number of links 125
Number of pollutants 0
Number of land uses 0

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Raingage Summary
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Name	Data Source	Data Type	Recording Interval
Chicago_3h	Chicago_3h	INTENSITY	5 min.
DailyRainfall_Canning	DailyRainfall_Canning	VOLUME	1440 min.
Florida_Type_II_1mm	Florida_Type_II_1mm	INTENSITY	30 min.
NOAA_Type_A_1mm	NOAA_Type_A_1mm	INTENSITY	6 min.
Precipitation_Net15012018	Precipitation_Net15012018	INTENSITY	30 min.
RainEvent_19072009	RainEvent_19072009	INTENSITY	30 min.

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Subcatchment Summary
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Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	0.37	37.17	52.14	0.5000	DailyRainfall_Canning	J80
S10	0.19	47.08	100.00	0.0500	DailyRainfall_Canning	S43_7
S11	0.16	40.77	100.00	0.0500	DailyRainfall_Canning	J80

S12	0.33	68.95	85.66	0.0500	DailyRainfall_Canning	J9
S13	0.06	70.00	48.57	0.5000	DailyRainfall_Canning	S23_4
S14	0.19	167.22	53.82	3.2000	DailyRainfall_Canning	J9
S15_1	0.08	12.25	38.01	3.8280	DailyRainfall_Canning	S15_10
S15_10	0.09	28.82	37.41	3.8280	DailyRainfall_Canning	J24
S15_12	0.14	30.75	64.07	3.8280	DailyRainfall_Canning	J2312
S15_2	0.78	58.65	65.84	3.8280	DailyRainfall_Canning	J20
S15_3	0.19	48.55	100.00	0.0500	DailyRainfall_Canning	J11
S15_4	0.20	27.15	56.80	3.8280	DailyRainfall_Canning	J17
S15_5	0.68	51.72	67.95	3.8280	DailyRainfall_Canning	J18
S15_6	0.14	35.02	100.00	0.0500	DailyRainfall_Canning	S29_1
S15_7	1.51	114.36	66.60	3.8280	DailyRainfall_Canning	J2181
S15_8	0.06	14.73	37.97	3.8280	DailyRainfall_Canning	J26
S15_9	0.39	41.54	26.28	3.8280	DailyRainfall_Canning	J23
S16	0.06	14.10	100.00	0.0500	DailyRainfall_Canning	J13
S17	0.18	45.40	100.00	0.0500	DailyRainfall_Canning	J2918
S18_2	0.67	67.03	98.67	0.0500	DailyRainfall_Canning	J32
S18_3	0.20	20.30	100.00	0.0500	DailyRainfall_Canning	J30
S18_4	0.23	41.84	100.00	0.5000	DailyRainfall_Canning	J30
S19	0.24	60.15	100.00	0.0500	DailyRainfall_Canning	J28
S2	1.17	276.27	98.79	0.0500	DailyRainfall_Canning	J79
S20	0.07	18.20	100.00	0.0500	DailyRainfall_Canning	J3
S21	0.18	45.73	100.00	0.0500	DailyRainfall_Canning	J26
S22	0.08	152.16	100.00	2.2180	DailyRainfall_Canning	J7
S23	0.13	60.00	58.39	0.5000	DailyRainfall_Canning	J25
S23_1	0.95	167.21	65.32	3.2000	DailyRainfall_Canning	J4
S23_3	0.56	54.50	60.55	3.2000	DailyRainfall_Canning	J12
S23_4	1.17	112.72	56.24	3.2000	DailyRainfall_Canning	J6
S24	0.06	14.90	100.00	0.0500	DailyRainfall_Canning	S15_9
S25	0.11	27.42	100.00	0.0500	DailyRainfall_Canning	J57
S26_1	0.14	23.02	56.39	3.2350	DailyRainfall_Canning	J2787
S26_3	0.96	156.38	60.17	3.2350	DailyRainfall_Canning	J2909
S29_1	0.46	200.89	45.59	3.2400	DailyRainfall_Canning	J9
S29_10	1.84	130.72	55.85	2.9450	DailyRainfall_Canning	J2931
S29_11	0.04	2.73	93.74	2.9450	DailyRainfall_Canning	J2931
S29_12	0.63	44.65	55.88	2.9450	DailyRainfall_Canning	J40
S29_13	0.65	46.11	56.91	2.9450	DailyRainfall_Canning	J35
S29_14	0.80	56.95	54.49	2.9450	DailyRainfall_Canning	J48
S29_15	0.43	101.00	60.75	0.0500	DailyRainfall_Canning	J29_14
S29_17	0.10	23.12	100.00	0.0500	DailyRainfall_Canning	S29_14
S29_2	0.31	261.45	98.90	3.2400	DailyRainfall_Canning	J2754
S29_3	0.83	200.89	59.35	3.2400	DailyRainfall_Canning	J11
S29_5	0.22	15.77	57.60	2.9450	DailyRainfall_Canning	J79
S29_7	0.20	14.58	64.04	2.9450	DailyRainfall_Canning	J63
S29_8	0.63	200.89	65.96	3.2400	DailyRainfall_Canning	J13
S29_9	0.18	13.12	47.15	2.9450	DailyRainfall_Canning	J83
S3	0.40	279.67	38.66	3.3800	DailyRainfall_Canning	S46_5
S30	0.13	29.48	93.35	0.0500	DailyRainfall_Canning	J355
S31	0.06	11.13	90.13	0.0500	DailyRainfall_Canning	J2712
S32	0.13	32.75	100.00	0.0500	DailyRainfall_Canning	J2717
S33	0.24	60.58	100.00	0.0500	DailyRainfall_Canning	J2717
S34	0.36	89.63	100.00	0.0500	DailyRainfall_Canning	J2722
S35	0.33	81.85	100.00	0.0500	DailyRainfall_Canning	J2692
S36	0.04	10.10	100.00	0.0500	DailyRainfall_Canning	J46
S37	0.07	40.06	72.13	3.3800	DailyRainfall_Canning	S46_5
S37_1	0.41	50.92	62.15	2.2180	DailyRainfall_Canning	J7
S37_10	0.05	16.55	13.97	2.2180	DailyRainfall_Canning	J22
S37_11	0.20	25.02	45.49	2.2180	DailyRainfall_Canning	J2510
S37_12	0.08	9.47	29.91	2.2180	DailyRainfall_Canning	J2510
S37_2	0.23	94.45	57.23	2.2180	DailyRainfall_Canning	J4
S37_3	0.14	57.71	46.87	2.2180	DailyRainfall_Canning	J4
S37_4	0.36	44.45	76.39	2.2180	DailyRainfall_Canning	J16
S37_8	0.13	16.37	22.60	2.2180	DailyRainfall_Canning	J1
S38	0.19	46.98	100.00	0.0500	DailyRainfall_Canning	S43_7
S39	0.47	74.72	72.47	0.0500	DailyRainfall_Canning	S63_9
S4	0.40	87.38	100.00	0.0640	DailyRainfall_Canning	J2722
S40	0.18	46.08	98.99	0.0500	DailyRainfall_Canning	S63_9
S41	0.27	68.30	100.00	0.0500	DailyRainfall_Canning	J2931
S42	0.41	102.70	100.00	0.0500	DailyRainfall_Canning	J1040
S43	1.67	236.18	22.43	4.3580	DailyRainfall_Canning	J1969
S43_2	0.55	28.64	25.35	5.2200	DailyRainfall_Canning	J56
S43_4	0.32	16.52	18.77	5.2200	DailyRainfall_Canning	J46
S43_5	0.96	49.81	42.96	5.2200	DailyRainfall_Canning	S43_7
S43_6	0.52	27.16	27.26	5.2200	DailyRainfall_Canning	S43
S43_7	0.60	31.07	56.61	5.2200	DailyRainfall_Canning	J46
S43_9	0.90	46.61	46.85	5.2200	DailyRainfall_Canning	S43
S44	0.71	178.32	100.00	0.0500	DailyRainfall_Canning	S43
S45	0.05	12.43	100.00	0.0500	DailyRainfall_Canning	J2510

S46	0.08	19.32	100.00	0.0500	DailyRainfall_Canning	J7
S46_1	0.56	68.57	54.56	3.3800	DailyRainfall_Canning	J2771
S46_10	0.11	35.10	66.12	3.3800	DailyRainfall_Canning	S63_3
S46_2	0.34	41.71	37.98	3.3800	DailyRainfall_Canning	J2594
S46_3	0.33	101.25	70.86	3.3800	DailyRainfall_Canning	S63_14
S46_4	0.53	64.73	61.82	3.3800	DailyRainfall_Canning	J16
S46_5	0.46	35.97	50.36	3.3800	DailyRainfall_Canning	J2722
S46_6	0.30	36.49	52.18	3.3800	DailyRainfall_Canning	J2678
S46_7	0.53	64.61	67.84	3.3800	DailyRainfall_Canning	J2722
S47	0.22	55.70	100.00	0.0500	DailyRainfall_Canning	J2839
S48	0.12	30.23	100.00	0.0500	DailyRainfall_Canning	J2847
S49	0.15	37.48	100.00	0.0500	DailyRainfall_Canning	J5
S5	0.23	56.48	100.00	0.0500	DailyRainfall_Canning	J63
S50	0.20	49.15	100.00	0.0500	DailyRainfall_Canning	J5
S51	0.18	45.77	100.00	0.0500	DailyRainfall_Canning	J3
S52_1	0.92	59.15	31.47	3.2350	DailyRainfall_Canning	S43
S52_2	0.84	304.44	48.21	2.9450	DailyRainfall_Canning	S43
S52_3	0.26	16.79	61.56	3.2350	DailyRainfall_Canning	J2909
S52_4	0.39	304.44	57.11	2.9450	DailyRainfall_Canning	J70
S52_6	0.86	55.37	73.37	3.2350	DailyRainfall_Canning	J2838
S52_7	0.75	48.08	50.07	3.2350	DailyRainfall_Canning	J2860
S53	0.26	65.65	100.00	0.0500	DailyRainfall_Canning	J4
S54	0.10	25.70	100.00	0.0500	DailyRainfall_Canning	S15_7
S55	0.01	3.05	100.00	0.0500	DailyRainfall_Canning	S15_7
S56	0.07	18.05	100.00	0.0500	DailyRainfall_Canning	S15_7
S57	0.06	200.89	100.00	3.2400	DailyRainfall_Canning	J13
S59	0.11	36.33	97.66	0.0500	DailyRainfall_Canning	J13
S63_1	0.61	180.24	38.35	4.5340	DailyRainfall_Canning	J355
S63_11	0.25	35.18	61.02	4.5340	DailyRainfall_Canning	J2728
S63_12	0.13	32.75	56.27	4.5340	DailyRainfall_Canning	J2822
S63_13	0.43	52.99	48.85	4.5340	DailyRainfall_Canning	J2794
S63_14	0.19	46.55	59.93	4.5340	DailyRainfall_Canning	J2757
S63_15	0.28	28.32	50.73	4.5340	DailyRainfall_Canning	J2709
S63_2	1.20	75.70	26.59	4.5340	DailyRainfall_Canning	J2855
S63_3	0.20	30.85	65.39	4.5340	DailyRainfall_Canning	J2719
S63_4	0.11	11.20	89.58	4.5340	DailyRainfall_Canning	S63_9
S63_5	0.00	5.89	90.88	4.5340	DailyRainfall_Canning	S63_1
S63_6	0.28	180.24	52.71	4.5340	DailyRainfall_Canning	J2785
S63_7	0.08	180.25	35.47	4.5340	DailyRainfall_Canning	J1969
S63_8	0.15	49.90	54.89	4.5340	DailyRainfall_Canning	J2730
S63_9	0.28	34.04	36.18	4.5340	DailyRainfall_Canning	J2785
S7	0.12	30.75	100.00	0.0500	DailyRainfall_Canning	J2757
S8	0.15	36.52	100.00	0.0500	DailyRainfall_Canning	J2755
S9	0.16	39.45	100.00	0.0500	DailyRainfall_Canning	S43_7

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LID Control Summary
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Subcatchment	LID Control	No. of Units	Unit Area	Unit Width	% Area Covered	% Imperv Treated	% Perv Treated
S43	BioSwale	1	16677.00	0.00	100.00	0.00	0.00

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Node Summary
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Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
J1	JUNCTION	13.40	1.00	0.0	
J10	JUNCTION	13.31	1.00	0.0	
J1040	JUNCTION	9.07	2.21	0.0	
J11	JUNCTION	13.02	1.00	0.0	
J12	JUNCTION	17.49	1.00	0.0	
J13	JUNCTION	14.72	1.00	0.0	
J14	JUNCTION	13.16	1.00	0.0	
J1415	JUNCTION	9.71	2.03	0.0	
J15	JUNCTION	13.77	1.00	0.0	
J16	JUNCTION	12.31	1.00	0.0	
J17	JUNCTION	13.64	1.00	0.0	
J1701	JUNCTION	14.30	1.00	0.0	
J1788	JUNCTION	9.08	1.72	0.0	
J18	JUNCTION	13.81	1.00	0.0	
J19	JUNCTION	12.48	1.00	0.0	
J1969	JUNCTION	9.10	1.11	0.0	
J2	JUNCTION	13.18	1.00	0.0	

J20	JUNCTION	13.78	1.00	0.0	
J21	JUNCTION	11.00	2.35	0.0	
J2181	JUNCTION	11.91	1.35	0.0	
J22	JUNCTION	11.50	3.50	0.0	
J2293	JUNCTION	11.60	1.40	0.0	
J23	JUNCTION	11.50	1.50	0.0	
J2312	JUNCTION	11.58	1.42	0.0	
J24	JUNCTION	11.55	1.44	0.0	
J25	JUNCTION	12.36	2.64	0.0	
J2510	JUNCTION	11.21	1.59	0.0	
J2594	JUNCTION	11.02	1.80	0.0	
J26	JUNCTION	13.36	1.00	0.0	
J2678	JUNCTION	10.50	2.15	0.0	
J2692	JUNCTION	10.61	1.87	0.0	
J27	JUNCTION	12.48	1.00	0.0	
J2709	JUNCTION	15.50	0.45	0.0	
J2712	JUNCTION	15.40	0.72	0.0	
J2717	JUNCTION	15.97	0.45	0.0	
J2719	JUNCTION	15.88	0.45	0.0	
J2722	JUNCTION	14.54	0.45	0.0	
J2728	JUNCTION	15.28	0.45	0.0	
J2730	JUNCTION	15.25	0.45	0.0	
J2749	JUNCTION	15.16	0.45	0.0	
J2754	JUNCTION	14.56	1.00	0.0	
J2755	JUNCTION	14.08	1.00	0.0	
J2757	JUNCTION	15.32	0.45	0.0	
J2764	JUNCTION	14.47	1.00	0.0	
J2771	JUNCTION	9.90	1.84	0.0	
J2779	JUNCTION	14.32	1.00	0.0	
J2785	JUNCTION	14.13	0.45	0.0	
J2786	JUNCTION	15.06	0.45	0.0	
J2787	JUNCTION	14.94	1.00	0.0	
J2794	JUNCTION	14.00	1.12	0.0	
J2797	JUNCTION	13.27	0.75	0.0	
J28	JUNCTION	13.29	1.00	0.0	
J2813	JUNCTION	12.42	1.00	0.0	
J2816	JUNCTION	12.29	1.00	0.0	
J2822	JUNCTION	12.93	0.75	0.0	
J2831	JUNCTION	12.64	0.75	0.0	
J2838	JUNCTION	12.29	0.75	0.0	
J2839	JUNCTION	14.09	1.00	0.0	
J2845	JUNCTION	12.62	0.75	0.0	
J2847	JUNCTION	13.58	1.00	0.0	
J2855	JUNCTION	9.01	2.29	0.0	
J2857	JUNCTION	9.64	2.06	0.0	
J2860	JUNCTION	12.49	1.00	0.0	
J2868	JUNCTION	12.78	1.00	0.0	
J2870	JUNCTION	12.80	1.00	0.0	
J2887	JUNCTION	9.57	2.05	0.0	Yes
J2890	JUNCTION	12.90	1.00	0.0	
J2891	JUNCTION	10.00	1.00	0.0	
J29	JUNCTION	12.67	1.00	0.0	
J29_14	JUNCTION	12.00	1.00	0.0	
J2909	JUNCTION	13.48	1.00	0.0	
J2915	JUNCTION	9.20	2.40	0.0	
J2918	JUNCTION	13.56	0.90	0.0	
J2921	JUNCTION	11.28	1.00	0.0	
J2931	JUNCTION	11.87	1.00	0.0	
J2938	JUNCTION	14.36	0.79	0.0	
J3	JUNCTION	13.59	1.00	0.0	
J30	JUNCTION	12.34	1.00	0.0	
J31	JUNCTION	12.66	1.00	0.0	
J32	JUNCTION	12.59	1.00	0.0	
J33	JUNCTION	12.31	1.00	0.0	
J34	JUNCTION	12.13	1.00	0.0	
J35	JUNCTION	11.50	1.00	0.0	
J36	JUNCTION	11.73	1.00	0.0	
J37	JUNCTION	12.21	1.00	0.0	
J38	JUNCTION	12.30	1.00	0.0	
J39	JUNCTION	12.12	1.00	0.0	
J4	JUNCTION	13.79	1.00	0.0	
J40	JUNCTION	11.99	1.00	0.0	
J41	JUNCTION	12.00	1.00	0.0	
J42	JUNCTION	12.24	1.00	0.0	
J43	JUNCTION	12.87	1.00	0.0	
J44	JUNCTION	12.87	1.00	0.0	
J45	JUNCTION	9.30	1.53	0.0	
J46	JUNCTION	9.70	1.40	0.0	Yes

J47	JUNCTION	11.65	1.00	0.0	
J48	JUNCTION	11.51	1.00	0.0	
J49	JUNCTION	9.09	1.83	0.0	
J5	JUNCTION	13.99	1.00	0.0	
J50	JUNCTION	12.20	1.00	0.0	
J52	JUNCTION	11.51	1.00	0.0	
J53	JUNCTION	11.51	1.00	0.0	
J55	JUNCTION	9.69	1.32	0.0	
J56	JUNCTION	13.19	1.00	0.0	
J57	JUNCTION	13.20	1.00	0.0	
J59	JUNCTION	12.50	1.00	0.0	
J6	JUNCTION	13.31	1.00	0.0	
J63	JUNCTION	12.24	1.00	0.0	
J64	JUNCTION	12.80	1.00	0.0	
J65	JUNCTION	11.79	1.00	0.0	
J66	JUNCTION	11.58	1.00	0.0	
J67	JUNCTION	11.92	1.00	0.0	
J68	JUNCTION	12.00	1.00	0.0	
J69	JUNCTION	11.76	1.00	0.0	
J7	JUNCTION	13.34	1.00	0.0	
J70	JUNCTION	12.67	1.00	0.0	
J72	JUNCTION	11.60	1.00	0.0	
J73	JUNCTION	12.86	1.00	0.0	
J78	JUNCTION	12.40	1.00	0.0	
J79	JUNCTION	12.19	1.00	0.0	
J8	JUNCTION	11.34	1.65	0.0	
J80	JUNCTION	11.83	1.00	0.0	
J83	JUNCTION	11.70	1.20	0.0	
J9	JUNCTION	16.37	1.00	0.0	
J355	OUTFALL	8.33	1.30	0.0	Yes
J54	STORAGE	8.80	2.17	0.0	

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Link Summary
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Name	From Node	To Node	Type	Length	%Slope	Roughness
206110366	J2510	J2594	CONDUIT	68.1	0.2791	0.0120
206110379_1	J2312	J24	CONDUIT	23.9	0.1340	0.0120
206110379_2	J8	J2510	CONDUIT	51.4	0.2529	0.0120
206110379_4	J23	J8	CONDUIT	67.9	0.2299	0.0120
206110379_5	J24	J23	CONDUIT	39.6	0.1312	0.0120
22803188_2	J45	J2915	CONDUIT	159.4	0.0627	0.0100
22803188_3	J54	J45	CONDUIT	89.8	0.1670	0.0100
22803188_4	J46	J55	CONDUIT	61.4	0.0163	0.0100
22803188_5	J55	J54	CONDUIT	24.5	3.6397	0.0100
22926618_1	J2915	J1969	CONDUIT	23.8	0.4207	0.0100
22926618_2	J1969	J49	CONDUIT	64.7	0.0155	0.0100
22926618_3	J1040	J2855	CONDUIT	33.6	0.1787	0.0140
22926618_4	J1788	J1040	CONDUIT	50.5	0.0198	0.0140
22926629	J2887	J2915	CONDUIT	19.7	1.8770	0.0270
23116769	J2594	J2678	CONDUIT	67.8	0.2627	0.0120
23116814	J1415	J2857	CONDUIT	21.5	0.3341	0.0120
23116826	J2857	J2887	CONDUIT	27.2	0.2577	0.0120
23405543	J2293	J2312	CONDUIT	8.1	0.2460	0.0120
23405563	J2181	J2293	CONDUIT	111.4	0.2782	0.0120
57466689_1	J2771	J1415	CONDUIT	34.8	0.5399	0.0120
57466741	J2692	J2771	CONDUIT	111.3	0.6378	0.0120
57466813	J2678	J2692	CONDUIT	18.8	1.0237	0.0120
C1	J10	J2	CONDUIT	4.6	2.8478	0.0120
C1_1	J2	J14	CONDUIT	9.0	0.1106	0.0120
C1_2	J14	J1	CONDUIT	58.5	-0.3965	0.0120
C10	J9	J5	CONDUIT	67.9	3.5079	0.0120
C108	J2921	J1969	CONDUIT	21.3	10.3196	0.0120
C109	J2831	J2845	CONDUIT	40.4	0.0421	0.0120
C11	J11	J14	CONDUIT	10.3	-1.3870	0.0120
C110	J2794	J1040	CONDUIT	48.7	9.2155	0.0120
C111	J2785	J2794	CONDUIT	97.3	-0.2466	0.0120
C112	J2717	J2719	CONDUIT	2.5	4.0096	0.0120
C113	J2918	J2909	CONDUIT	49.6	0.2096	0.0120
C12	J1	J7	CONDUIT	51.5	0.1107	0.0120
C126	J2890	J2870	CONDUIT	8.5	1.1745	0.0120
C127	J2816	J2813	CONDUIT	8.6	-1.5125	0.0120
C128	J2722	J2797	CONDUIT	104.3	1.2172	0.0120
C129_1	J2764	J1701	CONDUIT	7.0	2.4213	0.0120
C129_2	J1701	J2847	CONDUIT	42.9	1.6817	0.0120
C13	J12	J9	CONDUIT	67.5	1.6676	0.0120

C130	J2787	J2764	CONDUIT	47.7	0.9808	0.0120
C131	J2870	J2868	CONDUIT	1.7	1.1849	0.0120
C141	J2931	J2921	CONDUIT	13.0	4.5207	0.0120
C142	J2822	J2831	CONDUIT	53.4	0.5560	0.0120
C143	J2712	J2785	CONDUIT	77.2	1.9974	0.0120
C144	J2786	J2794	CONDUIT	10.8	9.9203	0.0120
C145	J2839	J2847	CONDUIT	7.5	6.8596	0.0120
C146	J2779	J1701	CONDUIT	4.4	0.5498	0.0120
C147	J2730	J2749	CONDUIT	16.8	0.5770	0.0120
C148	J2719	J2730	CONDUIT	33.0	1.8783	0.0120
C158	J2860	J2838	CONDUIT	85.2	0.2335	0.0120
C159	J2797	J2822	CONDUIT	5.7	5.9471	0.0120
C16	J13	J2	CONDUIT	107.9	1.4317	0.0120
C160	J2845	J2857	CONDUIT	10.3	30.0988	0.0120
C161	J2728	J2730	CONDUIT	5.6	0.4989	0.0120
C167_2	J47	J2931	CONDUIT	62.2	-0.3604	0.0120
C169	J2838	J1415	CONDUIT	29.5	8.7841	0.0120
C17	J17	J15	CONDUIT	17.3	-0.7497	0.0120
C170	J2813	J1415	CONDUIT	17.5	15.6546	0.0120
C176	J2855	J355	CONDUIT	190.0	0.3579	0.0140
C18	J18	J2293	CONDUIT	9.4	24.2248	0.0120
C182	J2757	J2786	CONDUIT	23.1	1.1206	0.0120
C185	J2868	J2860	CONDUIT	37.4	0.7763	0.0120
C186	J2909	J2868	CONDUIT	76.3	0.9153	0.0120
C19	J20	J17	CONDUIT	8.5	1.6156	0.0120
C193	J2709	J2712	CONDUIT	5.0	1.9932	0.0120
C194	J2749	J2786	CONDUIT	40.7	0.2335	0.0120
C195	J2754	J2764	CONDUIT	7.4	1.2425	0.0120
C196	J2891	J1788	CONDUIT	3.8	5.2209	0.0120
C20	J22	J8	CONDUIT	29.3	0.5459	0.0120
C21	J25	J8	CONDUIT	3.5	32.4388	0.0120
C22	J26	J23	CONDUIT	3.5	63.0111	0.0120
C23	J28	J24	CONDUIT	5.3	34.7854	0.0120
C24	J16	J21	CONDUIT	12.7	10.3694	0.0120
C25	J21	J2678	CONDUIT	29.9	1.6742	0.0120
C26	J27	J19	CONDUIT	1.4	0.0224	0.0120
C27	J30	J29	CONDUIT	9.3	-3.5776	0.0120
C28	J32	J31	CONDUIT	4.0	-1.8226	0.0120
C29	J34	J33	CONDUIT	1.8	-9.5778	0.0120
C3	J4	J3	CONDUIT	40.8	0.4975	0.0120
C30	J36	J35	CONDUIT	38.3	0.6030	0.0120
C31	J38	J37	CONDUIT	32.4	0.2839	0.0120
C32	J40	J39	CONDUIT	20.5	-0.6620	0.0120
C33	J41	J40	CONDUIT	2.0	0.6410	0.0120
C34	J42	J33	CONDUIT	24.6	-0.2842	0.0120
C35	J44	J43	CONDUIT	2.9	0.0103	0.0120
C37	J35	J47	CONDUIT	13.2	-1.1419	0.0120
C38	J52	J48	CONDUIT	3.3	0.0092	0.0120
C39	J37	J50	CONDUIT	31.4	0.0159	0.0120
C4	J5	J6	CONDUIT	79.2	0.8534	0.0120
C40	J39	J38	CONDUIT	19.1	-0.9215	0.0120
C41	J29_14	J40	CONDUIT	5.1	0.2542	0.0120
C42	J53	J52	CONDUIT	1.2	0.0827	0.0120
C44	J57	J56	CONDUIT	17.7	0.0338	0.0120
C45	J59	J19	CONDUIT	11.1	0.1527	0.0120
C46	J33	J47	CONDUIT	69.9	0.9454	0.0120
C47	J63	J42	CONDUIT	4.4	0.0069	0.0120
C49	J19	J33	CONDUIT	65.3	0.2666	0.0120
C5	J7	J2510	CONDUIT	44.9	3.4200	0.0120
C50	J56	J19	CONDUIT	66.2	1.0757	0.0120
C51	J64	J63	CONDUIT	9.0	6.2803	0.0120
C52	J65	J52	CONDUIT	9.7	2.9349	0.0120
C53	J66	J48	CONDUIT	18.5	0.4005	0.0120
C54	J67	J66	CONDUIT	36.2	0.9225	0.0120
C55	J68	J40	CONDUIT	16.7	0.0780	0.0120
C56	J69	J65	CONDUIT	1.9	-1.7813	0.0120
C57	J78	J70	CONDUIT	2.6	-10.5183	0.0120
C58	J72	J35	CONDUIT	1.3	7.6208	0.0120
C59	J50	J67	CONDUIT	19.4	1.4742	0.0120
C6	J15	J2312	CONDUIT	20.2	10.8994	0.0120
C60	J43	J70	CONDUIT	73.6	0.2771	0.0120
C61	J31	J43	CONDUIT	47.8	-0.4329	0.0120
C62	J73	J44	CONDUIT	2.9	-0.4154	0.0120
C63	J48	J36	CONDUIT	58.4	-0.3751	0.0120
C65	J70	J42	CONDUIT	64.4	0.6672	0.0120
C66	J29	J31	CONDUIT	3.7	0.2462	0.0120
C67	J79	J78	CONDUIT	9.1	-2.3432	0.0120
C68	J80	J67	CONDUIT	12.6	-0.7123	0.0120

C7	J6	J1	CONDUIT	17.5	-0.4911	0.0120
C70	J83	J72	CONDUIT	2.5	4.0667	0.0120
C8	J3	J6	CONDUIT	59.9	0.4671	0.0120
C95	J2755	J2860	CONDUIT	73.2	2.1774	0.0120
C96	J2847	J2909	CONDUIT	51.0	0.1960	0.0120
C97	J2938	J2918	CONDUIT	68.4	1.1342	0.0120
22926618_6	J49	J1788	WEIR			

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Cross Section Summary
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Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
206110366	CIRCULAR	1.35	1.43	0.34	1.35	1	3.06
206110379_1	CIRCULAR	1.35	1.43	0.34	1.35	1	2.12
206110379_2	CIRCULAR	1.35	1.43	0.34	1.35	1	2.91
206110379_4	CIRCULAR	1.35	1.43	0.34	1.35	1	2.77
206110379_5	CIRCULAR	1.35	1.43	0.34	1.35	1	2.10
22803188_2	AnvilTransect	0.65	5.53	0.47	11.50	1	8.40
22803188_3	AnvilTransect	0.65	5.53	0.47	11.50	1	13.70
22803188_4	AnvilTransect	0.65	5.53	0.47	11.50	1	4.28
22803188_5	AnvilTransect	0.65	5.53	0.47	11.50	1	63.98
22926618_1	AnvilTransect	0.65	5.53	0.47	11.50	1	21.75
22926618_2	AnvilTransect	0.65	5.53	0.47	11.50	1	4.17
22926618_3	Anvil_Transect2	1.30	7.80	0.48	9.00	1	14.38
22926618_4	Anvil_Transect2	1.30	7.80	0.48	9.00	1	4.79
22926629	PARABOLIC	1.35	1.80	0.51	2.00	1	5.85
23116769	CIRCULAR	1.35	1.43	0.34	1.35	1	2.96
23116814	CIRCULAR	1.35	1.43	0.34	1.35	1	3.34
23116826	CIRCULAR	1.35	1.43	0.34	1.35	1	2.94
23405543	CIRCULAR	1.35	1.43	0.34	1.35	1	2.87
23405563	CIRCULAR	1.35	1.43	0.34	1.35	1	3.05
57466689_1	CIRCULAR	1.35	1.43	0.34	1.35	1	4.25
57466741	CIRCULAR	1.35	1.43	0.34	1.35	1	4.62
57466813	CIRCULAR	1.35	1.43	0.34	1.35	1	5.85
C1	CIRCULAR	1.00	0.79	0.25	1.00	1	4.38
C1_1	CIRCULAR	1.00	0.79	0.25	1.00	1	0.86
C1_2	CIRCULAR	1.00	0.79	0.25	1.00	1	1.64
C10	CIRCULAR	1.00	0.79	0.25	1.00	1	4.87
C108	CIRCULAR	1.00	0.79	0.25	1.00	1	8.35
C109	CIRCULAR	0.75	0.44	0.19	0.75	1	0.25
C11	CIRCULAR	1.00	0.79	0.25	1.00	1	3.06
C110	CIRCULAR	0.75	0.44	0.19	0.75	1	3.66
C111	CIRCULAR	0.45	0.16	0.11	0.45	1	0.15
C112	CIRCULAR	0.45	0.16	0.11	0.45	1	0.62
C113	CIRCULAR	0.75	0.44	0.19	0.75	1	0.55
C12	CIRCULAR	1.00	0.79	0.25	1.00	1	0.86
C126	CIRCULAR	1.00	0.79	0.25	1.00	1	2.82
C127	CIRCULAR	1.00	0.79	0.25	1.00	1	3.19
C128	CIRCULAR	0.45	0.16	0.11	0.45	1	0.34
C129_1	CIRCULAR	1.00	0.79	0.25	1.00	1	4.04
C129_2	CIRCULAR	1.00	0.79	0.25	1.00	1	3.37
C13	CIRCULAR	1.00	0.79	0.25	1.00	1	3.35
C130	CIRCULAR	1.00	0.79	0.25	1.00	1	2.57
C131	CIRCULAR	1.00	0.79	0.25	1.00	1	2.83
C141	CIRCULAR	1.00	0.79	0.25	1.00	1	5.52
C142	CIRCULAR	0.75	0.44	0.19	0.75	1	0.90
C143	CIRCULAR	0.45	0.16	0.11	0.45	1	0.44
C144	CIRCULAR	0.45	0.16	0.11	0.45	1	0.97
C145	CIRCULAR	1.00	0.79	0.25	1.00	1	6.80
C146	CIRCULAR	1.00	0.79	0.25	1.00	1	1.93
C147	CIRCULAR	0.45	0.16	0.11	0.45	1	0.23
C148	CIRCULAR	0.45	0.16	0.11	0.45	1	0.42
C158	CIRCULAR	0.75	0.44	0.19	0.75	1	0.58
C159	CIRCULAR	0.75	0.44	0.19	0.75	1	2.94
C16	CIRCULAR	1.00	0.79	0.25	1.00	1	3.11
C160	CIRCULAR	0.75	0.44	0.19	0.75	1	6.62
C161	CIRCULAR	0.45	0.16	0.11	0.45	1	0.22
C167_2	CIRCULAR	1.00	0.79	0.25	1.00	1	1.56
C169	CIRCULAR	0.75	0.44	0.19	0.75	1	3.58
C17	CIRCULAR	1.00	0.79	0.25	1.00	1	2.25
C170	CIRCULAR	1.00	0.79	0.25	1.00	1	10.28
C176	Anvil_Transect2	1.30	7.80	0.48	9.00	1	20.35
C18	CIRCULAR	1.00	0.79	0.25	1.00	1	12.79
C182	CIRCULAR	0.45	0.16	0.11	0.45	1	0.33
C185	CIRCULAR	1.00	0.79	0.25	1.00	1	2.29

C186	CIRCULAR	1.00	0.79	0.25	1.00	1	2.49
C19	CIRCULAR	1.00	0.79	0.25	1.00	1	3.30
C193	CIRCULAR	0.45	0.16	0.11	0.45	1	0.44
C194	CIRCULAR	0.45	0.16	0.11	0.45	1	0.15
C195	CIRCULAR	1.00	0.79	0.25	1.00	1	2.90
C196	CIRCULAR	1.00	0.79	0.25	1.00	1	5.94
C20	CIRCULAR	1.65	2.14	0.41	1.65	1	7.30
C21	CIRCULAR	1.00	0.79	0.25	1.00	1	14.80
C22	CIRCULAR	1.00	0.79	0.25	1.00	1	20.62
C23	CIRCULAR	1.00	0.79	0.25	1.00	1	15.32
C24	CIRCULAR	1.00	0.79	0.25	1.00	1	8.37
C25	CIRCULAR	1.00	0.79	0.25	1.00	1	3.36
C26	CIRCULAR	1.00	0.79	0.25	1.00	1	0.39
C27	CIRCULAR	1.00	0.79	0.25	1.00	1	4.91
C28	CIRCULAR	1.00	0.79	0.25	1.00	1	3.51
C29	CIRCULAR	1.00	0.79	0.25	1.00	1	8.04
C3	CIRCULAR	1.00	0.79	0.25	1.00	1	1.83
C30	CIRCULAR	1.00	0.79	0.25	1.00	1	2.02
C31	CIRCULAR	1.00	0.79	0.25	1.00	1	1.38
C32	CIRCULAR	1.00	0.79	0.25	1.00	1	2.11
C33	CIRCULAR	1.00	0.79	0.25	1.00	1	2.08
C34	CIRCULAR	1.00	0.79	0.25	1.00	1	1.38
C35	CIRCULAR	1.00	0.79	0.25	1.00	1	0.26
C37	CIRCULAR	1.00	0.79	0.25	1.00	1	2.78
C38	CIRCULAR	1.00	0.79	0.25	1.00	1	0.25
C39	CIRCULAR	1.00	0.79	0.25	1.00	1	0.33
C4	CIRCULAR	1.00	0.79	0.25	1.00	1	2.40
C40	CIRCULAR	1.00	0.79	0.25	1.00	1	2.49
C41	CIRCULAR	1.00	0.79	0.25	1.00	1	1.31
C42	CIRCULAR	1.00	0.79	0.25	1.00	1	0.75
C44	CIRCULAR	1.00	0.79	0.25	1.00	1	0.48
C45	CIRCULAR	1.00	0.79	0.25	1.00	1	1.02
C46	CIRCULAR	1.00	0.79	0.25	1.00	1	2.53
C47	CIRCULAR	1.00	0.79	0.25	1.00	1	0.22
C49	CIRCULAR	1.00	0.79	0.25	1.00	1	1.34
C5	CIRCULAR	1.00	0.79	0.25	1.00	1	4.80
C50	CIRCULAR	1.00	0.79	0.25	1.00	1	2.69
C51	CIRCULAR	1.00	0.79	0.25	1.00	1	6.51
C52	CIRCULAR	1.00	0.79	0.25	1.00	1	4.45
C53	CIRCULAR	1.00	0.79	0.25	1.00	1	1.64
C54	CIRCULAR	1.00	0.79	0.25	1.00	1	2.50
C55	CIRCULAR	1.00	0.79	0.25	1.00	1	0.73
C56	CIRCULAR	1.00	0.79	0.25	1.00	1	3.47
C57	CIRCULAR	1.00	0.79	0.25	1.00	1	8.43
C58	CIRCULAR	1.00	0.79	0.25	1.00	1	7.17
C59	CIRCULAR	1.00	0.79	0.25	1.00	1	3.15
C6	CIRCULAR	1.00	0.79	0.25	1.00	1	8.58
C60	CIRCULAR	1.00	0.79	0.25	1.00	1	1.37
C61	CIRCULAR	1.00	0.79	0.25	1.00	1	1.71
C62	CIRCULAR	1.00	0.79	0.25	1.00	1	1.67
C63	CIRCULAR	1.00	0.79	0.25	1.00	1	1.59
C65	CIRCULAR	1.00	0.79	0.25	1.00	1	2.12
C66	CIRCULAR	1.00	0.79	0.25	1.00	1	1.29
C67	CIRCULAR	1.00	0.79	0.25	1.00	1	3.98
C68	CIRCULAR	1.00	0.79	0.25	1.00	1	2.19
C7	CIRCULAR	1.00	0.79	0.25	1.00	1	1.82
C70	CIRCULAR	1.00	0.79	0.25	1.00	1	5.24
C8	CIRCULAR	1.00	0.79	0.25	1.00	1	1.78
C95	CIRCULAR	1.00	0.79	0.25	1.00	1	3.83
C96	CIRCULAR	1.00	0.79	0.25	1.00	1	1.15
C97	CIRCULAR	0.75	0.44	0.19	0.75	1	1.28

****
Transect Summary
****

Transect Anvil_Transect2
Area:

0.0102	0.0208	0.0318	0.0432	0.0550
0.0672	0.0798	0.0928	0.1062	0.1200
0.1342	0.1488	0.1638	0.1792	0.1950
0.2112	0.2278	0.2448	0.2622	0.2800
0.2982	0.3168	0.3358	0.3552	0.3750
0.3952	0.4158	0.4368	0.4582	0.4800
0.5022	0.5248	0.5478	0.5712	0.5950
0.6192	0.6438	0.6688	0.6942	0.7200

```
            0.7462     0.7728     0.7998     0.8272     0.8550
            0.8832     0.9118     0.9408     0.9702     1.0000
Hrad:
            0.0311     0.0608     0.0894     0.1170     0.1436
            0.1694     0.1944     0.2188     0.2425     0.2657
            0.2884     0.3106     0.3324     0.3538     0.3749
            0.3956     0.4160     0.4361     0.4560     0.4756
            0.4950     0.5142     0.5332     0.5519     0.5706
            0.5890     0.6073     0.6254     0.6435     0.6613
            0.6791     0.6967     0.7143     0.7317     0.7490
            0.7663     0.7834     0.8005     0.8175     0.8344
            0.8512     0.8680     0.8847     0.9013     0.9179
            0.9344     0.9509     0.9673     0.9837     1.0000
Width:
            0.3467     0.3600     0.3733     0.3867     0.4000
            0.4133     0.4267     0.4400     0.4533     0.4667
            0.4800     0.4933     0.5067     0.5200     0.5333
            0.5467     0.5600     0.5733     0.5867     0.6000
            0.6133     0.6267     0.6400     0.6533     0.6667
            0.6800     0.6933     0.7067     0.7200     0.7333
            0.7467     0.7600     0.7733     0.7867     0.8000
            0.8133     0.8267     0.8400     0.8533     0.8667
            0.8800     0.8933     0.9067     0.9200     0.9333
            0.9467     0.9600     0.9733     0.9867     1.0000

Transect AnvilTransect
Area:
            0.0131     0.0264     0.0401     0.0540     0.0682
            0.0827     0.0975     0.1126     0.1279     0.1435
            0.1594     0.1756     0.1921     0.2088     0.2259
            0.2432     0.2608     0.2787     0.2968     0.3153
            0.3340     0.3530     0.3723     0.3919     0.4118
            0.4319     0.4523     0.4730     0.4940     0.5153
            0.5368     0.5587     0.5808     0.6032     0.6259
            0.6488     0.6721     0.6956     0.7194     0.7435
            0.7679     0.7926     0.8175     0.8427     0.8682
            0.8940     0.9201     0.9464     0.9731     1.0000
Hrad:
            0.0271     0.0536     0.0795     0.1050     0.1299
            0.1544     0.1785     0.2021     0.2254     0.2483
            0.2709     0.2931     0.3151     0.3367     0.3581
            0.3792     0.4001     0.4207     0.4411     0.4613
            0.4813     0.5010     0.5206     0.5400     0.5593
            0.5783     0.5972     0.6160     0.6346     0.6531
            0.6714     0.6896     0.7077     0.7257     0.7435
            0.7613     0.7789     0.7964     0.8139     0.8312
            0.8485     0.8656     0.8827     0.8997     0.9166
            0.9334     0.9502     0.9668     0.9835     1.0000
Width:
            0.4887     0.4991     0.5096     0.5200     0.5304
            0.5409     0.5513     0.5617     0.5722     0.5826
            0.5930     0.6035     0.6139     0.6243     0.6348
            0.6452     0.6557     0.6661     0.6765     0.6870
            0.6974     0.7078     0.7183     0.7287     0.7391
            0.7496     0.7600     0.7704     0.7809     0.7913
            0.8017     0.8122     0.8226     0.8330     0.8435
            0.8539     0.8643     0.8748     0.8852     0.8957
            0.9061     0.9165     0.9270     0.9374     0.9478
            0.9583     0.9687     0.9791     0.9896     1.0000


*********************************************************
NOTE: The summary statistics displayed in this report are
based on results found at every computational time step,
not just on results from each reporting time step.
*********************************************************

****************
Analysis Options
****************
Flow Units ............... CMS
Process Models:
  Rainfall/Runoff ........ YES
  RDII ................... NO
  Snowmelt ............... NO
  Groundwater ............ YES
  Flow Routing ........... YES
  Ponding Allowed ........ NO
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  Water Quality ........... NO
Infiltration Method ...... MODIFIED_HORTON
Flow Routing Method ...... DYNWAVE
Surcharge Method ......... EXTRAN
Starting Date ............ 01/01/2014 00:00:00
Ending Date .............. 12/31/2014 00:00:00
Antecedent Dry Days ...... 0.0
Report Time Step ......... 00:01:00
Wet Time Step ............ 00:05:00
Dry Time Step ............ 00:05:00
Routing Time Step ........ 5.00 sec
Variable Time Step ....... YES
Maximum Trials ........... 8
Number of Threads ........ 4
Head Tolerance ........... 0.001500 m

**************************        Volume         Depth
Runoff Quantity Continuity     hectare-m            mm
**************************     ---------       -------
Initial LID Storage ......         0.142         3.136
Total Precipitation ......        30.207       668.200
Evaporation Loss .........         3.486        77.104
Infiltration Loss ........         2.712        59.998
Surface Runoff ...........        24.011       531.147
Final Storage ............         0.142         3.136
Continuity Error (%) .....        -0.007

**************************        Volume        Volume
Flow Routing Continuity        hectare-m      10^6 ltr
**************************     ---------     ---------
Dry Weather Inflow .......         0.000         0.000
Wet Weather Inflow .......        24.011       240.115
Groundwater Inflow .......         0.000         0.000
RDII Inflow ..............         0.000         0.000
External Inflow ..........       263.125      2631.275
External Outflow .........       304.295      3042.978
Flooding Loss ............        17.457       174.570
Evaporation Loss .........         0.671         6.713
Exfiltration Loss ........         0.000         0.000
Initial Stored Volume ....         0.000         0.000
Final Stored Volume ......         0.069         0.687
Continuity Error (%) .....       -12.313

*************************
Highest Continuity Errors
*************************
Node J72 (-11.70%)
Node J35 (-8.63%)
Node J48 (1.07%)

***************************
Time-Step Critical Elements
***************************
Link C58 (51.75%)
Link C42 (26.86%)
Link C38 (6.66%)
Link C57 (4.69%)
Link C56 (3.08%)

*********************************
Highest Flow Instability Indexes
*********************************
Link C42 (35)
Link C58 (25)
Link C70 (23)
Link C56 (16)
Link C38 (15)

*************************
Routing Time Step Summary
*************************
Minimum Time Step           :     0.01 sec
```

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  Average Time Step           :     1.02 sec
  Maximum Time Step           :     5.00 sec
  Percent in Steady State     :    -0.00
  Average Iterations per Step :     2.52
  Percent Not Converging      :     1.30


  **************************
  Subcatchment Runoff Summary
  **************************
```

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10^6 ltr	Peak Runoff CMS	Runoff Coeff
S1	668.20	0.00	76.14	0.38	333.25	258.44	591.69	2.20	0.00	0.886
S10	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.18	0.00	0.934
S11	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.02	0.00	0.934
S12	668.20	0.00	39.50	0.12	538.88	89.78	628.65	2.06	0.00	0.941
S13	668.20	0.00	53.24	0.44	313.21	301.42	614.63	0.38	0.00	0.920
S14	668.20	0.00	57.78	0.39	350.37	259.97	610.34	1.18	0.00	0.913
S15_1	668.20	0.00	86.28	0.49	248.39	333.12	581.51	0.45	0.00	0.870
S15_10	668.20	482.72	91.00	0.49	425.99	633.88	1059.88	0.99	0.00	0.921
S15_12	668.20	0.00	66.47	0.29	406.67	194.83	601.50	0.81	0.00	0.900
S15_2	668.20	0.00	68.87	0.27	413.76	185.33	599.09	4.65	0.01	0.897
S15_3	668.20	0.00	43.91	0.00	624.31	0.00	624.31	1.18	0.00	0.934
S15_4	668.20	0.00	72.00	0.34	359.56	236.33	595.90	1.16	0.00	0.892
S15_5	668.20	0.00	66.47	0.26	427.57	173.95	601.51	4.11	0.00	0.900
S15_6	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.87	0.00	0.934
S15_7	668.20	77.26	65.46	0.27	474.07	205.70	679.77	10.28	0.01	0.912
S15_8	668.20	0.00	85.99	0.49	249.05	333.01	582.06	0.35	0.00	0.871
S15_9	668.20	95.28	113.17	0.56	198.08	451.77	649.85	2.54	0.00	0.851
S16	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.35	0.00	0.934
S17	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.13	0.00	0.934
S18_2	668.20	0.00	45.51	0.01	614.07	8.62	622.69	4.17	0.00	0.932
S18_3	668.20	0.00	45.54	0.00	622.67	0.00	622.67	1.26	0.00	0.932
S18_4	668.20	0.00	27.59	0.00	640.63	0.00	640.63	1.50	0.00	0.959
S19	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.50	0.00	0.934
S2	668.20	0.00	43.21	0.01	617.00	8.00	625.00	7.31	0.01	0.935
S20	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.45	0.00	0.934
S21	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.14	0.00	0.934
S22	668.20	0.00	31.05	0.00	637.33	0.00	637.33	0.49	0.00	0.954
S23	668.20	0.00	53.41	0.35	375.97	238.53	614.50	0.83	0.00	0.920

S23_1	668.20	0.00	61.93	0.28	416.06	189.98	606.04	5.74	0.01	0.907
S23_3	668.20	0.00	54.48	0.33	390.15	223.27	613.42	3.46	0.00	0.918
S23_4	668.20	32.78	70.46	0.35	377.10	253.10	630.20	7.36	0.01	0.899
S24	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.37	0.00	0.934
S25	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.68	0.00	0.934
S26_1	668.20	0.00	66.21	0.37	356.93	244.73	601.66	0.85	0.00	0.900
S26_3	668.20	0.00	61.08	0.34	385.95	220.87	606.82	5.81	0.01	0.908
S29_1	668.20	190.83	76.17	0.46	381.56	400.93	782.48	3.59	0.00	0.911
S29_10	668.20	0.00	65.44	0.37	358.59	243.82	602.41	11.06	0.01	0.902
S29_11	668.20	0.00	30.38	0.06	597.29	40.53	637.82	0.24	0.00	0.955
S29_12	668.20	0.00	65.38	0.37	358.56	243.91	602.47	3.78	0.00	0.902
S29_13	668.20	0.00	63.12	0.36	367.65	237.08	604.74	3.92	0.00	0.905
S29_14	668.20	77.78	67.46	0.39	393.91	284.26	678.16	5.42	0.01	0.909
S29_15	668.20	0.00	32.00	0.35	379.73	256.16	635.88	2.76	0.00	0.952
S29_17	668.20	0.00	42.47	0.00	625.75	0.00	625.75	0.62	0.00	0.936
S29_2	668.20	0.00	30.83	0.01	630.17	7.33	637.50	1.99	0.00	0.954
S29_3	668.20	0.00	63.49	0.34	379.72	224.70	604.42	5.00	0.01	0.905
S29_5	668.20	0.00	65.16	0.34	371.67	231.06	602.73	1.33	0.00	0.902
S29_7	668.20	0.00	61.29	0.30	407.64	198.99	606.63	1.24	0.00	0.908
S29_8	668.20	0.00	43.86	0.29	424.83	199.31	624.14	3.94	0.00	0.934
S29_9	668.20	0.00	84.51	0.41	305.59	277.71	583.30	1.07	0.00	0.873
S3	668.20	0.00	92.62	0.48	251.74	449.34	575.21	2.33	0.00	0.861
S30	668.20	0.00	42.59	0.06	582.46	43.11	625.57	0.80	0.00	0.936
S31	668.20	0.00	39.89	0.09	565.35	62.93	628.28	0.35	0.00	0.940
S32	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.82	0.00	0.934
S33	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.51	0.00	0.934
S34	668.20	0.00	43.95	0.00	624.27	0.00	624.27	2.24	0.00	0.934
S35	668.20	0.00	43.95	0.00	624.27	0.00	624.27	2.04	0.00	0.934
S36	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.25	0.00	0.934
S37	668.20	0.00	38.37	0.24	462.90	166.80	629.70	0.43	0.00	0.942
S37_1	668.20	0.00	47.81	0.32	401.85	218.30	620.14	2.56	0.00	0.928
S37_10	668.20	0.00	135.17	0.65	92.70	440.25	532.95	0.26	0.00	0.798
S37_11	668.20	0.00	72.12	0.44	296.75	299.13	595.88	1.21	0.00	0.892
S37_12	668.20	0.00	106.54	0.54	197.27	364.22	561.49	0.43	0.00	0.840
S37_2	668.20	0.00	69.73	0.34	366.25	231.95	598.20	1.37	0.00	0.895
S37_3	668.20	0.00	73.56	0.45	302.38	291.87	594.25	0.83	0.00	0.889
S37_4	668.20	0.00	35.17	0.20	490.61	142.28	632.89	2.28	0.00	0.947
S37_8	668.20	0.00	121.60	0.58	148.72	397.33	546.06	0.72	0.00	0.817
S38	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.17	0.00	0.934

S39	668.20	0.00	45.64	0.23	458.43	163.93	622.35	2.93	0.00	0.931
S4	668.20	0.00	43.93	0.00	624.29	0.00	624.29	2.49	0.00	0.934
S40	668.20	0.00	43.24	0.01	618.24	6.73	624.97	1.14	0.00	0.935
S41	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.71	0.00	0.934
S42	668.20	0.00	43.95	0.00	624.27	0.00	624.27	2.56	0.00	0.934
S43	668.20	1373.58	423.06	1618.71	0.00	0.00	0.00	0.00	0.00	0.000
S43_2	668.20	0.00	117.21	0.56	167.11	467.01	550.57	3.03	0.00	0.824
S43_4	668.20	0.00	117.33	0.64	116.22	434.02	550.24	1.75	0.00	0.823
S43_5	668.20	0.00	82.87	0.48	271.94	448.90	584.87	5.60	0.01	0.875
S43_6	668.20	0.00	108.69	0.57	173.20	472.35	558.95	2.92	0.00	0.837
S43_7	668.20	1495.78	62.65	0.37	1210.84	1495.62	2101.04	12.55	0.01	0.971
S43_9	668.20	0.00	74.45	0.45	304.71	441.02	593.37	5.32	0.01	0.888
S44	668.20	0.00	43.95	0.00	624.27	0.00	624.27	4.45	0.00	0.934
S45	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.31	0.00	0.934
S46	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.48	0.00	0.934
S46_1	668.20	0.00	68.83	0.38	348.79	250.23	599.02	3.34	0.00	0.896
S46_10	668.20	0.00	42.63	0.29	427.59	197.87	625.46	0.72	0.00	0.936
S46_2	668.20	0.00	86.63	0.49	247.88	333.25	581.13	1.97	0.00	0.870
S46_3	668.20	0.00	38.62	0.25	456.53	172.83	629.37	2.08	0.00	0.942
S46_4	668.20	0.00	63.26	0.32	395.10	209.55	604.65	3.18	0.00	0.905
S46_5	668.20	603.36	67.15	0.42	630.57	573.50	1204.07	5.50	0.01	0.947
S46_6	668.20	0.00	77.36	0.38	335.39	255.11	590.50	1.75	0.00	0.884
S46_7	668.20	0.00	42.10	0.27	436.86	189.03	625.89	3.29	0.00	0.937
S47	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.39	0.00	0.934
S48	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.75	0.00	0.934
S49	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.94	0.00	0.934
S5	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.41	0.00	0.934
S50	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.23	0.00	0.934
S51	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.14	0.00	0.934
S52_1	668.20	0.00	106.21	0.54	196.65	364.81	561.46	5.17	0.01	0.840
S52_2	668.20	0.00	68.22	0.44	308.18	291.42	599.60	5.05	0.01	0.897
S52_3	668.20	0.00	62.47	0.33	389.97	215.45	605.43	1.58	0.00	0.906
S52_4	668.20	0.00	63.40	0.36	368.75	235.79	604.54	2.37	0.00	0.905
S52_6	668.20	0.00	43.71	0.23	467.74	156.55	624.29	5.38	0.01	0.934
S52_7	668.20	0.00	69.36	0.42	322.53	275.92	598.44	4.48	0.00	0.896
S53	668.20	0.00	43.95	0.00	624.27	0.00	624.27	1.64	0.00	0.934
S54	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.64	0.00	0.934
S55	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.08	0.00	0.934
S56	668.20	0.00	43.95	0.00	624.27	0.00	624.27	0.45	0.00	0.934

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  S57                       668.20       0.00      30.94       0.00     637.29       0.00     637.29
0.36     0.00   0.954
  S59                       668.20       0.00      42.42       0.02     610.15      15.64     625.79
0.68     0.00   0.937
  S63_1                     668.20       4.37      85.75       0.49     248.72     337.66     586.39
3.60     0.00   0.872
  S63_11                    668.20       0.00      58.08       0.33     392.79     217.04     609.83
1.52     0.00   0.913
  S63_12                    668.20       0.00      56.29       0.37     361.71     249.89     611.61
0.80     0.00   0.915
  S63_13                    668.20       0.00      69.27       0.43     316.94     281.61     598.55
2.60     0.00   0.896
  S63_14                    668.20    1119.14      54.81       0.34    1057.36     675.00    1732.36
3.23     0.00   0.969
  S63_15                    668.20       0.00      63.94       0.42     328.51     275.39     603.90
1.71     0.00   0.904
  S63_2                     668.20       0.00     109.14       0.58     170.38     388.12     558.51
6.72     0.01   0.836
  S63_3                     668.20     352.67      56.36       0.29     648.21     316.07     964.29
1.96     0.00   0.945
  S63_4                     668.20       0.00      31.06       0.09     570.59      66.51     637.10
0.71     0.00   0.953
  S63_5                     668.20       0.00      29.62       0.08     580.16      58.53     638.70
0.03     0.00   0.956
  S63_6                     668.20       0.00      60.46       0.40     340.61     266.85     607.46
1.72     0.00   0.909
  S63_7                     668.20       0.00      90.12       0.51     230.40     347.36     577.76
0.44     0.00   0.865
  S63_8                     668.20       0.00      73.18       0.36     354.62     240.11     594.73
0.89     0.00   0.890
  S63_9                     668.20    1715.25     102.56       0.50     857.26    1424.01    2281.27
6.37     0.01   0.957
  S7                        668.20       0.00      43.95       0.00     624.27       0.00     624.27
0.77     0.00   0.934
  S8                        668.20       0.00      43.95       0.00     624.27       0.00     624.27
0.91     0.00   0.934
  S9                        668.20       0.00      43.95       0.00     624.27       0.00     624.27
0.99     0.00   0.934


  ************************
  LID Performance Summary
  ************************

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                                          Total      Evap     Infil   Surface    Drain    Initial
Final  Continuity
                                         Inflow      Loss      Loss   Outflow   Outflow   Storage
Storage       Error
  Subcatchment      LID Control             mm        mm        mm        mm        mm        mm
mm           %
  ---------------------------------------------------------------------------------------------------
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  S43               BioSwale           2041.78    423.06   1618.71      0.00      0.00     85.00
85.00       -0.00

  ******************
  Node Depth Summary
  ******************

  ---------------------------------------------------------------------------------
                                  Average  Maximum  Maximum  Time of Max    Reported
                                    Depth    Depth      HGL   Occurrence   Max Depth
  Node                  Type       Meters   Meters   Meters  days hr:min      Meters
  ---------------------------------------------------------------------------------
  J1                    JUNCTION     0.01     0.14    13.54   168  07:17        0.14
  J10                   JUNCTION     0.10     0.24    13.54   168  11:34        0.24
  J1040                 JUNCTION     0.04     0.30     9.37   127  02:16        0.30
  J11                   JUNCTION     0.37     0.52    13.54   168  15:43        0.52
  J12                   JUNCTION     0.00     0.03    17.52   168  07:00        0.03
  J13                   JUNCTION     0.00     0.03    14.75   168  07:12        0.03
  J14                   JUNCTION     0.23     0.38    13.54   168  15:39        0.38
  J1415                 JUNCTION     0.01     0.19     9.90   168  15:11        0.19
  J15                   JUNCTION     0.00     0.02    13.79   168  21:31        0.02
  J16                   JUNCTION     0.00     0.02    12.33   168  14:04        0.02
  J17                   JUNCTION     0.13     0.16    13.80   168  23:38        0.16
  J1701                 JUNCTION     0.00     0.02    14.32   168  10:44        0.02
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J1788	JUNCTION	0.07	0.38	9.46	168	01:56	0.38
J18	JUNCTION	0.00	0.01	13.82	168	18:11	0.01
J19	JUNCTION	0.00	0.04	12.52	168	05:24	0.04
J1969	JUNCTION	0.08	0.76	9.86	168	01:37	0.76
J2	JUNCTION	0.22	0.37	13.54	168	15:35	0.37
J20	JUNCTION	0.00	0.03	13.81	168	18:45	0.03
J21	JUNCTION	0.00	0.03	11.03	168	15:58	0.03
J2181	JUNCTION	0.00	0.06	11.97	168	13:53	0.06
J22	JUNCTION	0.00	0.01	11.51	168	03:49	0.01
J2293	JUNCTION	0.00	0.08	11.68	168	22:04	0.08
J23	JUNCTION	0.01	0.10	11.60	168	20:59	0.10
J2312	JUNCTION	0.01	0.10	11.68	168	18:25	0.10
J24	JUNCTION	0.01	0.11	11.65	168	23:18	0.11
J25	JUNCTION	0.05	0.06	12.41	168	05:25	0.06
J2510	JUNCTION	0.01	0.15	11.36	168	15:08	0.15
J2594	JUNCTION	0.01	0.16	11.18	168	15:09	0.16
J26	JUNCTION	0.00	0.01	13.37	168	18:57	0.01
J2678	JUNCTION	0.33	0.46	10.96	168	15:09	0.46
J2692	JUNCTION	0.01	0.14	10.75	168	15:10	0.14
J27	JUNCTION	0.00	0.04	12.52	168	12:47	0.04
J2709	JUNCTION	0.16	0.19	15.69	168	13:25	0.19
J2712	JUNCTION	0.26	0.29	15.69	168	13:36	0.29
J2717	JUNCTION	0.00	0.02	16.00	168	13:37	0.02
J2719	JUNCTION	0.00	0.03	15.91	168	20:41	0.03
J2722	JUNCTION	0.00	0.07	14.61	168	11:32	0.07
J2728	JUNCTION	0.00	0.03	15.31	168	12:14	0.03
J2730	JUNCTION	0.00	0.05	15.31	168	16:56	0.05
J2749	JUNCTION	0.00	0.07	15.23	168	07:00	0.07
J2754	JUNCTION	0.00	0.02	14.58	168	00:50	0.02
J2755	JUNCTION	0.00	0.01	14.10	168	11:42	0.01
J2757	JUNCTION	0.00	0.04	15.36	168	01:57	0.04
J2764	JUNCTION	0.00	0.02	14.49	168	15:43	0.02
J2771	JUNCTION	0.01	0.14	10.04	168	18:00	0.14
J2779	JUNCTION	0.00	0.00	14.32	0	00:00	0.00
J2785	JUNCTION	0.23	0.32	14.45	168	17:32	0.32
J2786	JUNCTION	0.00	0.03	15.10	168	07:11	0.03
J2787	JUNCTION	0.00	0.01	14.95	168	10:55	0.01
J2794	JUNCTION	0.35	0.41	14.41	168	12:11	0.41
J2797	JUNCTION	0.00	0.04	13.31	168	18:42	0.04
J28	JUNCTION	0.00	0.01	13.29	168	12:17	0.01
J2813	JUNCTION	0.00	0.00	12.42	0	00:00	0.00
J2816	JUNCTION	0.00	0.00	12.29	0	00:00	0.00
J2822	JUNCTION	0.00	0.07	13.00	168	14:49	0.07
J2831	JUNCTION	0.01	0.10	12.74	168	11:46	0.10
J2838	JUNCTION	0.00	0.05	12.34	168	18:10	0.05
J2839	JUNCTION	0.00	0.01	14.11	168	19:29	0.01
J2845	JUNCTION	0.00	0.03	12.65	168	12:28	0.03
J2847	JUNCTION	0.00	0.05	13.63	168	15:00	0.05
J2855	JUNCTION	0.04	0.27	9.28	127	02:26	0.27
J2857	JUNCTION	0.01	0.21	9.85	168	15:11	0.21
J2860	JUNCTION	0.01	0.10	12.59	168	15:09	0.10
J2868	JUNCTION	0.00	0.06	12.84	168	21:35	0.06
J2870	JUNCTION	0.00	0.04	12.84	168	15:25	0.04
J2887	JUNCTION	0.03	0.24	9.81	241	02:11	0.24
J2890	JUNCTION	0.00	0.00	12.90	0	00:00	0.00
J2891	JUNCTION	0.00	0.00	10.00	0	00:00	0.00
J29	JUNCTION	0.19	0.25	12.93	168	17:00	0.25
J29_14	JUNCTION	0.29	0.35	12.35	168	22:22	0.35
J2909	JUNCTION	0.00	0.05	13.53	168	15:25	0.05
J2915	JUNCTION	0.02	0.59	9.79	127	01:37	0.59
J2918	JUNCTION	0.02	0.04	13.61	168	11:21	0.04
J2921	JUNCTION	0.02	0.10	11.39	286	08:44	0.10
J2931	JUNCTION	0.03	0.13	12.00	286	08:44	0.11
J2938	JUNCTION	0.00	0.00	14.36	0	00:00	0.00
J3	JUNCTION	0.00	0.06	13.65	168	11:18	0.06
J30	JUNCTION	0.51	0.58	12.93	168	17:00	0.58
J31	JUNCTION	0.20	0.26	12.93	168	17:00	0.26
J32	JUNCTION	0.27	0.33	12.93	168	17:00	0.33
J33	JUNCTION	0.00	0.07	12.38	168	18:37	0.07
J34	JUNCTION	0.17	0.25	12.38	168	14:16	0.25
J35	JUNCTION	0.40	1.00	12.50	89	05:45	1.00
J36	JUNCTION	0.18	0.49	12.22	285	20:06	0.44
J37	JUNCTION	0.01	0.08	12.29	168	22:22	0.08
J38	JUNCTION	0.00	0.05	12.35	168	09:59	0.05
J39	JUNCTION	0.17	0.23	12.35	168	19:33	0.23
J4	JUNCTION	0.00	0.05	13.85	168	11:19	0.05
J40	JUNCTION	0.30	0.37	12.35	168	09:45	0.37
J41	JUNCTION	0.29	0.56	12.56	151	23:12	0.41

J42	JUNCTION	0.07	0.18	12.41	168	18:38	0.18
J43	JUNCTION	0.00	0.05	12.92	168	18:32	0.05
J44	JUNCTION	0.00	0.05	12.92	168	18:35	0.05
J45	JUNCTION	0.03	0.48	9.78	127	02:26	0.48
J46	JUNCTION	0.03	0.16	9.86	174	16:30	0.16
J47	JUNCTION	0.25	0.61	12.26	286	08:44	0.58
J48	JUNCTION	0.39	0.60	12.10	282	08:26	0.56
J49	JUNCTION	0.09	0.71	9.80	168	01:56	0.71
J5	JUNCTION	0.00	0.05	14.04	168	19:06	0.05
J50	JUNCTION	0.00	0.03	12.24	168	22:23	0.03
J52	JUNCTION	0.39	1.00	12.51	98	02:01	1.00
J53	JUNCTION	0.39	1.00	12.51	88	08:04	1.00
J55	JUNCTION	0.01	0.11	9.80	127	02:29	0.10
J56	JUNCTION	0.00	0.03	13.22	168	14:13	0.03
J57	JUNCTION	0.00	0.03	13.23	168	23:09	0.03
J59	JUNCTION	0.00	0.02	12.52	168	14:34	0.02
J6	JUNCTION	0.09	0.24	13.55	168	07:18	0.24
J63	JUNCTION	0.07	0.18	12.41	168	18:38	0.18
J64	JUNCTION	0.00	0.00	12.80	0	00:00	0.00
J65	JUNCTION	0.12	0.83	12.63	282	08:26	0.63
J66	JUNCTION	0.32	0.54	12.12	282	08:27	0.54
J67	JUNCTION	0.02	0.20	12.11	262	18:22	0.20
J68	JUNCTION	0.29	0.35	12.35	168	22:23	0.35
J69	JUNCTION	0.15	0.90	12.66	282	08:26	0.75
J7	JUNCTION	0.00	0.07	13.41	168	07:18	0.07
J70	JUNCTION	0.00	0.07	12.74	168	17:00	0.07
J72	JUNCTION	0.30	1.00	12.60	88	06:30	1.00
J73	JUNCTION	0.01	0.06	12.92	168	19:32	0.06
J78	JUNCTION	0.26	0.34	12.74	168	17:00	0.34
J79	JUNCTION	0.46	0.55	12.74	168	17:00	0.55
J8	JUNCTION	0.01	0.10	11.44	168	18:15	0.10
J80	JUNCTION	0.10	0.35	12.18	262	18:22	0.33
J83	JUNCTION	0.21	1.20	12.90	88	08:16	1.20
J9	JUNCTION	0.00	0.04	16.40	168	16:00	0.04
J355	OUTFALL	0.02	0.21	8.54	127	02:26	0.21
J54	STORAGE	0.67	0.98	9.78	127	02:29	0.98

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Node Inflow Summary
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Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min		Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
J1	JUNCTION	0.001	0.047	168	15:37	0.725	43.3	0.000
J10	JUNCTION	0.000	0.000	168	00:41	0	0.112	0.122
J1040	JUNCTION	0.003	0.994	168	01:57	2.56	1.56e+03	0.006
J11	JUNCTION	0.007	0.007	168	12:20	6.18	6.29	0.020
J12	JUNCTION	0.004	0.004	168	07:45	3.46	3.46	0.001
J13	JUNCTION	0.006	0.006	168	07:10	5.34	5.34	-0.007
J14	JUNCTION	0.000	0.012	168	15:42	0	12.2	0.041
J1415	JUNCTION	0.000	0.127	168	15:10	0	116	0.000
J15	JUNCTION	0.000	0.006	168	23:38	0	5.81	-0.000
J16	JUNCTION	0.006	0.006	168	11:25	5.46	5.46	0.004
J17	JUNCTION	0.001	0.006	168	16:09	1.16	5.81	0.011
J1701	JUNCTION	0.000	0.003	168	09:42	0	2.84	-0.005
J1788	JUNCTION	0.000	1.178	168	01:48	0	1.53e+03	-0.003
J18	JUNCTION	0.005	0.005	168	17:10	4.11	4.11	0.003
J19	JUNCTION	0.000	0.004	168	17:45	0	3.73	-0.004
J1969	JUNCTION	0.001	5.722	168	01:26	0.44	2.26e+03	0.136
J2	JUNCTION	0.000	0.006	168	21:54	0	6.01	0.120
J20	JUNCTION	0.005	0.005	168	17:55	4.65	4.65	0.000
J21	JUNCTION	0.000	0.006	168	10:10	0	5.46	-0.004
J2181	JUNCTION	0.011	0.011	168	15:15	10.3	10.3	-0.001
J22	JUNCTION	0.000	0.000	168	03:10	0.256	0.256	0.013
J2293	JUNCTION	0.000	0.016	168	16:56	0	14.4	0.000
J23	JUNCTION	0.003	0.030	168	18:55	2.54	27.5	-0.002
J2312	JUNCTION	0.001	0.023	168	22:10	0.814	21	-0.000
J24	JUNCTION	0.001	0.026	168	20:59	0.986	23.5	-0.000
J25	JUNCTION	0.001	0.001	168	06:15	0.827	0.827	0.040
J2510	JUNCTION	0.002	0.085	168	15:08	1.95	77.3	-0.000
J2594	JUNCTION	0.002	0.087	168	15:08	1.97	79.3	-0.000
J26	JUNCTION	0.002	0.002	168	12:28	1.49	1.49	0.017
J2678	JUNCTION	0.002	0.095	168	15:09	1.75	86.5	0.004

J2692	JUNCTION	0.002	0.097	168	15:10	2.04	88.6	-0.000	
J27	JUNCTION	0.000	0.000	168	02:35	0	0.0141	0.013	
J2709	JUNCTION	0.002	0.002	168	06:55	1.71	1.89	-0.059	
J2712	JUNCTION	0.000	0.002	168	13:26	0.351	2.24	-0.074	
J2717	JUNCTION	0.002	0.002	168	12:30	2.33	2.33	-0.000	
J2719	JUNCTION	0.002	0.005	168	11:46	1.96	4.29	0.000	
J2722	JUNCTION	0.015	0.015	168	12:40	13.5	13.5	-0.000	
J2728	JUNCTION	0.002	0.002	168	07:30	1.52	1.52	-0.000	
J2730	JUNCTION	0.001	0.007	168	11:05	0.89	6.71	-0.000	
J2749	JUNCTION	0.000	0.007	168	11:17	0	6.71	0.000	
J2754	JUNCTION	0.002	0.002	168	04:50	1.99	1.99	0.000	
J2755	JUNCTION	0.001	0.001	168	12:30	0.912	0.912	0.007	
J2757	JUNCTION	0.004	0.004	168	07:10	3.99	3.99	0.001	
J2764	JUNCTION	0.000	0.003	168	23:45	0	2.84	-0.002	
J2771	JUNCTION	0.004	0.100	168	15:10	3.34	91.9	0.000	
J2779	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2785	JUNCTION	0.009	0.011	168	20:05	8.08	10.2	0.041	
J2786	JUNCTION	0.000	0.011	168	07:10	0	10.7	-0.000	
J2787	JUNCTION	0.001	0.001	168	11:15	0.848	0.848	0.006	
J2794	JUNCTION	0.003	0.025	168	12:11	2.6	23.4	0.008	
J2797	JUNCTION	0.000	0.015	168	23:12	0	13.5	0.000	
J28	JUNCTION	0.002	0.002	168	12:30	1.5	1.5	0.002	
J2813	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2816	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2822	JUNCTION	0.001	0.016	168	11:54	0.801	14.3	-0.001	
J2831	JUNCTION	0.000	0.016	168	11:03	0	14.3	-0.005	
J2838	JUNCTION	0.006	0.026	168	18:10	5.38	24.3	-0.001	
J2839	JUNCTION	0.001	0.001	168	12:30	1.39	1.39	0.000	
J2845	JUNCTION	0.000	0.016	168	18:27	0	14.3	0.008	
J2847	JUNCTION	0.001	0.005	168	23:40	0.755	4.98	0.002	
J2855	JUNCTION	0.008	0.981	127	02:24	6.72	1.56e+03	0.001	
J2857	JUNCTION	0.000	0.142	168	15:11	0	131	0.001	
J2860	JUNCTION	0.005	0.020	168	21:35	4.48	18.9	0.001	
J2868	JUNCTION	0.000	0.015	168	15:25	0	13.5	-0.000	
J2870	JUNCTION	0.000	0.000	127	00:09	0	0.0057	0.010	
J2887	JUNCTION	0.001	0.143	168	15:11	31.4	163	0.018	
J2890	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J2891	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J29	JUNCTION	0.000	0.003	168	17:01	0	3.29	0.026	
J29_14	JUNCTION	0.003	0.019	308	03:51	2.76	3.23	0.011	
J2909	JUNCTION	0.008	0.015	168	15:55	7.39	13.5	-0.002	
J2915	JUNCTION	0.000	4.199	168	01:27	0	1.86e+03	0.014	
J2918	JUNCTION	0.001	0.001	168	12:30	1.13	1.13	0.017	
J2921	JUNCTION	0.000	0.170	286	08:44	0	243	0.022	
J2931	JUNCTION	0.014	0.199	286	08:44	13	244	0.491	
J2938	JUNCTION	0.000	0.000	0	00:00	0	0	0.000	ltr
J3	JUNCTION	0.002	0.012	168	12:29	1.6	11.2	-0.002	
J30	JUNCTION	0.003	0.003	168	22:11	2.77	2.97	0.060	
J31	JUNCTION	0.000	0.007	168	17:01	0	7.54	0.039	
J32	JUNCTION	0.004	0.004	168	22:50	4.17	4.45	0.008	
J33	JUNCTION	0.000	0.026	168	16:09	0	24.4	0.001	
J34	JUNCTION	0.000	0.000	299	00:25	0	0.0596	0.290	
J35	JUNCTION	0.004	7.860	325	06:50	3.92	1.12e+03	-7.942	
J36	JUNCTION	0.000	0.913	215	12:49	0	425	0.160	
J37	JUNCTION	0.000	0.007	168	09:59	0	6.53	0.001	
J38	JUNCTION	0.000	0.007	168	19:33	0	6.53	-0.001	
J39	JUNCTION	0.000	0.007	168	19:33	0	7.34	0.025	
J4	JUNCTION	0.010	0.010	168	12:30	9.57	9.57	-0.001	
J40	JUNCTION	0.004	0.280	317	09:28	3.78	9.76	0.130	
J41	JUNCTION	0.000	0.284	151	23:12	0	0.888	-0.884	
J42	JUNCTION	0.000	0.022	168	17:00	0	20.7	0.005	
J43	JUNCTION	0.000	0.007	168	18:35	0	6.96	0.006	
J44	JUNCTION	0.000	0.000	127	23:04	0	0.0422	0.004	
J45	JUNCTION	0.000	0.933	174	16:32	0	1.13e+03	-0.013	
J46	JUNCTION	0.941	0.941	174	16:30	1.14e+03	1.14e+03	0.001	
J47	JUNCTION	0.000	1.562	298	00:51	0	765	0.136	
J48	JUNCTION	0.006	2.708	359	05:53	5.42	488	1.079	
J49	JUNCTION	0.000	2.706	168	01:28	0	1.68e+03	0.181	
J5	JUNCTION	0.002	0.013	168	14:25	2.16	12.5	-0.002	
J50	JUNCTION	0.000	0.007	168	22:22	0	6.53	0.001	
J52	JUNCTION	0.000	8.588	244	09:54	0	347	-0.811	
J53	JUNCTION	0.000	3.245	359	05:53	0	95.8	-8.294	
J55	JUNCTION	0.000	0.941	174	16:30	0	1.14e+03	0.001	
J56	JUNCTION	0.004	0.004	168	14:08	3.03	3.72	-0.004	
J57	JUNCTION	0.001	0.001	168	12:30	0.685	0.685	0.001	
J59	JUNCTION	0.000	0.000	168	02:35	0	0.00281	0.018	
J6	JUNCTION	0.008	0.034	168	15:00	7.36	31	0.009	
J63	JUNCTION	0.003	0.003	168	15:15	2.65	2.78	0.007	

J64	JUNCTION	0.000	0.000	0	00:00	0	0	0.000 ltr
J65	JUNCTION	0.000	1.016	282	08:26	0	80.6	0.529
J66	JUNCTION	0.000	0.199	282	08:26	0	139	-0.176
J67	JUNCTION	0.000	0.109	262	18:21	0	38.7	0.566
J68	JUNCTION	0.000	0.005	223	22:00	0	1.06	0.145
J69	JUNCTION	0.000	0.571	298	23:09	0	26.1	0.778
J7	JUNCTION	0.004	0.051	168	07:17	3.54	46.7	0.000
J70	JUNCTION	0.003	0.019	168	18:32	2.37	18	-0.002
J72	JUNCTION	0.000	9.786	347	12:42	0	582	-10.478
J73	JUNCTION	0.000	0.000	127	23:05	0	0.0201	0.071
J78	JUNCTION	0.000	0.009	168	18:08	0	8.78	0.011
J79	JUNCTION	0.009	0.009	168	13:20	8.64	8.76	0.018
J8	JUNCTION	0.000	0.032	168	17:41	0	28.6	-0.001
J80	JUNCTION	0.004	0.054	262	18:22	3.22	10.8	0.517
J83	JUNCTION	0.001	3.373	201	16:44	1.07	172	-52.850
J9	JUNCTION	0.007	0.011	168	15:51	6.83	10.3	-0.001
J355	OUTFALL	0.052	1.030	127	02:26	1.48e+03	3.04e+03	0.000
J54	STORAGE	0.000	1.570	127	02:32	0	1.14e+03	0.005

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Node Surcharge Summary
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Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
J35	JUNCTION	1.08	0.000	0.000
J49	JUNCTION	0.04	0.007	1.121
J52	JUNCTION	0.12	0.000	0.000
J53	JUNCTION	5.66	0.000	0.000
J72	JUNCTION	23.41	0.000	0.000
J83	JUNCTION	10.35	0.200	0.000

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Node Flooding Summary
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Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CMS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 ltr	Maximum Ponded Depth Meters
J35	1.08	4.309	100 01:02	7.582	0.000
J52	0.12	4.998	244 09:54	1.522	0.000
J53	5.66	2.528	359 05:53	9.825	0.000
J72	23.41	5.944	174 00:31	186.797	0.000
J83	2.66	1.684	276 03:06	8.901	0.000

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Storage Volume Summary
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Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
J54	0.448	10	0	0	0.952	22	127 02:29	0.933

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Outfall Loading Summary
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Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
J355	100.00	0.092	1.030	3042.965

System	100.00	0.092	1.030	3042.965

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Link Flow Summary
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Link	Type	Maximum |Flow| CMS	Time of Max Occurrence days	hr:min	Maximum |Veloc| m/sec	Max/ Full Flow	Max/ Full Depth
206110366	CONDUIT	0.085	168	15:08	0.91	0.03	0.12
206110379_1	CONDUIT	0.023	168	18:43	0.46	0.01	0.08
206110379_2	CONDUIT	0.032	168	15:54	0.46	0.01	0.09
206110379_4	CONDUIT	0.030	168	17:41	0.64	0.01	0.07
206110379_5	CONDUIT	0.026	168	18:55	0.52	0.01	0.08
22803188_2	CHANNEL	0.967	127	00:09	0.92	0.12	0.82
22803188_3	CHANNEL	0.933	174	16:32	0.88	0.07	0.63
22803188_4	CHANNEL	0.941	174	16:30	1.43	0.22	0.20
22803188_5	CHANNEL	1.570	127	02:32	0.60	0.02	0.58
22926618_1	CHANNEL	4.817	168	01:26	1.05	0.22	0.95
22926618_2	CHANNEL	2.706	168	01:28	0.52	0.65	1.00
22926618_3	CHANNEL	0.976	127	02:24	0.95	0.07	0.22
22926618_4	CHANNEL	0.971	168	01:57	0.77	0.20	0.26
22926629	CONDUIT	0.154	142	07:25	1.55	0.03	0.30
23116769	CONDUIT	0.087	168	15:09	0.96	0.03	0.11
23116814	CONDUIT	0.127	168	15:11	0.99	0.04	0.14
23116826	CONDUIT	0.142	168	15:11	1.00	0.05	0.16
23405543	CONDUIT	0.016	168	18:43	0.37	0.01	0.07
23405563	CONDUIT	0.011	168	13:56	0.38	0.00	0.05
57466689_1	CONDUIT	0.100	168	15:10	1.01	0.02	0.12
57466741	CONDUIT	0.097	168	15:10	1.24	0.02	0.10
57466813	CONDUIT	0.095	168	15:10	1.52	0.02	0.09
C1	CONDUIT	0.000	168	00:41	0.00	0.00	0.30
C1_1	CONDUIT	0.006	169	00:04	0.03	0.01	0.37
C1_2	CONDUIT	0.012	168	15:37	0.08	0.01	0.26
C10	CONDUIT	0.011	168	14:25	0.90	0.00	0.04
C108	CONDUIT	0.172	286	08:44	5.52	0.02	0.41
C109	CONDUIT	0.016	168	18:27	0.86	0.06	0.08
C11	CONDUIT	0.007	168	15:44	0.02	0.00	0.45
C110	CONDUIT	0.025	168	12:11	2.38	0.01	0.06
C111	CONDUIT	0.011	168	18:09	0.17	0.07	0.44
C112	CONDUIT	0.002	168	11:46	0.64	0.00	0.06
C113	CONDUIT	0.001	168	11:25	0.14	0.00	0.05
C12	CONDUIT	0.047	168	07:17	1.02	0.05	0.11
C126	CONDUIT	0.000	0	00:00	0.00	0.00	0.02
C127	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
C128	CONDUIT	0.015	168	23:12	1.37	0.04	0.12
C129_1	CONDUIT	0.003	168	09:42	0.70	0.00	0.02
C129_2	CONDUIT	0.003	168	21:12	0.40	0.00	0.04
C13	CONDUIT	0.004	168	07:00	0.53	0.00	0.03
C130	CONDUIT	0.001	168	10:55	0.31	0.00	0.02
C131	CONDUIT	0.000	169	00:05	0.03	0.00	0.05
C141	CONDUIT	0.170	286	08:44	3.46	0.03	0.11
C142	CONDUIT	0.016	168	11:03	0.57	0.02	0.11
C143	CONDUIT	0.002	168	13:32	0.04	0.01	0.38
C144	CONDUIT	0.011	168	07:11	0.15	0.01	0.49
C145	CONDUIT	0.001	168	11:41	0.22	0.00	0.03
C146	CONDUIT	0.000	0	00:00	0.00	0.00	0.01
C147	CONDUIT	0.007	168	11:17	0.55	0.03	0.14
C148	CONDUIT	0.005	168	11:04	0.61	0.01	0.10
C158	CONDUIT	0.020	168	18:10	0.91	0.04	0.10
C159	CONDUIT	0.015	168	11:54	1.05	0.00	0.07
C16	CONDUIT	0.006	168	07:12	0.05	0.00	0.20
C160	CONDUIT	0.016	168	10:52	0.54	0.00	0.15
C161	CONDUIT	0.002	168	07:02	0.23	0.01	0.09
C167_2	CONDUIT	0.199	286	08:44	0.87	0.13	0.35
C169	CONDUIT	0.026	168	18:10	0.63	0.01	0.15
C17	CONDUIT	0.006	168	23:38	0.18	0.00	0.09
C170	CONDUIT	0.000	0	00:00	0.00	0.00	0.09
C176	CHANNEL	0.979	127	02:26	1.15	0.05	0.18
C18	CONDUIT	0.005	168	16:24	0.37	0.00	0.05
C182	CONDUIT	0.004	168	07:10	0.77	0.01	0.08
C185	CONDUIT	0.015	168	21:35	0.50	0.01	0.08
C186	CONDUIT	0.015	168	14:48	0.84	0.01	0.06
C19	CONDUIT	0.005	168	16:09	0.13	0.00	0.10

C193	CONDUIT	0.002	168	10:27	0.02	0.00	0.54
C194	CONDUIT	0.007	168	13:19	0.71	0.05	0.11
C195	CONDUIT	0.002	168	02:00	0.56	0.00	0.02
C196	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
C20	CONDUIT	0.000	168	03:42	0.06	0.00	0.03
C21	CONDUIT	0.001	168	05:33	0.16	0.00	0.05
C22	CONDUIT	0.002	168	10:55	0.16	0.00	0.05
C23	CONDUIT	0.002	168	12:03	0.11	0.00	0.06
C24	CONDUIT	0.006	168	10:10	1.07	0.00	0.03
C25	CONDUIT	0.006	168	10:02	0.04	0.00	0.25
C26	CONDUIT	0.000	168	02:35	0.07	0.00	0.04
C27	CONDUIT	0.003	168	17:01	0.01	0.00	0.42
C28	CONDUIT	0.004	168	20:49	0.02	0.00	0.30
C29	CONDUIT	0.000	299	00:25	0.01	0.00	0.16
C3	CONDUIT	0.010	168	10:52	0.59	0.01	0.06
C30	CONDUIT	0.913	215	12:49	3.89	0.45	0.65
C31	CONDUIT	0.007	168	09:59	0.31	0.01	0.07
C32	CONDUIT	0.007	168	19:33	0.04	0.00	0.30
C33	CONDUIT	0.284	151	23:12	1.69	0.14	0.43
C34	CONDUIT	0.022	168	22:33	0.39	0.02	0.12
C35	CONDUIT	0.000	127	23:04	0.09	0.00	0.05
C37	CONDUIT	1.562	298	00:51	4.62	0.56	0.69
C38	CONDUIT	2.687	359	05:53	4.31	10.78	0.78
C39	CONDUIT	0.007	168	22:22	0.38	0.02	0.06
C4	CONDUIT	0.013	168	13:52	0.20	0.01	0.15
C40	CONDUIT	0.007	168	19:33	0.10	0.00	0.14
C41	CONDUIT	0.022	308	03:51	0.11	0.02	0.36
C42	CONDUIT	7.800	244	09:54	19.48	10.44	0.98
C44	CONDUIT	0.001	168	02:32	0.16	0.00	0.03
C45	CONDUIT	0.000	168	02:35	0.03	0.00	0.03
C46	CONDUIT	0.026	168	12:12	0.22	0.01	0.30
C47	CONDUIT	0.003	168	17:01	0.03	0.01	0.18
C49	CONDUIT	0.004	168	05:24	0.30	0.00	0.06
C5	CONDUIT	0.051	168	07:18	1.99	0.01	0.07
C50	CONDUIT	0.004	168	11:25	0.51	0.00	0.04
C51	CONDUIT	0.000	0	00:00	0.00	0.00	0.09
C52	CONDUIT	1.016	282	08:26	5.40	0.23	0.72
C53	CONDUIT	0.197	357	13:09	0.59	0.12	0.54
C54	CONDUIT	0.116	262	18:22	0.63	0.05	0.34
C55	CONDUIT	0.005	223	22:00	0.03	0.01	0.36
C56	CONDUIT	0.571	298	23:09	5.83	0.16	0.87
C57	CONDUIT	0.009	168	17:01	0.08	0.00	0.20
C58	CONDUIT	7.831	363	02:10	13.81	1.09	0.98
C59	CONDUIT	0.007	168	22:23	0.59	0.00	0.10
C6	CONDUIT	0.006	168	16:38	0.33	0.00	0.06
C60	CONDUIT	0.007	168	18:32	0.39	0.01	0.06
C61	CONDUIT	0.007	168	17:01	0.09	0.00	0.16
C62	CONDUIT	0.000	127	23:05	0.07	0.00	0.06
C63	CONDUIT	0.283	357	13:09	1.01	0.18	0.46
C65	CONDUIT	0.019	168	17:00	0.35	0.01	0.12
C66	CONDUIT	0.003	168	17:01	0.11	0.00	0.26
C67	CONDUIT	0.009	168	18:08	0.03	0.00	0.44
C68	CONDUIT	0.055	262	18:22	0.56	0.02	0.26
C7	CONDUIT	0.034	168	13:16	0.32	0.02	0.19
C70	CONDUIT	8.162	164	11:41	>50.00	1.56	1.00
C8	CONDUIT	0.012	168	11:00	0.16	0.01	0.15
C95	CONDUIT	0.001	168	11:09	0.06	0.00	0.06
C96	CONDUIT	0.005	168	11:54	0.35	0.00	0.05
C97	CONDUIT	0.000	0	00:00	0.00	0.00	0.02
22926618_6	WEIR	1.178	168	01:48			1.00

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Flow Classification Summary
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Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class: Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
206110366	1.00	0.04	0.31	0.00	0.65	0.00	0.00	0.00	0.74	0.00
206110379_1	1.00	0.04	0.05	0.00	0.91	0.00	0.00	0.00	0.79	0.00
206110379_2	1.00	0.35	0.29	0.00	0.36	0.00	0.00	0.00	0.78	0.00
206110379_4	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.49	0.00
206110379_5	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.46	0.00
22803188_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.04	0.00
22803188_3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.98	0.00

22803188_4	1.00	0.00	0.00	0.00	0.97	0.03	0.00	0.00	0.00	0.00
22803188_5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
22926618_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.88	0.00
22926618_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
22926618_3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.80	0.00
22926618_4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
22926629	1.00	0.00	0.00	0.00	0.06	0.94	0.00	0.00	0.07	0.00
23116769	1.00	0.04	0.00	0.00	0.32	0.00	0.00	0.64	0.00	0.00
23116814	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.46	0.00
23116826	1.00	0.00	0.40	0.00	0.60	0.00	0.00	0.00	0.78	0.00
23405543	1.00	0.09	0.54	0.00	0.37	0.00	0.00	0.00	0.71	0.00
23405563	1.00	0.14	0.00	0.00	0.86	0.00	0.00	0.00	0.65	0.00
57466689_1	1.00	0.04	0.04	0.00	0.92	0.00	0.00	0.00	0.79	0.00
57466741	1.00	0.04	0.00	0.00	0.84	0.12	0.00	0.00	0.49	0.00
57466813	1.00	0.04	0.00	0.00	0.00	0.00	0.00	0.96	0.00	0.00
C1	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C1_1	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C1_2	1.00	0.04	0.27	0.00	0.69	0.00	0.00	0.00	0.18	0.00
C10	1.00	0.39	0.00	0.00	0.45	0.16	0.00	0.00	0.75	0.00
C108	1.00	0.00	0.05	0.00	0.39	0.56	0.00	0.00	0.80	0.00
C109	1.00	0.04	0.00	0.00	0.94	0.02	0.00	0.00	0.00	0.00
C11	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C110	1.00	0.05	0.00	0.00	0.00	0.00	0.00	0.95	0.00	0.00
C111	1.00	0.04	0.01	0.00	0.84	0.00	0.11	0.00	0.08	0.00
C112	1.00	0.06	0.06	0.00	0.71	0.16	0.00	0.00	0.76	0.00
C113	1.00	0.04	0.23	0.00	0.73	0.00	0.00	0.00	0.68	0.00
C12	1.00	0.04	0.32	0.00	0.63	0.02	0.00	0.00	0.32	0.00
C126	1.00	0.96	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C127	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C128	1.00	0.04	0.00	0.00	0.64	0.32	0.00	0.00	0.01	0.00
C129_1	1.00	0.04	0.00	0.00	0.77	0.19	0.00	0.00	0.44	0.00
C129_2	1.00	0.17	0.39	0.00	0.44	0.00	0.00	0.00	0.80	0.00
C13	1.00	0.30	0.12	0.00	0.55	0.03	0.00	0.00	0.70	0.00
C130	1.00	0.04	0.04	0.00	0.92	0.00	0.00	0.00	0.80	0.00
C131	1.00	0.64	0.31	0.00	0.04	0.00	0.00	0.00	0.58	0.00
C141	1.00	0.04	0.00	0.00	0.00	0.95	0.00	0.00	0.03	0.00
C142	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C143	1.00	0.04	0.10	0.00	0.86	0.00	0.00	0.00	0.76	0.00
C144	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C145	1.00	0.05	0.25	0.00	0.71	0.00	0.00	0.00	0.76	0.00
C146	1.00	0.56	0.44	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C147	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C148	1.00	0.15	0.00	0.00	0.83	0.02	0.00	0.00	0.79	0.00
C158	1.00	0.04	0.00	0.00	0.86	0.11	0.00	0.00	0.00	0.00
C159	1.00	0.57	0.00	0.00	0.22	0.21	0.00	0.00	0.77	0.00
C16	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C160	1.00	0.40	0.24	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C161	1.00	0.45	0.00	0.00	0.55	0.00	0.00	0.00	0.80	0.00
C167_2	1.00	0.04	0.01	0.00	0.96	0.00	0.00	0.00	0.05	0.00
C169	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C17	1.00	0.04	0.56	0.00	0.40	0.00	0.00	0.00	0.20	0.00
C170	1.00	0.04	0.96	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C176	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
C18	1.00	0.20	0.01	0.00	0.79	0.00	0.00	0.00	0.79	0.00
C182	1.00	0.31	0.00	0.00	0.52	0.17	0.00	0.00	0.48	0.00
C185	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C186	1.00	0.04	0.00	0.00	0.85	0.11	0.00	0.00	0.64	0.00
C19	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C193	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C194	1.00	0.04	0.00	0.00	0.93	0.03	0.00	0.00	0.00	0.00
C195	1.00	0.04	0.43	0.00	0.47	0.06	0.00	0.00	0.69	0.00
C196	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C20	1.00	0.64	0.09	0.00	0.27	0.00	0.00	0.00	0.80	0.00
C21	1.00	0.64	0.07	0.00	0.29	0.00	0.00	0.00	0.80	0.00
C22	1.00	0.04	0.66	0.00	0.30	0.00	0.00	0.00	0.80	0.00
C23	1.00	0.04	0.71	0.00	0.25	0.00	0.00	0.00	0.76	0.00
C24	1.00	0.22	0.00	0.00	0.44	0.33	0.00	0.00	0.71	0.00
C25	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C26	1.00	0.07	0.00	0.00	0.93	0.00	0.00	0.00	0.00	0.00
C27	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C28	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C29	1.00	0.04	0.57	0.00	0.39	0.00	0.00	0.00	0.45	0.00
C3	1.00	0.61	0.00	0.00	0.39	0.00	0.00	0.00	0.75	0.00
C30	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C31	1.00	0.05	0.53	0.00	0.41	0.00	0.00	0.00	0.64	0.00
C32	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C33	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C34	1.00	0.04	0.49	0.00	0.47	0.00	0.00	0.00	0.31	0.00

C35	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C37	1.00	0.04	0.00	0.00	0.95	0.01	0.00	0.00	0.02	0.00
C38	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C39	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C4	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C40	1.00	0.05	0.50	0.00	0.45	0.00	0.00	0.00	0.34	0.00
C41	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C42	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.01	0.00
C44	1.00	0.05	0.23	0.00	0.72	0.00	0.00	0.00	0.47	0.00
C45	1.00	0.61	0.36	0.00	0.03	0.00	0.00	0.00	0.62	0.00
C46	1.00	0.04	0.56	0.00	0.39	0.00	0.00	0.00	0.79	0.00
C47	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C49	1.00	0.57	0.04	0.00	0.39	0.00	0.00	0.00	0.75	0.00
C5	1.00	0.04	0.00	0.00	0.00	0.00	0.00	0.96	0.00	0.00
C50	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.38	0.00
C51	1.00	0.04	0.96	0.00	0.00	0.00	0.00	0.00	0.00	0.00
C52	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C53	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.02	0.00
C54	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.65	0.00
C55	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C56	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C57	1.00	0.04	0.40	0.00	0.56	0.00	0.00	0.00	0.33	0.00
C58	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C59	1.00	0.05	0.53	0.00	0.38	0.04	0.00	0.00	0.76	0.00
C6	1.00	0.08	0.55	0.00	0.37	0.00	0.00	0.00	0.80	0.00
C60	1.00	0.06	0.00	0.00	0.94	0.00	0.00	0.00	0.32	0.00
C61	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.28	0.00
C62	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C63	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C65	1.00	0.04	0.57	0.00	0.39	0.00	0.00	0.00	0.80	0.00
C66	1.00	0.05	0.00	0.00	0.95	0.00	0.00	0.00	0.00	0.00
C67	1.00	0.04	0.00	0.00	0.96	0.00	0.00	0.00	0.00	0.00
C68	1.00	0.04	0.01	0.00	0.95	0.00	0.00	0.00	0.08	0.00
C7	1.00	0.04	0.14	0.00	0.82	0.00	0.00	0.00	0.08	0.00
C70	1.00	0.04	0.01	0.00	0.94	0.01	0.00	0.00	0.05	0.00
C8	1.00	0.04	0.60	0.00	0.36	0.00	0.00	0.00	0.80	0.00
C95	1.00	0.04	0.71	0.00	0.25	0.00	0.00	0.00	0.76	0.00
C96	1.00	0.04	0.13	0.00	0.83	0.00	0.00	0.00	0.73	0.00
C97	1.00	0.27	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00

****
Conduit Surcharge Summary
****

Conduit	Hours Full: Both Ends	Hours Full: Upstream	Hours Full: Dnstream	Hours Above Full Normal Flow	Hours Capacity Limited
22803188_5	0.01	0.01	8713.78	0.01	0.01
22926618_1	0.01	0.01	23.94	0.01	0.01
22926618_2	12.57	23.94	22.14	0.01	2.38
C30	0.01	0.01	1.04	0.01	0.01
C37	0.01	0.01	1.04	0.01	0.01
C38	0.01	0.27	0.01	2.96	0.01
C42	0.01	7.78	0.27	5.39	0.01
C52	0.01	0.01	0.27	0.01	0.01
C58	0.01	23.33	1.04	0.15	0.01
C70	0.01	6.61	30.86	7.15	0.01

Analysis begun on: Thu Feb 13 00:42:43 2020
Analysis ended on: Thu Feb 13 01:39:37 2020

Thank you in advance for any feedback you could provide.

From: SWMM-USERS On Behalf Of Robert Dickinson
Sent: Friday, February 28, 2020 03:22 AM [UTC]
Subject: Groundwater results interpretation

A sample as Stephen suggests would be ideal. It looks like based on no groundwater flow and less evaporation that you have the GW table too high and no evaporation in your GW. Your LID seems inactive as you have the same initial and final storage. If you cannot post your whole model a look at the input

echo from the report file might help. Your infiltration is practically the same. It looks as if you have effectively a nonactive GW component.

From: SWMM-USERS On Behalf Of Stephen Jarman
Sent: Friday, February 28, 2020 01:07 AM [UTC]
Subject: Groundwater results interpretation

H Belen,
Please can you open up your input file in notepad and select all / copy & paste the contents into an email to the swmm list. It's much easier to debug the issue if we can open it in swmm. If you have big external timeseries its better to send these as separate emails.

From: SWMM-USERS On Behalf Of Belen Aguirre
Sent: Friday, February 28, 2020 01:01 AM [UTC]
Subject: Groundwater results interpretation

Good morning everyone,

I am calibrating my first SWMM model with groundwater interaction and I am having some troubles interpreting my results. The study area is on asmall urban sub-catchment (46 hec), with sandy soils, high groundwater table and a wetland in the centre. 43% of the area are roofs (routed to pervious areas or to the drainage network) and 7% are roads (routed to drainage system). 25% is considered sand and the rest trees (3.5%), grass (2.9%) and water(1.5%).
When I run the build-up model with groundwater and without groundwater components for a whole year rainfall my results differ very little.

In the model that has Groundwater components:

```
  **************************        Volume         Depth
  Runoff Quantity Continuity     hectare-m            mm
  **************************     ---------       -------
  Initial LID Storage ......         0.142         3.136
  Total Precipitation ......        30.207       668.200
  Evaporation Loss .........         3.483        77.054
  Infiltration Loss ........         2.712        60.000
  Surface Runoff ...........        24.013       531.196
  Final Storage ............         0.142         3.136
  Continuity Error (%) .....        -0.008

  **************************        Volume         Depth
  Groundwater Continuity         hectare-m            mm
  **************************     ---------       -------
  Initial Storage ..........       219.516      5949.824
  Infiltration .............         2.712        73.511
  Upper Zone ET ............         8.162       221.221
  Lower Zone ET ............         0.004         0.115
  Deep Percolation .........         0.538        14.582
  Groundwater Flow .........         3.733       101.179
  Final Storage ............       209.775      5685.815
  Continuity Error (%) .....         0.007

  **************************        Volume        Volume
  Flow Routing Continuity        hectare-m      10^6 ltr
  **************************     ---------     ---------
  Dry Weather Inflow .......         0.000         0.000
  Wet Weather Inflow .......        24.013       240.137
  Groundwater Inflow .......         3.733        37.327
  RDII Inflow ..............         0.000         0.000
  External Inflow ..........       263.125      2631.275
  External Outflow .........       308.064      3080.675
  Flooding Loss ............        17.360       173.601
  Evaporation Loss .........         0.673         6.727
  Exfiltration Loss ........         0.000         0.000
  Initial Stored Volume ....         0.000         0.000
  Final Stored Volume ......         0.068         0.678
```

In the model without groundwater connection:

```
  **************************        Volume         Depth
  Runoff Quantity Continuity     hectare-m            mm
  **************************     ---------       -------
  Initial LID Storage ......         0.142         3.136
  Total Precipitation ......        30.207       668.200
  Evaporation Loss .........         3.486        77.104
```

```
  Infiltration Loss ........          2.712        59.998
  Surface Runoff ...........         24.011       531.147
  Final Storage ............          0.142         3.136
  Continuity Error (%) .....         -0.007

  **************************        Volume        Volume
  Flow Routing Continuity         hectare-m      10^6 ltr
  **************************      ---------     ---------
  Dry Weather Inflow .......          0.000         0.000
  Wet Weather Inflow .......         24.011       240.115
  Groundwater Inflow .......          0.000         0.000
  RDII Inflow ..............          0.000         0.000
  External Inflow ..........        263.125      2631.275
  External Outflow .........        304.295      3042.978
  Flooding Loss ............         17.457       174.570
  Evaporation Loss .........          0.671         6.713
  Exfiltration Loss ........          0.000         0.000
  Initial Stored Volume ....          0.000         0.000
  Final Stored Volume ......          0.069         0.687
```

It probably makes sense that I have more evaporation without groundwater interaction since there is more water on the surface exposed for evaporation. Still, I do not understand why can runoff be slightly higher with than without groundwater components. The variation seems to occur at the beginning of each event. Could it be that the subsurface gets saturated and discharges to the outlet node, while when not considering groundwater the infiltrated water is retained in the soil?

Does someone has any experience modelling groundwater within urban subcatchments? Every feedback, advice or comment of its expected behaviour would be highly appreciated!
Thank you very much!


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*************************************************************
* To sign off, email to:   listserv@listserv.uoguelph.ca *
* In the body of the message type: signoff swmm-users  *
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