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Passaic Valley Sewerage Commissioners

Passaic Valley Sewerage Commissioners
Response to Request for Information
USEPA, Region 2

Item No. 10.a
PVSC Report

Document order #36

946510001

Passaic Valley Sewerage Commissioners
Response to Request for Information
USEPA, Region 2

Passaic Valley Sewera PVSC Report Item No. 10.a

COMBINED SEW... FACILITY PLAN

PHASE I

Volume 1

System, Water Quality & Alternative Control Analyses and Recommendations for the Lower Passaic River

PASSAIC VALLEY SEWERAGE COMMISSIONERS

Richard M. Giacomarro, Sr.	–	Chairman
Isaac Thomas, Jr.	–	Vice Chairman
Thomas J. Cifelli	–	Commissioner
Vincent Corrado, Sr.	–	Commissioner
Robert J. Davenport	–	Commissioner
Joseph M. Keegan	–	Commissioner
Charles A. Lagos	–	Commissioner
Carmine T. Perrapato	–	Executive Director

1983

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

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Passaic Valley Sewerage Commissioners

COMBINED SEWER OVERFLOW FACILITY PLAN

PHASE I

Volume 1

Passaic Valley Sewerage Commissioners'
Combined Sewer Overflow Facility Plan

PASSAIC VALLEY SEWERAGE COMMISSIONERS

Richard M. Giacomarro, Sr.	– Chairman
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Joseph M. Keegan	– Commissioner
Charles A. Lagos	– Commissioner
Carmine T. Perrapato	– Executive Director

1983

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Environmental and Hydraulic Engineers

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Environmental and Hydraulic Engineers

Eugene J. DeStefano, P.E., L.S.
Vice President

December 28, 1983

Passaic Valley Sewerage Commissioners
600 Wilson Avenue
Newark, New Jersey 07105

Attention: Mr. Carmine Perrapato
Executive Director

Reference: Combined Sewer Overflow
Facility Plan-Phase I

Gentlemen:

We are pleased to submit our report upon Phase I of the Combined Sewer Overflow Facility Plan for the PVSC District, in accordance with our agreement dated October 15, 1980. The report has been separated into three volumes, each of which covers a specific area:

Volume 1 - The Alternative Analysis
Volume 2 - The Modeling Analysis
Volume 3 - Environmental Inventory & Assessment

We recommend that the Commissioners proceed with Phase II of the Facility Plan which includes a detailed analysis and design of alternative control measures. Although the modeling analysis has shown that the Commissioners' Combined Sewer Overflows do not have a significant impact upon stream C-BOD and dissolved oxygen, there are areas wherein the improved operation and control of the overflow regulators could provide greater flexibility in line and plant operations. Additional recommendations have been made which are essential for the improvement of water quality within the Lower Passaic River but which fall beyond the scope of the original Facility Plan.

Accordingly, we recommend that the results of the Phase I Facility Plan, as reported herein be transmitted to the state and federal regulatory agencies for their review and comment. Specific recommendations made within the Facility Plan would have regional implications and would require state coordination.

We, of course, would be pleased to assist the Commissioners in the coordination of Phase II of the Facility Plan, including professional engineering services in accordance with our agreement with the Commissioners.

We would be pleased to discuss the scheduling of the Phase II portion of the Facility Plan at your convenience, as well as any comments concerning this report.

Very truly yours,

ELSON T. KILLAM ASSOCIATES, INC.

Eugene J. DeStefano, P.E./L.S.

EJD:mm
Encl.

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TABLE OF CONTENTS

DESCRIPTION	PAGE NO.
LETTER OF TRANSMITTAL	
LIST OF TABLES	iii
LIST OF FIGURES	v
1. INTRODUCTION	1-1
a. Previous Studies	1-3
b. Combined Sewer Overflow Facility Plan	1-5
2. METHODOLOGY	
a. Hydraulic Data- Lower Passaic River	2-1
River Gaging	2-1
Cross Sectional Velocities	2-4
b. Water Quality Data- Lower Passaic River	2-6
c. Drainage Area Data	2-14
Meteorological Data	2-14
Land Use	2-17
System Information	2-19
d. Alternative Control Analysis	2-21
e. Water Quality Analysis	2-24
Liquid Phase Analysis	2-24
Benthic Core Analysis	2-27
3. RESULTS OF SYSTEM ANALYSIS	
a. River Water Quality Data	3-1
b. Drainage Area Investigations	3-3
Land Use	3-5
System Information	3-6
4. ALTERNATIVE ANALYSIS	4-1
a. Best Management Practices	4-3
Source Management	4-4
Collection System Management	4-7
b. Minor Regulator Reconstruction	4-13
c. Inline Storage	4-33
d. Attenuation of Stormwater	4-47
e. Initial Screening Process	4-53
f. Offline Storage	4-57
g. Physical Treatment	4-76
Swirl & Helical Bend Regulators	4-77
Coarse Screening	4-92
Deep Rock Tunnel	4-100
Instream Aeration	4-102
h. Other Considerations	4-111

946510005

TABLE OF CONTENTS
(Continued)

DESCRIPTION	PAGE NO.
5. AESTHETIC IMPROVEMENTS	
a. Introduction	5-1
b. Passaic River Restoration Project	5-1
c. Alternative Strategies	5-4
Dredging	5-4
Erosion Control	5-7
Removal of Floatables	5-9
Funding	5-11
6. CONCLUSIONS AND RECOMMENDATIONS	6-1
Appendix - Passaic River Water Quality Data	Rear of Report

LIST OF TABLES

NO.	DESCRIPTION	PAGE NO.
2.1	River Gaging Stations	2-3
2.2	Passaic River Water Quality Sampling Stations	2-8
2.3	Combined Sewer Overflow & Storm System - Bypass Monitoring	2-10
2.4	Rain Gaging Stations	2-15
2.5	Primary Drainage Areas (1976 Analysis)	2-18
2.6	Laboratory Analysis Methodoloy	2-26
3.1	Passaic River Water Quality	3-2
3.2	Preliminary Ranking of CSOs (Based on 1976 Analysis)	3-4
4.1	Summary of Street Sweeping Operations within PVSC District (non-combined areas)	4-8
4.2	Results of Preliminary Investigations into Weir Raising/Inline Storage	4-23
4.3	Ultimate C-BOD Loading Discharged from Major Combined Sewer Overflows	4-29
4.4	Ranking of Major CSOs Based Upon C-BOD Loading per Unit Volume Discharged	4-31
4.5	Inline Storage Analysis Upstream Areas	4-45
4.6	Inline Storage Anlaysis Ultimate C-BOD Retained	4-46
4.7	Separate Storm Sewers Discharging to Combined Sewer Systems	4-49
4.8	Results of Initial Screening of Moderate and Minor Overflows	4-54
4.9	Sites Feasible for Offline Storage Preliminary Analysis	4-62

946510006

LIST OF TABLES
(Continued)

NO.	DESCRIPTION	PAGE NO.
4.10	Results of Initial Feasibility Screening for Helical Bend and Swirl Regulators	4-85
4.11	Results of Feasibility Screening for Helical Bend and Swirl Regulators	4-87
4.12	Results of Initial Feasibility Analysis for Coarse Screening with Mechanical Bar Screens	4-97
4.13	Preliminary Coarse Screening Analysis	4-99

946510007

LIST OF FIGURES

FIGURE #	DESCRIPTION	PAGE NO.
1.1	The Passaic River Basin	1-2
1.2	Flow Schematic (Planning Process)	1-9
1.3	Alternative Control Analysis Flow Schematic	1-10
2.1	Combined Sewer Overflow Facility Plan Planning Area	2-2
2.2	Monitoring Stations	2-5
2.3	Rain Gaging Stations	2-16
	Town of Kearny - Land Use	
3.1	Ivy Street Overflow	3-9
3.2	Johnston Avenue Overflow	3-10
	City of Newark - Land Use	
3.3	City Dock Overflow	3-11
3.4	Clay Street Overflow	3-12
3.4A	Sub-area J	3-13
3.4B	Sub-area J1	3-14
3.4C	Sub-area J2	3-15
3.4D	Sub-area K	3-16
3.5	Fourth Avenue Overflow	3-17
3.6	Herbert Place Overflow	3-18
3.7	Jackson Street Overflow	3-19
3.8	Polk Street Overflow	3-20
3.9	Rector Street Overflow	3-21
3.10	Saybrook Place Overflow	3-22
3.11	Verona Avenue Overflow	3-23
	City of Paterson - Land Use	
	Curtis Place Overflow	
3.12A	Sub-area AA	3-24
3.12B	Sub-area A1	3-25
3.13	Hudson Street Overflow	3-26

946510008

LIST OF FIGURES
(Continued)

FIGURE #	DESCRIPTION	PAGE NO.
4.6	Inline Storage Analysis - S. 14th Street-City of Newark	4-37
4.7	Inline Storage Analysis - Duryea Street-City of Newark	4-38
4.8	Inline Storage Analysis - Branch Brook Park-City of Newark	4-39
4.9	Inline Storage Analysis - 8th Avenue-City of Newark	4-40
4.10	Inline Storage Analysis - Saybrook Place-City of Newark	4-41
4.11	Inline Storage Analysis - Forest Street Easement-Town of Kearny	4-42
4.12	Schematic of Storage Volume Analysis	4-43
4.13	Separate Storm Sewer-Combined Sewer Connection	4-48
4.14	Schematic-Hydrobrake® Regulator with Area Detention	4-52
4.15	Offline Storage Reservoir Schematic	4-58
4.16	Preliminary Sites for Offline Storage Curtis Place, Mulberry St, Northwest & W. Broadway Overflows	4-63
4.17	Preliminary Sites for Offline Storage Montgomery & Straight Street Overflows	4-64
4.18	Preliminary Sites for Offline Storage Verona Avenue Overflow	4-65
4.19	Preliminary Sites for Offline Storage Herbert Place Overflow	4-66
4.20	Preliminary Sites for Offline Storage Fourth Avenue Overflow	4-67
4.21	Preliminary Sites for Offline Storage Clay Street Overflow	4-68

946510009

LIST OF FIGURES
(Continued)

FIGURE #	DESCRIPTION	PAGE NO.
4.22	Preliminary Sites for Offline Storage Clay Street Overflow	4-69
4.23	Preliminary Sites for Offline Storage Saybrook & Rector Street Overflows	4-70
4.24	Preliminary Sites for Offline Storage City Dock Overflow	4-71
4.25	Preliminary Sites for Offline Storage Jackson Street Overflow	4-72
4.26	Preliminary Sites for Offline Storage Tappans Street Overflow	4-73
4.27	Preliminary Sites for Offline Storage Marshall & Johnston Street Overflows	4-74
4.28	Preliminary Sites for Offline Storage Hamilton St, Cleveland St. & Harrison Ave. Overflows	4-75
4.29	Isometric View of a Swirl Combined Sewer Overflow Regulator	4-78
4.30	Schematic Helical Bend Combined Sewer Overflow Regulator	4-80
4.31	Hydraulic Profile-Swirl Regulator	4-82
4.32	Schematic-Helical Bend Regulator Bergen Avenue Overflow-Kearny	4-88
4.33	Schematic-Swirl Regulator E. 11th St. Overflow-Paterson	4-89
4.34	Schematic-Helical Bend Regulator Straight St.Overflow-Paterson	4-90
4.35	Schematic-Swirl Regulator Warren St. Overflow-Paterson	4-91
4.36	Isometric View of a Coarse Screening Facility	4-96
4.37	Long Term Analysis-Summer 1981 Dissolved Oxygen Profile	4-105

946510010

LIST OF FIGURES
(Continued)

FIGURE #	DESCRIPTION	PAGE NO.
4.38	Air-Aqua Aeration Station for Utilization within the Lower Passaic River	4-108
4.39	Air-Aqua Aeration System Module Detail	4-109
5.1	Passaic River Restoration Project	5-5
6.0	Pollutant Loadings to the Lower Passaic River During the Summer of 1981	6-1
6.1	Regional Water Management Planning Process - Flow Schematic	6-16

946510011

1. INTRODUCTION

1. INTRODUCTION

The Passaic River is approximately 75 miles long. Its headwaters start north of Millington, New Jersey, located on the Somerset-Morris County boundary line and empty into Newark Bay, approximately 20 miles east of its origin. (See Figure 1.1). From its headwaters it runs 32 miles northeast to the Great Piece Meadows above Caldwell and then due east to the Great Falls of Paterson. The lower Passaic River Basin begins at the Great Falls and terminates approximately 24 miles south where it empties into Newark Bay.

The total drainage area of the Passaic River, including its tributary River System of which the Pompton, Ramapo, Rockaway, Saddle, Wanaque and Whippany Rivers are the largest, is approximately 935 square miles. The lower Passaic River Basin which runs from the Great Falls in Paterson to Newark Bay is approximately 100 square miles. The watershed is flat, wide, densely populated and heavily industrialized. The lower Passaic River Basin is under the jurisdiction of the Passaic Valley Sewerage Commissioners (PVSC). One of their responsibilities is to monitor and maintain water quality within the lower basin of the River.

The Passaic Valley Sewerage Commissioners' service district encompasses twenty eight municipalities within the area of interest with total population of over 1,100,000. Five of these municipalities, the Borough of East Newark, the Towns of Harrison and Kearny and the Cities of Newark and Paterson, (total population of over 517,000), presently maintain combined (storm and sanitary) sewer systems that discharge to the trunk sewer facilities of the Commissioners. Sixteen square miles of approximately twenty four square miles of combined sewer areas served by PVSC are included in the facility plan. These areas are situated in the upper and lower portions of the PVSC Service district.

946510013

portions of the sewer systems, either directly to adjacent storm systems or to nearby streams, ditches, etc. Since these overflows were considered internal to the various municipal combined systems and not related to PVSC discharge permits, they were not included within the Phase I Overflow Analysis.

Measurements were made at all of the active PVSC overflow chambers to determine the quantity and quality of overflow, as well as the relative pollutional load being contributed by each. Measurements were conducted over a one year period (1974-1975) during which 70-80% of all recorded rainfalls produced an overflow. In general, rainfall intensities exceeding 0.04 inches per hour produced an overflow within fifteen to twenty minutes while the duration of the overflow period generally coincided with the time of rainfall and the change in rainfall intensity.

Other factors established through the Phase I Analysis included:

- peak overflow rates ranged from twenty to thirty times the dry weather flow in the collection system tributary to the overflow chamber.
- the volume of overflow was found to be a function of rainfall intensity, duration of the storm and total rainfall.
- generally, the initial overflow contained a higher degree of pollution than found in waste characteristics of the dry weather flow.
- at the start of the overflow suspended solids were generally high, reflecting a flushing action through the sewers.
- BOD and COD were often a function of the non-storm waste characteristics of the tributary area.

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- o suspended solids indicated a wide variation in concentration and appeared to have no correlation with the storm overflow rates and duration.
- o although a measurable pollutional load is exerted upon the Passaic River through the combined sewer overflows, another major pollutional load is generated through the storm water discharge throughout the non-combined sewered areas.

The Phase I Overflow Analysis had determined that the overflows within the combined sewered areas were contributing a measurable loading to the Passaic River, however, this analysis did not evaluate the relative significance of that loading. Originally, the Phase I Analysis had intended to utilize an existing River Model, developed by "Teledyne" under a separate contract for the State of New Jersey, to study the effect of loadings on the River. It was determined however, that because of the model's limitations under actual dynamic conditions, a new dynamic model would be needed before an assessment could be made as to the true effect of the various loadings. The Phase I Analysis therefore recommended the development of a dynamic river model and the compilation of supplemental overflow and river data to study the impact of the Passaic Valley Sewerage Commissioners' overflows on the lower Passaic River.

b. Combined Sewer Overflow Facility Plan

The 1976 Overflow Analysis was conducted to determine only the relative magnitude of pollutants contributed by Combined Sewer Overflows (CSOs) to the lower Passaic River. Although the Phase I Analysis provided valuable information, it did not determine or separate the impact

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of the CSOs from other point and non-point sources. As such, the Combined Sewer Overflow Facilities Plan was initiated to determine the impact of the CSO discharge on the receiving waters (Passaic River) and to compile and evaluate possible alternatives for each overflow on an individual and regional basis.

The Combined Sewer Overflow Facility Plan has been separated into three sections:

1) Development of a Mathematical Model or Engineering "Tool" to Evaluate the Impact of the CSOs Upon the lower Passaic River System.
2) Development of Alternative Considerations for Combined Sewer Overflow Areas.
3) Final Analysis of Alternative Considerations and Selection of an Optimum Facility Plan.

Section 3 of the Facility Plan will be considered for implementation only after state and federal review of the results and recommendations of Section 1 & 2 are completed. In addition, state and federal agencies have added two tasks outside the actual facility planning:

4) Internal Combined Sewer Overflow Monitoring (City of Newark).
5) Toxic Sampling and Analysis.

Both of these sections will be submitted to the State and Commissioners as a separate report.

A primary requirement of the Facility Plan was the development of an engineering "tool" (river model) to evaluate the impact of the CSO discharge upon the Passaic River within the planning area. Specifically, the model was developed to determine the degree of involvement of the CSOs in the violation of water quality standards and to evaluate the effective-

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ness of possible alternatives in rectifying or improving the state of the lower Passaic River.

An existing dynamic network model, (hereafter referred to as MIT-DNM), developed at MIT under the support of the National Coastal Pollution Research Program, has been modified and calibrated under the Facility Plan. The MIT-DNM is a "real time", one dimensional network model which includes both hydrodynamic and ecologic/water quality components. Being a network model, it can integrate riverine, estuarine reaches and tidal tributaries into a compiled system of reaches.

Prior to the adaption of the MIT-DNM, an extensive data base was acquired and compiled so that the verified model accurately represents the condition prevalent in the river. Available information on hydrography and water quality of the Passaic River was obtained from several sources including the Passaic Valley Water Commissioners, the United States Coast & Geodetic Survey, the New Jersey Department of Environmental Protection, as well as data obtained from the Phase I Overflow Analysis. In addition, real time hydraulic and water quality data, obtained by sampling the river (including several major tributaries), were utilized within the calibration and verification of the MIT-DNM model.

The Phase I Facility Plan required the completion and coordination of twenty-four individual, yet interrelated, major tasks. In addition to the development of a dynamic river model, an assessment of the pollutional load exerted by stormwater runoff was required within both combined and separated areas. The Storm Water Management Model (SWMM) developed by EPA was calibrated and verified within the Lower Passaic River Drainage Basin to provide a means of assessing the significance of stormwater discharge.

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The various major tasks included within the Phase I Facility Plan are illustrated in Figure 1.2. This flow schematic provides information upon the approximate sequence of each task group as well as the relationship and interdependence of the various tasks. At the top of the schematic is an indication of the three volumes which comprise the Phase I Report and the various tasks included within each volume.

The sequence of tasks within individual volumes approximates the same order as shown within the schematic. To provide additional information upon the alternative selection process a detailed breakdown of the alternative control screening analysis is included as Figure 1.3. Figures 1.3 and 1.4 can thus be utilized to focus upon specific areas of the Phase I Facility Planning process as reported upon within the three volumes.

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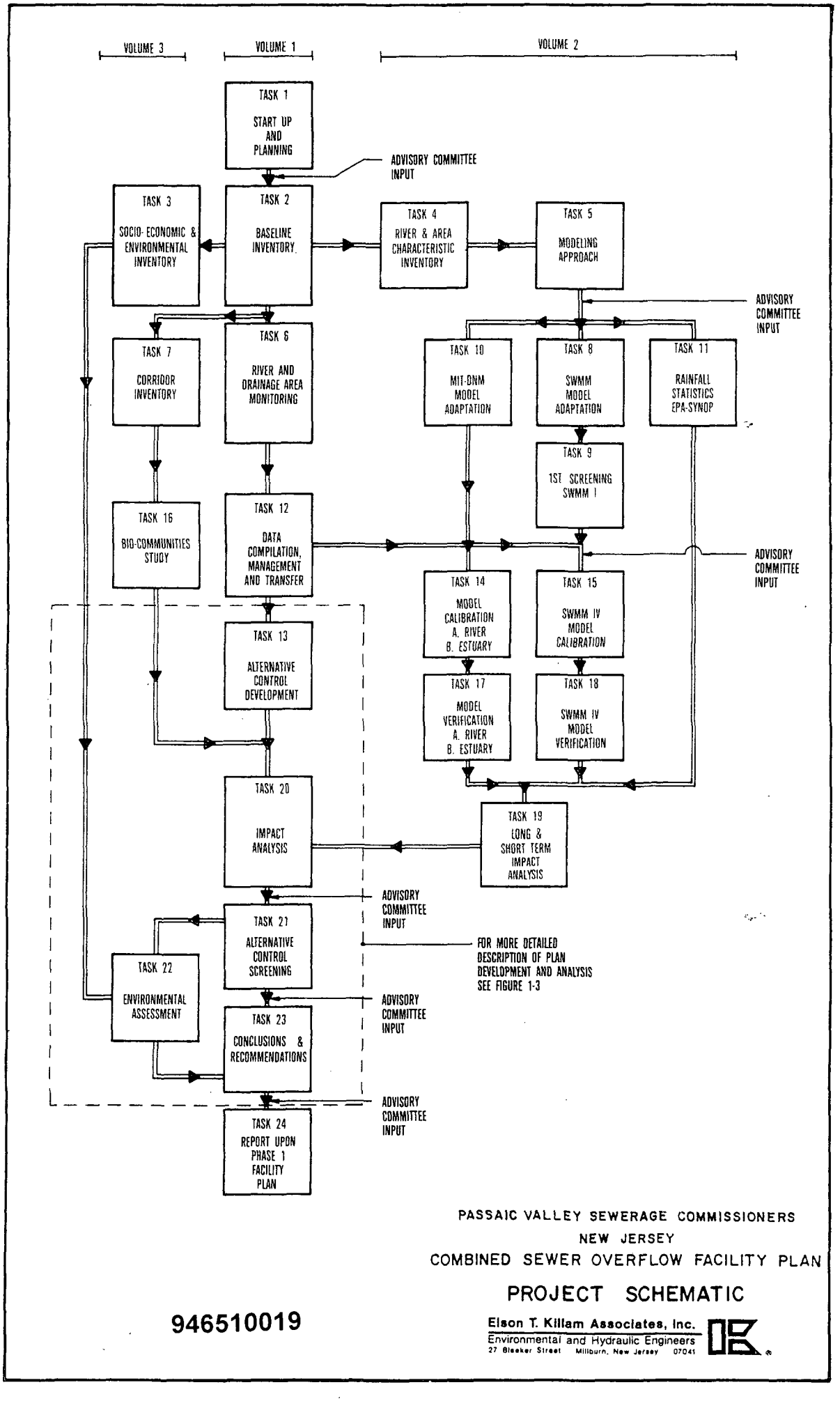

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

PROJECT SCHEMATIC

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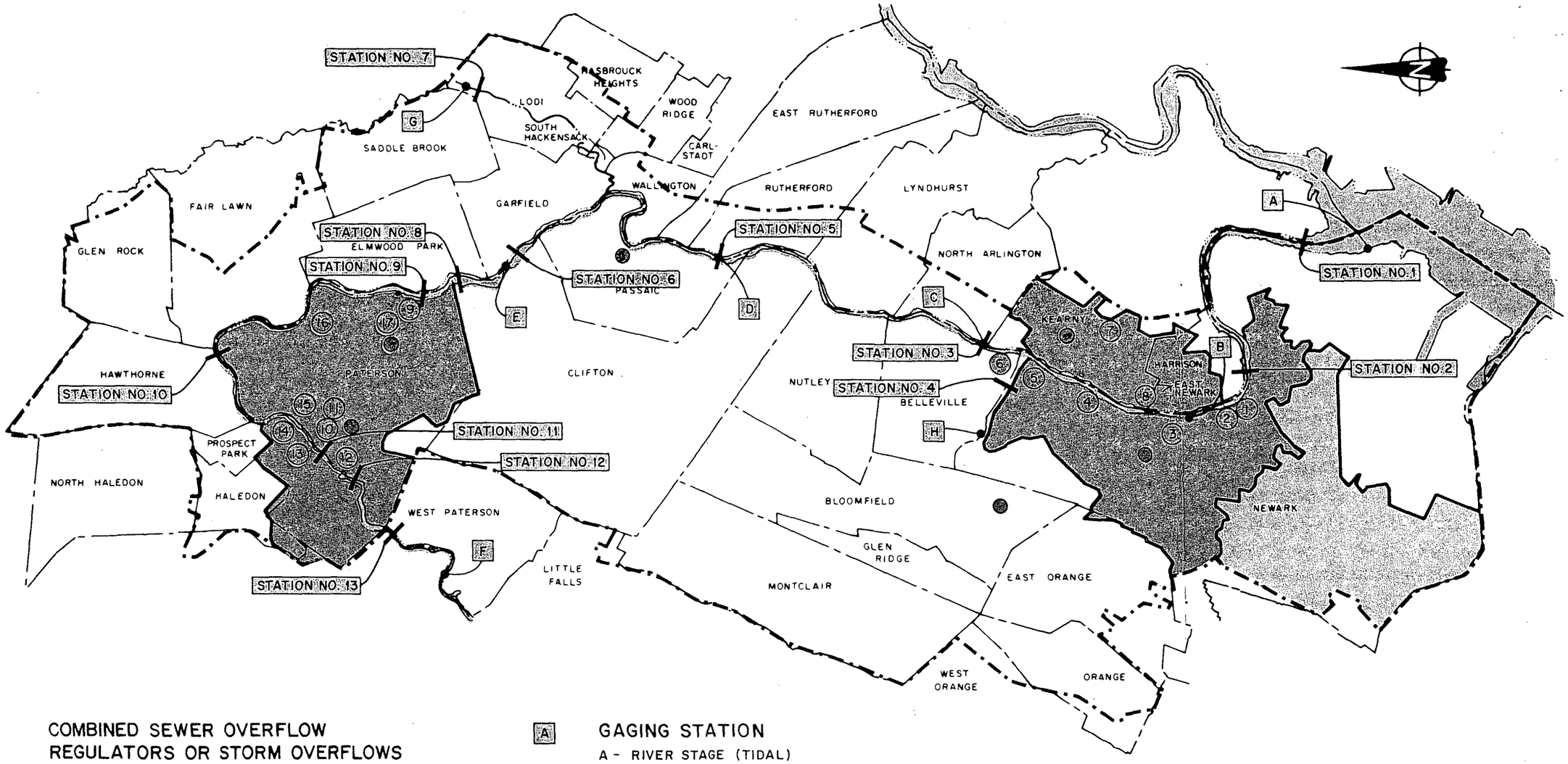
FIGURE 1.2

2. METHODOLOGY



LEGEND

COMBINED SEWER OVERFLOW REGULATORS OR STORM OVERFLOWS

1. CITY DOCK
2. SAYBROOK PLACE
3. CLAY STREET
4. HERBERT PLACE
5. VERONA AVENUE
6. UNION OUTLET BY-PASS
7. IVY STREET (KEARNY)
8. JOHNSTON AVE. (KEARNY)
9. MARKET STREET
10. LOOP ROAD NO. 1
11. LOOP ROAD NO. 2
12. CURTIS PLACE
13. NORTHWEST AVENUE
14. HUDSON STREET
15. MONTGOMERY STREET
16. 10 TH. AVE. & 33 RD. ST.
17. 19 TH. AVENUE

STATION NO. 1 — RIVER WATER QUALITY SAMPLING STATION

RAIN GAGING STATION

LIMITS OF PVSC SERVICE AREA

GAGING STATION

- A - RIVER STAGE (TIDAL)
- B - TIDE GAGE
- C - TIDE GAGE
- D - TIDE GAGE
- E - RIVER STAGE
- F - LITTLE FALLS
- G - SADDLE RIVER

LIMITS OF COMBINED SEWER FACILITY PLANNING AREA

LIMITS OF COMBINED SEWER AREAS EXCLUDED FROM FACILITY PLANNING

PASSAIC VALLEY SEWERAGE AUTHORITY
NEWARK, NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

MONITORING STATIONS

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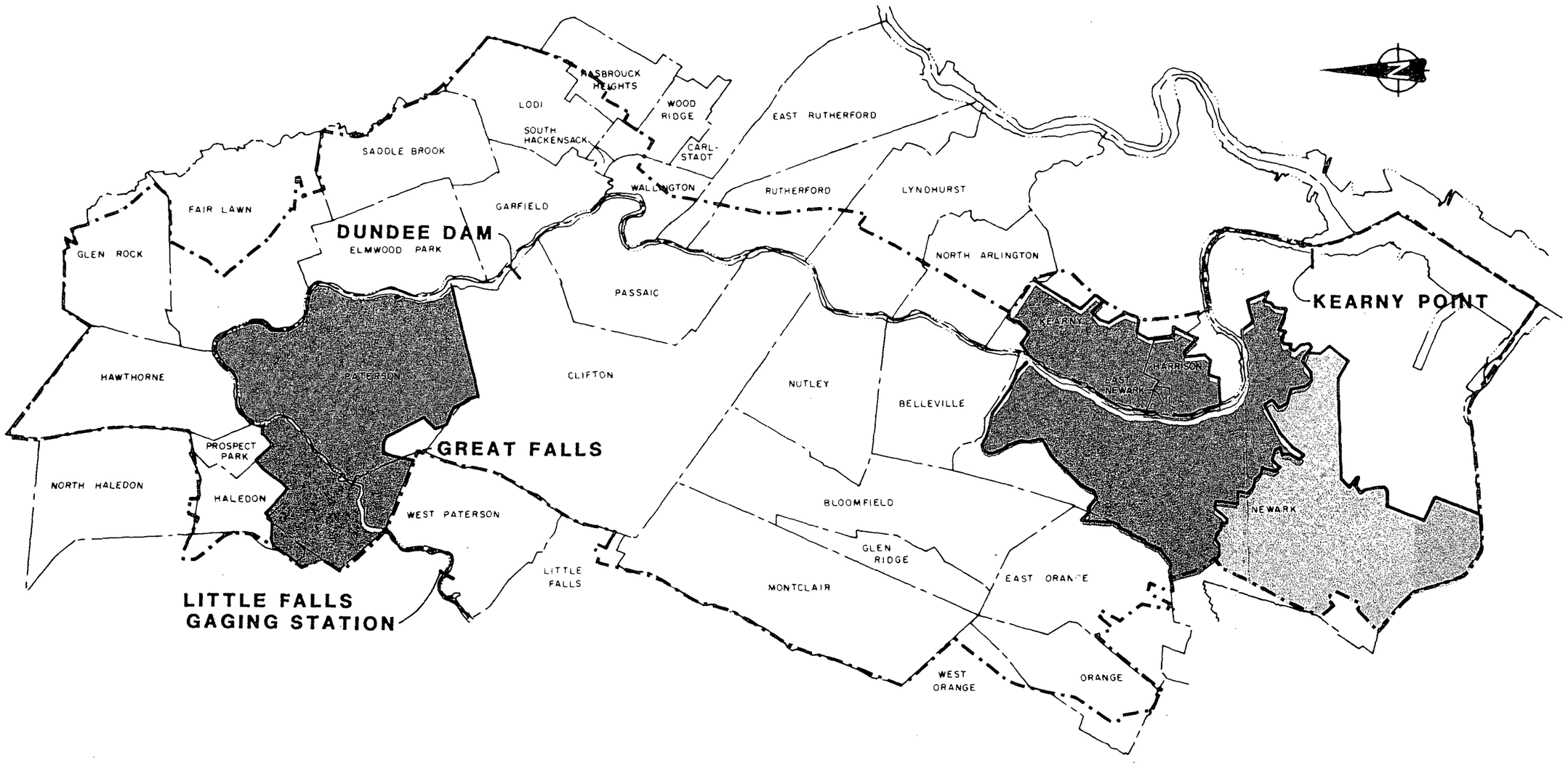
FIGURE 1.2



LEGEND

- LIMITS OF PVSC SERVICE AREA
- LIMITS OF COMBINED SEWER FACILITY PLANNING AREA
- LIMITS OF COMBINED SEWER AREA EXCLUDED FROM FACILITY PLANNING

PASSAIC VALLEY SEWERAGE AUTHORITY
NEWARK, NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

PLANNING AREA

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FIGURE 2-1

TABLE 2.1

RIVER GAGING STATIONS

Location	Approximate Distance Upstream of Kearny Point	Site Description	Gage Description	Approx. Period Recorded
PVSC Dock	-	Newark Bay Boundary	ETK Temporary Tide Gage	9 months
Bridge St.	4 miles	For Calibration/ Verification	ETK Temporary Tide Gage	9 months
Second River	8 miles	Riverine Boundary	ETK Temporary River Gage	9 months
Belleville Turnpike Bridge	8 miles	For Calibration/ Verification	ETK Temporary Tide Gage	9 months
Third River	11 miles	Riverine Boundary	U.S.G.S. River Stage Recorder	12 months
Union Avenue Bridge	12 miles	For Calibration/ Verification	ETK Temporary Tide Gage	9 months
Dundee Dam	17 miles	Estuary Boundary	ETK Temporary River Gage	9 months
Saddle River @ Outwater Lane Bridge	17 miles	Upstream Riverine Boundary	U.S.G.S. River Stage Recorder	12 months
Passaic River @ Little Falls	26 miles	Upstream Riverine Boundary	U.S.G.S. River Stage Recorder	12 months

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variations within the study area. Key locations were established, see Table 2.1, wherein fresh water inflows were obtained. Little Falls (the fresh water input into the river), the Saddle River, and the Third River (fresh water inflows into the estuarine reach) are monitored on a continuous basis by the U.S.G.S., and stream flow information is readily available. Other locations, such as Dundee Dam (the major input of fresh water to the estuarine reach), and Second River (another fresh water input into the estuarine reach), required temporary installation of automatic river gaging equipment. All monitoring stations utilized within the Facility Plan are illustrated in Figure 2.2

The temporary gaging equipment consisted of a continuously recording Steven's Type F Water Recorder installed in a lockable housing with an attached stilling well. Each location was surveyed from a U.S.G.S. monument to establish the actual level of flow referenced to mean sea level. Each site was monitored and serviced weekly to ensure the accuracy of the obtained information and was maintained for approximately nine months.

Accurate determinations of tidal elevations throughout the estuary section was accomplished by establishing temporary gaging stations at four locations spaced throughout the estuary from Kearny Point to Dundee Dam. These included sites at Union Avenue Bridge (Passaic-East Rutherford), Rutgers Bridge (Belleville-North Arlington), Bridge Street Bridge (Newark-Harrison), and PVSC Dock. (See Figure 2.2). The equipment and methods involved were identical to the installations at Dundee Dam and Second River.

Cross-Sectional Velocities

In addition to the hydraulic gaging stations, geometric data was

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necessary to define the hydraulic characteristics of the lower Passaic River. Extensive cross-sectional and sounding survey data was made available by the U. S. Army Corps of Engineers for the entire lower Passaic River. Along with these profiles, cross-sectionally averaged velocity determinations were made to verify tidal induced velocity variations in two locations, the Central Railroad Bridge (Newark-South Kearny Point) and Union Avenue Bridge (Passaic-East Rutherford).

The cross-sectional velocities were obtained for every other day during the two seasonal (10 day baseline) samplings. The Union Avenue Bridge velocity determinations were conducted from the Bridge at ten foot intervals. One-third, and two-thirds depth velocity readings were taken at each interval utilizing a weighted and calibrated (to attain proper depths) Marsh-McBirney velocity probe. The other location, the Central Railroad Bridge, necessitated the use of a motor boat. The boat was tied off between each pier of the bridge and then pulled across the span stopping at each ten foot interval to make velocity determinations in the same manner. Detailed geometric information was obtained at each location to ensure proper interpretation of all recorded data.

b. Water Quality Data - Lower Passaic River

River Sampling

In conjunction with hydraulic data, real time water quality data was collected to calibrate and verify the model. The hydrodynamic model of the lower Passaic River required data to calibrate the model to existing conditions.

Two extreme situations normally occur during the annual cycle of the lower Passaic River. The months of February, March and April, are characterized by heavy precipitation yielding high flow and increased

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loadings of pollutants in the Passaic River from runoff in the catchment areas. The months of July and August are characterized by short duration, high intensity precipitation yielding low river flows and high water temperatures.

These two situations necessitated the sampling of the river during two distinct periods to assess the basic water quality of the river under varying conditions. One ten-day non-storm sampling period was therefore conducted during March 1983 and a second during July 1983. In addition, three sampling periods were conducted during major storm events in the Passaic River Basin. Data obtained during all sampling periods constituted the basis for calibration and verification of the model.

Water quality monitoring stations were established to reflect the location of CSO areas (i.e. the Cities of Newark and Paterson, the Towns of Kearny and Harrison, and the Borough of East Newark) in addition to the various major fresh water inflows into the Lower Passaic River. The locations of river water quality stations are shown on Figure 2.2 while information on sampling frequency and duration at each station is shown on Table 2.2.

Major inputs into the system, such as flow from Combined Sewer Overflows (CSOs) were monitored during several transient river stages. The Phase I Analysis (1976) of the Combined Sewer Overflows indicated that thirteen (13) CSOs contributed over 80% of the known discharge from combined sewer overflow chambers. The screening analysis of all the CSOs within the PVSC service district corroborated the findings of the Phase I Analysis of 1976. In fact, the application of SWMM level I to all the CSO basins made it possible to classify the CSOs in ascending order of their total contribution of pollutants to the lower Passaic River. (See Volume 3).

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TABLE 2.2

PASSAIC RIVER WATER QUALITY SAMPLING STATIONS

STATION DESIGNATION	LOCATION	APPROXIMATE DISTANCE UPSTREAM OF NEWARK BAY BOUNDARY (STATION 1) (Miles)	QUALIFIER	DESCRIPTION OF SAMPLING SAMPLE (1) RETRIEVAL	PARAMETERS (2) ANALYZED	DURATION (3) OF SAMPLING (Days)	FREQUENCY (4) OF SAMPLING (Sampling Times/ Day)
1	Central R.R. Bridge	-0-	Newark Bay	2	All	10/10	24
2	Jackson Street Bridge	3.2	Calib./Verif.	2	All	10/10	8
3	Rutgers Street Bridge	7.5	Calib./Verif.	2	All	10/10	8
4	Second River	7.0	Tributary Boundary	1	All	10/3	8
5	Union Avenue Bridge	11.8	Calib./Verif.	1	All	10/3	8
6 & 8	Dundee Dam (Downstream & Upstream)	16.8	Estuary Boundary	1	D.O.	10/10	8
7	Saddle River @ Outwater Lane	16.6	Tributary	1	All	10/3	8
9	Market Street Bridge	17.9	Calib./Verif.	1	All	10/3	8
10	Lincoln Avenue Bridge	21.9	Calib./Verif.	1	All	10/3	8
11	Market Island Bridge	23.5	Calib./Verif.	1	All	10/3	8
12	McBride Avenue Bridge	24.0	Calib./Verif.	1	All	10/3	8
13	Hillery Street Bridge	26.0	Upstream	1	All	10/3	8

(1) - 2 indicates sample retrieval @ 1/3 and 2/3's of depth - 1 indicates sample retrieval @ 1/2 of depth.
(2) - All analyses as indicated in text. D.O. = Dissolved Oxygen.
(3) - Base non-storm event/storm event.
(4) - At equal intervals of time.

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Each of the thirteen major overflow chambers were monitored during the storm events analyzed. In addition to these thirteen CSOs, one major bypass (normally activated during significant rainfall events), and two major storm sewer systems within the City of Paterson (which accept overflows from the combined system upstream of the Overflow Chambers) were included within the monitoring program. Table 2.3 lists the overflows, storm outlets, and the bypass monitored, and indicates their location of discharge along the Passaic River. (See Figure 2.2).

Prior to the initiation of sampling within the lower Passaic River, a detailed investigation of each sampling site was conducted to establish the logistics involved within the sampling effort. Travel routes were established and tested for each sampling group to insure the completion of each loop within the time period specified (each location was sampled on a three hour cycle). In addition, detailed instructions were established for all sampling procedures, as well as the proper handling of all collected samples, and proper maintenance of all field records.

Within each ten day baseline (non-storm) sampling period, approximately 1,500 samples were collected and analyzed. To insure the integrity of each sample, a special numbering sequence was established wherein each sample was assured its own distinctive number. Each sampling location was given a station number, which was incorporated into the sample numbering system. Special field cards were developed so that all necessary information could be recorded in a standardized manner. In addition, field books were utilized as a backup system to cross-check any questionable or incomplete information.

The analysis of water quality was directed towards determining the variables that directly influence variation of dissolved oxygen (DO) concentrations in the lower Passaic River. As such, the following

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TABLE 2.3

COMBINED SEWER OVERFLOW &

STORM SYSTEM/BYPASS MONITORED

SITE DESCRIPTION	DRAINAGE AREA (ACRES)	APPROXIMATE DISTANCE UPSTREAM OF KEARNY POINT (MILES)
Ivy Street Overflow (Kearny)*	610	3
City Dock Overflow (Newark)	380	3.8
Saybrook Place Overflow (Newark)	310	4.1
Clay Street Overflow (Newark)	1,600	4.7
Johnston Avenue Overflow (Kearny)	210	5.2
Herbert Place Overflow (Newark)	300	6.3
Verona Avenue Overflow (Newark)	370	7.1
Union Outlet Bypass ** (2nd River Joint Meeting)	10,200	7.3
Market Street Overflow (Paterson)	1,500	17.9
19th Avenue Storm Sewer (Paterson)		18.3
10th Avenue & 33rd Street Overflow (Paterson)	700	19.9
Hudson Street Overflow (Paterson)	450	22.7
Montgomery Street Overflow (Paterson)	670	22.7
Loop Road Storm Sewer (Paterson)		23.0
Northwest Street Overflow (Paterson)	280	23.2
Curtis Place Overflow (Paterson)	970	23.4

* Discharges to Frank's Creek
** Separate Sanitary Systems

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variables were monitored both instream, at the tributaries and at the Newark Bay and Little Falls boundaries of the system.

(a) C-BOD	(e) NO_2-N	(i) NO_3-N
(b) Temperature	(f) DO	(j) pH
(c) Salinity	(g) Chlorophyll a	(k) Turbidity
(d) NH_3-N	(h) TKN (Total Kjeldahl Nitrogen)	

Several of the above parameters were measured in situ utilizing electronic measuring equipment. These parameters included salinity, temperature and dissolved oxygen. All measuring equipment was maintained to insure the accuracy of the instrument and was calibrated against established standards on a daily basis. All other water quality parameters were analyzed within the laboratory facilities utilizing the procedures as outlined within the laboratory methodology section.

In addition to obtaining the detailed water quality analysis within each river station, a cross-sectional water quality sampling was conducted twice during each seasonal period. This cross-sectional water quality data was obtained at the Central Railroad Bridge at Kearny Point and at the Union Avenue Bridge between Passaic and Rutherford.

During the several storm events monitored within the lower Passaic River, the CSO monitoring stations listed in Table 2.3 were manned and equipped to obtain samples every fifteen minutes throughout actual overflow events. These samples were analyzed for all water quality variables listed above with the exception of (b) temperature, (c) salinity, (f) DO, and (g) Chorophyll a. In addition, during each storm event, temporary metering equipment was installed at each CSO monitoring station to record discharge of overflows to the river.

Although a substantial monitoring effort was involved within the Combined Sewer Overflow Facility Plan, it was not feasible to monitor or sample all pollutional inputs into the lower Passaic River. As such, major inputs derived from separated storm sewers within the Passaic Valley District were determined through a SWMM-4 (Storm Water Management Model) analysis of these areas. Loading factors utilized within these SWMM-4 were derived from actual water quality and quantity measurements within the Second River and Saddle River drainage basins.

Reaeration and production of dissolved oxygen by primary producers through photosynthesis constitute the sources of dissolved oxygen within the system. C-BOD, N-BOD (NH_3-N and NO_2-N) along with benthic demand constitute the sinks of dissolved oxygen in the system. Whereas C-BOD and N-BOD decay causes DO depletion within the water column, the benthic uptake of dissolved oxygen and its contribution to instream C-BOD and N-BOD is effected at the water/sediment interface.

To assess the benthic contribution of C-BOD and N-BOD in addition to the benthic demand on dissolved oxygen within the water column, a benthic monitoring program was established at five locations in the Lower Passaic River. These locations include:

Central Railroad Bridge at Kearny Point

Jackson Avenue Bridge - Newark Area

Belleville Turnpike Bridge - Belleville Area

Union Avenue Bridge - Passaic Area

Upstream of Dundee Dam - (Route 46 bridge at Elmwood Park)

Each of these stations were sampled and analyzed on a monthly basis throughout the nine month study period.

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The benthos sampling conducted within the Facility Plan consisted of obtaining a core and near bottom water sample at each of the monitoring stations. Each core sample consisted of twenty to thirty centimeters of sediment at the bottom and twenty to thirty centimeters of overlying water. In addition to the core samples, a sample of the core overlying water at interstitial level was collected and subjected to a similar chemical analysis. Samples were collected with great care to insure that no bottom sediments were entrained in the samples. This approach permitted a determination of the effects of disturbance during coring on the concentration of the parameters of interest in the overlying water.

The core samples obtained were carefully transported to the laboratories of Elson T. Killam Associates, Inc., for incubation experiments within two hours of core collection. Core samples and nearby water samples were incubated in the dark at the in situ temperature. The samples were handled with great care to insure that no air from the atmosphere was entrained into any sample.

Both the water overlying core and near bottom water samples were monitored for dissolved oxygen for a 24 hour time period. In addition, the overlying water and near bottom water were analyzed for C-BOD, TKN, NO_2, NH_4 one or more times during the monitoring period.

A separate set of core samples were taken to properly assess the ultimate release of organic matter to the water column from the interstitial water for diffusion. These samples were also analyzed to determine the ultimate reserve capacity of the solids in the sediment. The collection and the incubation of these core samples were similar to the other benthic cores, however, the extent of the laboratory analysis was diminshed.

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c. Drainage Area Data

The adaptation of the SWMM-4 Model to the numerous drainage areas within the lower Passaic River Basin required an adequate knowledge of each system's hydraulics, in addition to detailed rainfall information within the surrounding area. Field information was obtained on the runoff characteristics of each area, including land use, topography, and detailed information on each sewer system (slope, pipe size, capacity, etc.). This, in conjunction with real time flow and rainfall data, was utilized in the calibration and verification of the SWMM-4 Model. The following sections summarize the methods utilized to compile and evaluate the data within this area.

Meteorological Data

Meteorological information was obtained during the study period through a network of rain gages established throughout the Passaic Valley District. These gaging stations, listed on Table 2.4, and illustrated on Figure 2.3 were sited so as to provide adequate resolution within each of the catchment areas involved. Two National Oceanic and Atmospheric Administration gages were utilized in addition to the temporary gages installed. The NOAA stations utilized were at Little Falls and at Newark International Airport.

The temporary gages were established within both public and private locations. Weighing bucket rain gages or tipping bucket rain gages were installed at the various locations depending upon available access and security within the area. Figure 2.3 illustrates the relative placement of all rain gages and their relationship to the overall study area. Each site was carefully chosen to ensure accurate rainfall determinations with special consideration given to other buildings and wind velocities within each area.

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TABLE 2.4

RAIN GAGE STATIONS

LOCATION	GAGE DESCRIPTION	PERIOD OF RECORD
Town of Kearny Public Works	ETK - Weighing Bucket	30 months
City of Newark Summer Street Fire Station	ETK - Tipping Bucket	30 months
Town of Bloomfield Fire Department Headquarters	ETK - Tipping Bucket	16 months
PVSC-Wallington Pump Station Passaic	ETK - Weighing Bucket	30 months
City of Paterson Madison Fire Station	ETK - Weighing Bucket	24 months
City of Paterson PVWC Grand Street Reservoir	ETK - Tipping Bucket	24 months
Elson T. Killam Assoc. Millburn	ETK - Tipping Bucket	36 months
City of Newark Newark International Airport	NOAA Station	-
Little Falls -PVWC	NOAA Station	-

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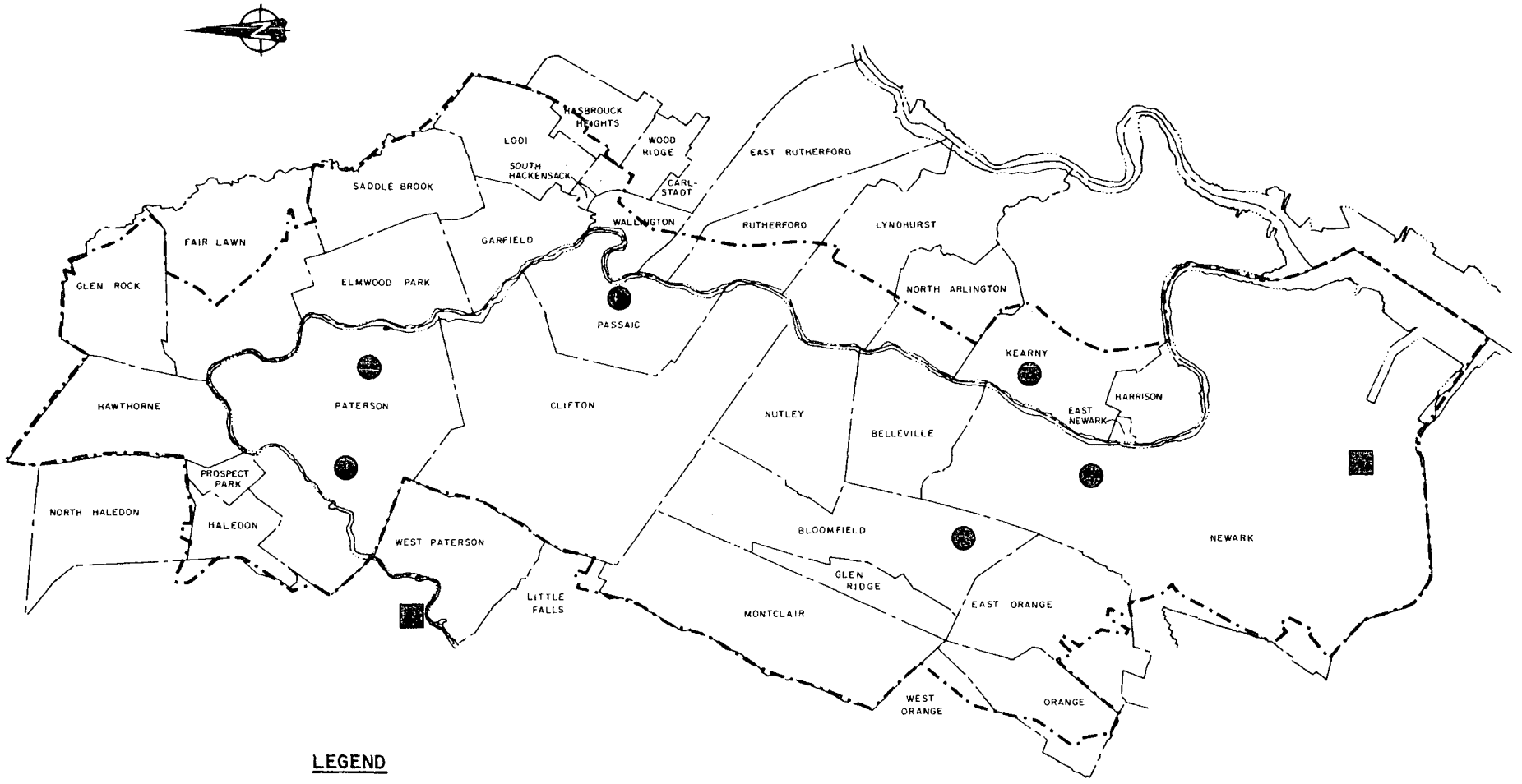

LEGEND

- NOAA GAGE
- E.T.K. GAGE

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

RAIN GAGING STATIONS

Elson T. Killam Associates, Inc.

Environmental and Hydraulic Engineers

27 Bleeker Street Millburn, New Jersey 07041

FIGURE 2.3

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Each gage was serviced on a weekly basis to ensure accurate results by minimizing possible malfunctions. The collected data provided detailed information which was separated into 15 minute increments to identify intensity and duration of precipitation during sampling events.

Land Use

The runoff characteristics of any drainage basin is directly affected by the land use within the area. Pollutional loadings, as well as runoff coefficients are determined by the extent of impervious area, as well as population density.

Detailed land use information was developed for each of the major, and several of the larger moderate overflows. The drainage areas analyzed were predicated upon the quality and quantity of discharge measured or observed during the Phase I Analysis, as well as the relative drainage areas upstream of each overflow regulator chamber. The drainage areas analyzed are included within Table 2.5. Each is identified by overflow area in addition to the sub-area notation corresponding to the Phase II I/I delineations.

Initial investigations within each of the primary drainage areas were conducted utilizing topographic mapping and aerial photographs prepared under the facility plan. Preliminary land uses within each drainage area were delineated and prepared for detailed field investigations. Each land use area was field checked for consistency, and area boundaries were adjusted as required. Once finalized, each land use area was investigated utilizing random selection of typical areas for detailed analysis.

Intensive field investigations were conducted within random areas of each land use region. Detailed information on the number and types of buildings, area drainage, impervious areas and apparent location of roof

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TABLE 2.5

PASSAIC VALLEY SEWERAGE COMMISSIONERS
COMBINED SEWER OVERFLOW FACILITY PLAN
PRIMARY DRAINAGE AREAS
(1976 ANALYSIS)

MUNICIPALITY	SUB-AREA(s)	OVERFLOW	DRAINAGE AREA (Acres)
Paterson	AA & A1	Curtis Place	970
	B1	Northwest Street	280
	B2	Hudson Street	450
	F	Montgomery Street	670
	R & S	10th Ave. and 33rd St.	700
	V1 & V2	Market Street	1500
Newark	B	Verona Avenue	370
	E	Herbert Place	300
	I	Fourth Avenue	225
	J, J1 & J2	Clay Street	1600
	M	Rector Street	180
	N	Saybrook Place	310
	P1 & P2	City Dock	380
	Q	Jackson Street	80
	R	Polk Street	200
Kearny	B	Johnston Avenue	210
	C	Ivy Street	610

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drainage was recorded for further analysis. In addition, topographic detailed plans were utilized to denote major paved and open areas within each region.

The detailed field information was broken down into major components and summarized for each land use area. Land use within each drainage area was separated into one of four categories:

residential

commercial

industrial

open area/park land

In addition, the total drainage area, as well as the calculated percent of impervious area for each land use section was calculated and weighed to obtain a drainage basin average.

System Information

Prior to the consideration of alternative control strategies for combined sewer overflows, it was necessary to derive and compile detailed information upon each drainage area tributary to the overflow facilities. Specific data has been developed upon the CSO drainage areas for use in the alternative evaluation.

In order to accurately show physical characteristics within each drainage area, topographic base maps (scale 1" = 200') have been prepared from aerial photos of the study area taken in April 1980. The maps identify the conditions of each drainage area in terms of building, expected population densities, in addition to parks and open areas. The prepared base maps provide a means of identifying system conditions, as well as physical characteristics that may effect various alternative controls under consideration within the Facility Plan.

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In conjunction with the preparation of topographic base maps, a system survey was conducted to identify the locations of existing storm drainage systems (both combined and separate) within each CSO drainage area. The survey also identified those areas wherein separate sanitary sewer systems exist. The survey included the location of existing drainage inlets, storm piping, including manhole diversion chambers, internal overflows and outlet facilities within each drainage area. Field investigations were conducted throughout the combined sewer areas under investigation to provide an accurate representation of the existing storm drainage facilities.

Information derived from field surveys, augmented by existing sewer mapping, has been compiled and is provided as a separate portion of the facility plan entitled Passaic Valley Sewerage Commissioners' Combined Sewer Overflow Facility Plan, Area Plan. This mapping includes the location of existing combined, storm, and sanitary sewers within each area, known bypasses and overflows, as well as the Passaic Valley Commissioners trunk and regulator systems.

In addition to the detailed area mapping of the combined sewer overflow drainage areas, the hydraulic profiles of major interceptor sewers within the CSO drainage areas included in Table 2.5 have been obtained and plotted to a convenient scale. Field crews were utilized to obtain system grades as well as to verify available information as to pipe sizes and existing connections. Included within the profiles, is information on pipe size, slope and developed theoretical capacity of the major interceptor sewers. The data collection on the existing system has been limited to those catchment areas that are of sufficient size to warrant upstream storage for alternative considerations.

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Those areas requiring additional data have been monitored for flow quality and quantity. Field crews have installed temporary flow monitoring equipment at selected key locations to monitor flows during storm conditions and to record system surcharging or backup occurring at specific locations. This equipment primarily consisted of a level sensing device set to continuously record the depth of water flowing within the sewers. This depth was related to hydraulic characteristics of the sewer at each location to obtain the flow measurement. The level sensing device recorded the depth variation to the sewer section which was directly related to the instantaneous flow passing through the sewer (normally determined in million gallons per day, MGD). These charts were analyzed to determine average flows, as well as the relationship between peak flows and peak rainfall intensities. The temporary flow recording equipment was maintained for a period of time sufficient to obtain data from several storm events for each catchment area within Table 2.5.

Sewage samples have been obtained near the flow monitoring location during rainfall events to determine the quality of runoff in the various segments of the drainage areas monitored. The samples obtained were analyzed at the laboratory facilities of Elson T. Killam Associates, Inc., for C-BOD, N-BOD, Suspended Solids and Volatile Solids. Information derived from this phase of the investigation is included under Section 3.

d. Alternative Control Analysis

Subsequent to the development of baseline information upon the physical, environmental, and hydraulic characteristics of the CSO drainage areas, and in conjunction with the results of the MIT-DNM analysis of CSO impacts, a listing of possible and feasible alternatives has been prepared. The list of possible alternatives includes both structural and

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non-structural considerations and has been developed from present state-of-the-art information on CSO control, as well as case history information for other urban areas of the United States wherein CSO facility planning has been undertaken.

The short term and long term analysis of CSO impacts upon the lower Passaic River (Volume II of the Facility Plan) has shown that CSO discharges have a marginal effect on dissolved oxygen within the lower Passaic River. Although the combined sewer overflows have an appreciable impact on increasing the C-BOD and N-BOD concentrations in the receiving water, these impacts are transient and prevail over a short time period. Furthermore, it was shown that CSO contribution of pollutants to the river represents less than 10% of the total long term loadings to the lower Passaic River. The bulk of the total pollutional load is contributed by the upper Passaic River (approx. 40-50%), the Saddle River (8-13%), and separate storm sewers within the lower Passaic River Basin (30-40%). Therefore, those alternative controls which involve regional or massive individual overflow treatment have been eliminated from consideration due to their ineffectiveness in changing the overall water quality of the lower Passaic River at the present time.

Although the modeling analysis has not shown a significant impact from CSOs upon the dissolved oxygen and long term loads of C-BOD and N-BOD, CSO discharges could and probably do, have a substantial effect on the amount of floating material and debris within the lower Passaic River. Accordingly, the thrust of the alternative analysis has been towards those control measures which could reduce the floatable solids within the lower Passaic River, and as such improve the aesthetics of the river within this region.

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The list of alternatives developed includes only those considered generally feasible within the Passaic Valley Sewerage Commissioners' service area. Alternatives were considered for each CSO area, as well as for regional areas (groups of CSO drainage areas adjacent to each other).

Each CSO drainage area has been reviewed separately as well as combined for regional considerations. The preparation of an alternative list for each CSO or group of CSO areas is predicated upon the existing physical and environmental conditions previously developed. Accordingly, only those alternatives that are considered generally feasible for an area under study will be included in more detailed analysis.

An analysis of the socio-economic impact of each alternative has been conducted (see Volume III). The analysis has considered preliminary impacts for each overflow area, classifying the alternatives into non-restricted, or restrictive discharge categories. Each alternative has been evaluated for feasibility, as well as an environmental assessment of the alternative's impact upon existing and anticipated land use (reference Volume III).

Environmental considerations have been predicated upon the location of the CSO drainage area and the local characteristics of the area. Effects on land values, taxes, housing, public acceptance, aesthetics, and cultural resources have been considered. Short term localized construction-related impacts (noise, traffic, disruption, street closure) have been evaluated and are included within the assessment. In addition, primary impacts upon the natural environment have been assessed in terms of land loss, vegetation loss, siltation and erosion problems.

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e. Water Quality Analysis

Liquid Phase Analysis

The problems involved in the collection of all water quality samples within the Facility Plan were only one aspect of the logistics associated with the sampling effort. More than 9,200 samples were collected from the sixteen storm flow locations (overflows and major storm sewers) and eleven river stations on the lower Passaic River and its tributaries over a nine month period. These samples involved the determination and data management of 82,000 separate analyses within the five sampling periods. As such, it required special planning and procedures to assure the accuracy of each analysis.

Water quality samples collected from the various river stations were, immediately after collection, placed in thermally insulated, light tight coolers. Two samples were collected at each sampling station to assure flexibility in the analysis and an adequate sample size. Each sample was then iced or frozen by utilizing dry ice, depending upon the analyses to be completed upon the sample. All samples were collected and transported to the laboratory within a twelve hour period.

Samples were collected from the combined sewer overflow monitoring stations and/or other internal monitoring locations by means of automatic samplers capable of collecting 24 discrete samples. Each automatic sampler was set for discrete samples every 15 minutes which completed the 24 bottles within a six hour period. Samples were stored within their respective bottle cases during sampling and were iced and transported to the Elson T. Killam Associates, Inc., laboratory as soon as possible.

Analyses of the samples commenced upon delivery of the samples to the laboratory. If storage was found to be necessary, the samples were

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refrigerated at 4°C, however, storage was not allowed to exceed 24 hours unless the samples contained an appropriate preservative.

Prior to initiating any of the required analyses, all samples were checked for continuity of sample stations, dates, and time of sample collection. All samples wherein inconstant or illegible sample numbers existed were checked against field books and field cards to verify the correct sequence and/or sample number. In those rare cases wherein the sample number could not be verified or reconstructed from available information, the samples were discarded and were not analyzed.

Special handling procedures were established for those samples in which the chlorophyll-a analysis was to be conducted. As with all samples collected, the chlorophyll-a samples were maintained within thermally sealed, light tight coolers immediately after sample collection. To minimize light exposure during laboratory procedures, the chlorophyll-a filtration was the first procedure initialized and completed during the processing of samples for the various analyses required. The filter paper was then labelled and stored under appropriate conditions until analysis could be completed.

The methods utilized within the laboratory for the various water quality parameters are shown in Table 2.6, Laboratory Analysis Methodology. Dissolved oxygen, temperature and salinity were measured in situ and as such are not included within this table.

In an effort to assure the reliability of the analytical results generated by the Facility Plan, extensive quality assurance procedures were implemented in accordance with the Handbook for Analytical Quality Control in Water and Wastewater Laboratories, USEPA, 1979. The quality assurance practices, as stated within the above referenced handbook were

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TABLE 2.6

PASSAIC VALLEY SEWERAGE COMMISSIONERS
COMBINED SEWER OVERFLOW FACILITY PLAN
LABORATORY ANALYSIS METHODOLOGY

PARAMETER	METHOD USED	REFERENCE
BOD	Dilution	Method 405.1 (1)
COD	Colorimetric, Manual	Method 410.4 (1)
Suspended Soids	Glass Fiber Filter	Method 160.2 (1)
Volatile Suspended Solids	Glass Fiber Filter	Method 160.2 (1)
Ammonia Nitrogen	Automated Phenate	Method 350.1 (1)
Total Kjeldahl Nitrogen	Semi-Automated	Method 351.2 (1)
Nitrate-Nitrite	Automated Cadmium Reduction	Method 353.2 (1)
Total Phosphorous	Semi-Automated	Method 365.4 (1)
Turbidity	Nephelometric	Method 180.1 (1)
pH	Electrometric	Method 150.1 (1)
Chlorophyll	Fluorometric	Method 1002 G (2)
Specific Gravity	Hydrometer	Method D 1429-76 (3)

(1) Methods for Chemical Analysis of Water and Wastes, U.S.E.P.A. (1979).

(2) Standard Methods For the Examination of Water and Wastewater, 14th Edition, American Public Health Association, New York (1975).

(3) Annual Book of ASTM Standards, Part 31, Water, American Society For Testing and Materials (1981).

946510045

strictly followed in all chemical analyses and data management procedures.

Benthic Core Analysis

A proper assessment of the benthic demand upon the water column required the analyses of not only the water-sediment interface, but also of the ultimate oxygen demand available within the benthos. Following collection procedures as previously discussed within section 2b., the concentration changes in the parameters of interest were measured under laboratory conditions to assess the benthic oxygen demand and the rate of release of oxygen consuming organics into the waters of the lower Passaic River.

Dissolved oxygen was monitored within both the core and overlying water samples for a 24 hour period or until the dissolved oxygen level fell below 2 mg/l. Initial measurements of temperature, dissolved oxygen and salinity were done in situ just prior to coring. Subsequent dissolved oxygen measurements were made within the laboratory using electronic metering equipment. Each core was incubated in the dark at the in situ temperature during the monitoring period. Special consideration was give to each core sample to assure that the sediment/water interface was not disturbed during each DO determination.

Upon arrival of each core and near bottom water sample, a sample of the overlying water within the near bottom water sample was obtained by siphoning an aliquot of the sample into a 300 ml. BOD bottle. This sample was subsequently analyzed for C-BOD, TKN, NO_2, and NH_4. At the termination of the dissolved oxygen monitoring period, the overlying water in the core was siphoned and analyzed for the same parameters. Changes caused by the interaction of the water/sediment interface could thus be gauged by the change within the monitored parameters.

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In addition to the analysis of the overlying water within the core, a separate analysis for C-BOD, TKN, NO_2, and NH_4 was conducted on the interstitial water obtained by compressing the "solid" portion of each core. Each core was extruded and the upper 3-5 centimeters of sediment was placed in a squeezing device especially designed to extract the interstitial water. At least 10 ml of the interstitial water was collected using all the procedures required to assure a non-contaminated sample. Analysis for BOD was initiated immediately while nutrient samples were preserved for future analysis using accepted USEPA laboratory procedures. Analysis was also conducted on the compacted core following the procedures outlined in Procedures for Handling Analysis of Sediment and Water Samples, USEPA, 1981.

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3. RESULTS OF SYSTEM ANALYSIS

3. RESULTS OF SYSTEM ANALYSIS

Calibration and verification of the SWMM-3 and MIT-DNM models required an adequate data base to assure successful adaptation to the various drainage areas and the lower Passaic River. A major portion of this data base consisted of real time water quality and quantity information obtained through the various sampling and monitoring efforts within both the river and individual drainage areas. In addition, detailed system information within specific drainage areas was obtained through field investigations upon land use, drainage areas, and system characteristics. Appropriate information was thus utilized on the various modeling efforts analyzed within the Facility Plan.

a. River Water Quality Data

The water quality data base for the lower Passaic River and related boundary locations has been compiled within Appendix A for each of the five, ten day sampling periods. (Two non-storm and three storm conditions). An example of the information provided and the format utilized is included as Table 3.1.

All data within Appendix A has been separated by sampling period and station. In addition, those locations which were sampled at two levels, Level A being 1/3 of flow depth, and Level B being 2/3 of flow depth, are separated by sampling depth. These include Kearny Point, (Central R.R. Bridge), Jackson Street in Newark, and Rutgers Street in Belleville (Stations No. 1, 2, and 3). All other stations were sampled at a single level indicated as depth C (1/2 depth).

The frequency and duration of sampling at each station is summarized in Table 2.2, "Passaic River Water Quality Stations." All sampling was conducted on a continuous 24 hour basis for the specified duration.

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TABLE 3.1

PASSAIC RIVER WATER QUALITY

BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	830	8.5	1	A	7.45	6.0	3.4	2.080	NA	NA	3.45	0.418	15.58	6.0	8.10	14.3
3	10	1030	10.5	1	A	7.53	5.3	2.2	1.230	NA	NA	NA	NA	6.68	5.0	8.30	17.3
3	10	1230	12.5	1	A	7.54	4.7	2.7	1.520	NA	NA	2.69	0.324	6.31	5.8	8.00	15.5
3	10	1445	14.8	1	A	7.45	5.9	2.1	1.440	0.032	0.714	NA	NA	8.16	5.5	7.90	10.8
3	10	1709	17.1	1	A	7.43	33.0	6.3	1.130	0.042	0.935	1.98	0.340	10.35	5.0	7.50	9.0
3	10	1930	19.5	1	A	7.39	15.0	3.9	1.630	0.037	0.940	NA	NA	8.53	5.0	9.30	14.0
3	10	2125	21.4	1	A	7.52	10.0	3.4	1.470	0.034	0.585	2.34	0.310	8.90	5.5	8.40	17.0
3	10	2255	22.9	1	A	7.55	10.0	2.7	1.170	0.032	0.524	NA	NA	8.53	5.0	9.10	18.0
3	11	45	24.8	1	A	7.44	5.0	2.7	NA	NA	NA	2.62	0.412	NA	5.0	8.20	16.5
3	11	345	27.8	1	A	7.36	6.5	3.4	1.680	0.039	0.791	NA	NA	4.38	5.1	8.00	11.2
3	11	605	30.1	1	A	7.33	8.0	4.8	1.650	0.039	0.896	NA	NA	5.40	5.0	7.70	7.2
3	11	830	32.5	1	A	7.39	15.0	5.8	1.460	0.042	0.759	2.84	0.694	8.76	6.0	7.75	12.5
3	11	1035	34.6	1	A	7.41	6.0	2.0	1.340	0.039	0.721	NA	NA	6.07	5.0	7.40	17.5
3	11	1240	36.7	1	A	7.51	6.2	3.6	0.761	0.018	0.560	1.96	0.251	8.76	4.8	7.10	17.5
3	11	1530	39.5	1	A	7.46	5.4	3.8	1.460	0.039	0.944	1.64	0.274	4.05	5.0	9.70	11.0
3	11	1705	41.1	1	A	7.42	7.0	3.9	1.490	0.039	1.020	NA	NA	6.41	5.9	7.10	11.2
3	11	1910	43.2	1	A	7.44	9.0	3.6	1.730	0.034	1.200	3.72	0.781	4.72	5.0	7.50	8.1
3	11	2100	45.0	1	A	7.45	5.5	2.9	1.430	0.005	0.634	2.51	0.475	1.01	6.0	7.80	14.9
3	11	2240	46.7	1	A	7.41	44.0	17.1	1.140	0.018	0.601	NA	NA	0.67	4.9	8.20	16.5
3	12	35	48.6	1	A	7.54	5.0	3.9	1.340	0.037	0.582	2.42	0.353	6.07	4.5	7.70	19.8
3	12	220	50.3	1	A	7.44	50.0	16.5	0.936	0.029	0.448	NA	NA	14.11	4.9	8.00	19.0
3	12	445	52.8	1	A	7.46	15.0	6.8	1.630	0.031	0.770	3.58	1.160	7.52	5.0	8.10	11.8
3	12	635	54.6	1	A	7.49	35.0	12.3	1.230	0.029	0.529	NA	NA	13.17	5.0	8.20	11.5
3	12	815	56.2	1	A	7.20	15.0	6.4	1.450	0.044	1.020	2.56	0.716	11.80	4.0	8.00	10.0
3	12	935	57.6	1	A	7.20	7.5	5.1	1.420	0.034	0.585	NA	NA	12.14	5.0	7.40	15.0
3	12	1124	59.4	1	A	7.30	4.5	3.9	1.330	0.039	0.559	2.25	0.341	12.14	5.0	7.40	15.3

946510050

The following information will be helpful in the interpretation of the compiled data:

(1) The site number on Table 3.1 corresponds to the station numbers as given on Table 2.2.

(2) The following abbreviations were utilized within:

TURB - Turbidity
BOD - 5 day C-BOD
NH_3 - Ammonia in terms of nitrogen
NO_2 - Nitrites in terms of nitrogen
NO_3 - Nitrates in terms of nitrogen
TKN - Total Kjeldahl Nitrogen
TP - Total Phosphorus
CHLOR - Chlorophyll-a
TEMP - Temperature in degrees Celsius
D.O. - Dissolved oxygen
SAL - Salinity

(3) NA indicates that the value is not available.

(4) TKN and TP analyses were only conducted on every other sample due to small variations within measured parameters.

(5) Salinity was only measured at stations 1, 2, 3, and 4.

(6) Only temperature and dissolved oxygen (D.O.) were measured at station numbers 6 and 8.

Water quality data obtained and compiled within the Facility Plan has been utilized for the calibration and the verification of the MIT-DNM model, and the subsequent short and long term analysis of the impact of combined sewer overflow discharge upon the lower Passaic River. Modeling results and the interpretation of that analysis is given in Volume 2 of the Facility Plan.

b. Drainage Area Investigations

In addition to the comprehensive river monitoring involved within the Facility Plan, detailed system data has been developed upon specific drainage areas. Table 3.2 illustrates the preliminary ranking of overflow

946510051

TABLE 3.2
PRELIMINARY RANKING OF COMBINED SEWER OVERFLOWS BASED UPON PHASE I ANALYSIS (1976)

MAJOR OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	APPROXIMATE DRAINAGE AREA (ACRES)	RECORDED PEAK OVERFLOW TO RIVER (MGD)
Clay St. - Newark	1600	337
Market St. - Paterson	1500	93
Curtis Pl. - Paterson	970	23
10th Ave. & 33rd St.-Paterson	700	92
Montgomery St. - Paterson	670	44
Ivy St. - Kearny	610	244
Hudson St. - Paterson (1)	450	18
City Dock - Newark	380	111
Verona Ave. - Newark	370	80
Saybrook Pl. - Newark	310	89
Herbert Pl. - Newark	300	110
Northwest St. - Paterson	280	90
Johnston Ave. - Kearny	210	112

MODERATE OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	APPROXIMATE DRAINAGE AREA (ACRES)	RECORDED PEAK OVERFLOW TO RIVER (MGD)
Fourth Ave. - Newark	225	62
Polk St. - Newark	200	62
Rector St. - Newark	180	68
Worthington Ave - Harrison	180	9
Nairn Ave. - Kearny	175	3
Freeman St. - Newark	150	16
Straight St. - Paterson	120	57
Bergen Ave. - Kearny	110	29
E. 11th St. - Paterson	105	46
20th Ave. - Paterson	95	17
Delavan Ave. - Newark	90	None
Jackson St. - Newark	80	67
Warren St. - Paterson	80	11
Third Ave. - Paterson	75	21
Bergen St. - Harrison	70	17
Harrison Ave. - Harrison	65	20
Bridge St. - Paterson	60	40
Middlesex St. - Harrison	60	13
Sixth Ave. - Paterson	50	19
S.U.M. Park - Paterson	45	20
Second Ave. - Paterson	45	13

MINOR OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	APPROXIMATE DRAINAGE AREA (ACRES)	RECORDED PEAK OVERFLOW TO RIVER (MGD)
Washington Ave. - Kearny	37	5
Tappan St. - Kearny	35	9
Stewart Ave. - Kearny	34	14
Arch St. - Paterson	32	15
Short St. - Paterson	30	9
Hamilton St. - Harrison	30	18
Passaic St. - Newark	30	7
Central Ave. - East Newark	25	62
Dukes St. - Kearny	25	6
Marshall St. - Kearny	25	5
12th St. & 4th Ave. - Paterson	20	12
Orange St. - Newark	15	None
Bergen Ave. - Kearny	10	2
Cleveland Ave. - Harrison	10	12
Keen St. - Paterson	10	19
Bergen St. - Paterson	10	6
Bridge St. - Newark	10	None
E. 5th St. & 5th Ave. - Paterson	10	12
Third Ave. - Newark	10	-
West Broadway - Paterson	5	8
Dey St. - Harrison	5	8
Mulberry St. - Paterson	5	10
Bank St. - Paterson	5	-
Franklin St. - Paterson	2	-

(1) Includes North Straight, Jefferson, and Stout Street Overflows

946510052

areas developed through an investigation of the Phase I Overflow Analysis completed by Elson T. Killam Associates, Inc., in 1976. This listing represents a preliminary ranking which is predicated upon the quality and quantity of discharge measured or observed during the Phase I Analysis, as well as the relative drainage areas upstream of the overflow regulator channels, for each area. Included within this table are the approximate drainage areas of each overflow system, as well as the peak overflow observed during the Phase I Analysis. This information formed the basis for the determination of the level of effort necessary to evaluate each of the 58 Combined Sewer Overflow Areas.

Land Use

Detailed land use information has been developed upon each of the major and four of the moderate overflow areas (Fourth Avenue, Polk Street, Rector Street and Jackson Street). All segments of the CSO drainage areas have been inspected by field crews in order to develop an accurate understanding of the physical runoff characteristics of each segment and the drainage areas as a whole. As per the methodology section, intensive field investigations were utilized to obtain detailed information upon the number and types of buildings, area drainage, impervious areas, and roof drainage. This information, in conjunction with the 200' scale topographic mapping (5' intervals), was utilized to develop land use and runoff characteristics within each area.

Schematics have been developed to summarize the field investigations on land use for specific drainage areas. Plates 3-1 through 3-18 illustrate the detailed information gathered for the sixteen overflow areas investigated. Each schematic shows the relative shape of the drainage area, the main interceptor sewers, the sub-catchment boundaries

946510053

separated into residential, commercial, industrial, and open/park areas, and the average percent impervious area within each sub-catchment.

Drainage areas have been separated by municipality and overflow. In those locations wherein the drainage area is extensive and in which several sub-areas are located, the land use has been separated by sub-area. The larger drainage areas have been separated into several areas so that land use changes within each drainage area could be delineated in greater detail.

System Information

Besides the compilation of land use data, information upon the physical and hydraulic characteristics have been derived and compiled for each drainage area tributary to the overflow facilities. The level of effort within each drainage area was established in such detail as was required by the various levels of modeling utilized within each catchment area.

Specific data related to each Combined Sewer Overflow area has been obtained and plotted upon 200' scale topographic base maps. Included within the mapping are the location of existing drainage inlets, combined, sanitary and storm piping, manhole division chambers, internal overflows and outlet facilities in each drainage area. In addition, each drainage area has been delineated and plotted to provide a clearer understanding of the areas involved. This information is provided in a separate portion of the facility plan entitled Passaic Valley Sewerage Commissioners' Combined Sewer Overflow Facility Plan Area Plan.

946510054

Additional information has been compiled upon the hydraulic profiles of major interceptor sewers within each of the major and moderate overflow areas as listed on Table 3.2. The profiled sewer reaches have been shown as shaded areas on the Area Plans thus making their identification easier. Information on pipe size, slope, lateral connections, and computed capacity has been plotted to a convenient scale. All profiles have been compiled and are provided in a separate portion of the facility plan entitled Passaic Valley Sewerage Commissioners' Combined Sewer Overflow Facility Plan, Profiles of Major Interceptor Sewers.

Monitoring of quality and quantity of flow has been completed for Fourth Avenue, Polk Street, Rector Street, and Jackson Avenue overflows in addition to each of the major overflow areas.

Flow monitoring was conducted during several rainfall events to assess the loadings contributed by the various sub-basins within each overflow area and to obtain data necessary for the calibration and the verification of drainage area modeling. The level of effort applied to each drainage area was dependent upon various physical parameters including total area, peak flow conditions, and the number and configuration of major interceptor sewers. In all, over fifty individual locations have been monitored within the seventeen combined sewer overflow areas requiring detailed investigation.

Schematics and computer graphics have been used to summarize the data compiled during this phase of the facility plan. Plates 3-19 through 3-38 illustrate in tabular and graphic form the data obtained upon flow quality and quantity within each of the drainage areas monitored. The information

946510055

provided includes data on the general layout of each drainage area, the number and general location of monitoring stations, and flow quality/ quantity information. This data has been tabulated according to the monitoring station. The minimum flow, the maximum flow, and the average daily flow are recorded for each station for each day of monitoring, in addition to the minimum and the maximum concentrations for C-BOD, TVSS, TSS, NO_2, NO_3, and NH_3.

For each drainage area analysis, the water quality/quantity data has been plotted to illustrate the relative distribution of flow, C-BOD, TSS and NH_3 for each overflow area. This information has been provided for one day within the monitoring period to provide a better understanding of the flow and water quality dynamics for each drainage area monitored. The graphics are utilized to display general trends within each drainage ares and are not meant to give clear graphic displays of specific flow and water quality parameters.

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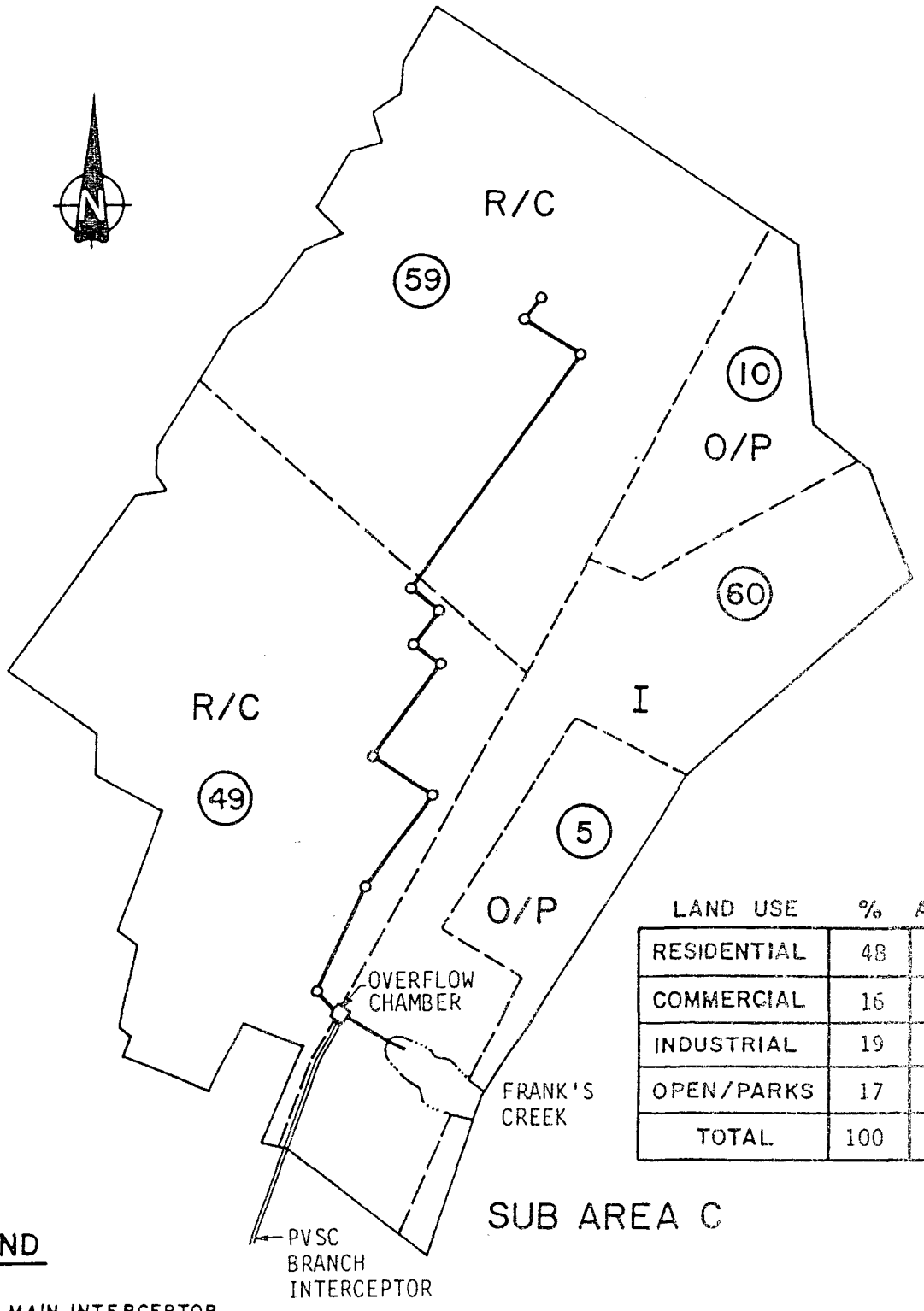


LAND USE	%	ACRES
RESIDENTIAL	48	398
COMMERCIAL	16	131
INDUSTRIAL	19	163
OPEN/PARKS	17	139
TOTAL	100	831

SUB AREA C

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

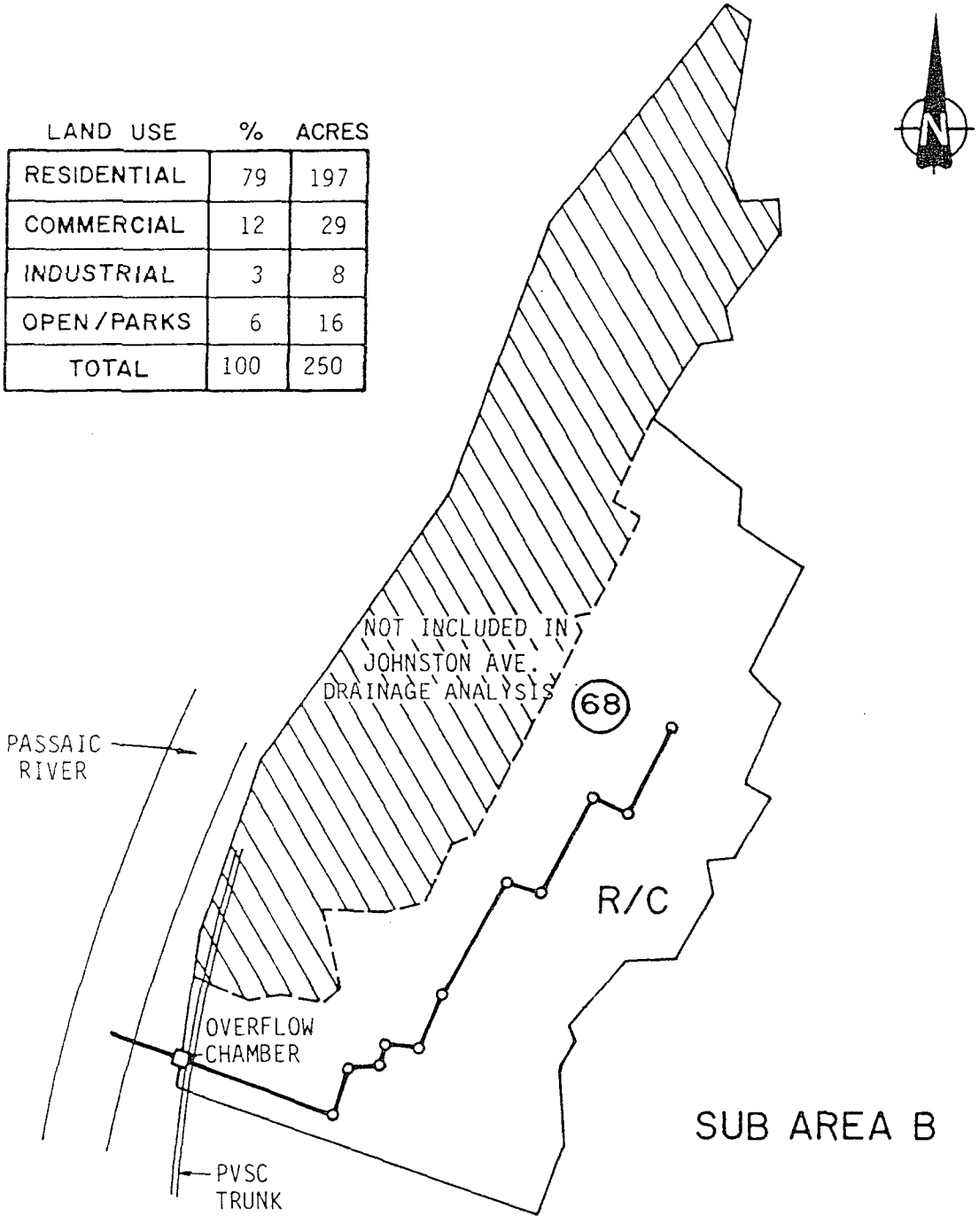
LAND USE
IVY STREET OVERFLOW
TOWN OF KEARNY

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510057

FIGURE 3-1

LAND USE	%	ACRES
RESIDENTIAL	79	197
COMMERCIAL	12	29
INDUSTRIAL	3	8
OPEN/PARKS	6	16
TOTAL	100	250



LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

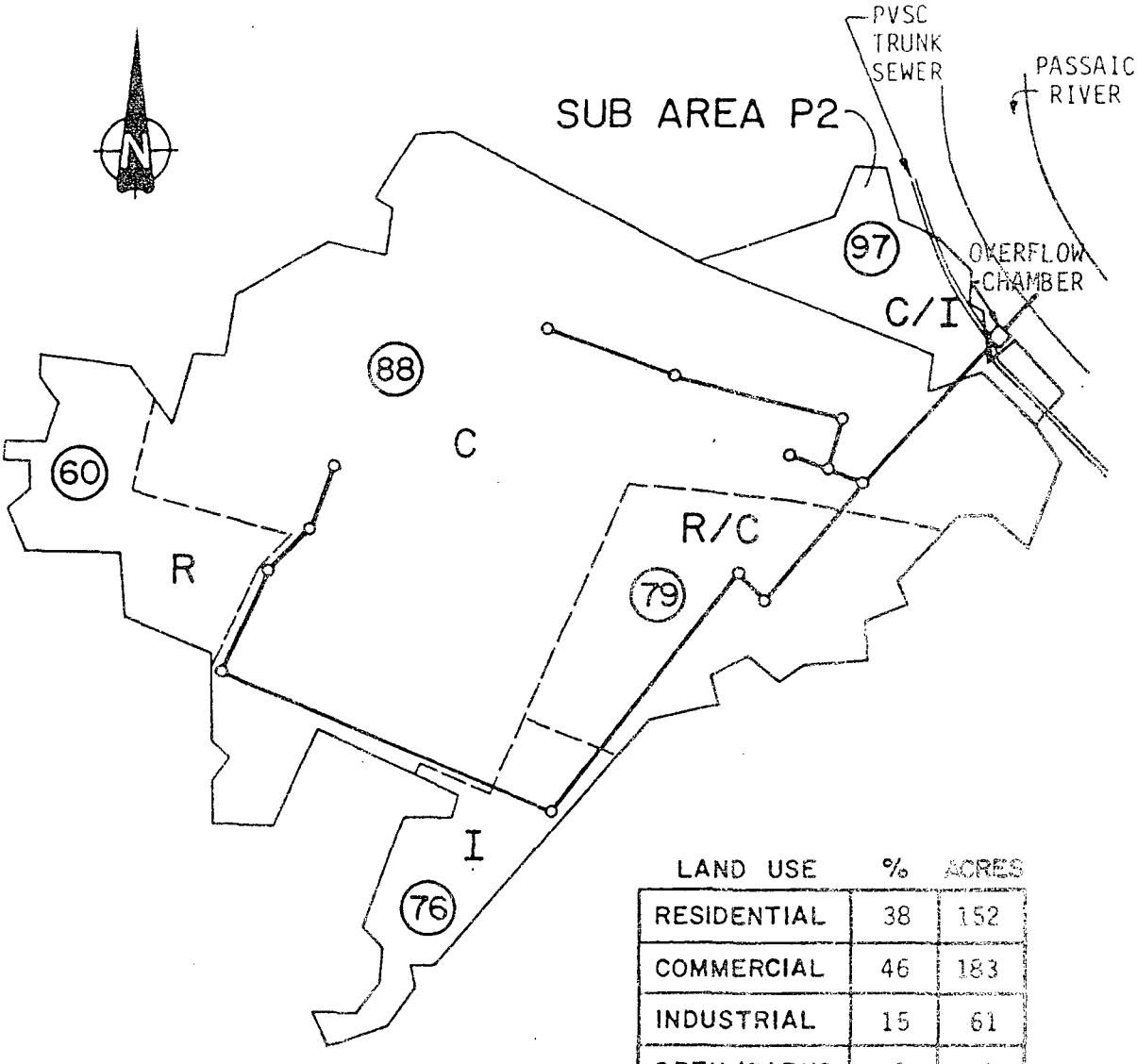
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
JOHNSTON AVE. OVERFLOW
TOWN OF KEARNY

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510058

FIGURE 3-2



LAND USE	%	ACRES
RESIDENTIAL	38	152
COMMERCIAL	46	183
INDUSTRIAL	15	61
OPEN/PARKS	1	1
TOTAL	100	397

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

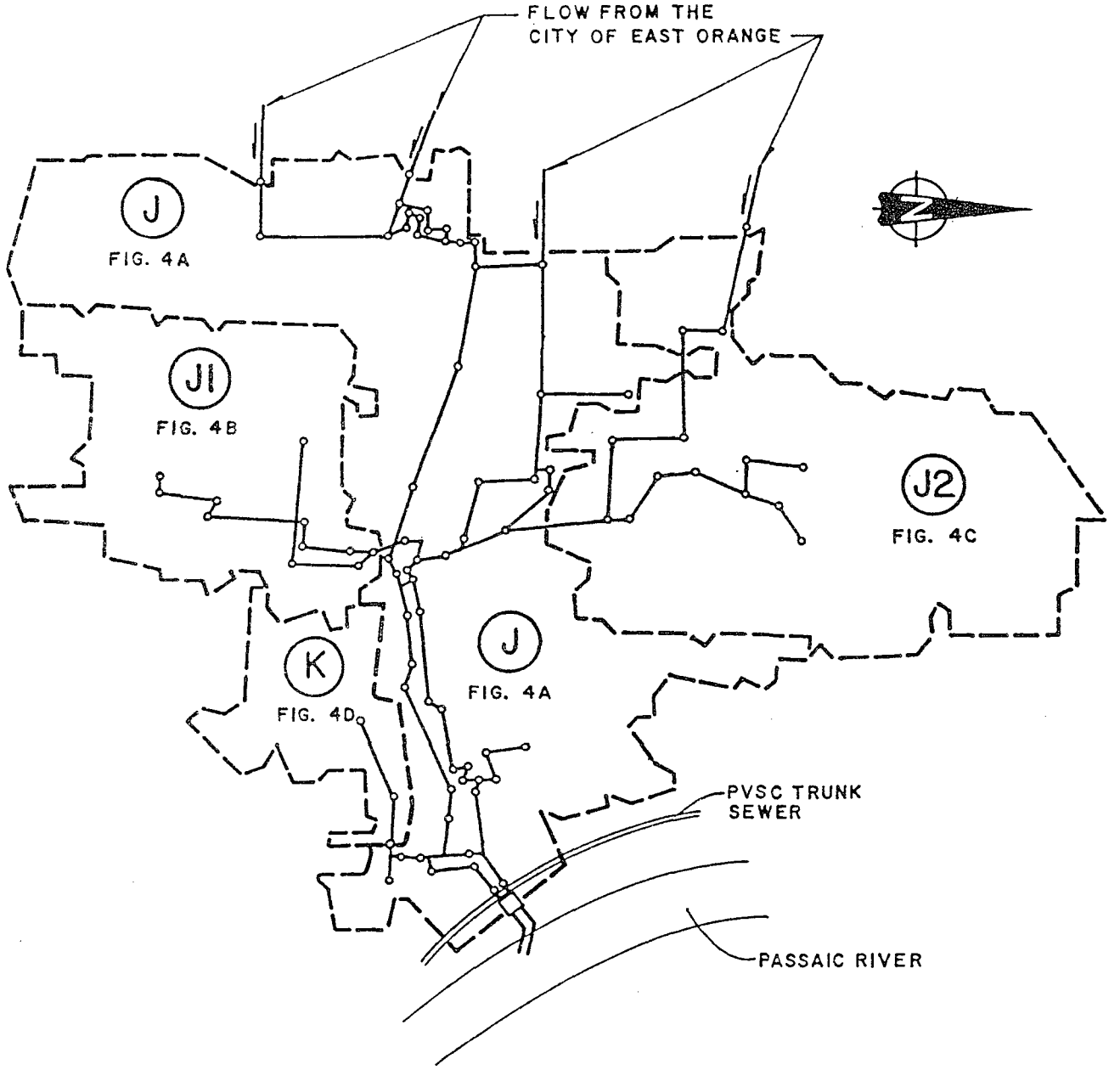
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
CITY DOCK OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Chester Street Millburn New Jersey 07041

946510059

FIGURE 3-3



LEGEND

- MAIN INTERCEPTOR
- SUBCATCHMENT BOUNDARY
- (J) SUBCATCHMENT AS INDICATED IN PHASE IIA I/I REPORT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

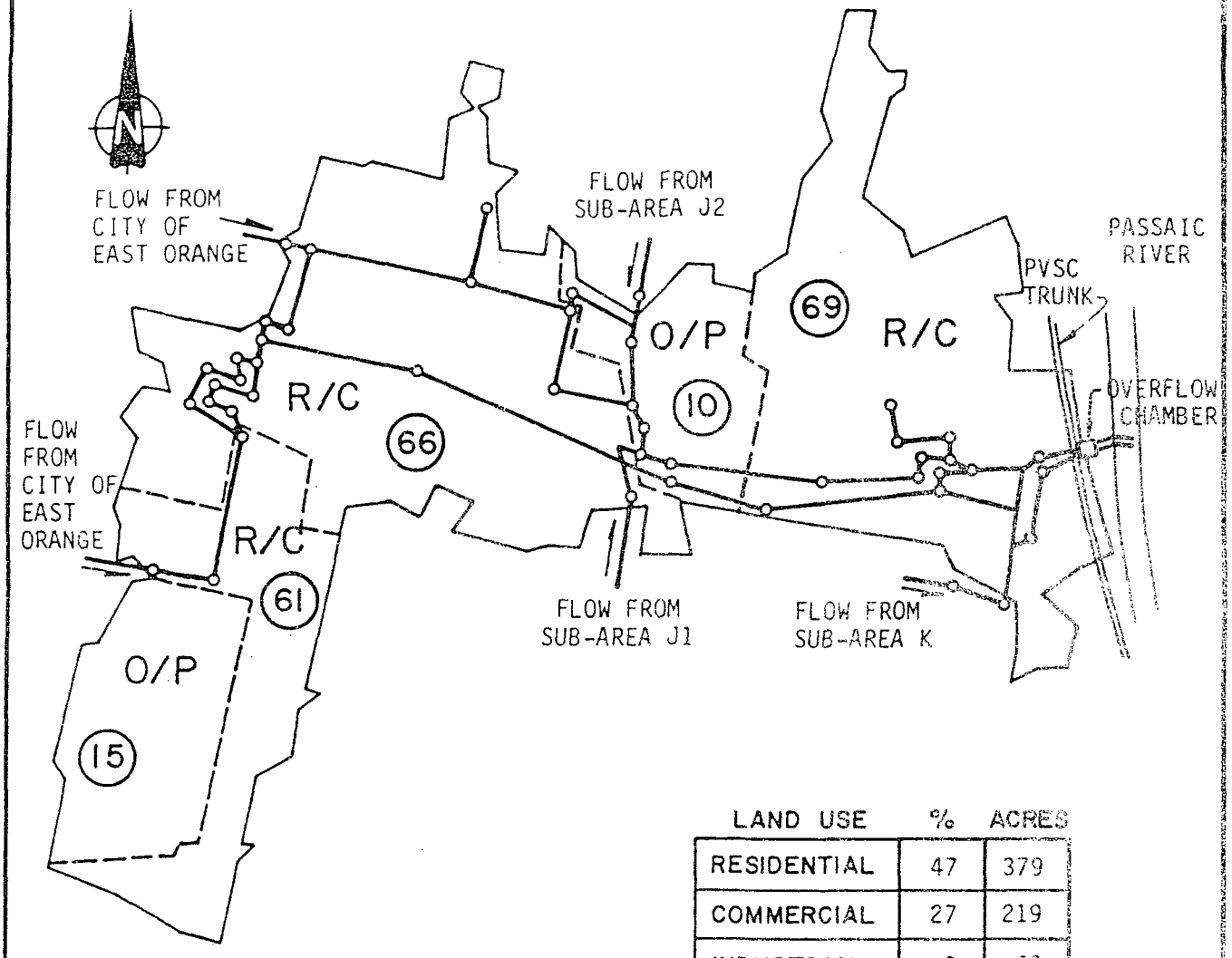
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

946510060

FIGURE 3-4



LAND USE	%	ACRES
RESIDENTIAL	47	379
COMMERCIAL	27	219
INDUSTRIAL	8	60
OPEN/PARKS	18	147
TOTAL	100	805

SUB AREA J

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

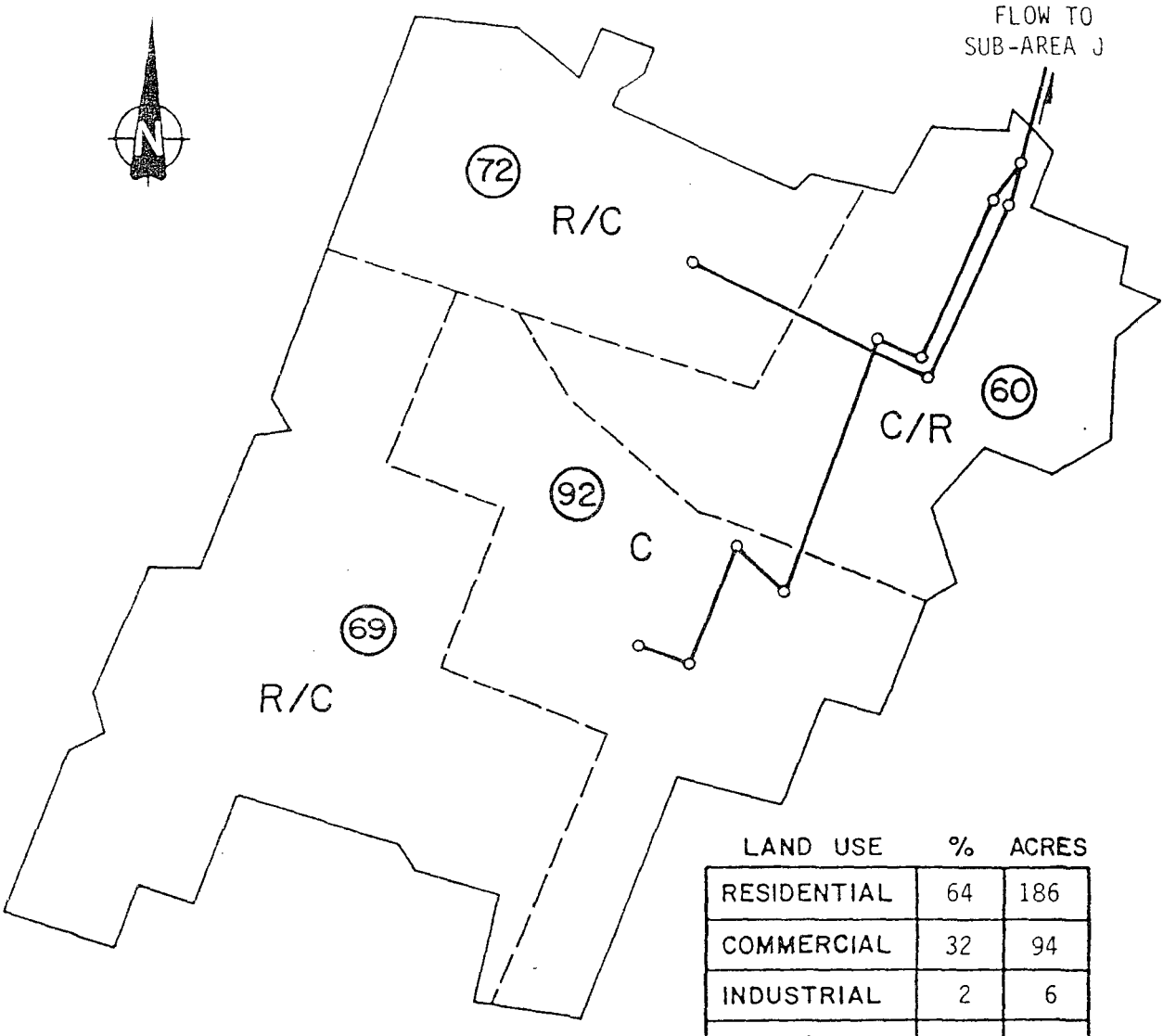
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

946510061

FIGURE 3-4A



LAND USE	%	ACRES
RESIDENTIAL	64	186
COMMERCIAL	32	94
INDUSTRIAL	2	6
OPEN/PARKS	2	7
TOTAL	100	293

SUB AREA J1

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

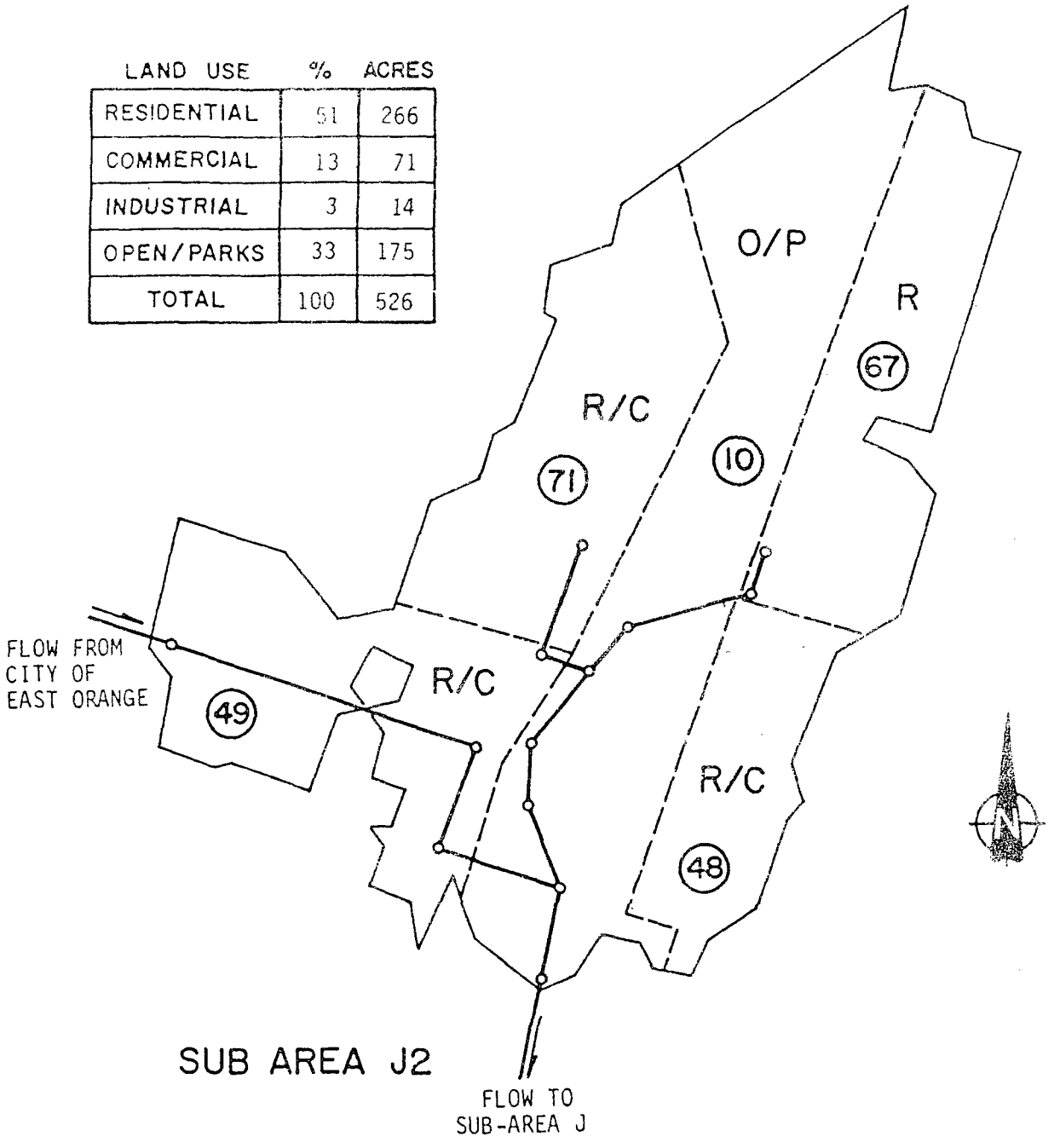
LAND USE
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

946510062

FIGURE 3-4B

LAND USE	%	ACRES
RESIDENTIAL	51	266
COMMERCIAL	13	71
INDUSTRIAL	3	14
OPEN/PARKS	33	175
TOTAL	100	526



LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE

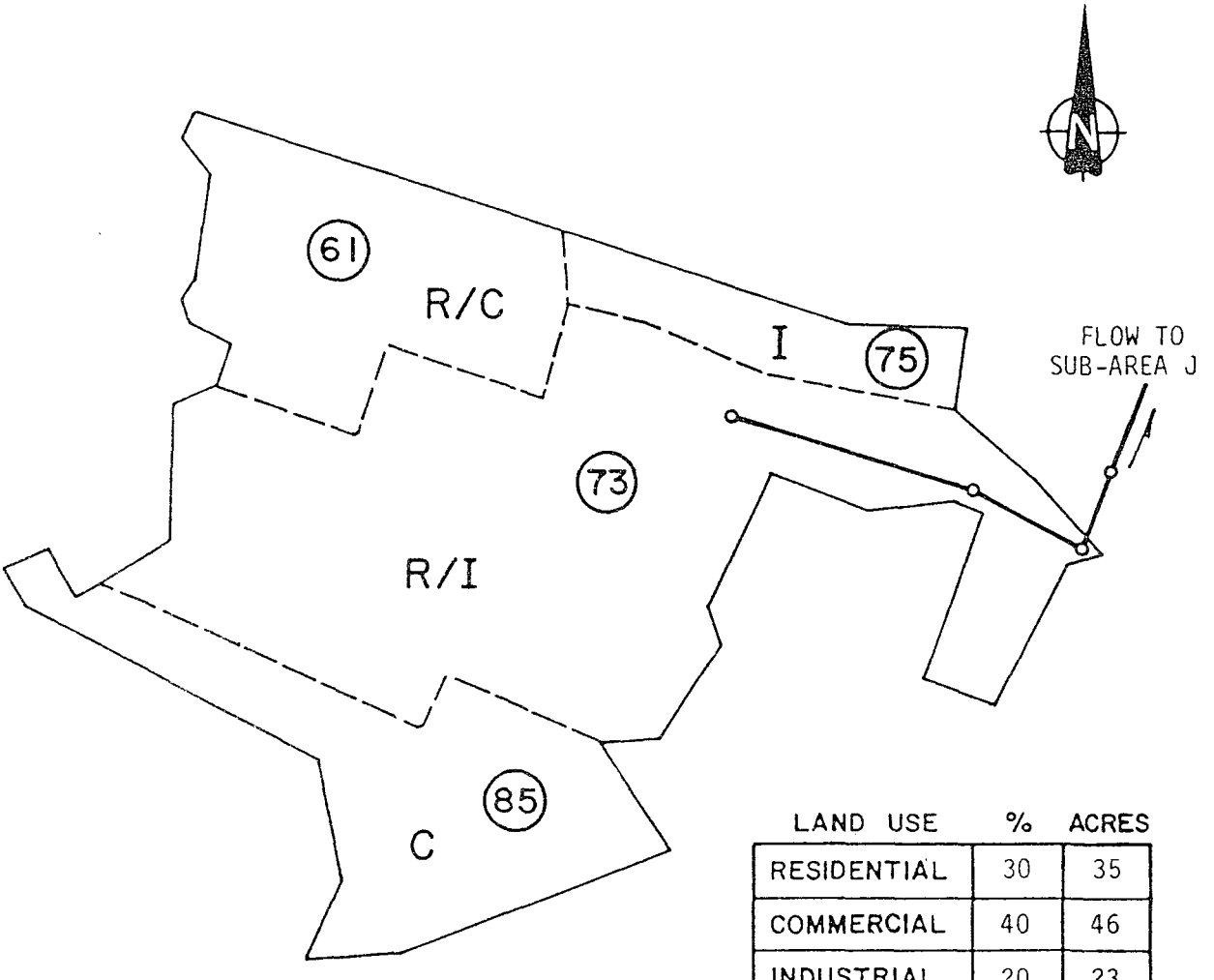
CLAY STREET OVERFLOW

CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510063

FIGURE 3-4C



SUB AREA K

LAND USE	%	ACRES
RESIDENTIAL	30	35
COMMERCIAL	40	46
INDUSTRIAL	20	23
OPEN/PARKS	10	11
TOTAL	100	115

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

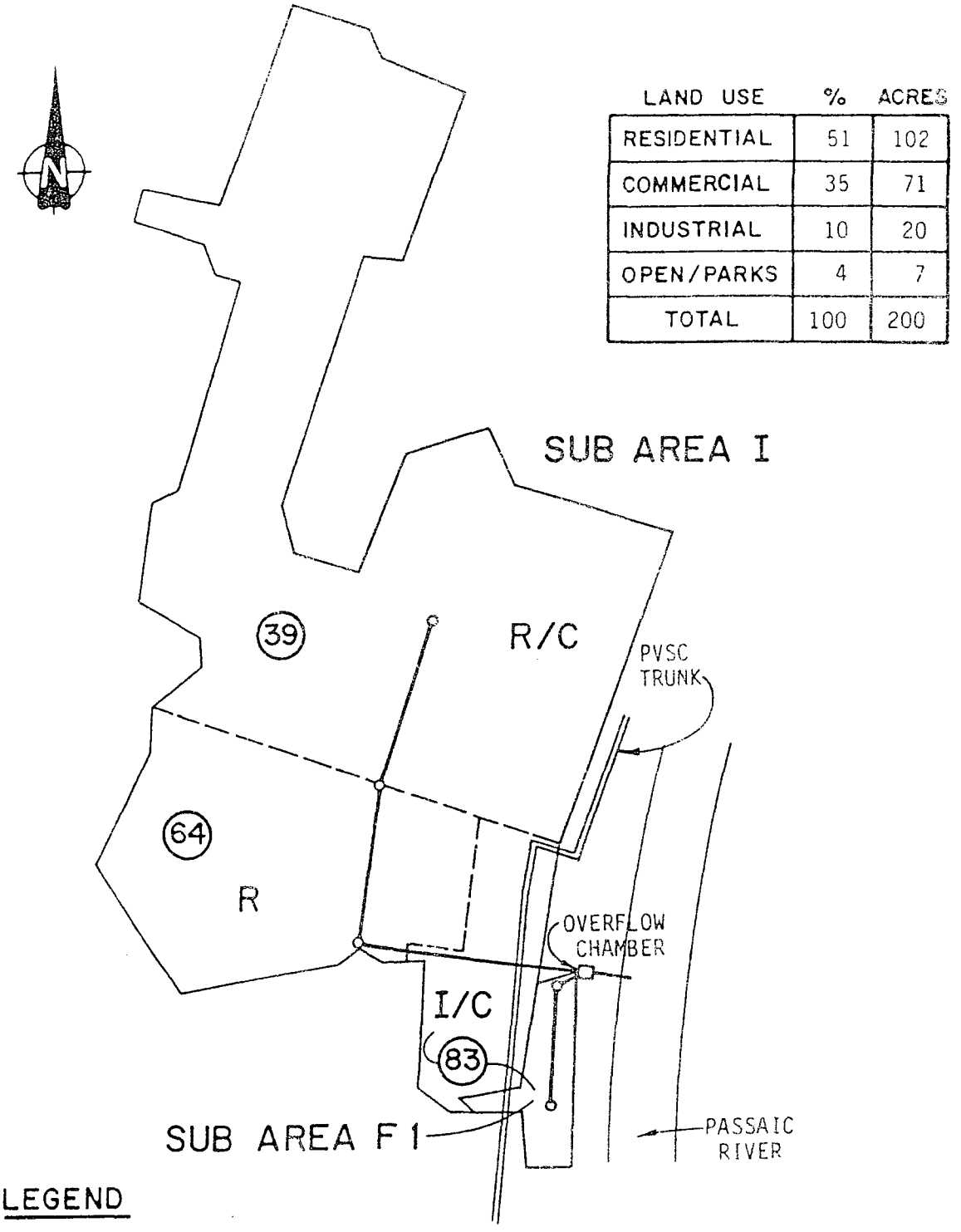
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510064

FIGURE 3-4D



LAND USE	%	ACRES
RESIDENTIAL	51	102
COMMERCIAL	35	71
INDUSTRIAL	10	20
OPEN/PARKS	4	7
TOTAL	100	200

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

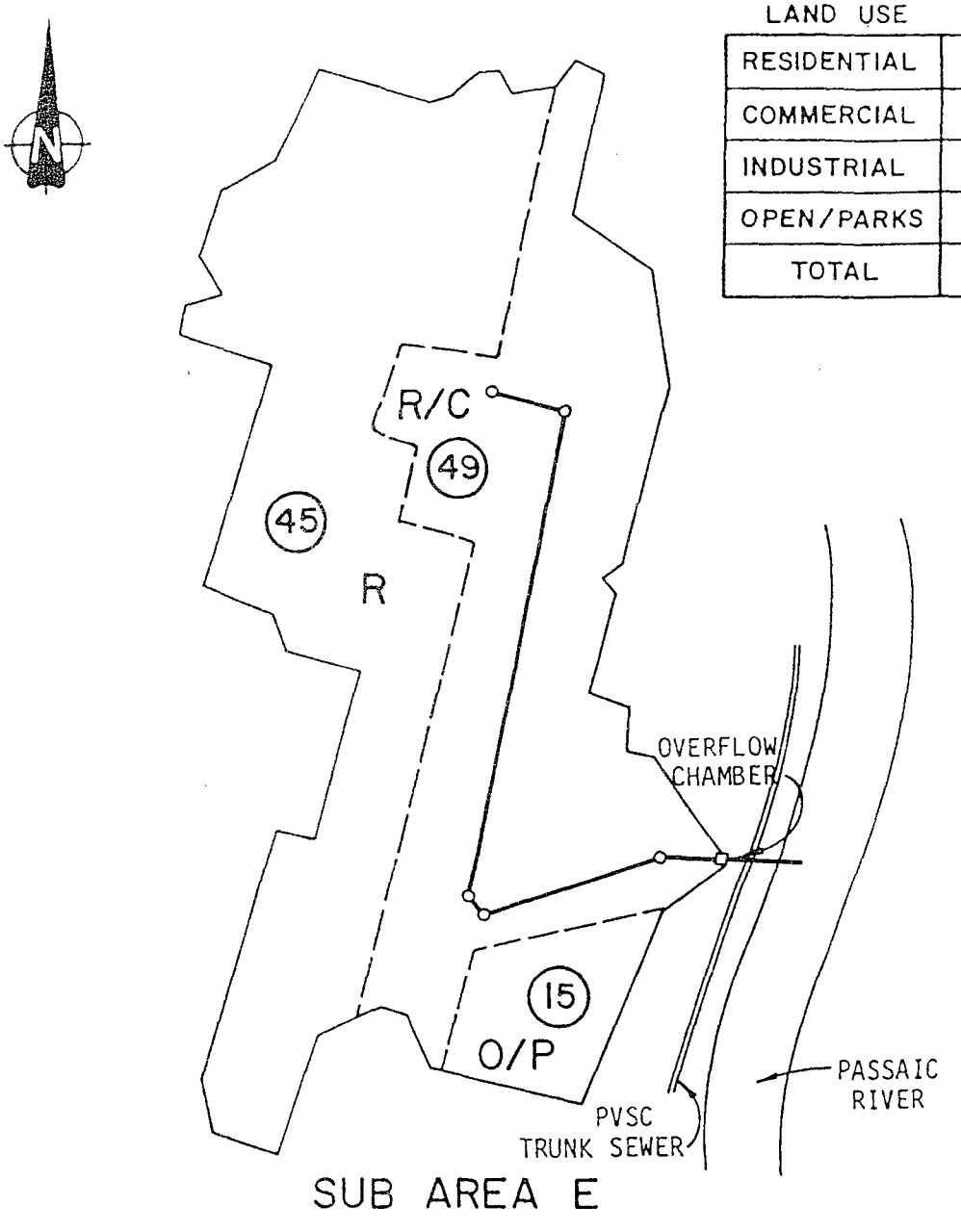
LAND USE
FOURTH AVENUE OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
22 Bleeker Street Millburn New Jersey 07041

946510065

FIGURE 3-5

LAND USE	%	ACRES
RESIDENTIAL	85	204
COMMERCIAL	9	23
INDUSTRIAL	-	-
OPEN/PARKS	6	14
TOTAL	100	241



SUB AREA E

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE

HERBERT PLACE OVERFLOW

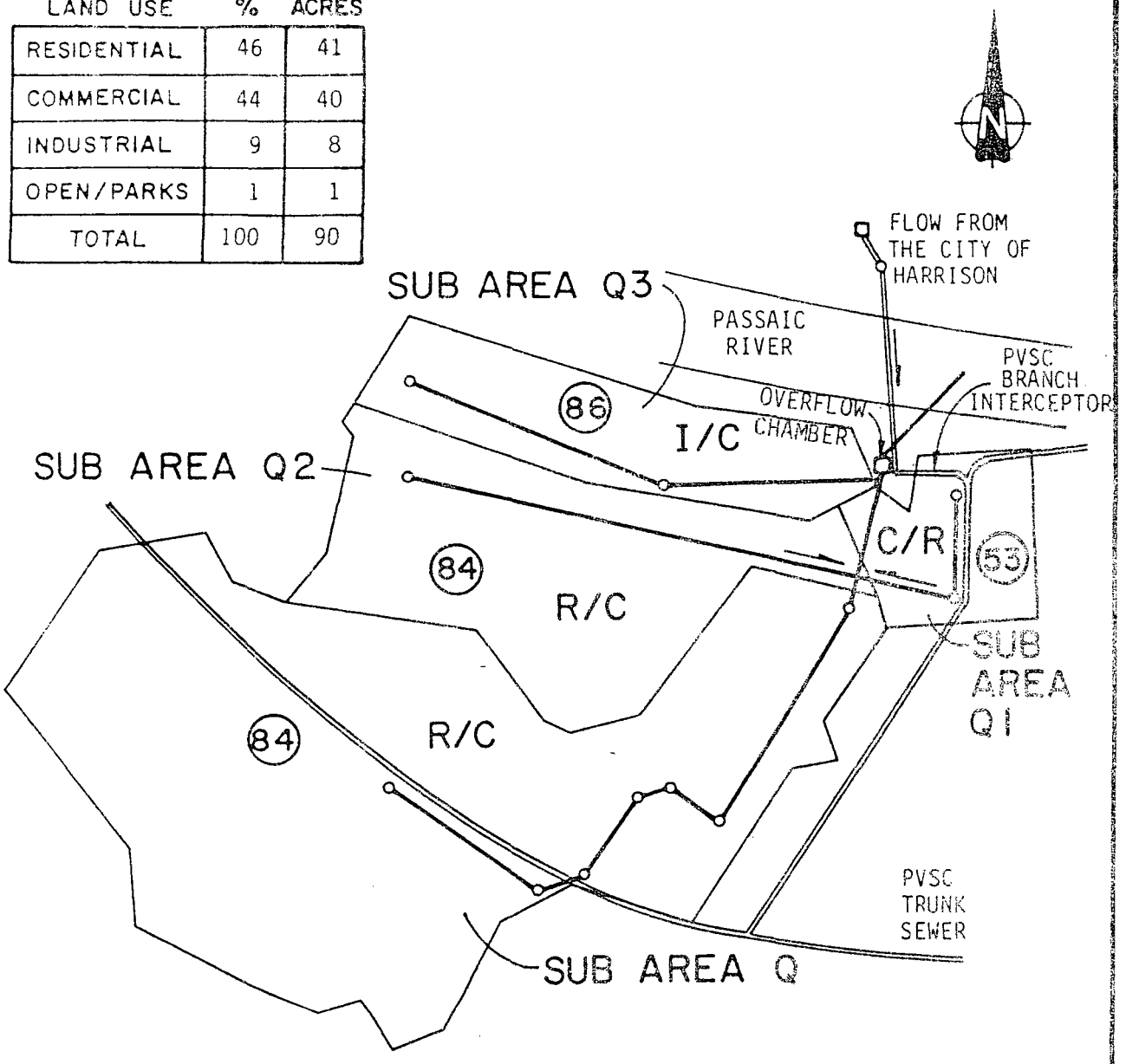
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510066

FIGURE 3-6

LAND USE	%	ACRES
RESIDENTIAL	46	41
COMMERCIAL	44	40
INDUSTRIAL	9	8
OPEN/PARKS	1	1
TOTAL	100	90



LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

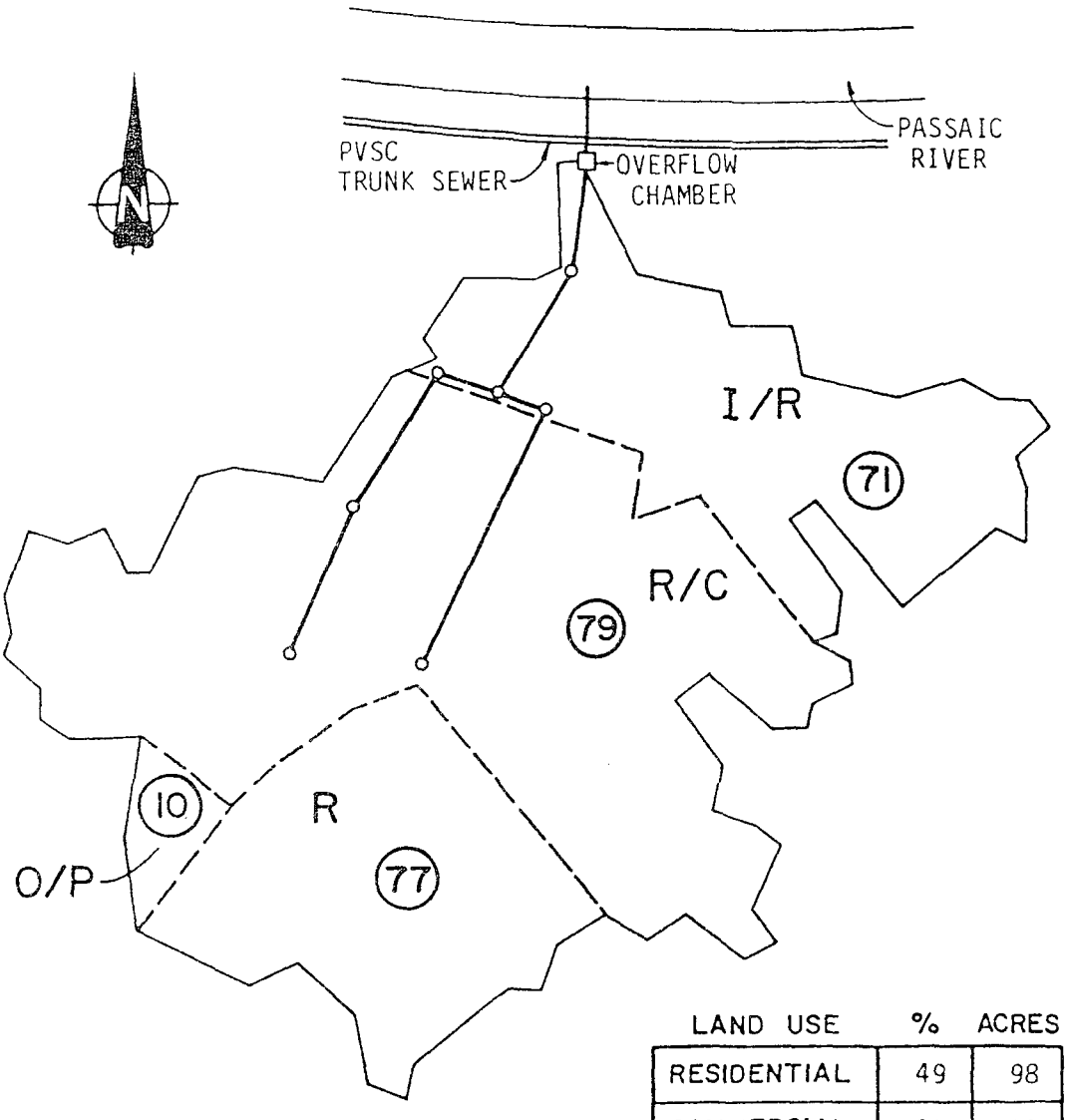
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
JACKSON STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510067

FIGURE 3-7



LAND USE	%	ACRES
RESIDENTIAL	49	98
COMMERCIAL	29	49
INDUSTRIAL	25	50
OPEN/PARKS	2	4
TOTAL	100	201

SUB AREA R

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

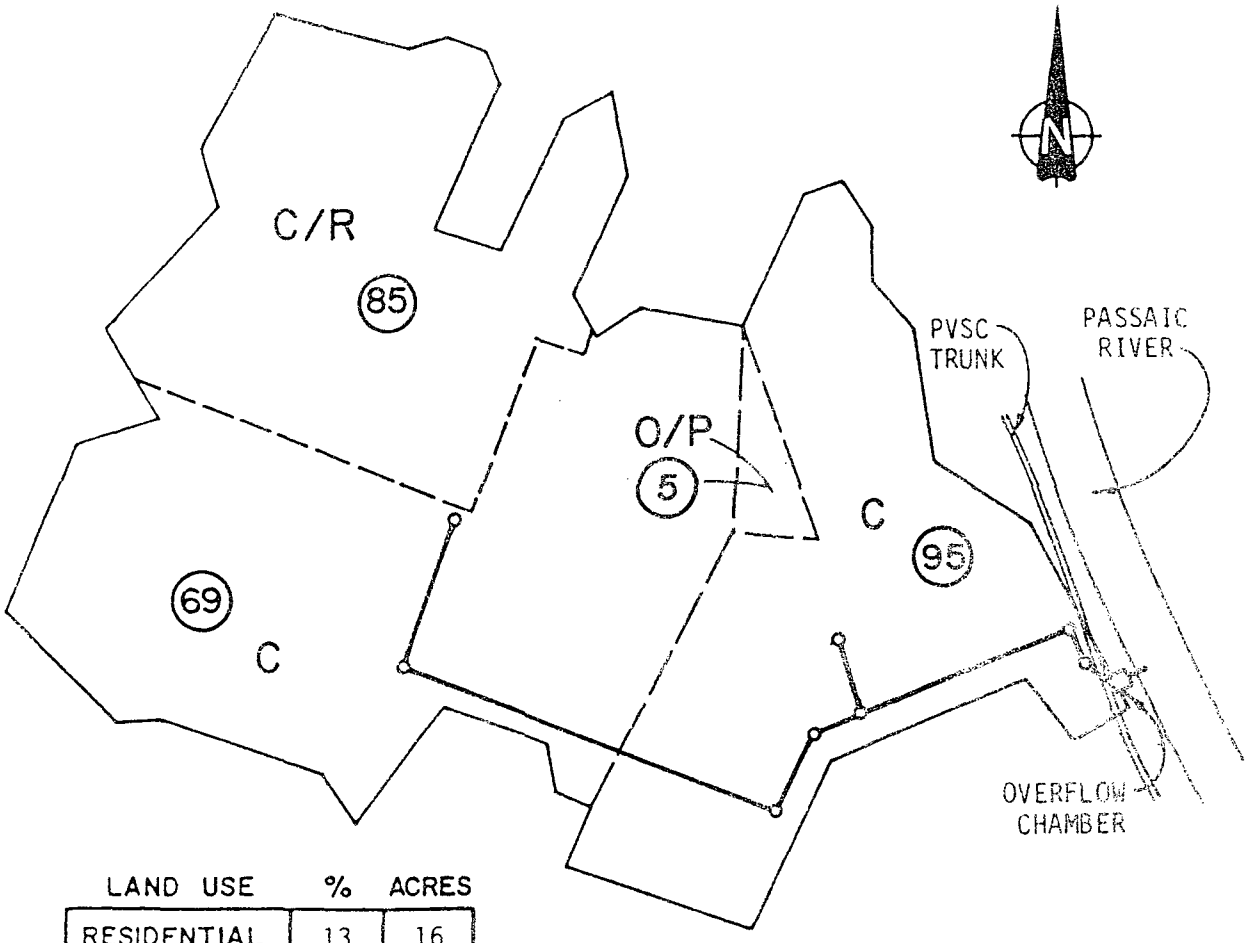
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
POLK STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510068

FIGURE 3-8



LAND USE	%	ACRES
RESIDENTIAL	13	16
COMMERCIAL	80	103
INDUSTRIAL	-	-
OPEN/PARKS	7	9
TOTAL	100	128

SUB AREA M

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

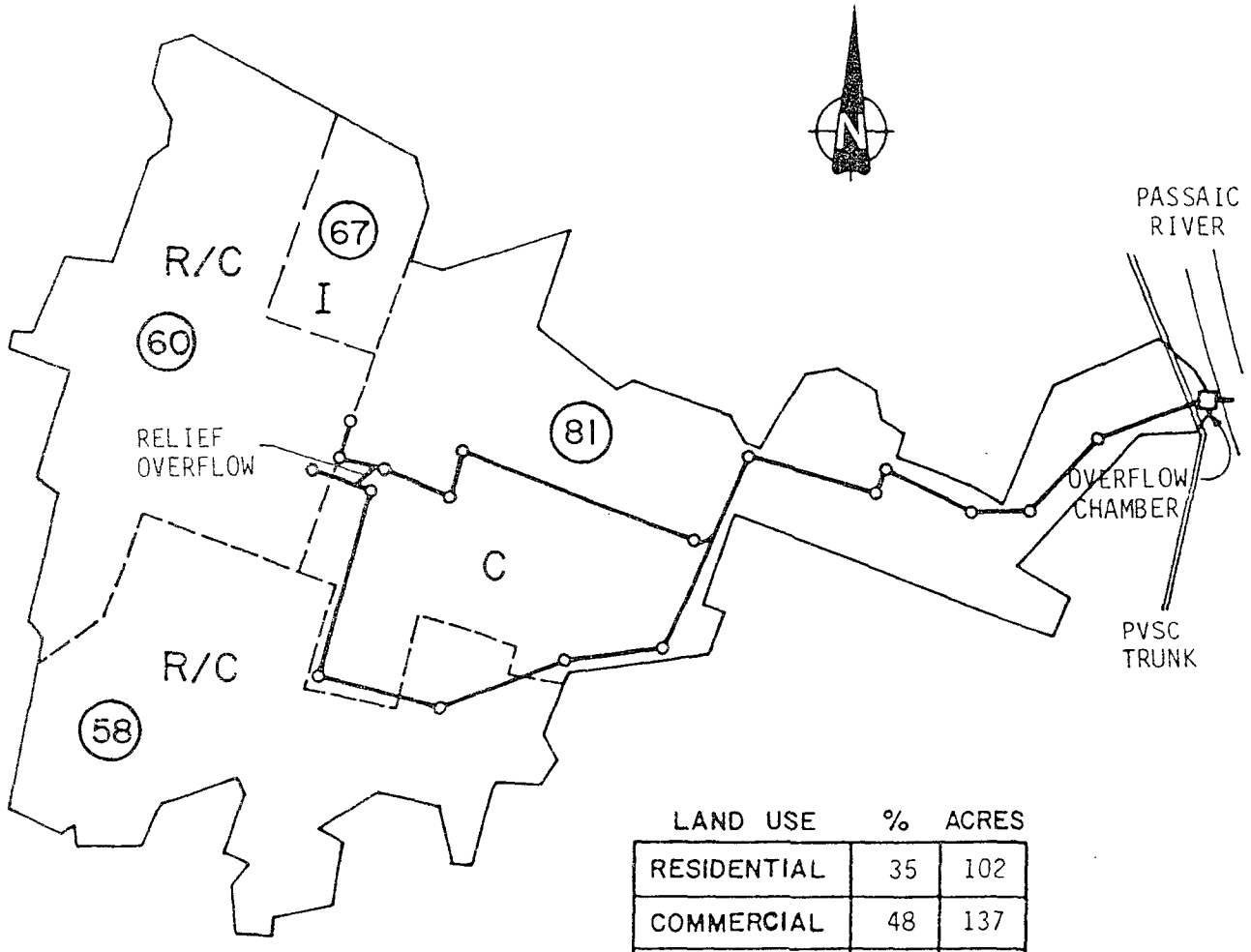
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
RECTOR STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510069

FIGURE 3-9



LAND USE	%	ACRES
RESIDENTIAL	35	102
COMMERCIAL	48	137
INDUSTRIAL	17	48
OPEN/PARKS	-	-
TOTAL	100	287

SUB AREA N

LEGEND

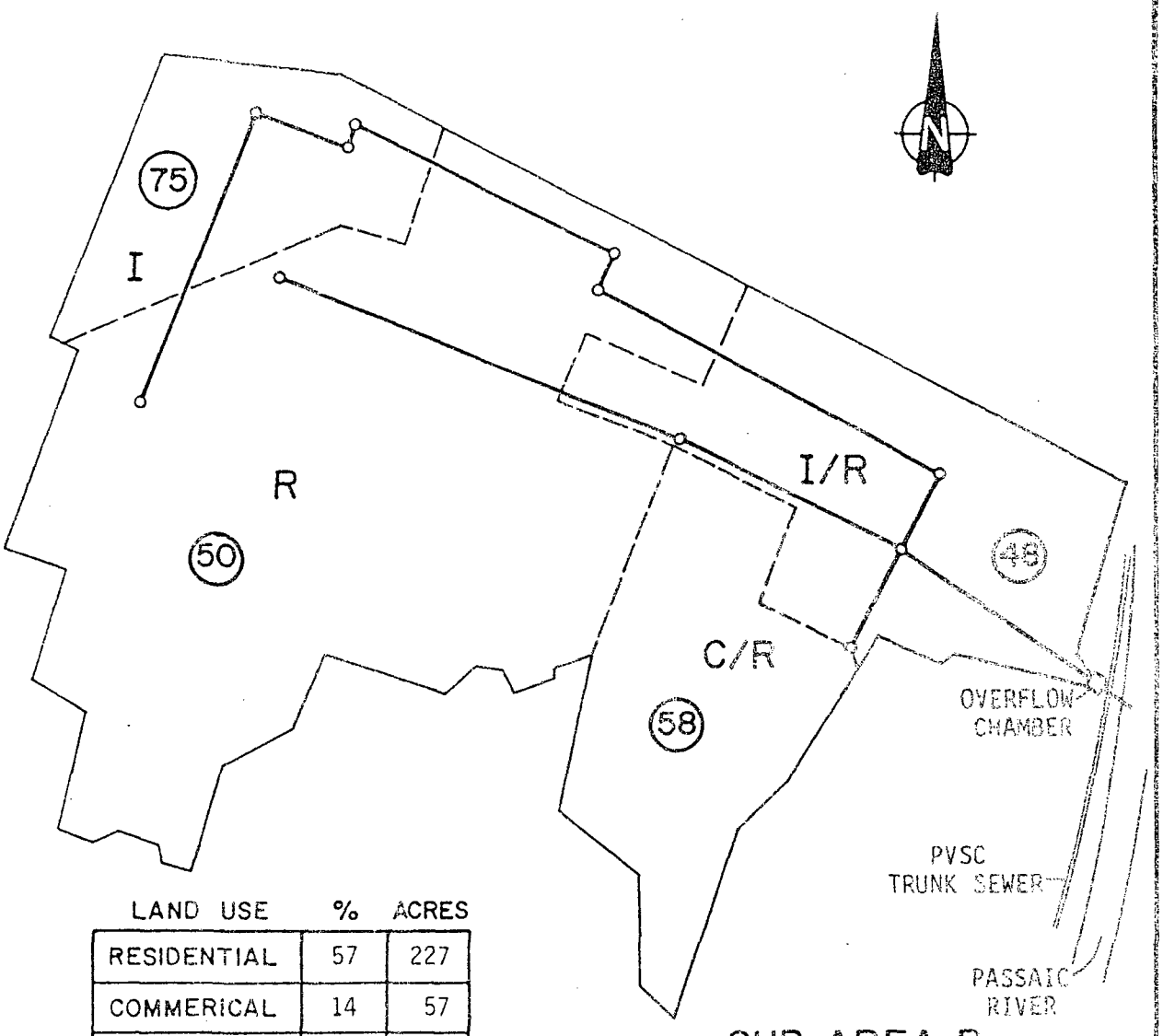
- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
LAND USE
SAYBROOK PLACE OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510070

FIGURE 3-10



LAND USE	%	ACRES
RESIDENTIAL	57	227
COMMERICAL	14	57
INDUSTRIAL	21	83
OPEN/PARKS	0	0
TOTAL	100	370

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

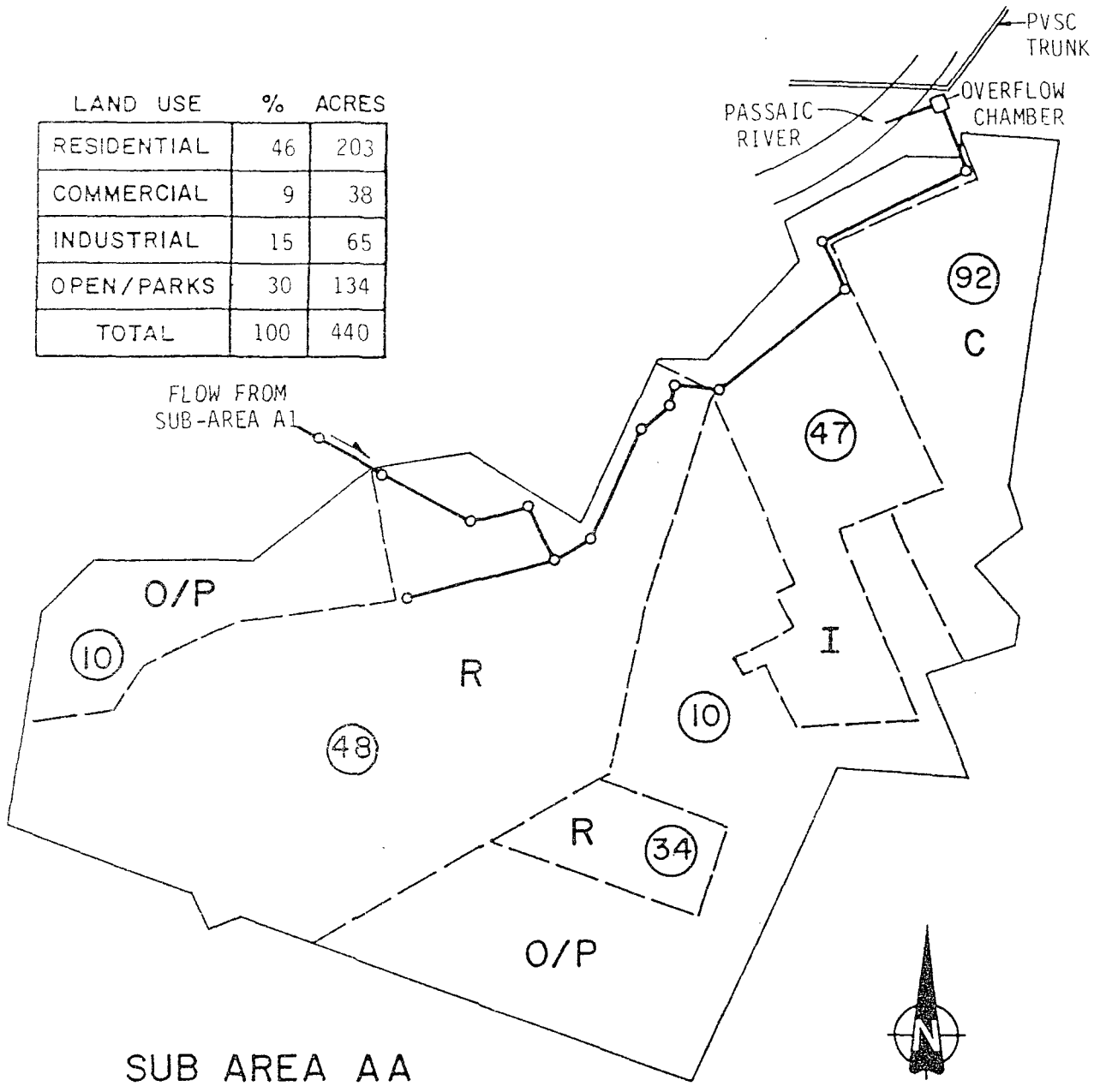
LAND USE
VERONA AVENUE OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

946510071

FIGURE 3-11

LAND USE	%	ACRES
RESIDENTIAL	46	203
COMMERCIAL	9	38
INDUSTRIAL	15	65
OPEN/PARKS	30	134
TOTAL	100	440



SUB AREA AA

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

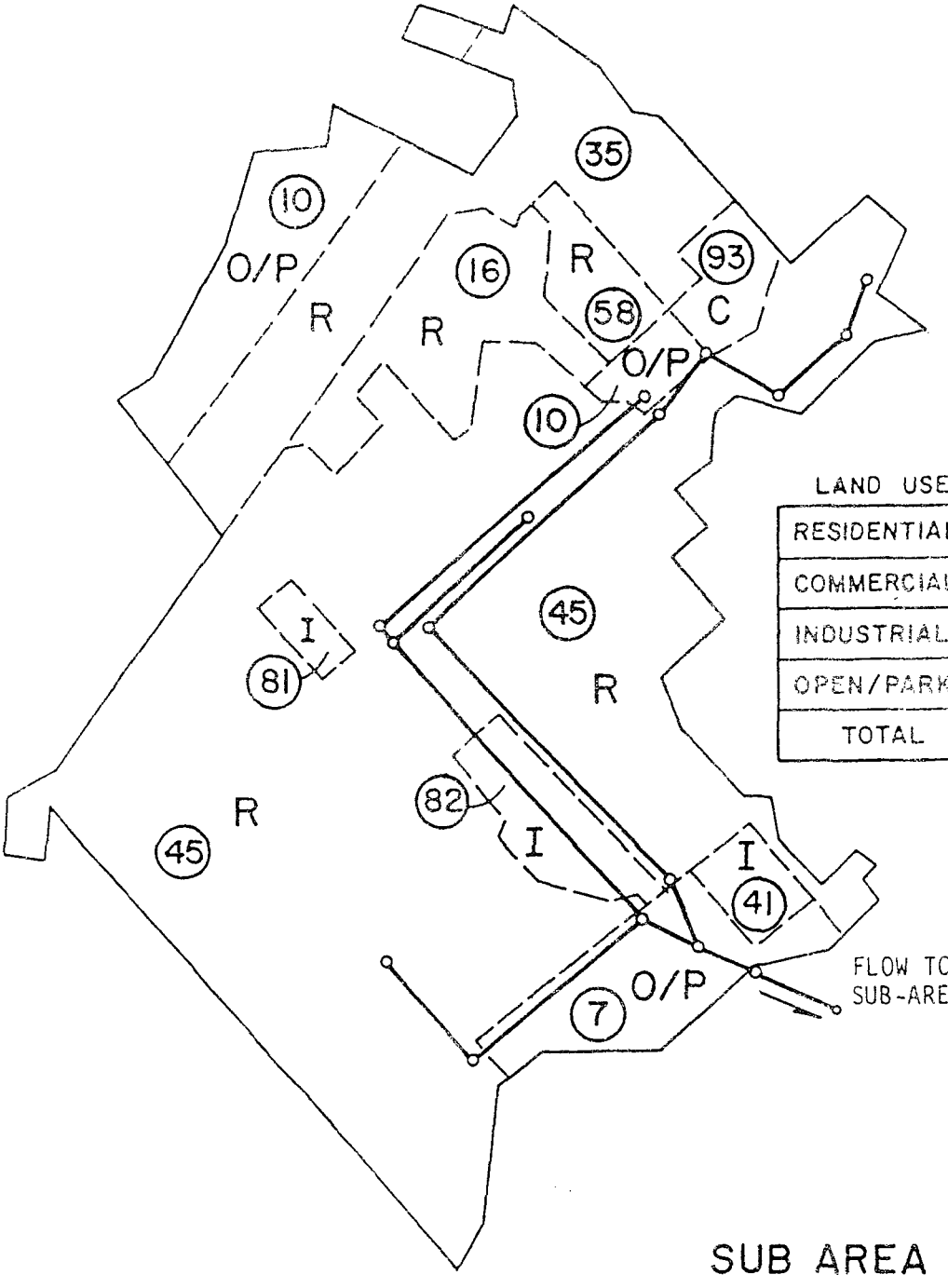
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
CURTIS PLACE OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

946510072

FIGURE 3-12A



LAND USE	%	ACRES
RESIDENTIAL	72	560
COMMERCIAL	2	19
INDUSTRIAL	5	36
OPEN/PARKS	21	159
TOTAL	100	774

SUB AREA A1

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE

CURTIS PLACE OVERFLOW

CITY OF PATERSON

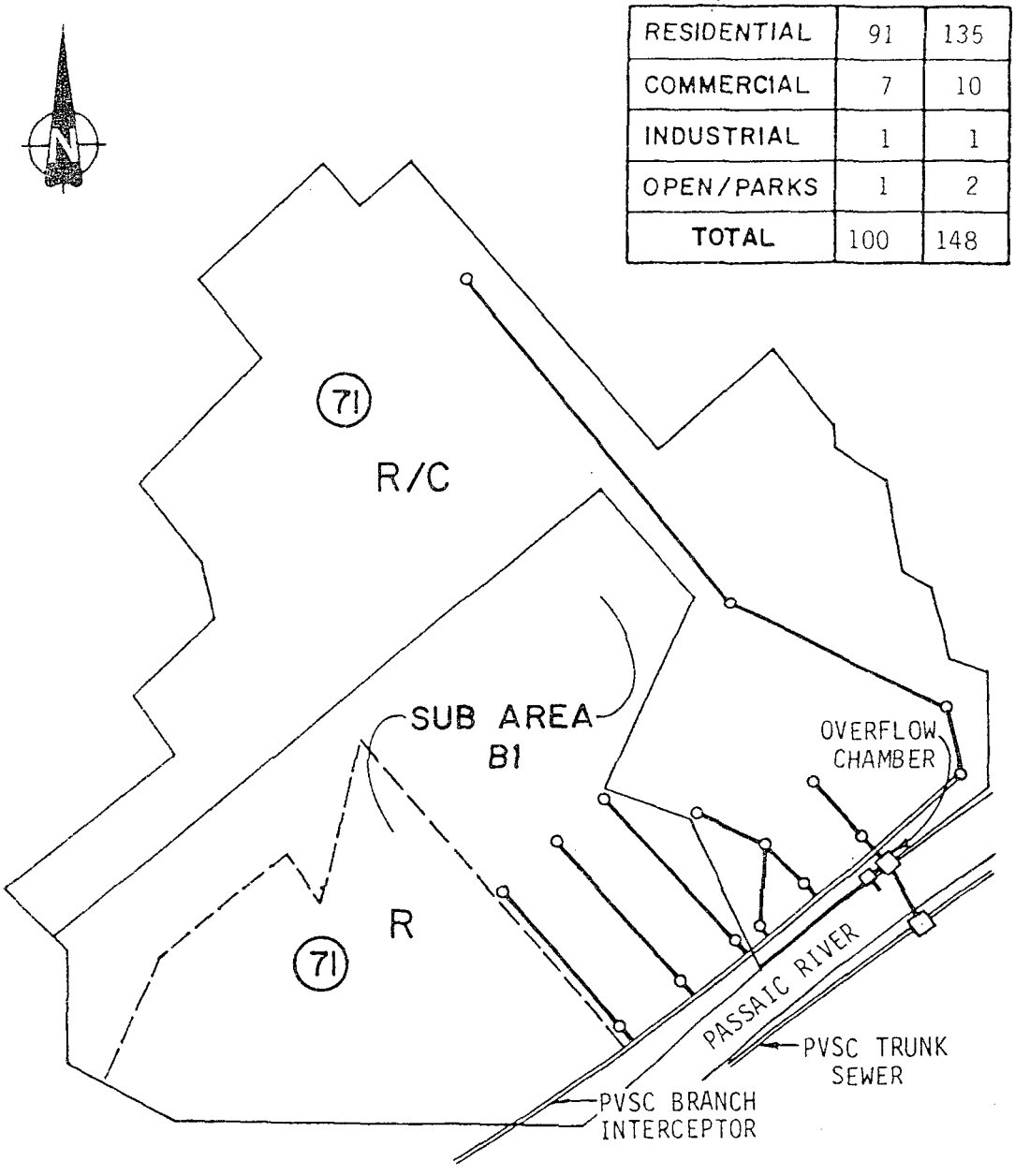
Elson T. Killam Associates, Inc.

Environmental and Hydraulic Engineers

946510073

FIGURE 3-12B

LAND USE	%	ACRES
RESIDENTIAL	91	135
COMMERCIAL	7	10
INDUSTRIAL	1	1
OPEN/PARKS	1	2
TOTAL	100	148



SUB AREA B2

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE

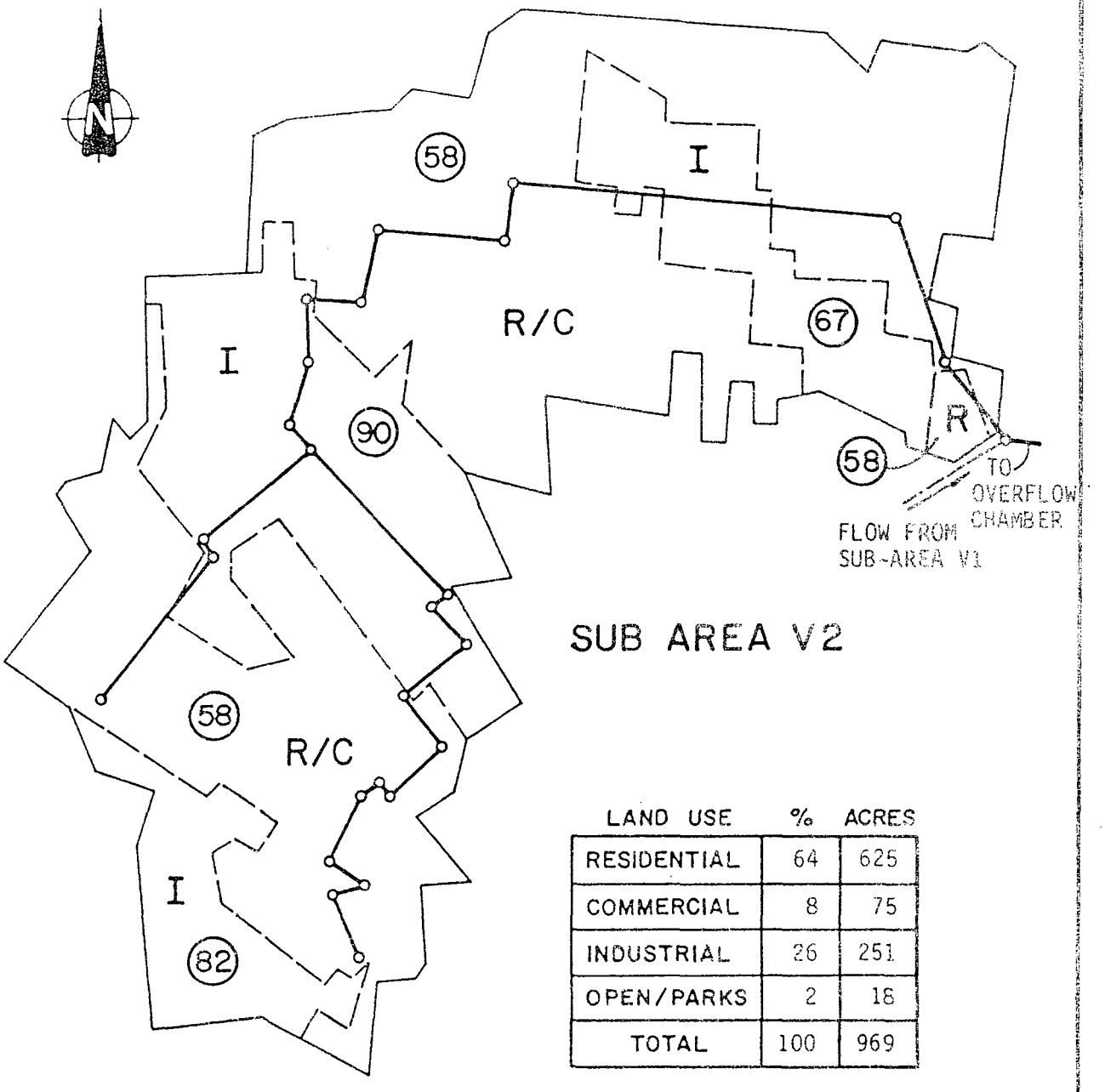
HUDSON STREET OVERFLOW

CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
Millburn New Jersey 07041

946510074

FIGURE 3-13



LAND USE	%	ACRES
RESIDENTIAL	64	625
COMMERCIAL	8	75
INDUSTRIAL	26	251
OPEN/PARKS	2	18
TOTAL	100	969

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

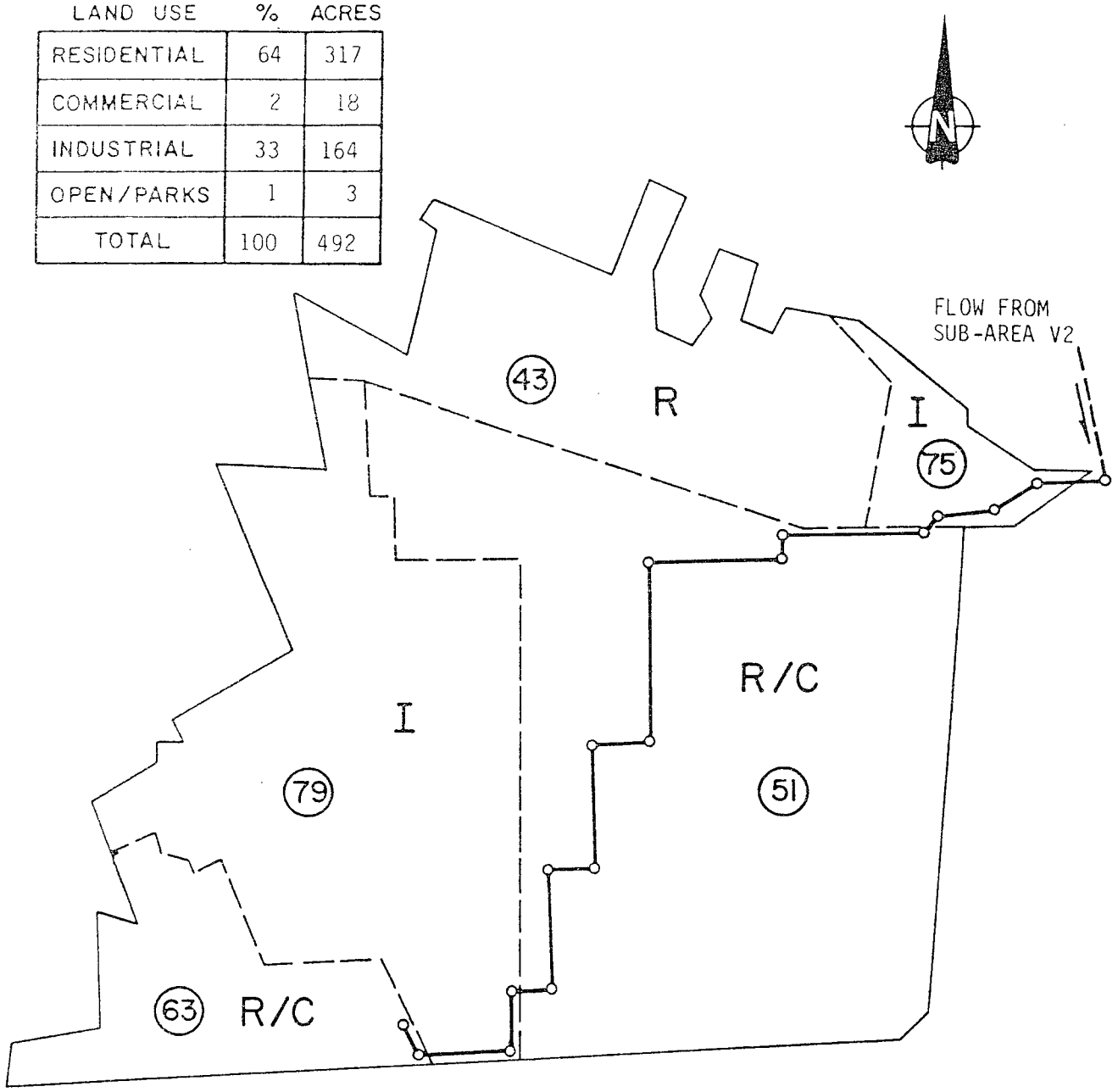
LAND USE
MARKET STREET OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

946510075

FIGURE 3-14A

LAND USE	%	ACRES
RESIDENTIAL	64	317
COMMERCIAL	2	18
INDUSTRIAL	33	164
OPEN/PARKS	1	3
TOTAL	100	492



SUB AREA V1

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

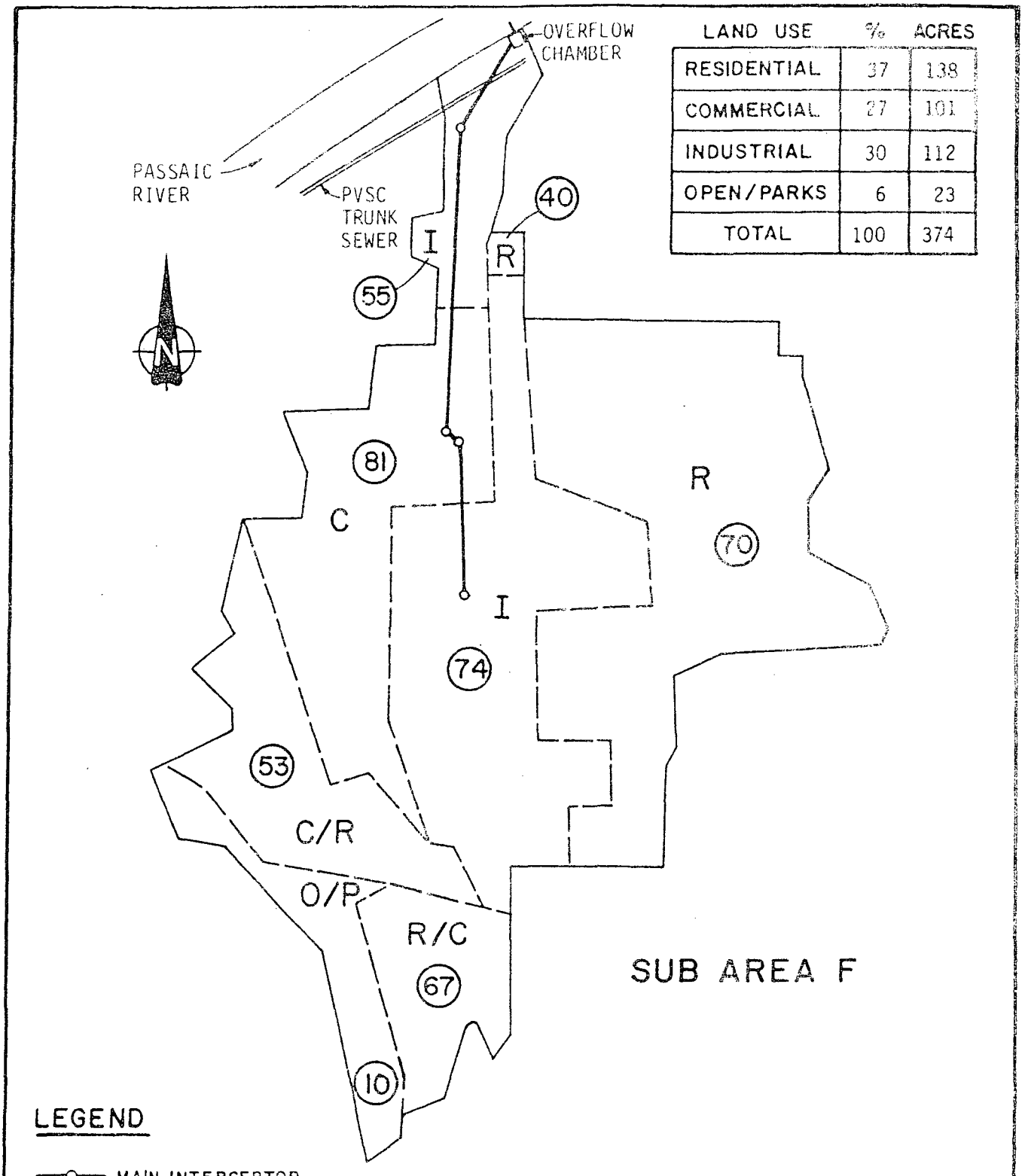
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
MARKET STREET OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510076

FIGURE 3-14B



LAND USE	%	ACRES
RESIDENTIAL	37	138
COMMERCIAL	27	101
INDUSTRIAL	30	112
OPEN/PARKS	6	23
TOTAL	100	374

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

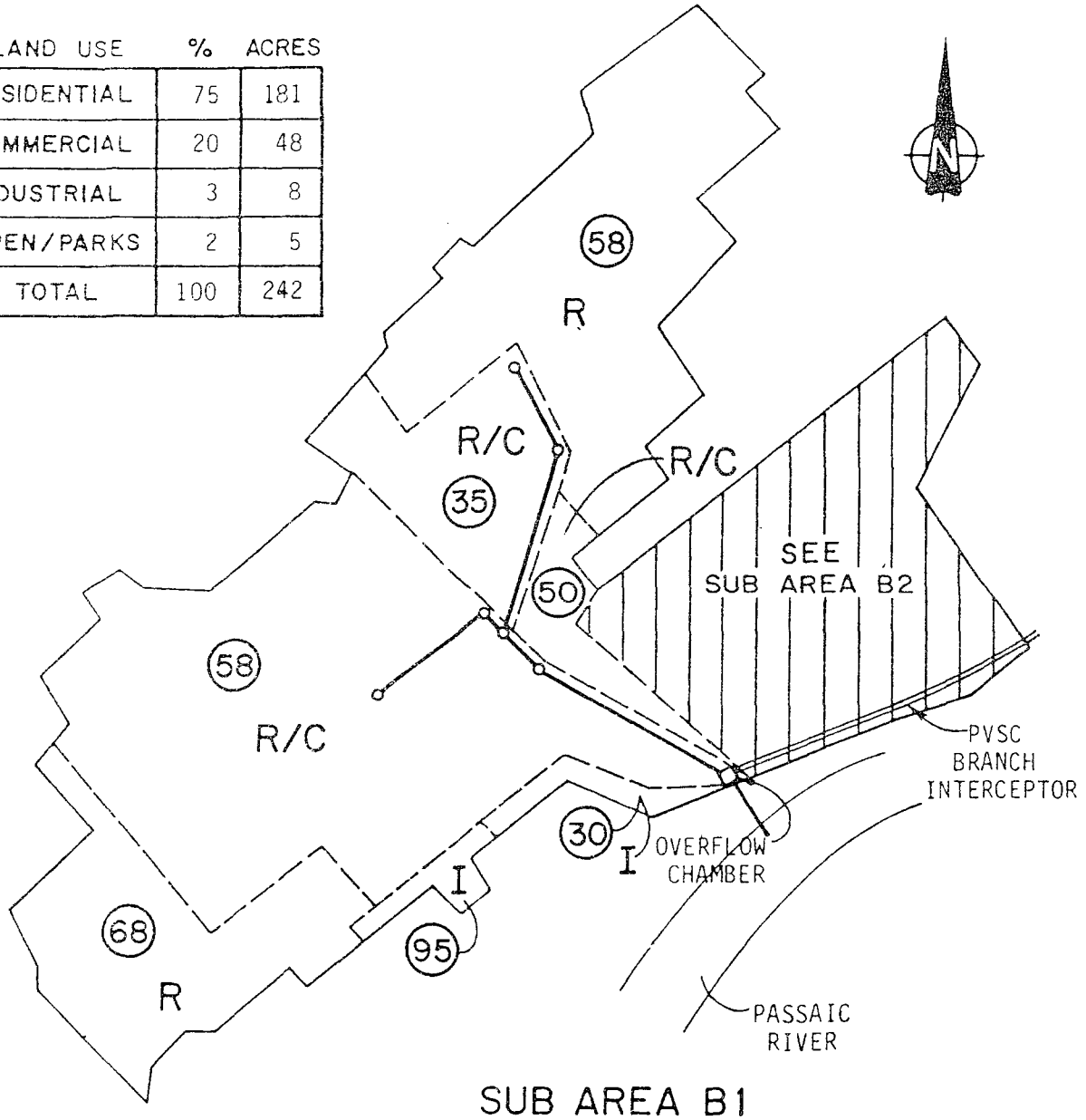
LAND USE
MONTGOMERY ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

946510077

FIGURE 3-15

LAND USE	%	ACRES
RESIDENTIAL	75	181
COMMERCIAL	20	48
INDUSTRIAL	3	8
OPEN/PARKS	2	5
TOTAL	100	242



SUB AREA B1

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

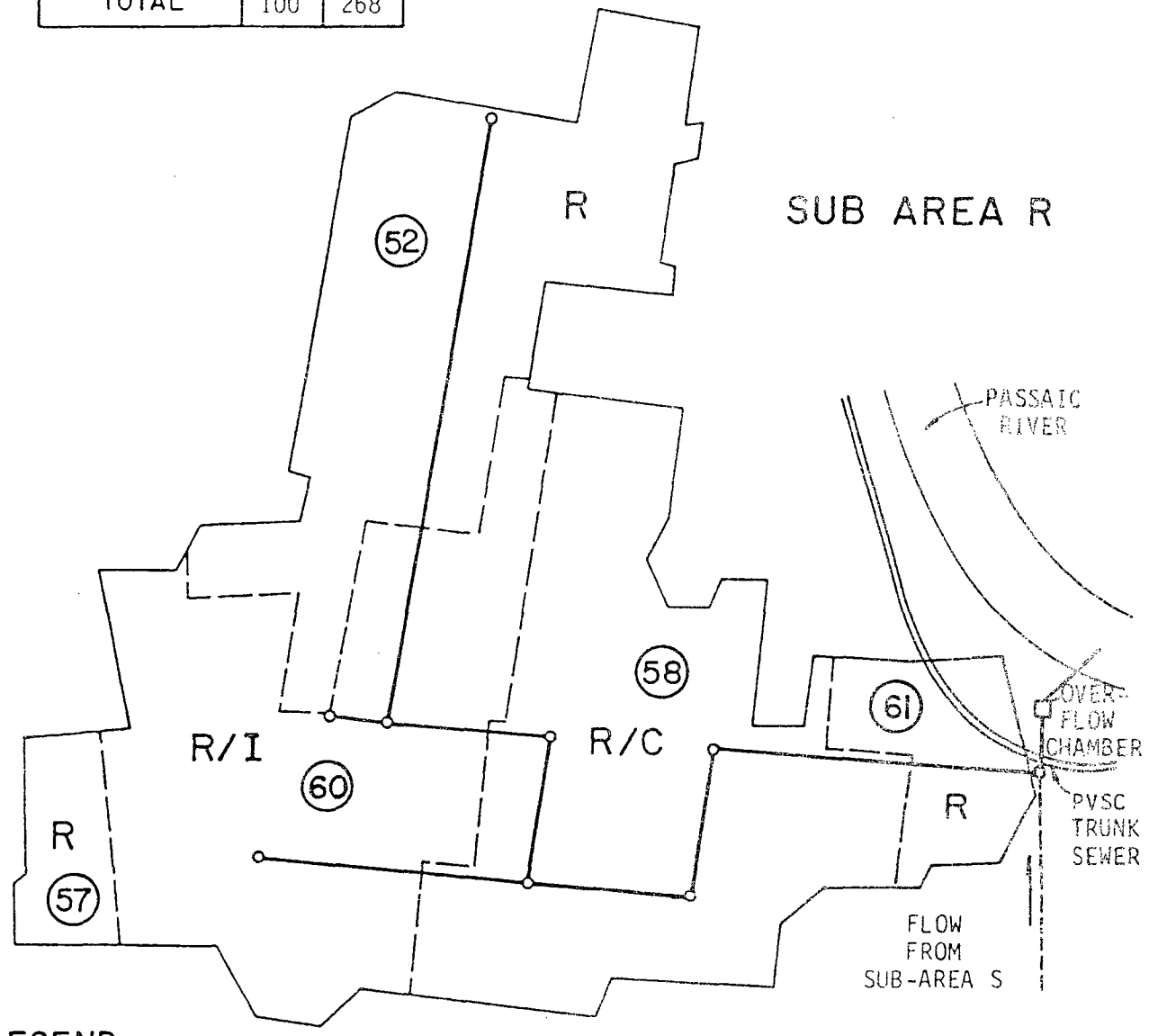
LAND USE
NORTHWEST ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn N... 07041

946510078

FIGURE 3-16

LAND USE	%	ACRES
RESIDENTIAL	90	240
COMMERCIAL	4	12
INDUSTRIAL	5	14
OPEN/PARKS	1	2
TOTAL	100	268



LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

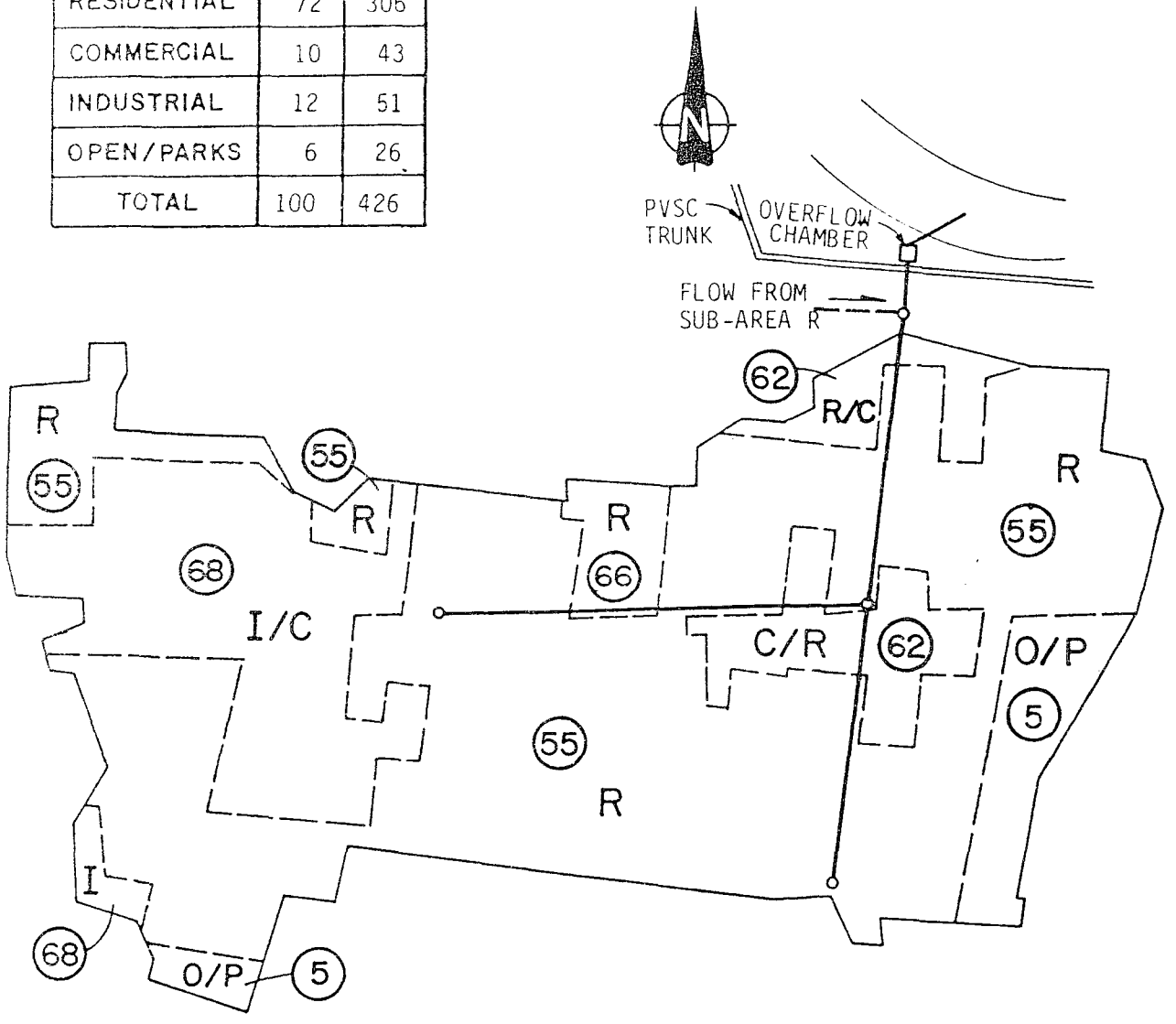
LAND USE
10TH. AVE & 33RD. ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

946510079

FIGURE 3-17A

LAND USE	%	ACRES
RESIDENTIAL	72	306
COMMERCIAL	10	43
INDUSTRIAL	12	51
OPEN/PARKS	6	26
TOTAL	100	426



SUB AREA S

LEGEND

- MAIN INTERCEPTOR
- R RESIDENTIAL
- C COMMERCIAL
- I INDUSTRIAL
- O/P OPEN/PARK
- SUBCATCHMENT BOUNDARY
- (15) PERCENT IMPERMEABLE AREA WITHIN SUBCATCHMENT

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

LAND USE
10TH. AVE. & 33RD. ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
Millburn New Jersey 07041

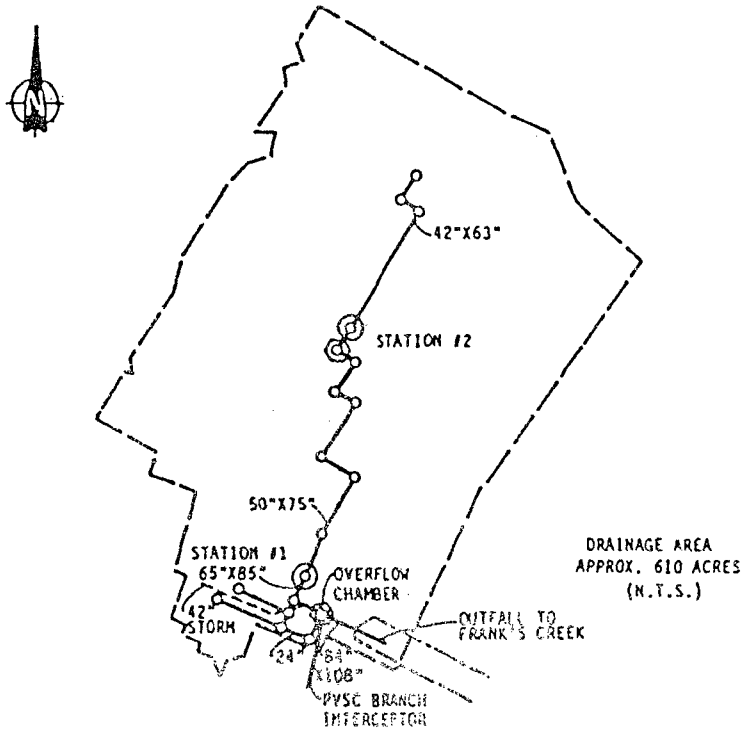
946510080

FIGURE 3-17B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
9-20-82	1	2.84	42.17	8.43	50	500	20	500	55	773	0.02	0.41	0.02	0.78	1.54	18.9
	2	0.39	4.86	0.97	56	520	30	410	40	620	0.02	0.07	0.02	0.29	3.21	11.8
11-5-82	1	2.23	50.61	8.97	210	430	113	340	140	400	0.02	0.06	0.02	0.04	12.4	23.0
	2	0.56	7.93	1.37	190	440	60	570	100	810	0.02	0.02	0.02	0.08	16.6	21.2
11-12/13-82	1	28.17	189.49	80.84	51	350	40	330	50	500	0.02	0.02	0.02	0.12	0.24	20.0
	2	0.58	7.99	2.39	58	360	20	245	32	355	0.02	0.04	0.02	0.34	0.16	20.7



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

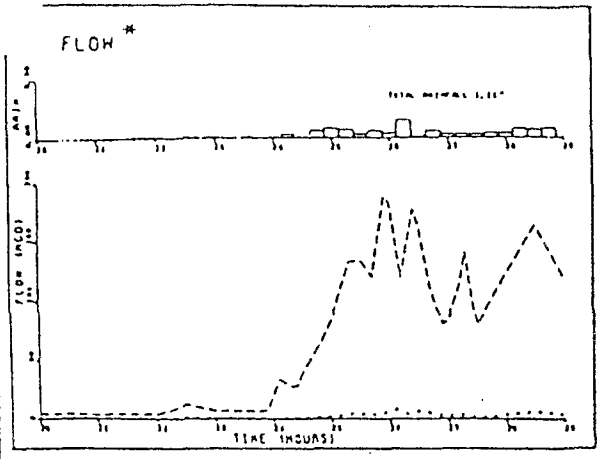
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
IVY STREET OVERFLOW
TOWN OF KEARNY

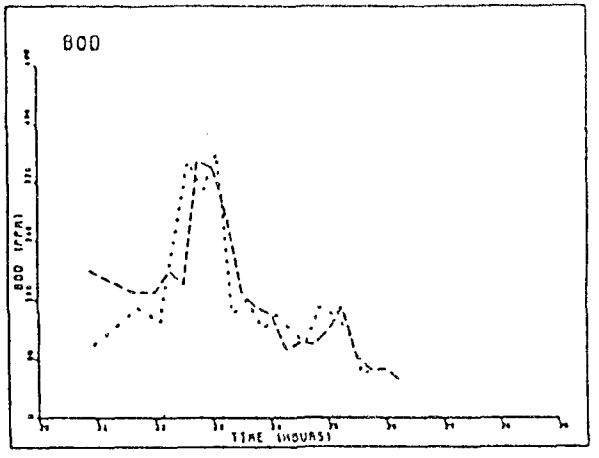
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
Millburn, New Jersey 07041

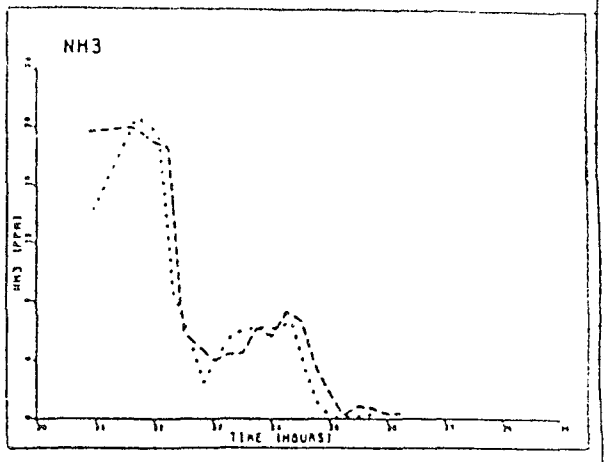
FIGURE 3-18A

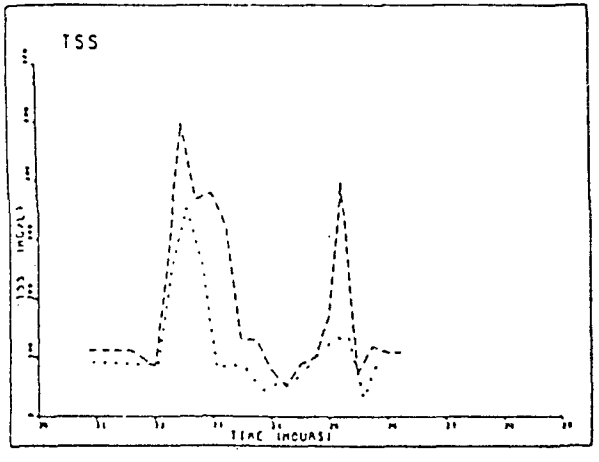
946510081

946510082









LEGEND

---------- (STA. 1)

- - - - - - - - - (STA. 2)

---------- (STA. 3)

———————— (STA. 4)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 11/12/82

IVY STREET OVERFLOW

TOWN OF KEARNY

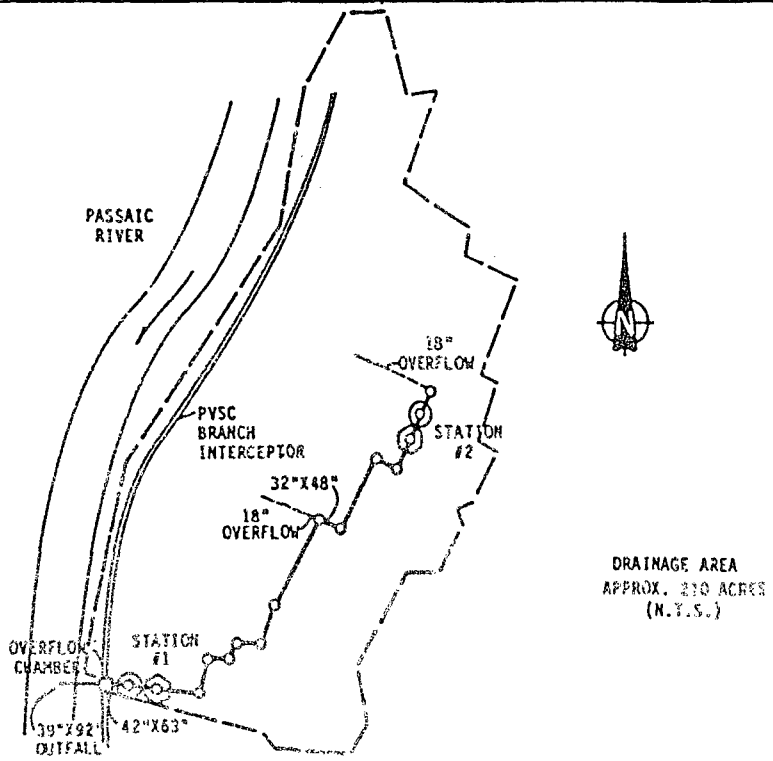
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 18B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
9-20-82	1	1.01	6.16	1.69	42	200	32	152	44	228	0.02	0.16	0.03	0.61	1.47	7.84
	2	0.09	4.91	0.47	30	170	32	136	52	244	0.02	0.26	0.02	1.20	1.79	9.06
9-26/27-82	1	0.90	23.40	3.20	12	131	4	140	8	208	0.02	0.23	0.02	1.16	1.17	16.2
	2	0.16	7.49	0.80	15	130	8	104	16	156	0.02	0.12	0.02	1.09	1.33	23.7
11-12-82	1	1.01	22.79	6.32	26	240	16	188	28	276	0.02	0.40	0.02	0.40	0.28	17.4
	2	0.71	11.39	3.44	22	260	16	204	24	312	0.02	0.02	0.02	0.36	0.06	12.6



DRAINAGE AREA
APPROX. 210 ACRES
(N.Y.S.)

LEGEND
(FOR SCHEMATIC)

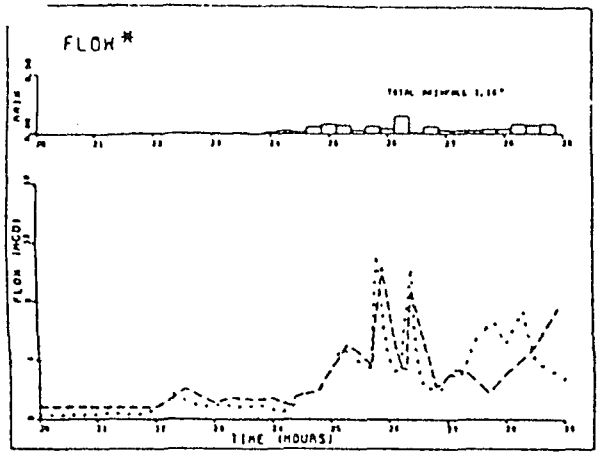
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

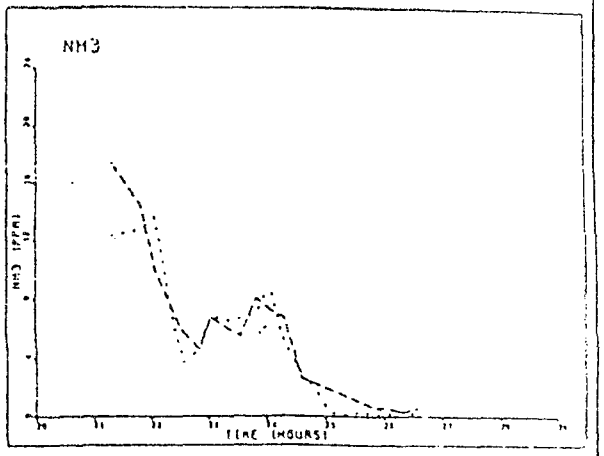
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
JOHNSTON AVE. OVERFLOW
TOWN OF KEARNY

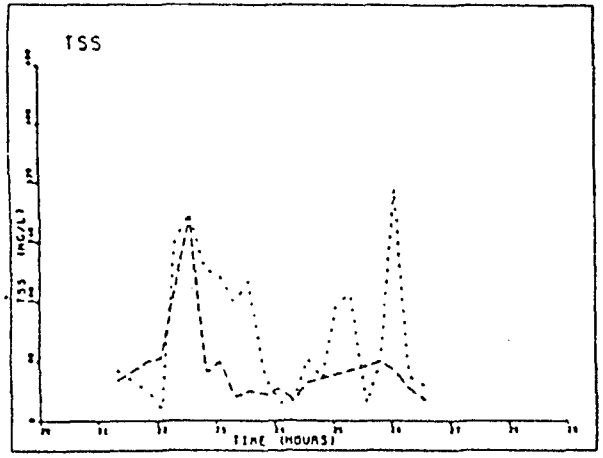
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

FIGURE 3-19A

946510083







LEGEND

---------- (STA. 1)

- - - - - - - - - (STA. 2)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 11/12/82

JOHNSTON AVE. OVERFLOW
TOWN OF KEARNY

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

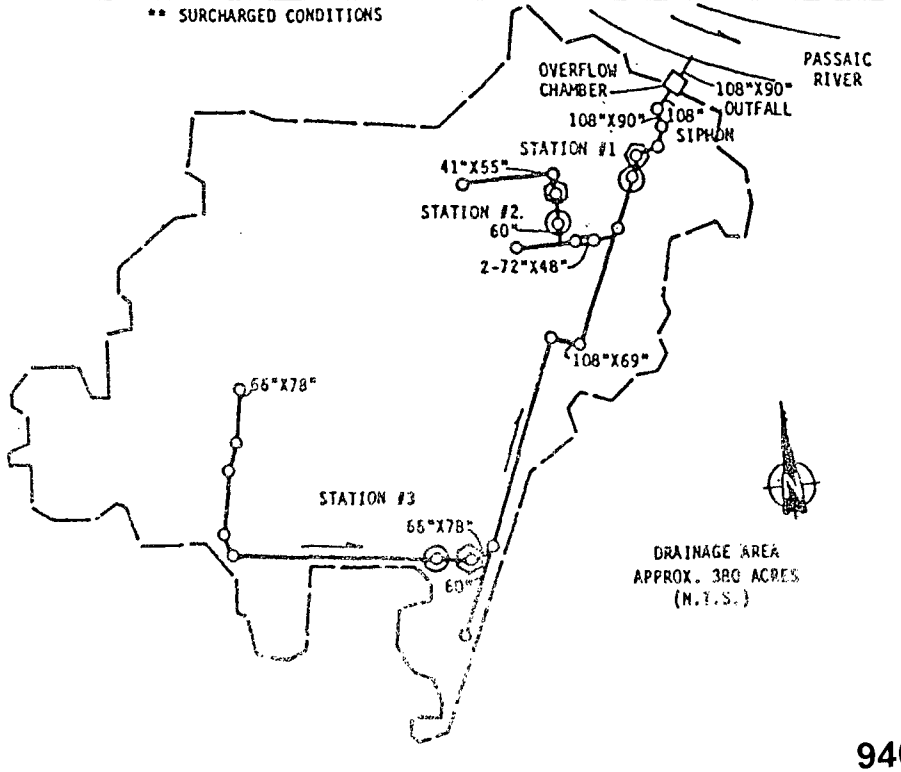
FIGURE 3-19B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM * - ONLY ONE SAMPLE

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
4-24-83	1	0.22	141	36.3	23	159	16	272	36	468	0.02	0.14	0.03	0.79	0.37	4.22
	2	0.21	9.14	1.61	17	90	8	104	11	166	0.04	0.10	0.34	1.33	0.02	0.36
	3	1.16	11.0	3.09	23	126	4	212	20	324	0.02	0.06	0.02	0.71	0.03	7.28
6-28-83	1	0.31	68.9	4.36	33	285	28	390	36	690	0.02	0.28	0.04	1.20	0.76	10.6
	2	-	-	-	32	285	20	185	52	305	0.02	0.30	0.02	1.42	2.23	20.5
	3	1.75	12.44	2.93	44	270	20	340	32	640	0.02	0.24	0.04	0.79	2.12	13.1
9-21-83	1	0.52	225**	39.6	72	86	58	100	84	186	0.02	0.02	0.02	0.02	8.04	11.0
	2	0.29	18.1	3.16	33	128	20	96	44	120	0.02	0.40	0.02	1.22	0.20	14.0
	3	0.66	15.8	3.08	105	*	120	*	246	*	0.02	*	0.02	*	7.72	*

** SURCHARGED CONDITIONS



LEGEND
(FOR SCHEMATIC)

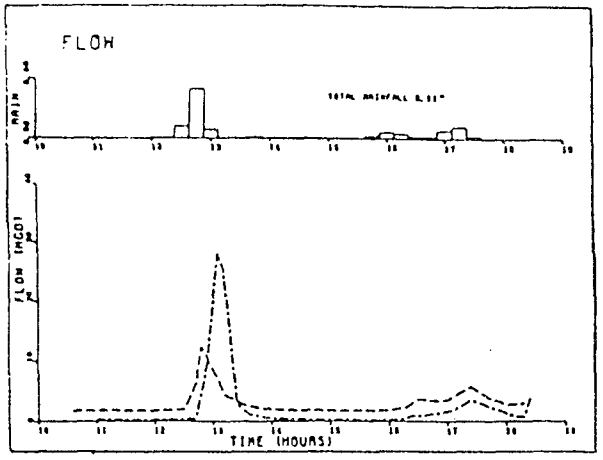
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

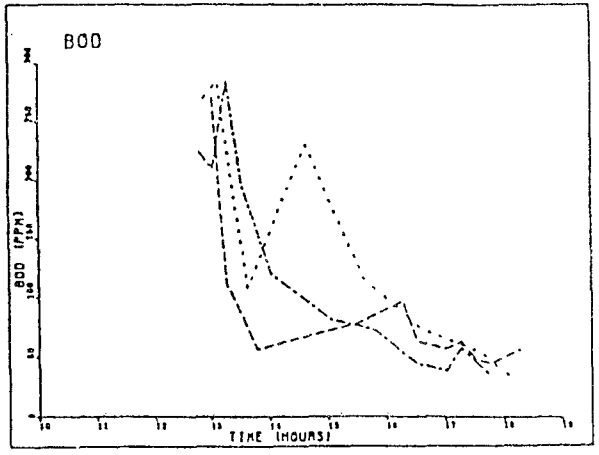
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CITY DOCK OVERFLOW
CITY OF NEWARK

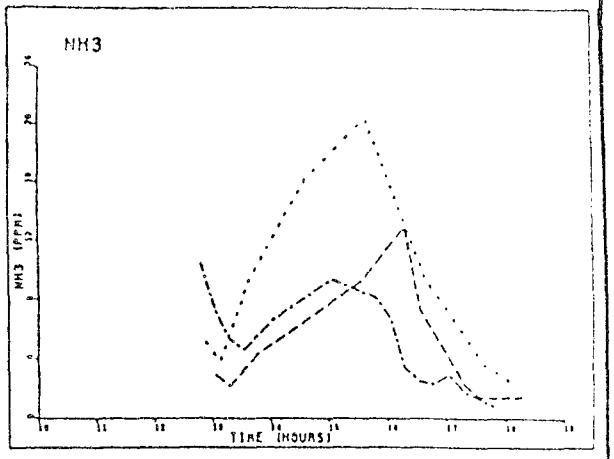
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

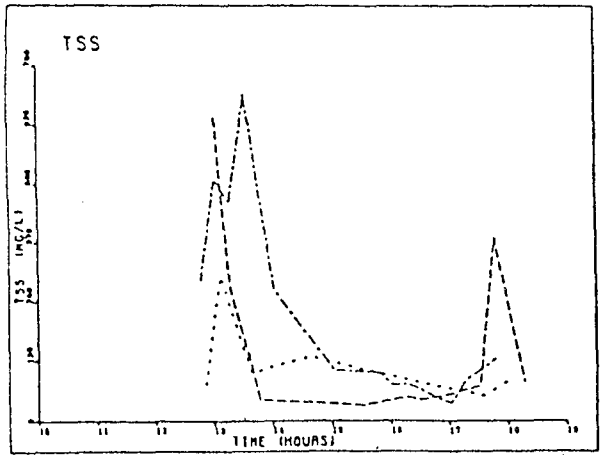
946510085

FIGURE 3-20A









LEGEND

---------- (STA. 1)

- - - - - - - - - (STA. 2)

———————— (STA. 3)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 6/28/83

CITY DOCK OVERFLOW

CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

946510086

FIGURE 3-20B

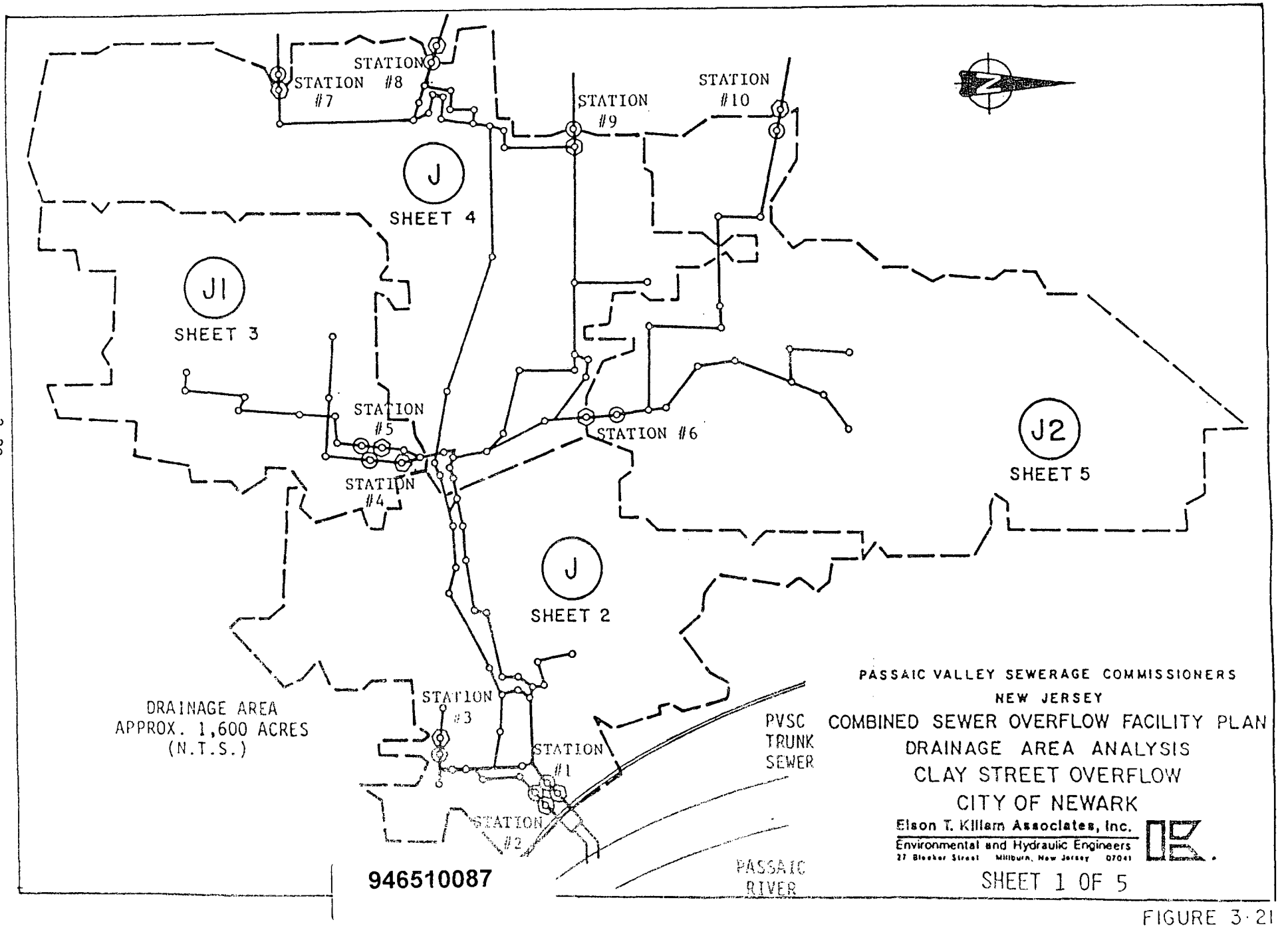
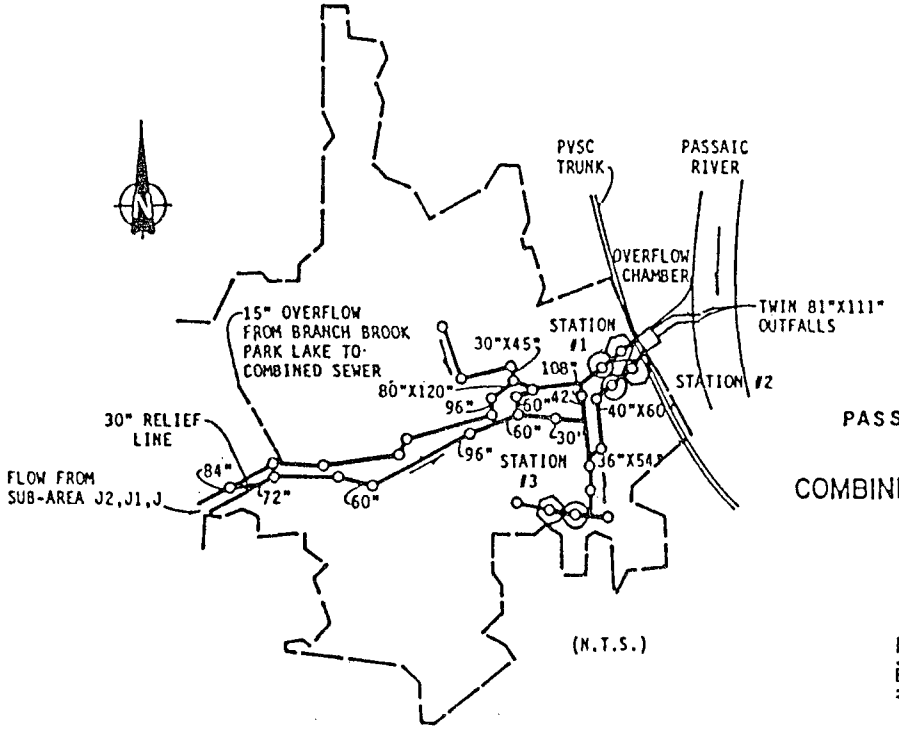

STATION #7
STATION #8
STATION #9
STATION #10
J
SHEET 4
J1
SHEET 3
STATION #5
STATION #4
STATION #6
J2
SHEET 5
J
SHEET 2
STATION #3
STATION #1
STATION #2
DRAINAGE AREA
APPROX. 1,600 ACRES
(N.T.S.)
PVSC
TRUNK
SEWER
PASSAIC
RIVER
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CLAY STREET OVERFLOW
CITY OF NEWARK
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041
SHEET 1 OF 5
946510087

FIGURE 3-21

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM * SURCHARGED CONDITIONS

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
5-11-81	1	7.57	*320.00	102.48	35	132	76	148	132	500	0.02	0.15	0.02	0.67	0.94	7.88
	2	10.64	162.32	40.78	62	310	72	292	188	744	0.02	0.09	0.02	0.54	0.69	11.0
	3	0.15	44.39	6.61	8	139	24	296	36	524	0.02	0.08	0.30	4.15	0.40	2.64
5-15-81	1	5.26	98.66	38.03	51	184	36	132	72	260	0.02	0.03	0.02	0.43	0.58	4.92
	2	8.65	36.57	19.23	45	250	40	176	40	176	0.02	0.06	0.20	0.62	0.46	7.75
	3	0.29	11.53	3.25	-	-	-	-	-	-	-	-	-	-	-	-
9-8-81	1	7.23	*310.00	53.87	-	-	-	-	-	-	-	-	-	-	-	-
	2	9.54	215.50	34.51	162	258	98	108	124	220	0.01	0.03	0.01	0.01	2.47	8.39
	3	1.03	99.35	13.63	3	72	8	36	40	62	0.01	0.12	0.12	0.82	0.05	1.00



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

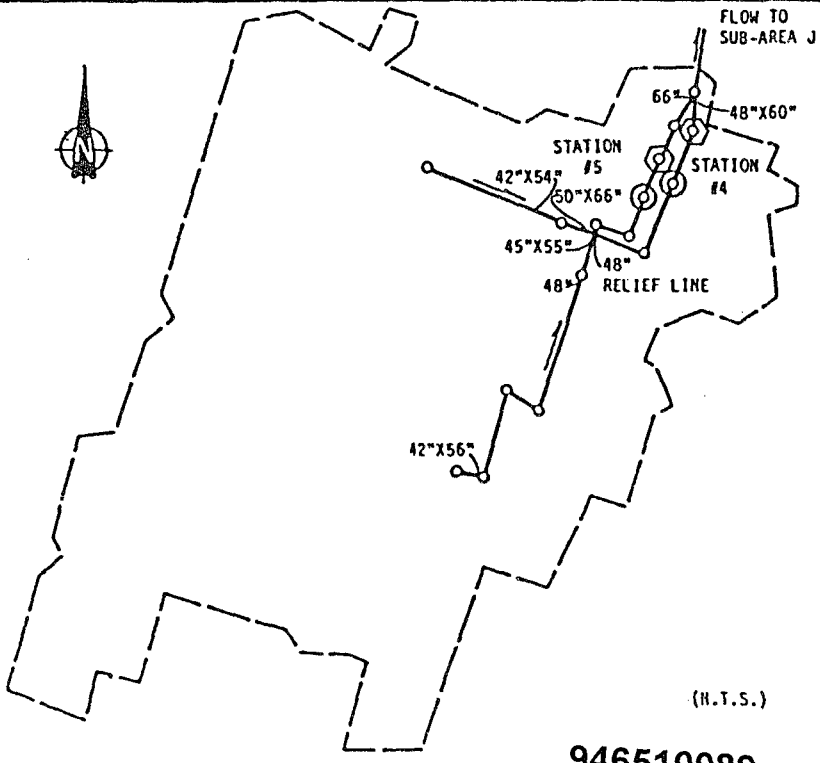
SHEET 2 OF 5 FIGURE 3-21A

946510088

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
5-11-81	4	0.29	10.42	1.75	15	98	16	256	44	936	0.02	0.08	0.02	0.74	0.41	8.55
	5	2.57	83.08	20.48	14	74	28	112	60	256	0.01	0.10	0.37	0.77	0.05	6.10
5-15-81	4	0.25	2.40	0.99	23	39	8	32	32	76	0.02	0.02	0.49	0.63	0.68	4.23
	5	1.06	28.69	7.82	23	30	12	44	52	72	0.02	0.02	0.42	0.59	0.09	23.5
9-8-81	4	0.09	25.30	1.96	3	42	12	76	38	186	0.01	0.07	0.45	0.77	0.14	0.62
	5	-	-	-	3	44	28	46	52	114	0.10	1.27	0.93	1.01	0.55	0.94



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

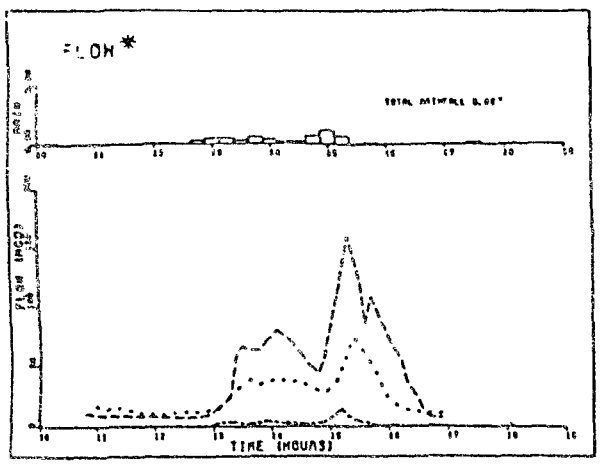
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CLAY STREET OVERFLOW
CITY OF NEWARK

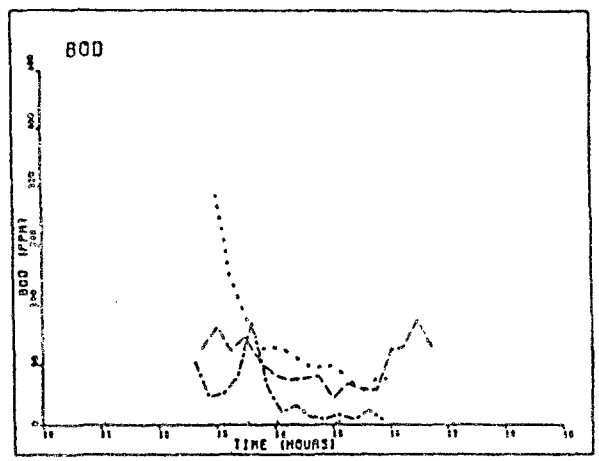
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

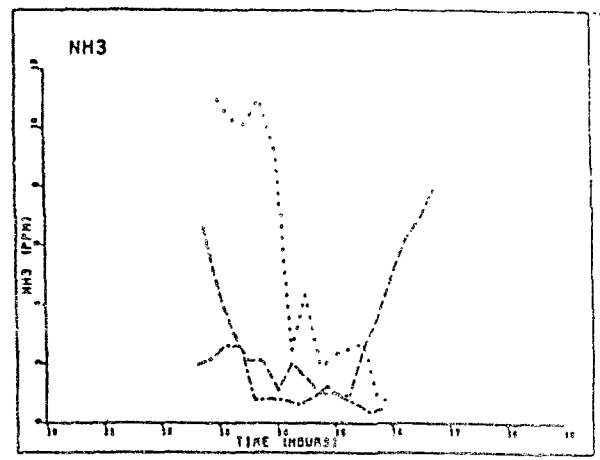
SHEET 3 OF 5

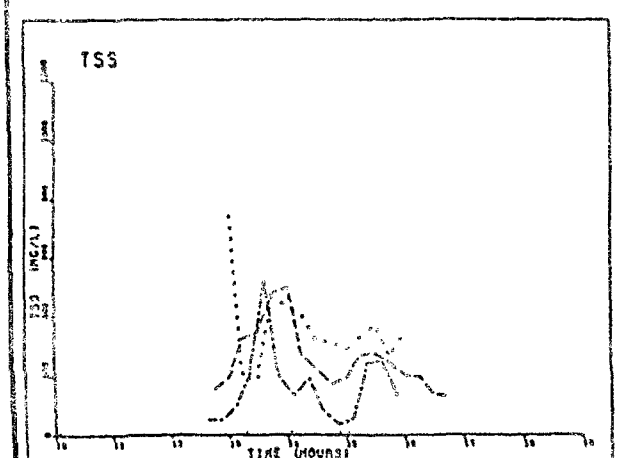
FIGURE 3-21C

946510089









LEGEND

———————— (STA. 1)

– – – – – – – – – (STA. 2)

———————— (STA. 3)

*NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 5/11/81

CLAY STREET OVERFLOW

CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
[illegible]

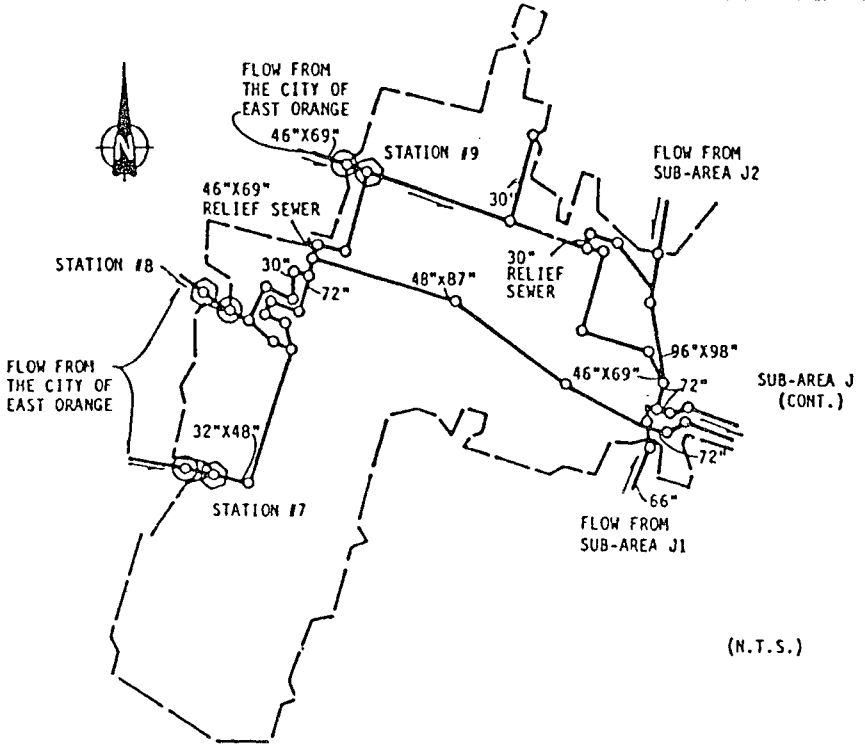
946510090

FIGURE 3-21B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM
* - ONLY ONE SAMPLE

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
5-11-81	7	0.86	16.14	3.54	470	750	130	1256	250	1396	0.01	0.27	0.23	0.74	0.01	1.69
	8	0.04	0.09	0.06	*	300	*	140	*	176	*	0.01	*	0.01	*	20.5
	9	0.92	1.94	1.36	152	178	144	248	200	328	0.01	0.01	0.01	0.14	15.8	18.5
5-15-81	7	0.07	2.97	1.16	98	548	76	580	96	744	0.02	0.75	0.02	1.03	0.17	2.57
	8	0.12	0.24	0.19	218	308	56	124	72	144	0.02	0.26	0.02	0.89	8.72	18.8
	9	1.26	1.30	1.26	158	435	32	76	52	88	0.02	0.02	0.02	0.02	15.8	18.6
9-8-81	7	-	*	-	*	1830	*	640	*	780	*	0.03	*	1.14	*	0.74
	8	0.52	0.78	0.64	3	186	40	96	116	188	0.01	0.01	0.01	0.01	8.80	10.0
	9	2.10	4.99	2.64	132	180	100	108	180	200	0.01	0.01	0.01	0.01	9.56	12.4



(N.T.S.)

LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

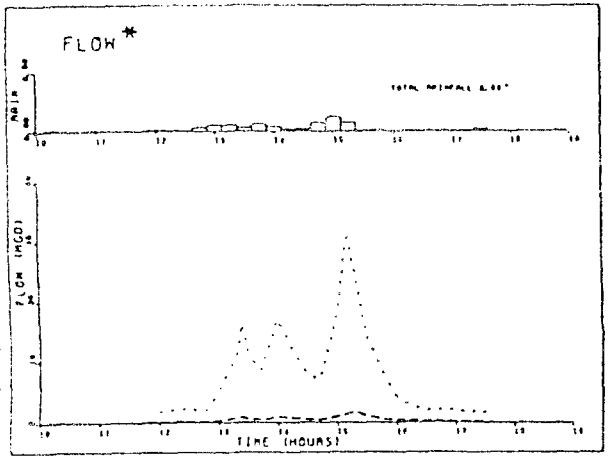
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CLAY STREET OVERFLOW
CITY OF NEWARK

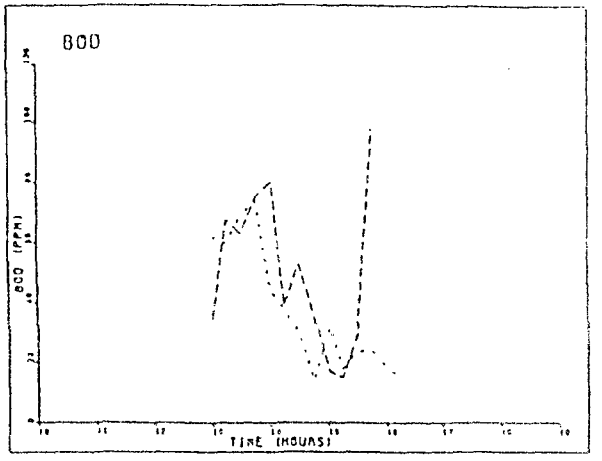
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

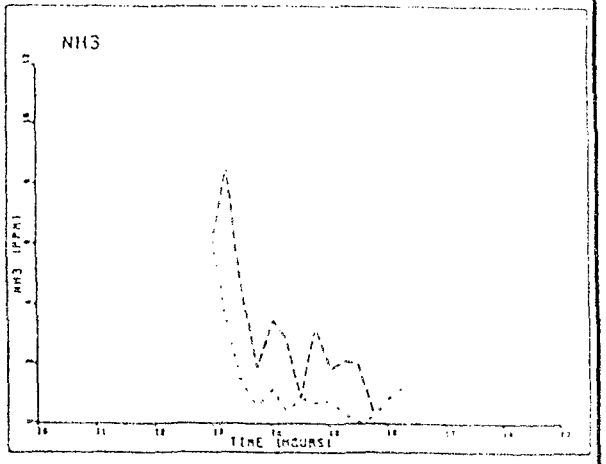
SHEET 4 OF 5

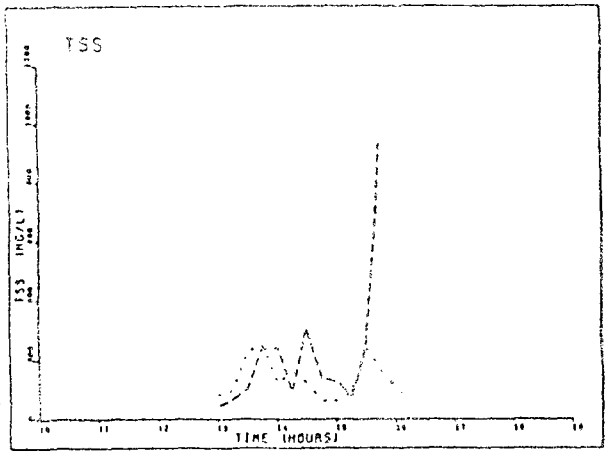
FIGURE 3-21E

94510091









LEGEND

———————— (STA. 4)

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* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 5/11/81
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

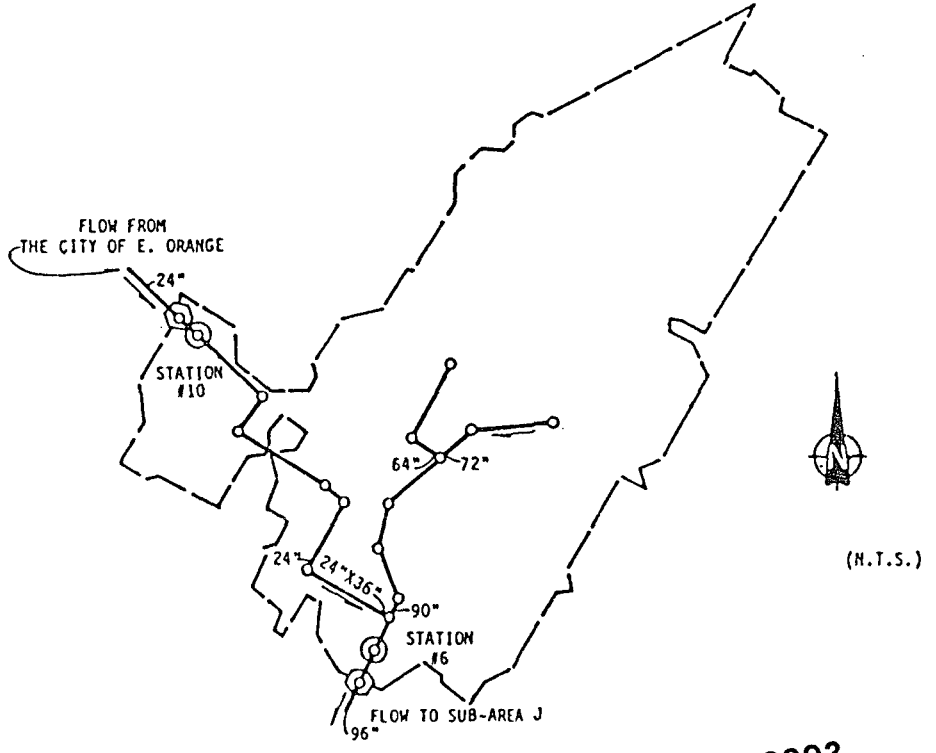
946510092

FIGURE 3.21D

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
5-11-81	6	5.86	30.70	14.47	44	102	64	272	112	348	0.01	0.23	0.01	0.68	1.12	14.7
	10	3.49	8.88	4.39	121	142	104	128	124	164	0.01	0.01	0.01	0.01	1.93	16.8
5-15-81	6	7.39	21.26	14.16	-	-	-	-	-	-	-	-	-	-	-	-
	10	1.74	2.10	1.98	158	315	56	108	80	136	0.02	0.02	0.03	0.03	17.3	37.0
9-8-81	6	5.69	41.83	16.79	3	38	100	140	400	580	0.01	0.01	0.32	0.43	0.64	0.76
	10	0.03	2.86	0.27	138	144	88	96	164	184	0.01	0.01	0.01	0.01	10.2	11.2



(N.T.S.)

LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

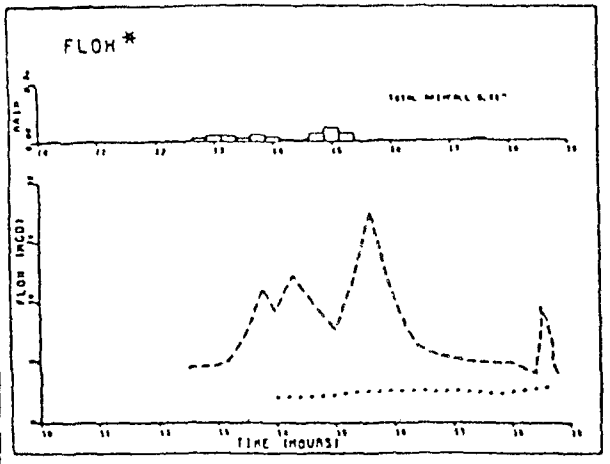
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CLAY STREET OVERFLOW
CITY OF NEWARK

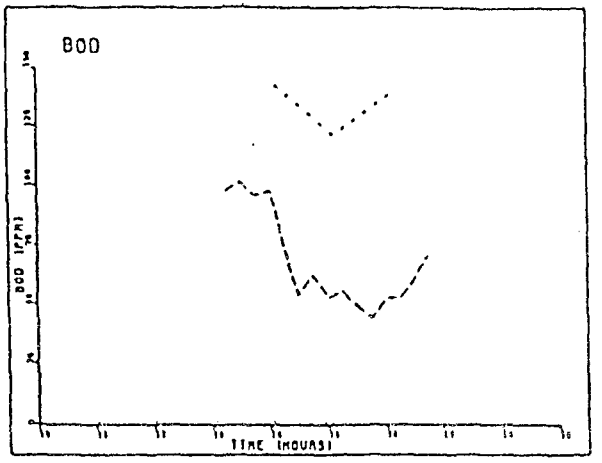
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

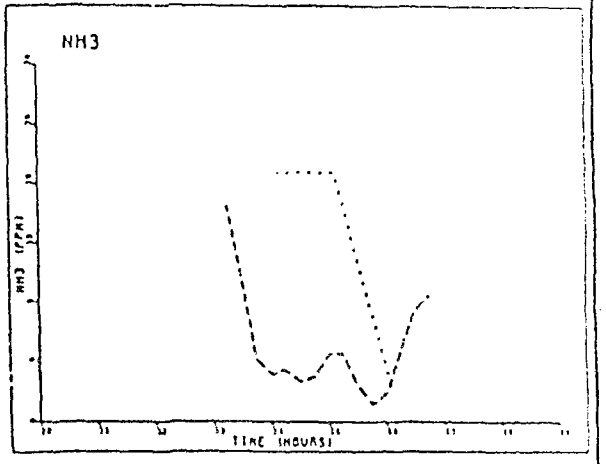
SHEET 5 OF 5

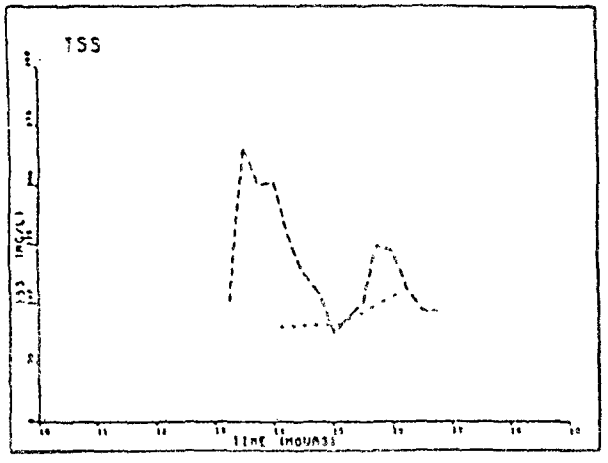
FIGURE 3-21G

946510093









LEGEND

---------- (STA. 6)

- - - - - - - - - - (STA. 10)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 5/11/81
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

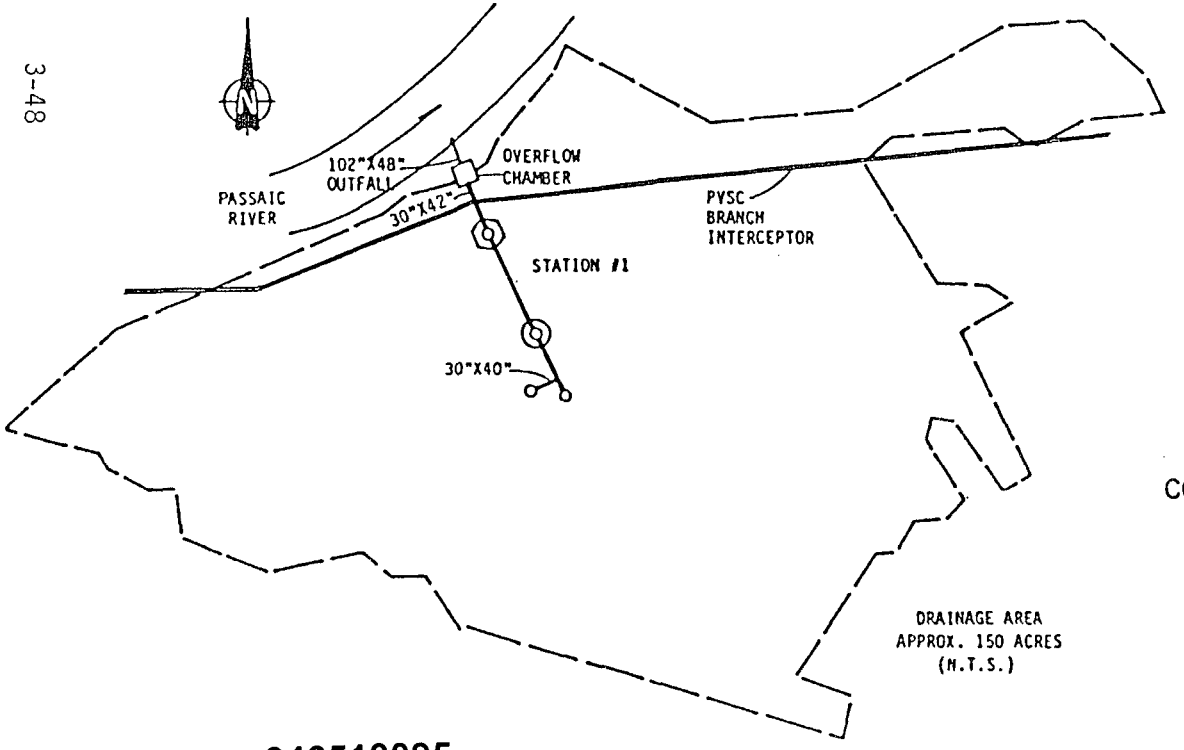
946510094

FIGURE 3-21F

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
4-24-83	1	0.14	6.46	1.26	35	183	34	352	72	480	0.02	0.02	0.02	0.51	1.98	13.4
6-28-83	1	0.38	9.21	1.77	61	162	55	400	75	600	0.02	0.38	0.02	0.05	0.52	20.6
9-21-83	1	0.25	13.8	3.17	27	225	24	244	42	628	0.02	0.09	0.02	0.51	0.10	13.2



LEGEND
(FOR SCHEMATIC)

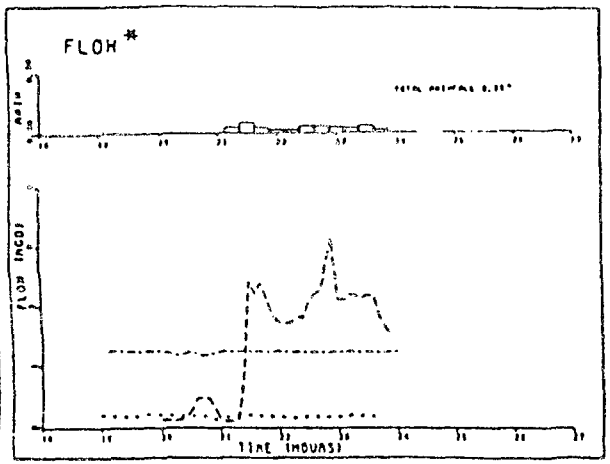
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

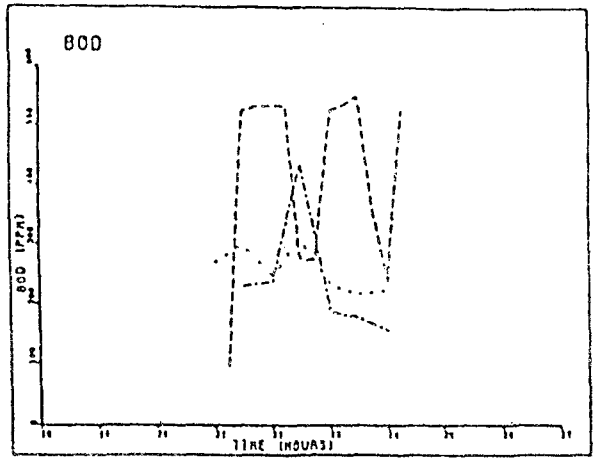
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
FREEMAN STREET OVERFLOW
CITY OF NEWARK

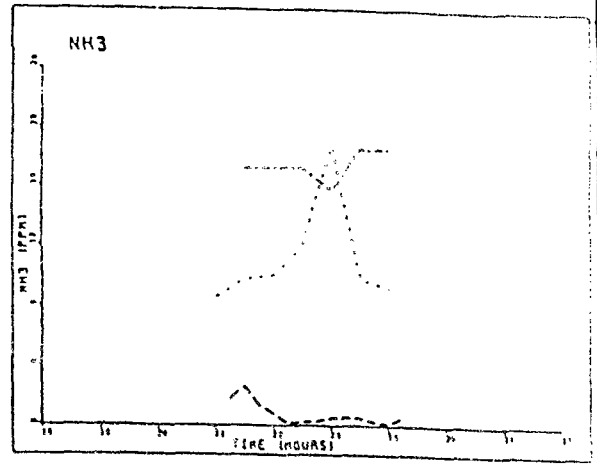
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

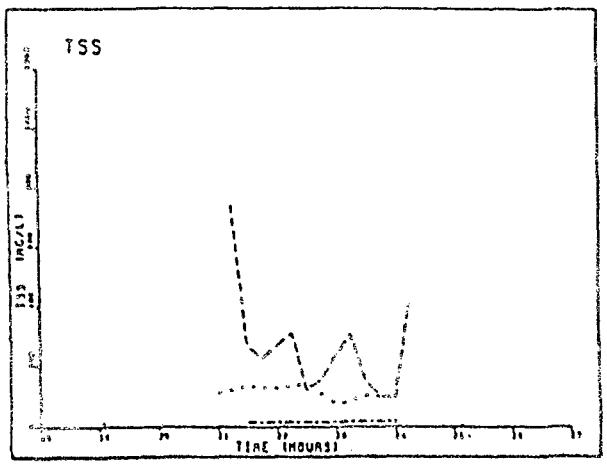
FIGURE 3-22A

946510095









LEGEND

---------- (STA. 7)

- - - - - - - - - (STA. 8)

———————— (STA. 9)

*NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 5/15/81
CLAY STREET OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
87 Bleeker Street Millburn, New Jersey 07041

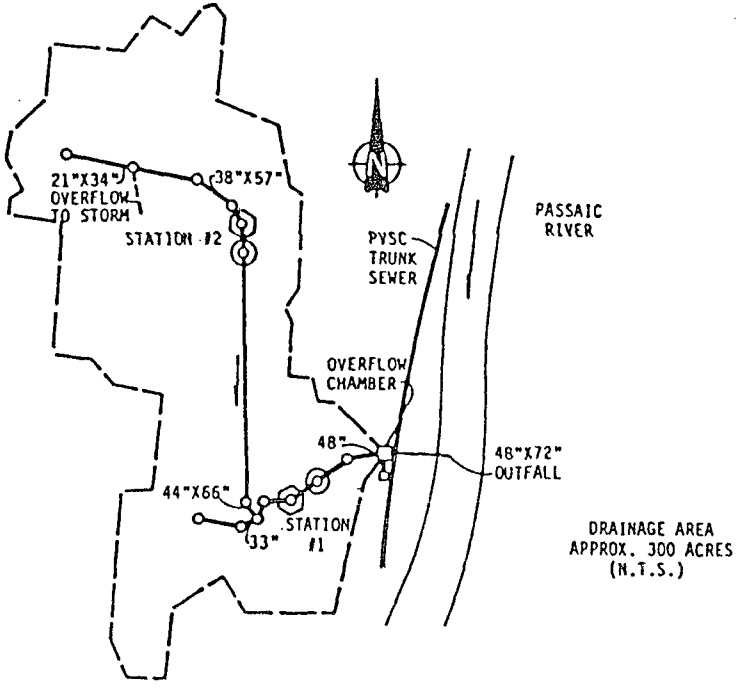
946510096

FIGURE 3-211H

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
9-20-82	1	0.76	7.42	2.24	78	420	65	195	75	320	0.02	0.45	0.02	0.36	1.68	10.1
	2	0.67	4.79	1.62	44	260	35	125	75	235	0.02	0.18	0.02	1.05	1.80	11.3
9-27-82	1	0.36	13.85	2.37	15	200	8	164	20	312	0.02	0.14	0.02	0.72	0.88	9.96
	2	0.46	12.15	1.63	120	350	5	128	32	276	0.02	0.14	0.02	0.70	0.85	14.8
11-5-82	1	0.71	13.13	2.27	195	430	104	450	144	590	0.02	0.02	0.02	0.33	9.06	13.3
	2	0.49	9.87	1.49	170	340	56	140	100	240	0.02	0.02	0.03	0.85	10.2	20.8
11-13-82	1	0.74	3.31	1.17	45	410	48	260	40	373	0.02	0.04	0.03	0.18	0.05	14.6
	2	0.57	1.96	0.79	28	450	8	472	24	536	0.02	0.40	0.02	0.64	0.05	19.7



LEGEND
(FOR SCHEMATIC)

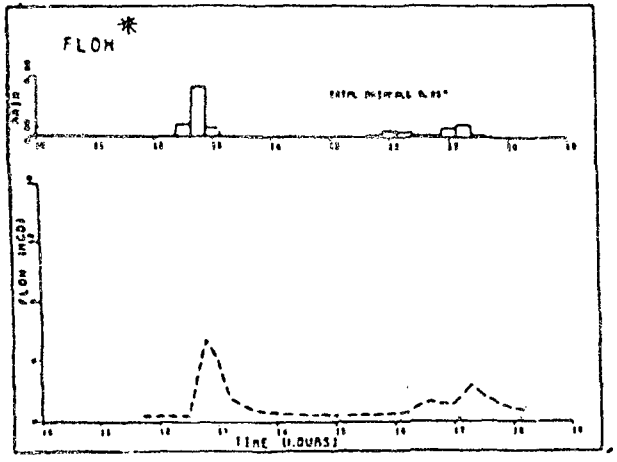
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

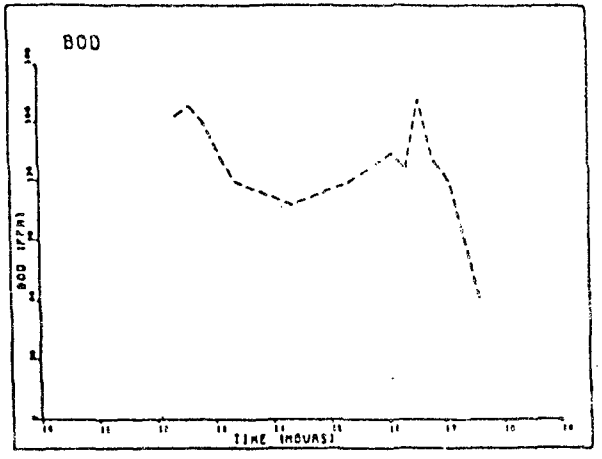
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
HERBERT PLACE OVERFLOW
CITY OF NEWARK

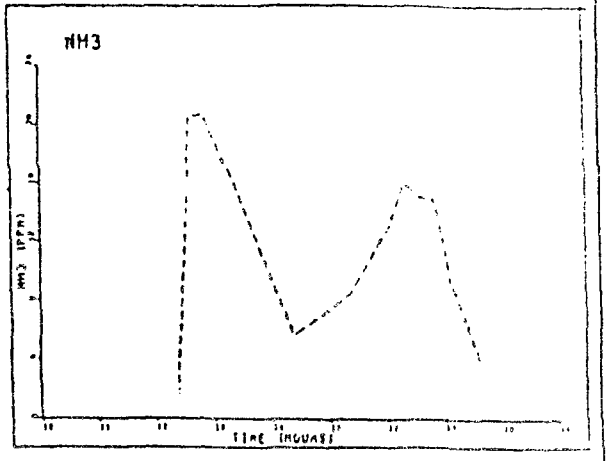
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

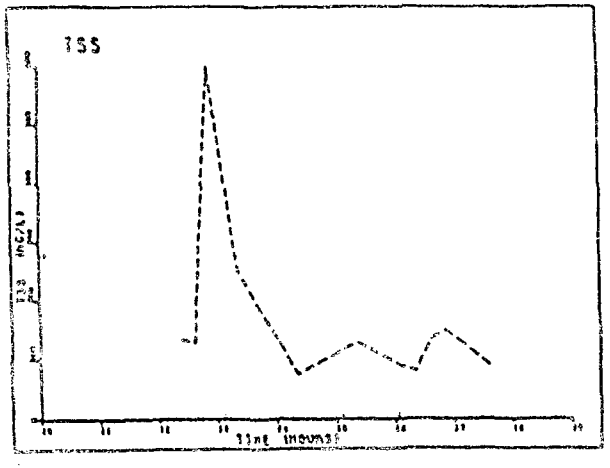
FIGURE 3-23A

946510097









LEGEND

———————— (STA. I)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 6/28/83
FREEMAN ST. OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

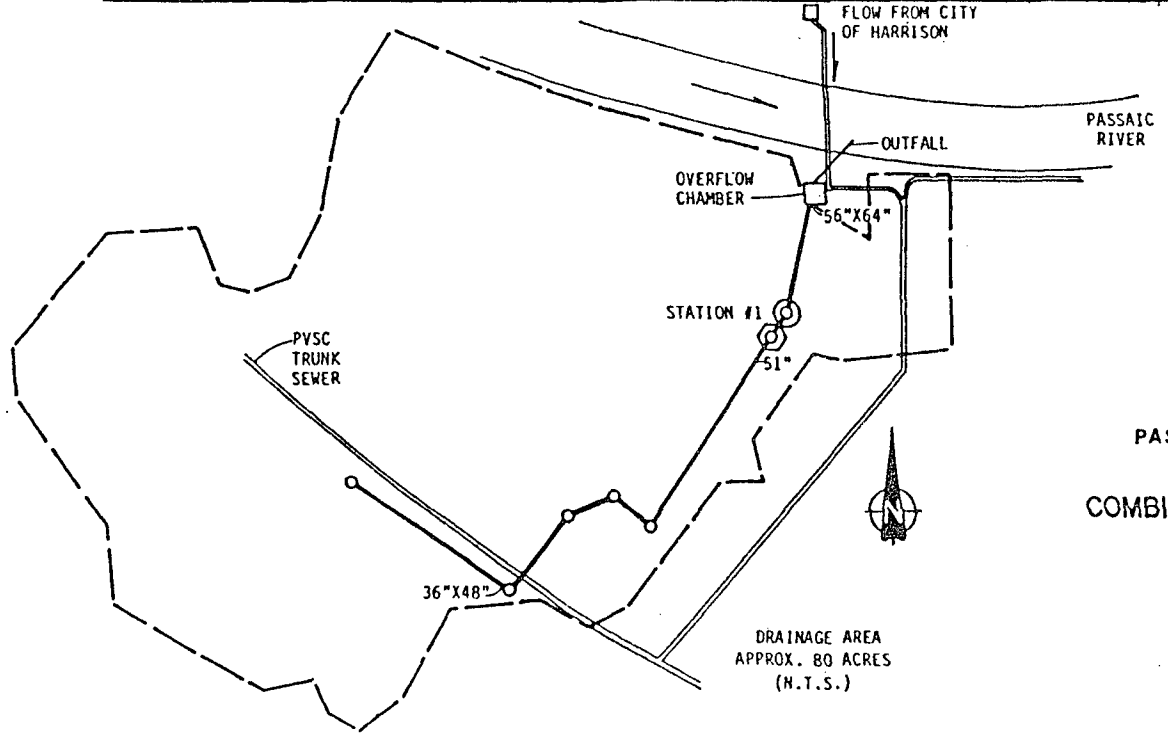
946510098

FIGURE 3.22B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
4-24-83	1	0.02	9.64	2.84	29	153	22	156	48	312	0.02	0.02	0.02	0.41	1.62	9.66
6-28-83	1	0.15	4.55	0.59	23	330	24	300	36	450	0.02	0.27	0.02	0.78	0.46	17.3
9-21-83	1	0.07	14.2	3.17	23	60	14	40	48	144	0.02	0.02	0.20	0.29	0.02	0.22



LEGEND
(FOR SCHEMATIC)

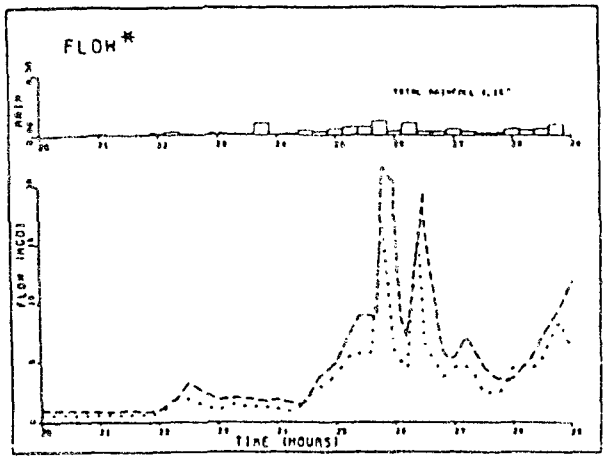
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

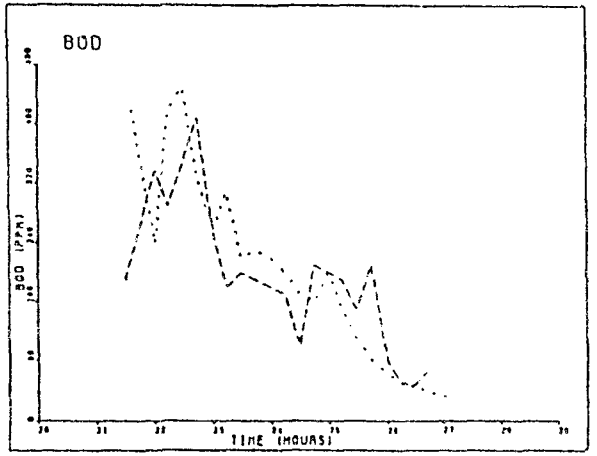
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
JACKSON STREET OVERFLOW
CITY OF NEWARK

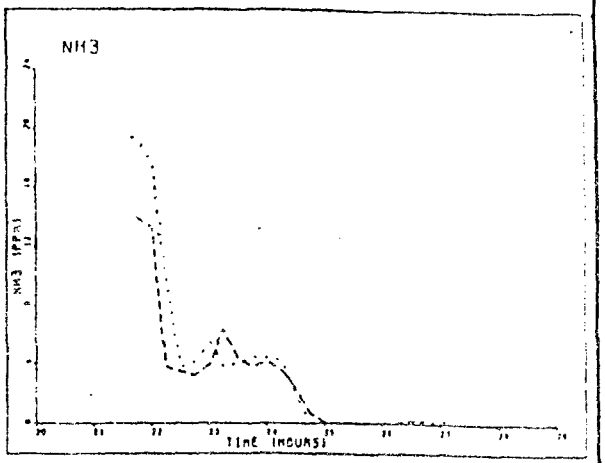
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

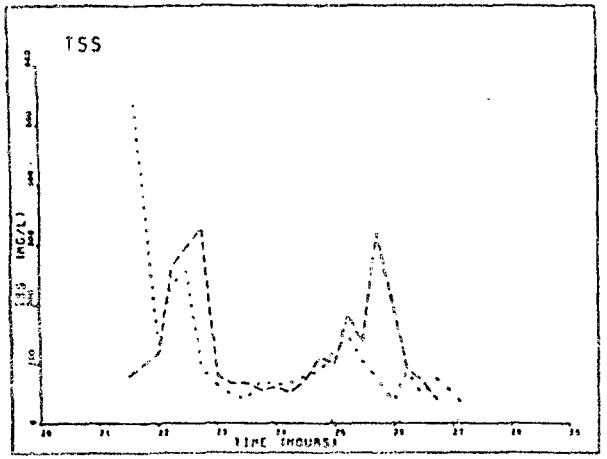
FIGURE 3-24A

946510099









LEGEND

———————— (STA. 1)

– – – – – – – – – (STA. 2)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 11/12/82
HERBERT PLACE OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

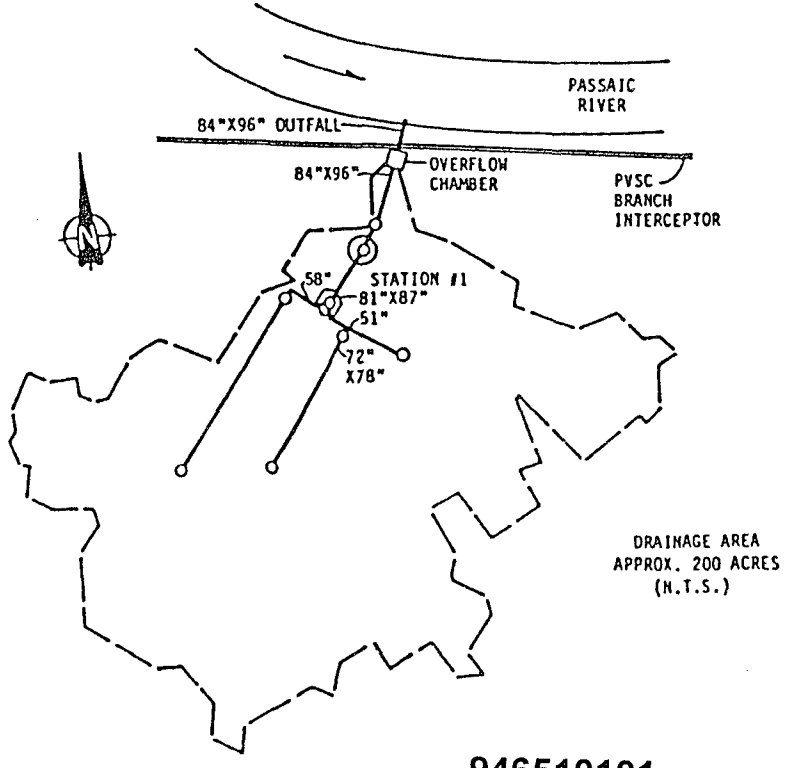
946510100

FIGURE 3.23B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
6-28-83	1	1.67	114	27.8	38	156	40	196	48	288	0.02	0.40	0.02	0.28	1.04	10.4
9-21-83	1	0.61	222	81.0	50	83	40	60	76	112	0.05	0.15	0.40	0.79	0.44	1.3
10-5-83	1	-	-	-	42	195	20	270	56	520	0.02	0.23	0.01	0.19	1.79	11.3



DRAINAGE AREA APPROX. 200 ACRES (N.T.S.)

LEGEND
(FOR SCHEMATIC)

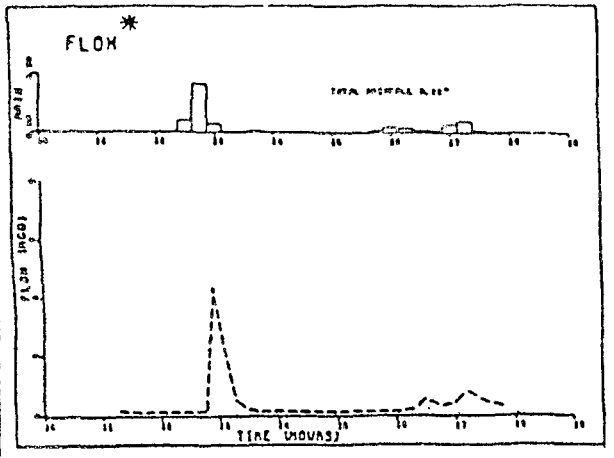
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

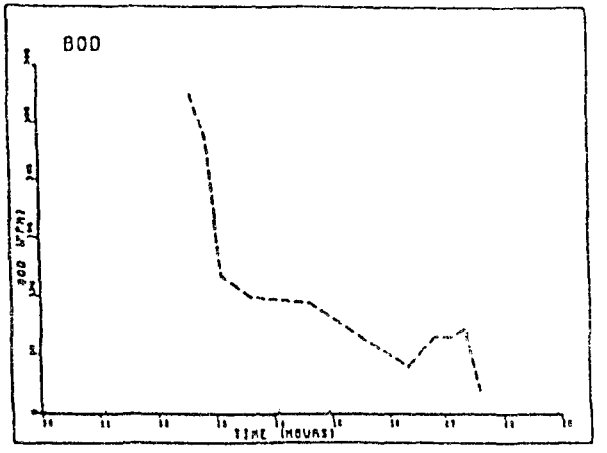
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
POLK STREET OVERFLOW
CITY OF NEWARK

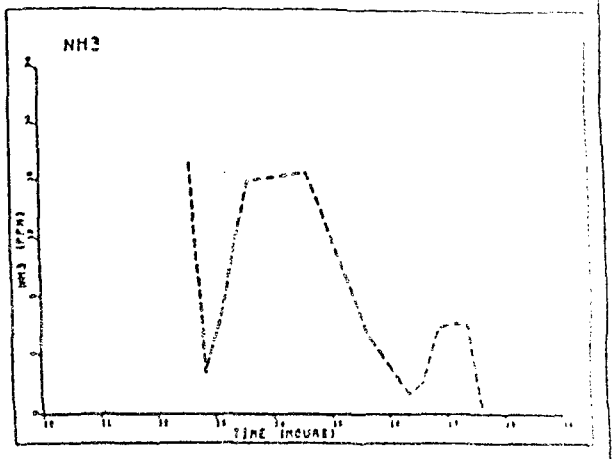
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

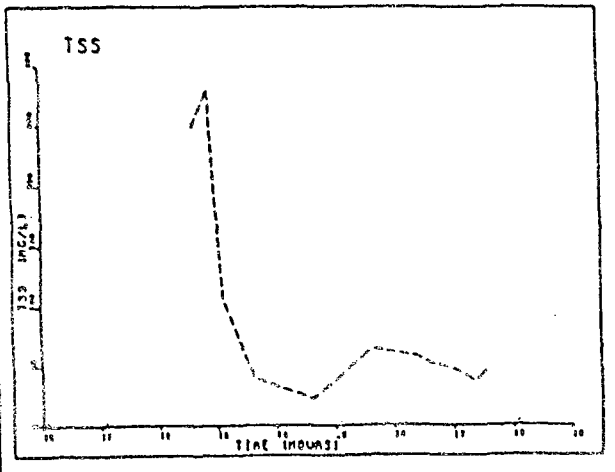
FIGURE 3-25A

946510101









LEGEND

---------- (STA. I)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

946510102

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 6/28/83
JACKSON ST. OVERFLOW
CITY OF NEWARK

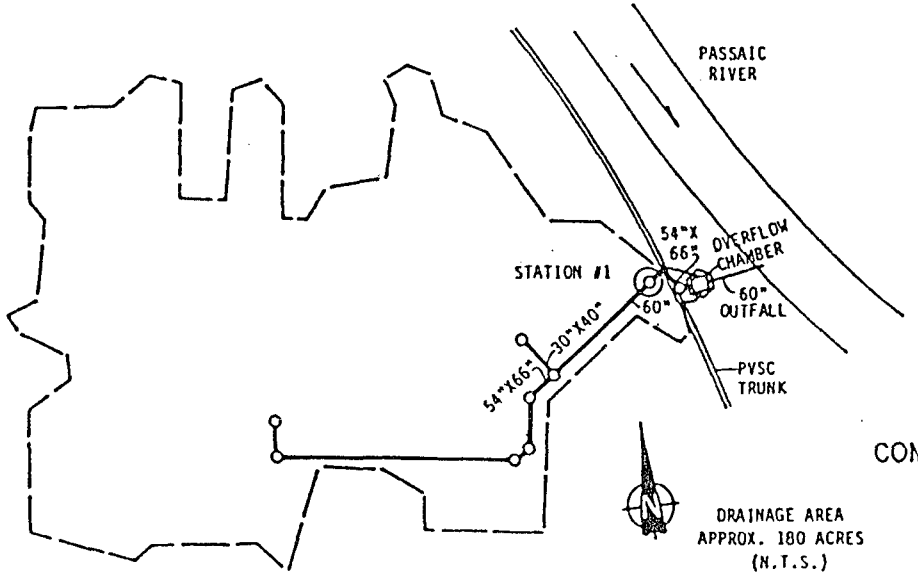
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Brook Street Millburn, New Jersey 07041

FIGURE 3-24B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
6-28-83	1	0.80	11.7	2.29	33	141	55	200	75	310	0.05	0.17	0.04	1.60	1.78	10.6
9-21-83	1	0.62	21.5	3.37	15	60	10	60	28	90	0.02	0.10	0.02	0.57	0.40	8.60



LEGEND
(FOR SCHEMATIC)

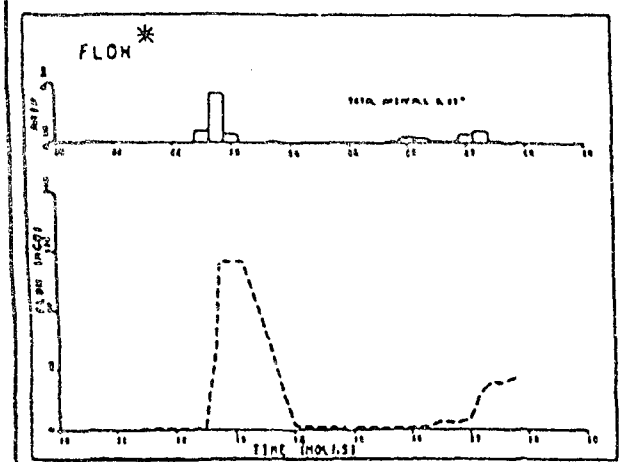
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

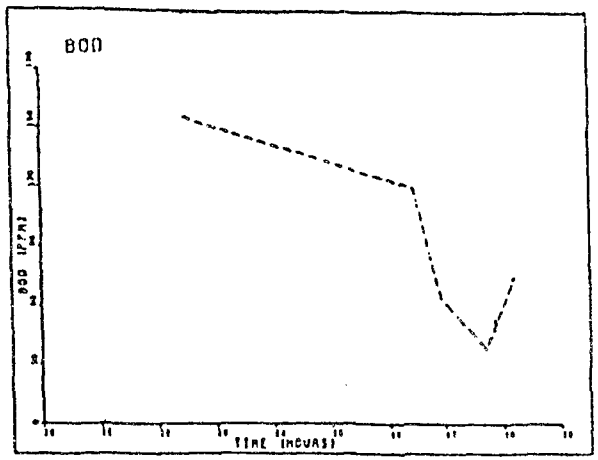
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RECTOR STREET OVERFLOW
CITY OF NEWARK

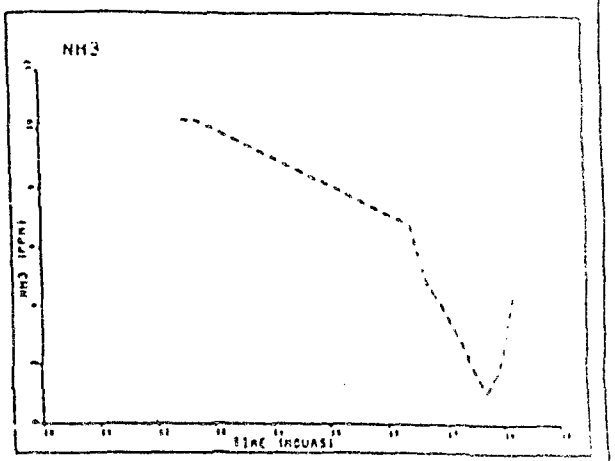
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

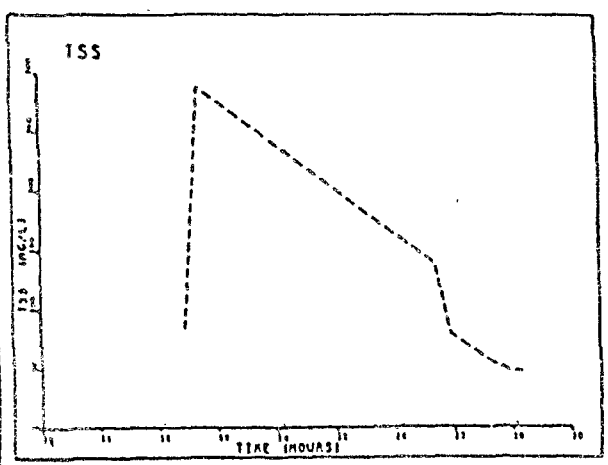
FIGURE 3-26A

946510103









LEGEND

---------- (STA. 1)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 6/28/83
POLK ST. OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

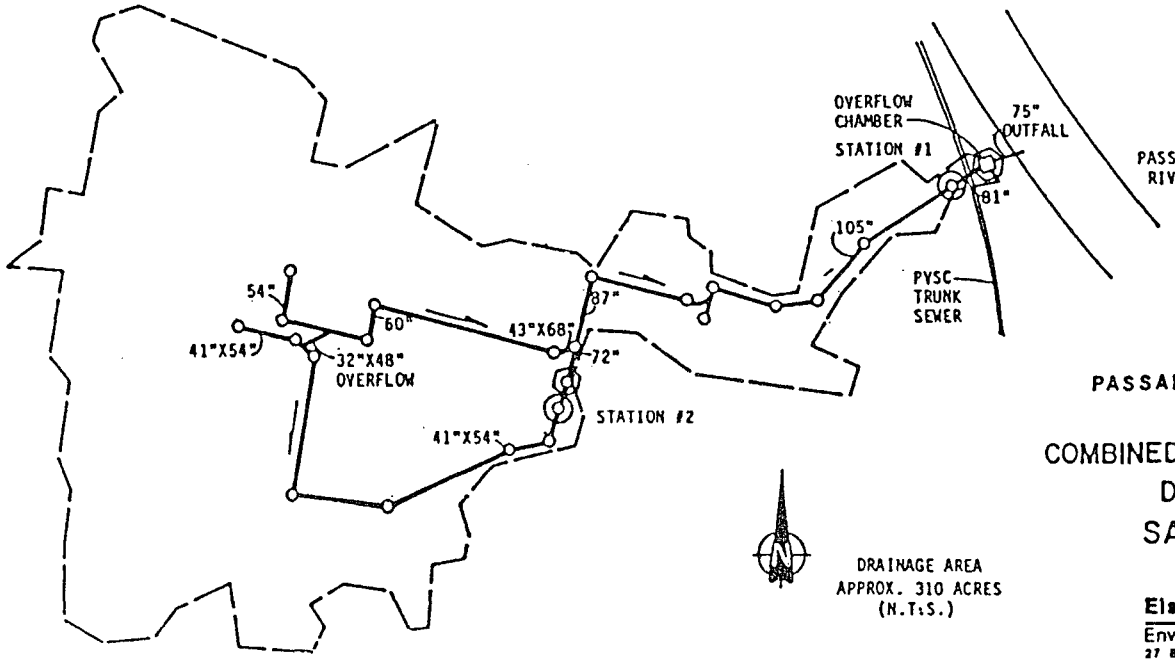
946510104

FIGURE 3.25B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
4-24-83	1	3.27	25.0	7.41	26	66	24	106	22	190	0.02	0.10	0.38	1.08	0.27	2.15
	2	0.38	1.87	0.71	21	48	10	70	16	144	0.02	0.08	0.37	0.16	0.25	0.60
6-28-83	1	3.55	23.45	6.29	24	210	15	180	20	350	0.05	0.33	0.03.	1.50	0.80	7.68
	2	0.38	1.87	0.71	29	126	24	160	36	300	0.02	0.17	0.25	1.03	0.02	5.56
9-21-83	1	2.59	33.7	6.33	42	72	22	40	36	56	0.02	0.34	0.02	0.32	2.68	6.84
	2	0.25	2.66	0.57	12	96	12	34	18	78	0.02	0.16	0.02	0.67	0.02	4.20



LEGEND
(FOR SCHEMATIC)

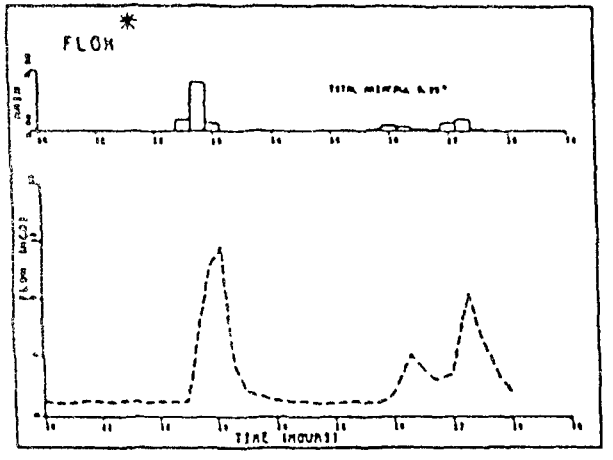
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

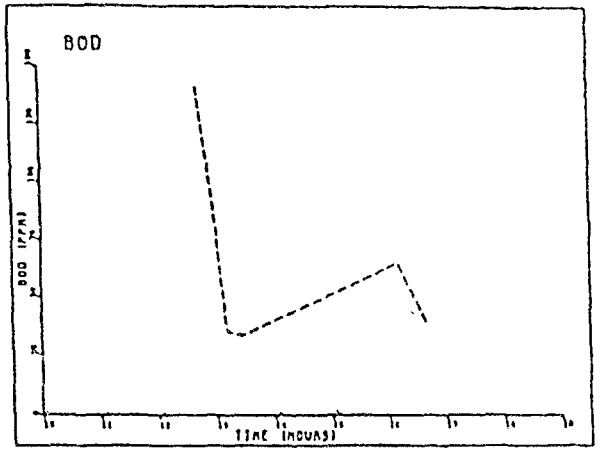
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
SAYBROOK PLACE OVERFLOW
CITY OF NEWARK

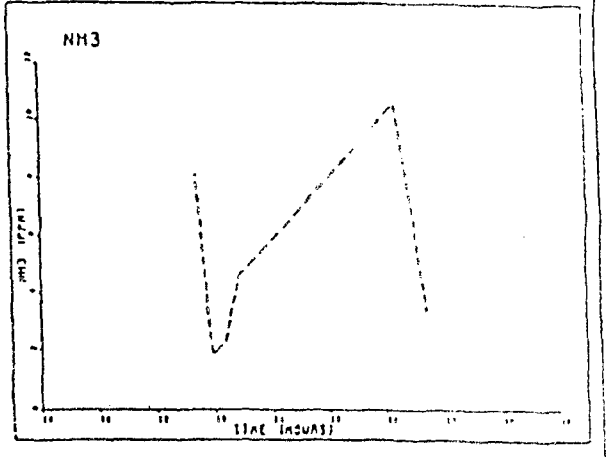
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

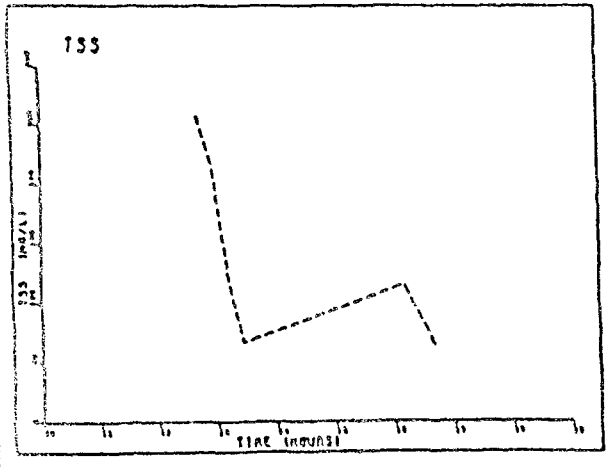
FIGURE 3-27A

946510105









LEGEND

---------- (STA. I)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 6/28/83
RECTOR ST. OVERFLOW
CITY OF NEWARK

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
17 Becker Street Millburn, New Jersey 07041

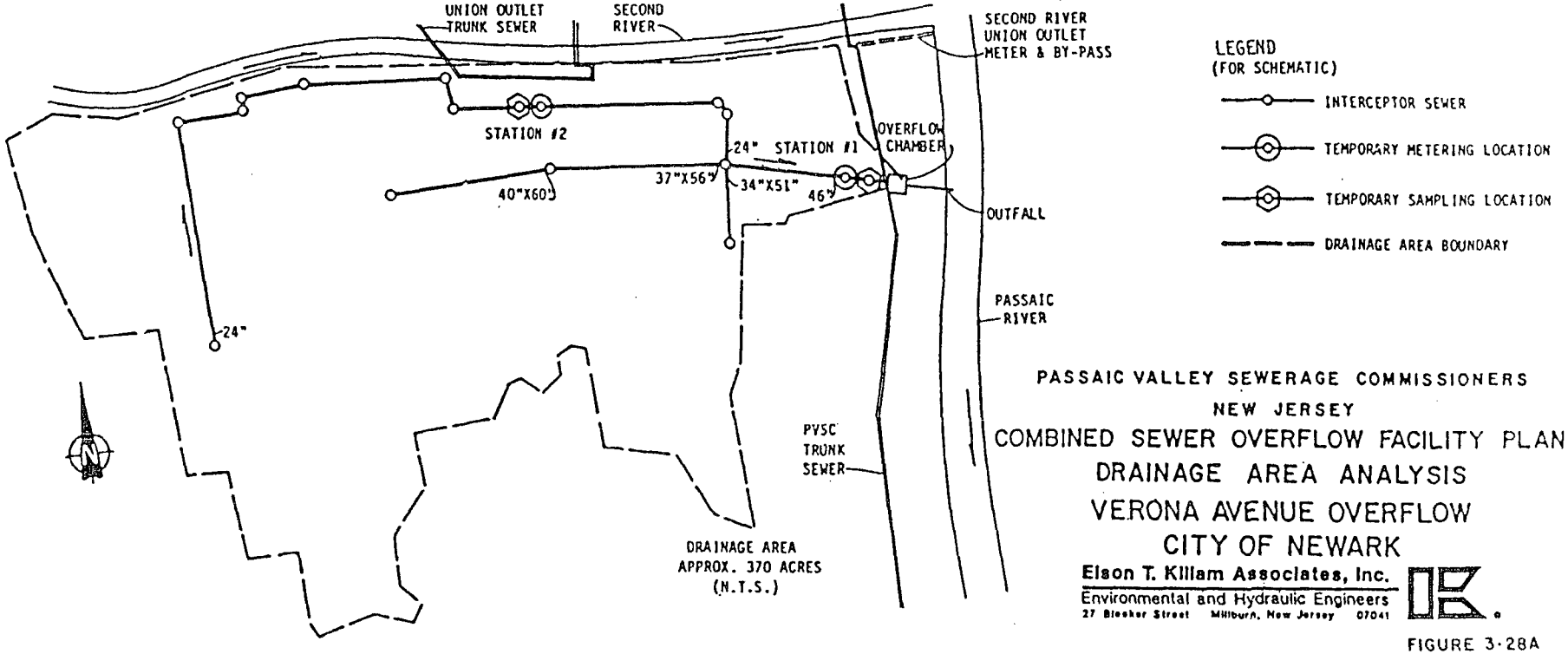
946510106

FIGURE 3.26B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
9-20-82	1	0.44	11.45	2.92	200	690	127	445	140	1020	0.02	0.09	0.02	1.37	5.06	66.8
	2	0.19	0.81	0.37	69	380	40	405	50	725	0.02	0.11	0.03	0.67	5.34	10.8
9-27-82	1	1.09	21.39	4.19	110	690	30	550	70	2190	0.02	0.41	0.02	0.84	0.82	21.6
	2	0.23	0.95	0.42	50	290	8	215	20	375	0.02	0.14	0.02	0.66	2.64	24.5
11-5-82	1	1.59	17.61	3.76	260	410	167	280	193	320	0.02	0.02	0.03	0.48	9.64	17.4
	2	0.24	1.08	0.44	200	260	60	93	100	113	0.02	0.02	0.02	0.11	15.7	16.5
11-13-82	1	1.16	32.93	6.37	58	740	20	2020	30	2185	0.02	0.12	0.02	1.2	0.14	19.8
	2	0.32	0.89	0.55	39	180	56	196	36	312	0.02	0.04	0.02	0.38	2.40	17.8

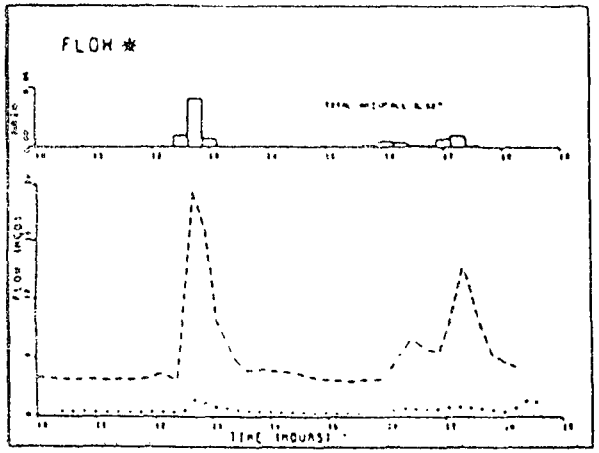


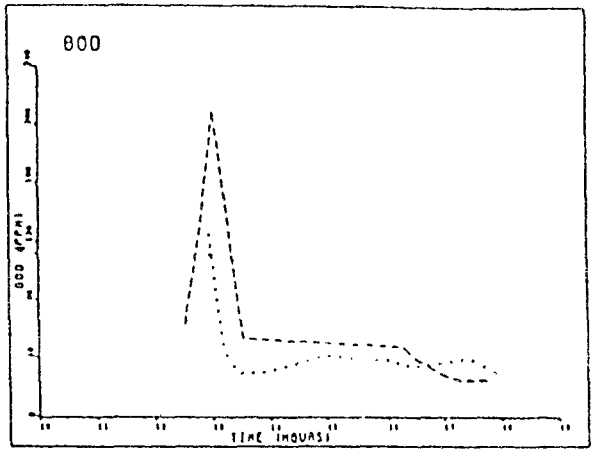
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
VERONA AVENUE OVERFLOW
CITY OF NEWARK

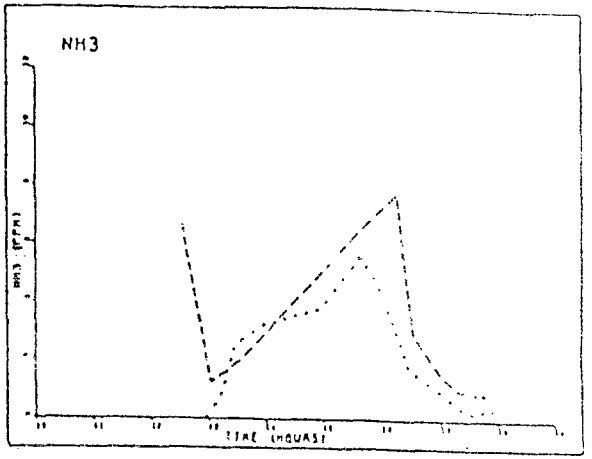
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

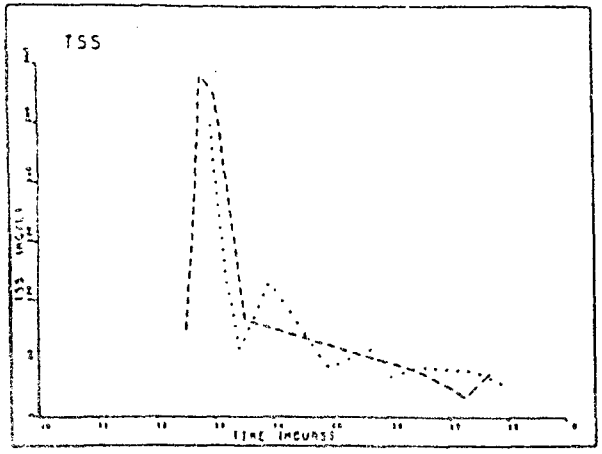
FIGURE 3-28A

946510107









LEGEND

---------- (STA. 1)

- - - - - - - - - (STA. 2)

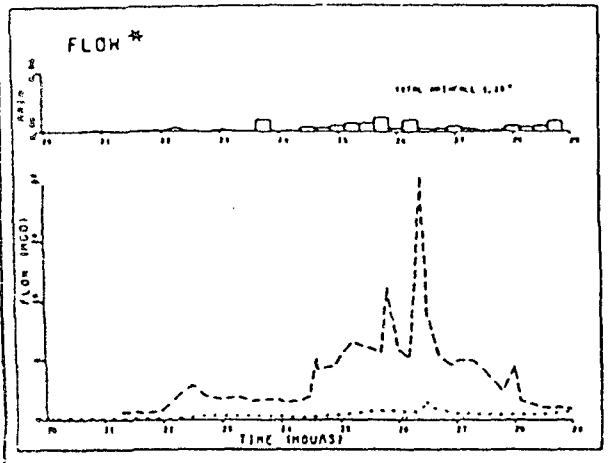
* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

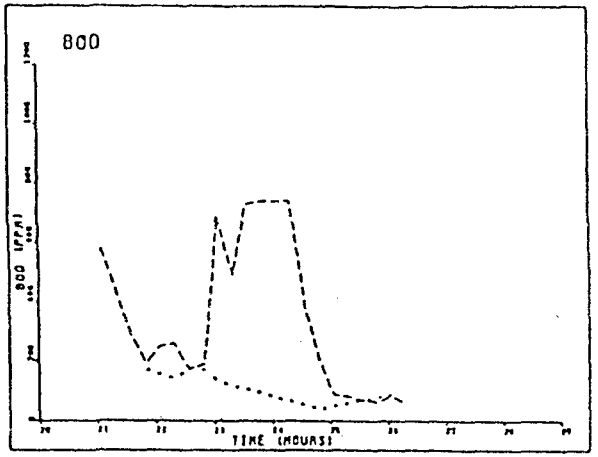
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 6/28/83
SAYBROOK PLACE OVERFLOW
CITY OF NEWARK

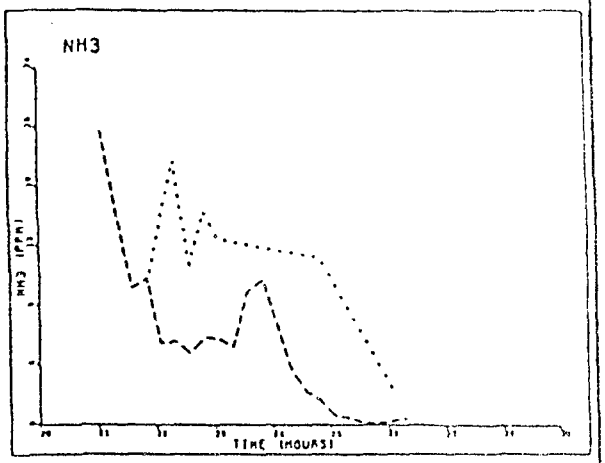
946510108

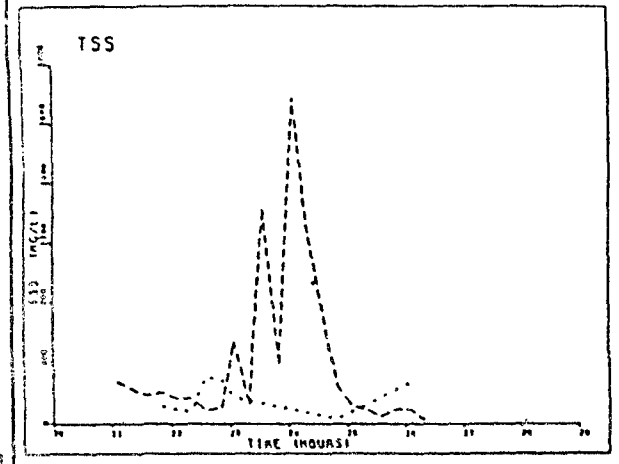
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Sleeker Street Millburn, New Jersey 07041

FIGURE 3.27B









LEGEND

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* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 11/12/82

VERONA AVENUE OVERFLOW
CITY OF NEWARK

946510109

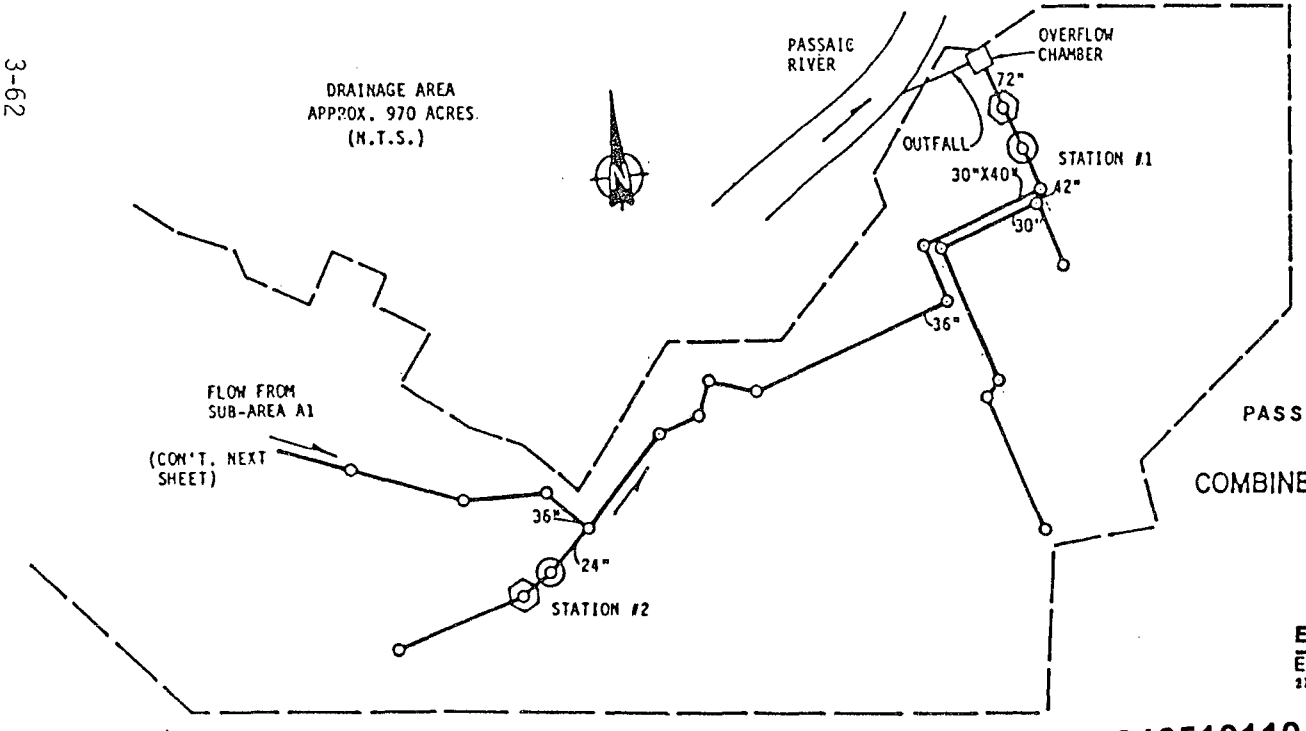
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers

FIGURE 3-28B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	1	11.05	21.49	15.91	570	730	120	250	128	260	0.01	0.01	0.01	0.08	19.0	43.6
	2	0.82	2.12	1.18	70	93	36	56	56	72	0.01	0.52	0.07	1.05	3.72	6.16
3-16-82	1	8.44	16.64	11.09	195	375	140	170	200	230	0.01	0.05	0.31	0.46	50.0	73.2
	2	0.67	1.98	0.78	75	81	36	40	56	68	0.06	0.08	0.27	0.82	5.10	10.1
4-3-82	1	11.23	26.92	15.06	60	405	50	180	50	290	0.00	0.20	0.00	0.11	4.00	25.9
	2	0.57	7.67	1.18	40	130	10	110	20	180	0.00	0.27	0.01	0.16	5.30	16.9



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CURTIS PLACE OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

SHEET 1 OF 2

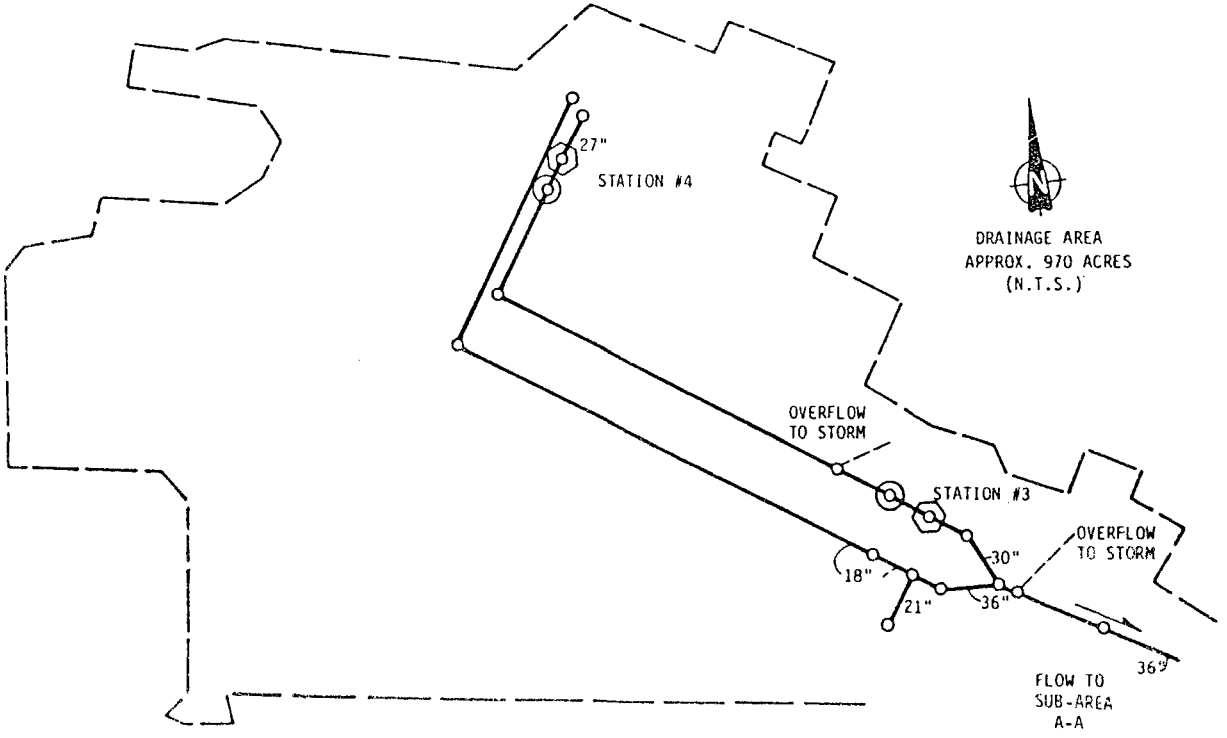
FIGURE 3-29A

946510110

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	3	5.82	7.11	6.51	750	760	330	630	340	650	0.01	0.01	0.01	0.09	8.72	14.9
	4	2.02	2.65	2.43	390	740	140	220	250	330	0.07	0.14	0.36	0.91	49.6	202.
3-16-82	3	5.51	6.30	5.81	-	-	-	-	-	-	-	-	-	-	-	-
	4	2.16	3.12	2.48	228	228	40	40	60	60	0.01	0.01	0.46	0.46	219.	219.
4-3-82	3	2.15	6.89	3.01	140	240	70	230	152	340	0.00	0.84	0.00	0.70	4.24	18.8
	4	-	-	-	110	220	40	200	55	310	0.00	0.79	0.00	0.49	5.44	21.5



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

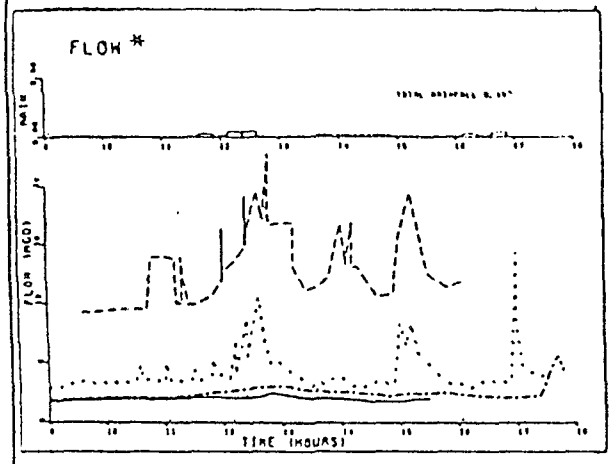
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
CURTIS PLACE OVERFLOW
CITY OF PATERSON (Con't)

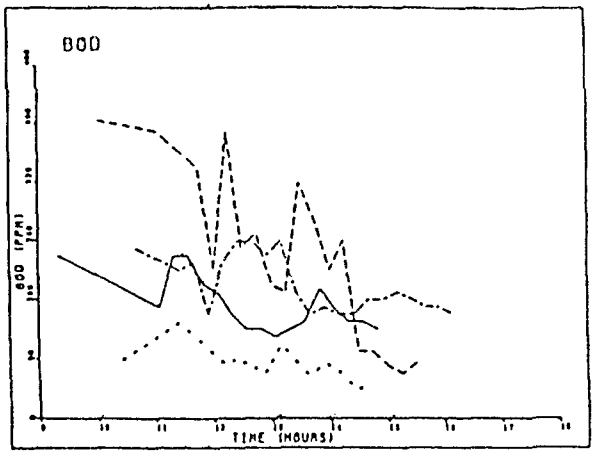
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

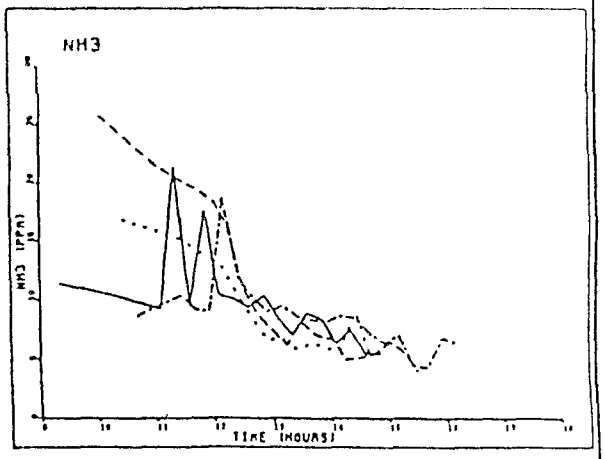
SHEET 2 OF 2

FIGURE 3-23B

946510111







LEGEND

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---------- (STA. 3)

———————— (STA. 4)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

946510112

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 4/3/82

CURTIS PLACE OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
31 Bleeker Street Millburn, New Jersey 07041

3-64

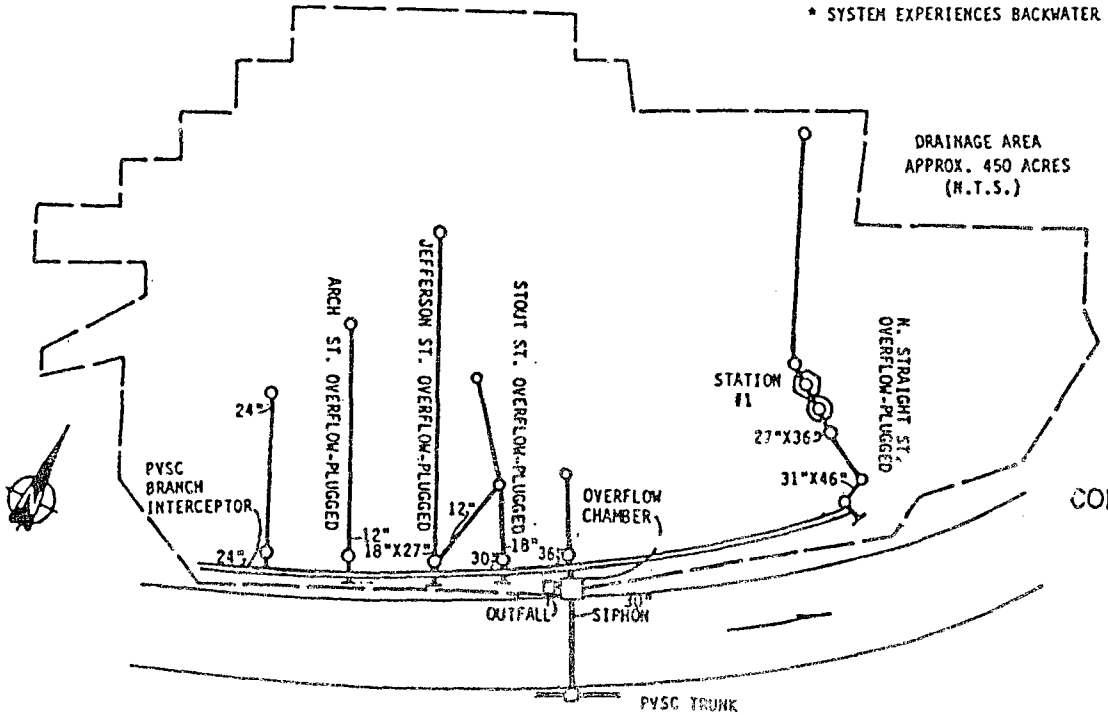
FIGURE 3.29C

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD) *			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	1	3.98	11.44	10.13	56	84	34	52	38	60	0.04	0.25	0.34	1.54	1.92	3.32
4-3-82	1	0.26	8.17	2.47	75	200	90	190	100	400	0.00	0.00	0.00	0.00	5.16	23.9

* SYSTEM EXPERIENCES BACKWATER AFFECTS UNDER CERTAIN CONDITIONS.



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY
- PLUGGED OFF OVERFLOW

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
HUDSON ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Blecker Street Millburn, New Jersey 07041

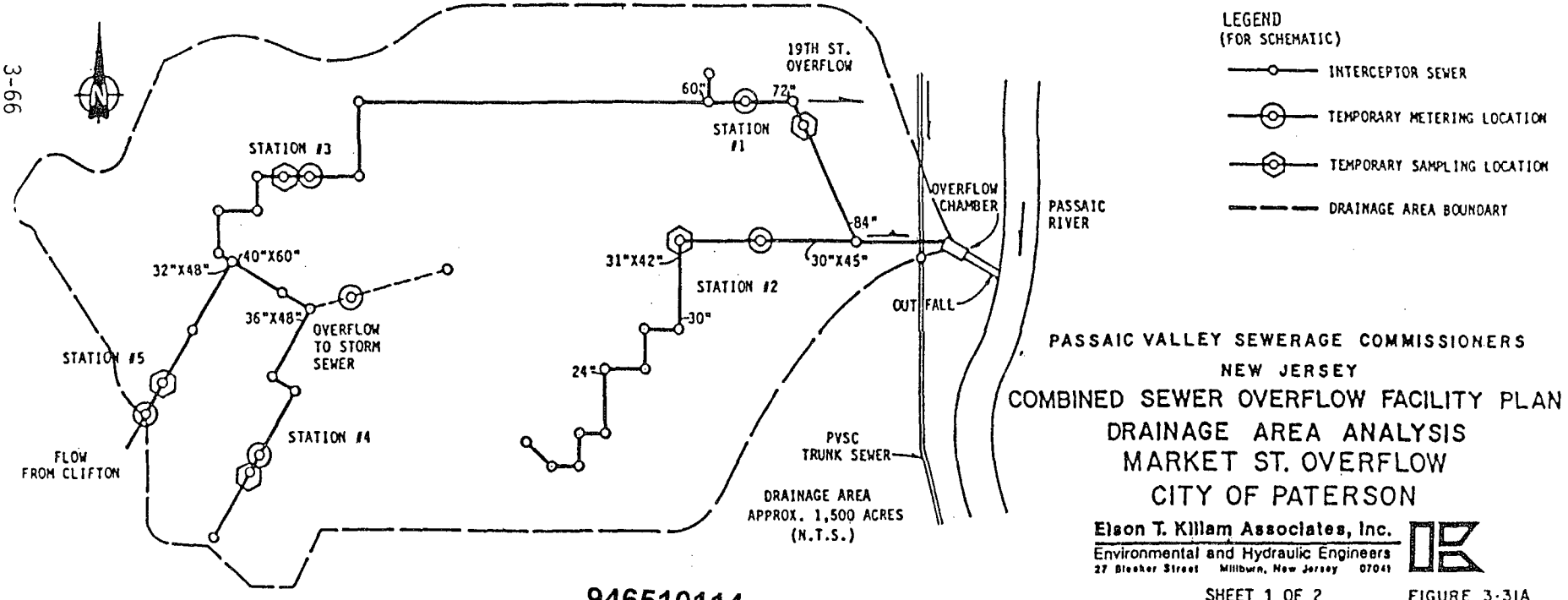
FIGURE 3-30

946510113

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
4-26-82	1	5.17	31.65	15.50	30	156	12	208	56	340	0.01	0.35	0.01	0.58	0.60	6.80
	2	0.28	1.97	1.24	34	102	16	200	36	300	0.01	0.07	0.33	1.24	1.07	6.84
	3	3.57	30.59	12.85	20	114	20	200	32	310	0.02	0.59	0.01	1.03	0.50	3.90
	4	0.52	4.73	2.26	14	51	4	88	24	212	0.01	0.07	0.31	1.20	0.59	4.08
	5	0.49	0.60	0.54	64	140	20	66	48	104	0.01	0.45	0.01	0.88	10.4	12.6
6-16-82	1	-	-	-	21	140	40	200	105	755	0.01	0.18	0.01	0.58	0.56	8.84
	2	1.36	12.92	2.93	34	250	40	260	60	490	0.01	0.03	0.01	0.30	0.97	15.8
	3	3.15	44.09	9.87	16	192	40	175	75	460	0.01	0.09	0.01	0.58	0.24	8.16
	4	2.23	24.42	4.76	16	170	10	160	20	200	0.01	0.07	0.01	0.71	0.34	17.7
	5	-	-	-	32	150	66	108	80	144	0.01	0.10	0.01	0.05	10.3	22.4



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
MARKET ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

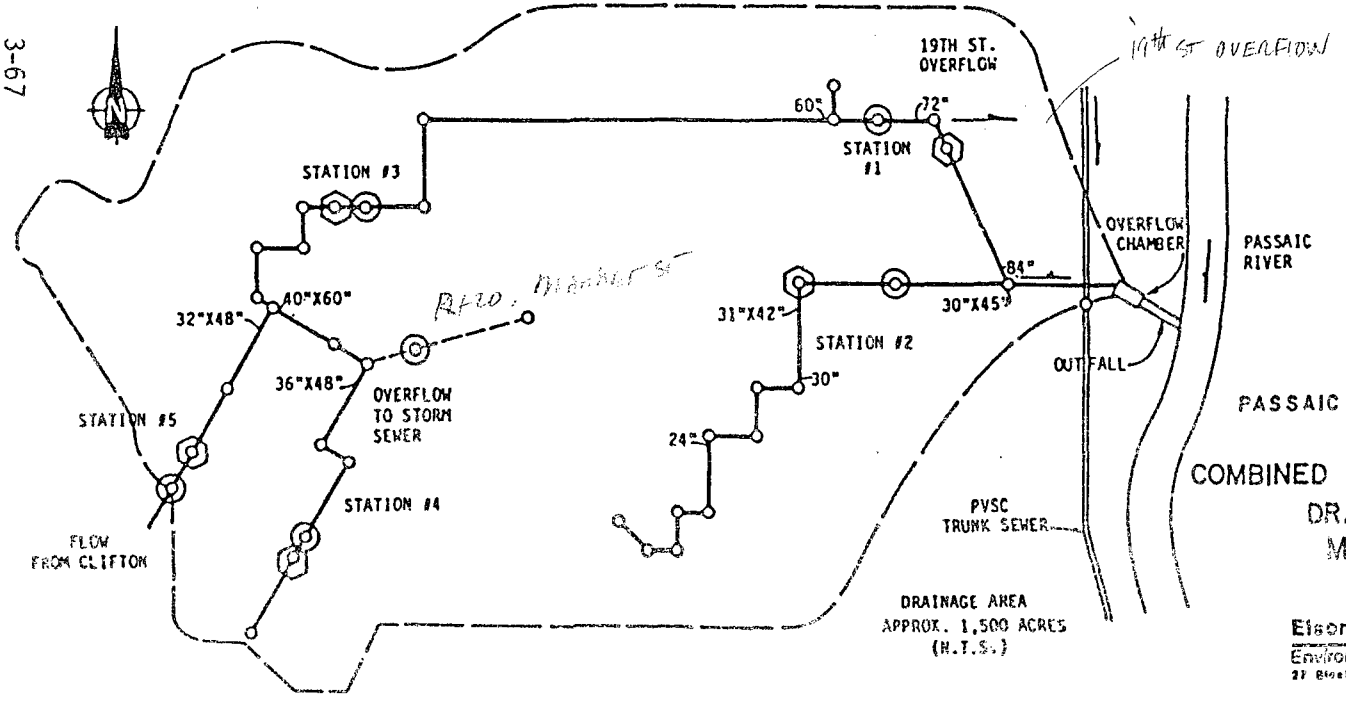
SHEET 1 OF 2 FIGURE 3-31A

946510114

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
7-27-82	1	6.19	66.88	17.18	27	180	20	124	32	248	0.02	0.22	0.02	0.78	0.20	14.1
	2	1.39	18.83	3.83	27	86	32	128	44	296	0.02	0.24	0.16	1.34	0.45	7.76
	3	1.61	42.94	7.81	27	120	8	160	24	344	0.02	0.48	0.02	1.01	0.21	12.6
	4	0.15	22.92	1.66	-	-	-	-	-	-	-	-	-	-	-	-
	5	0.03	0.21	0.06	57	155	72	120	84	180	0.02	0.23	0.03	0.45	14.1	25.8
9-2-82	1	6.77	67.21	27.05	22	220	12	208	24	536	0.02	0.20	0.02	1.51	0.42	12.1
	2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	3	3.37	43.32	12.77	15	180	8	76	20	156	0.02	0.24	0.02	1.85	0.66	13.3
	4	0.75	39.57	3.37	22	200	8	176	40	424	0.02	0.11	0.02	1.16	0.04	8.50
	5	0.06	0.24	0.13	41	260	24	140	56	292	0.02	0.10	0.02	0.35	8.64	22.6



LEGEND
(FOR SCHEMATIC)

- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

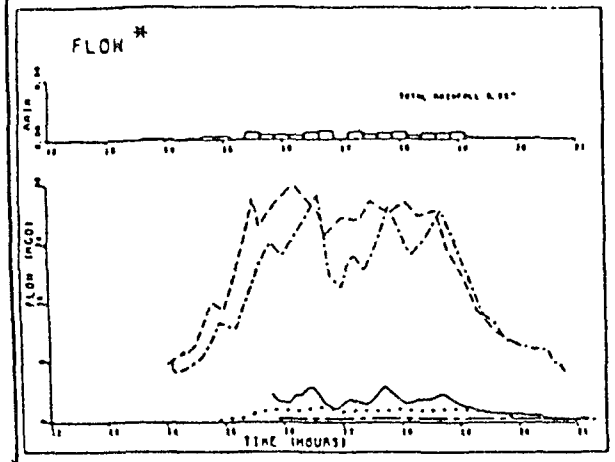
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
MARKET ST. OVERFLOW
CITY OF PATERSON

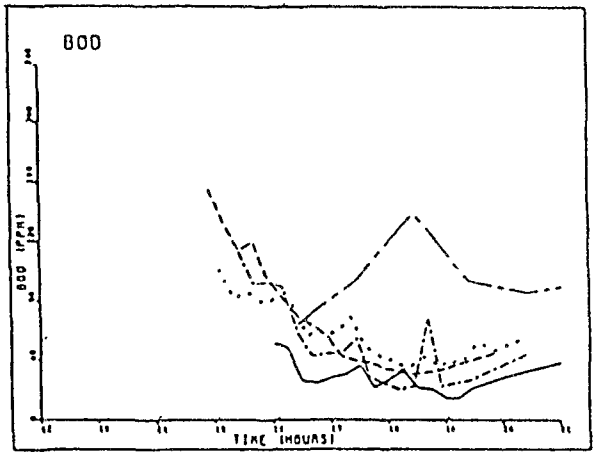
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

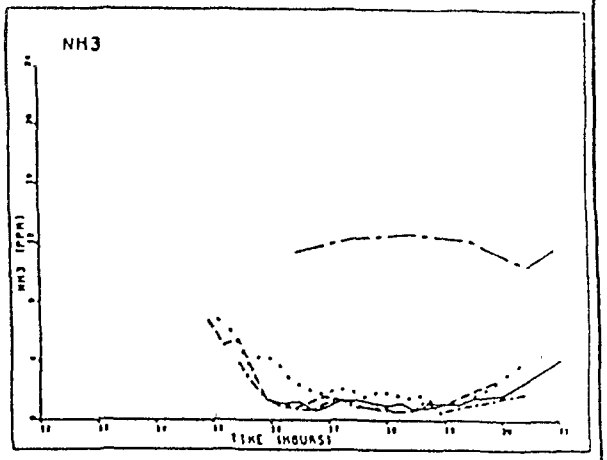
SHEET 2 OF 2

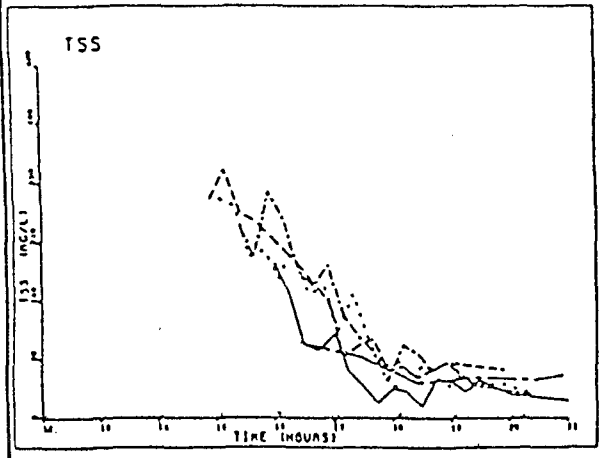
FIGURE 3-31B

946510115









LEGEND

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———————— (STA. 4)
— — — — — (STA. 5)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

946510116

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 4/26/82
MARKET STREET OVERFLOW
CITY OF PATERSON

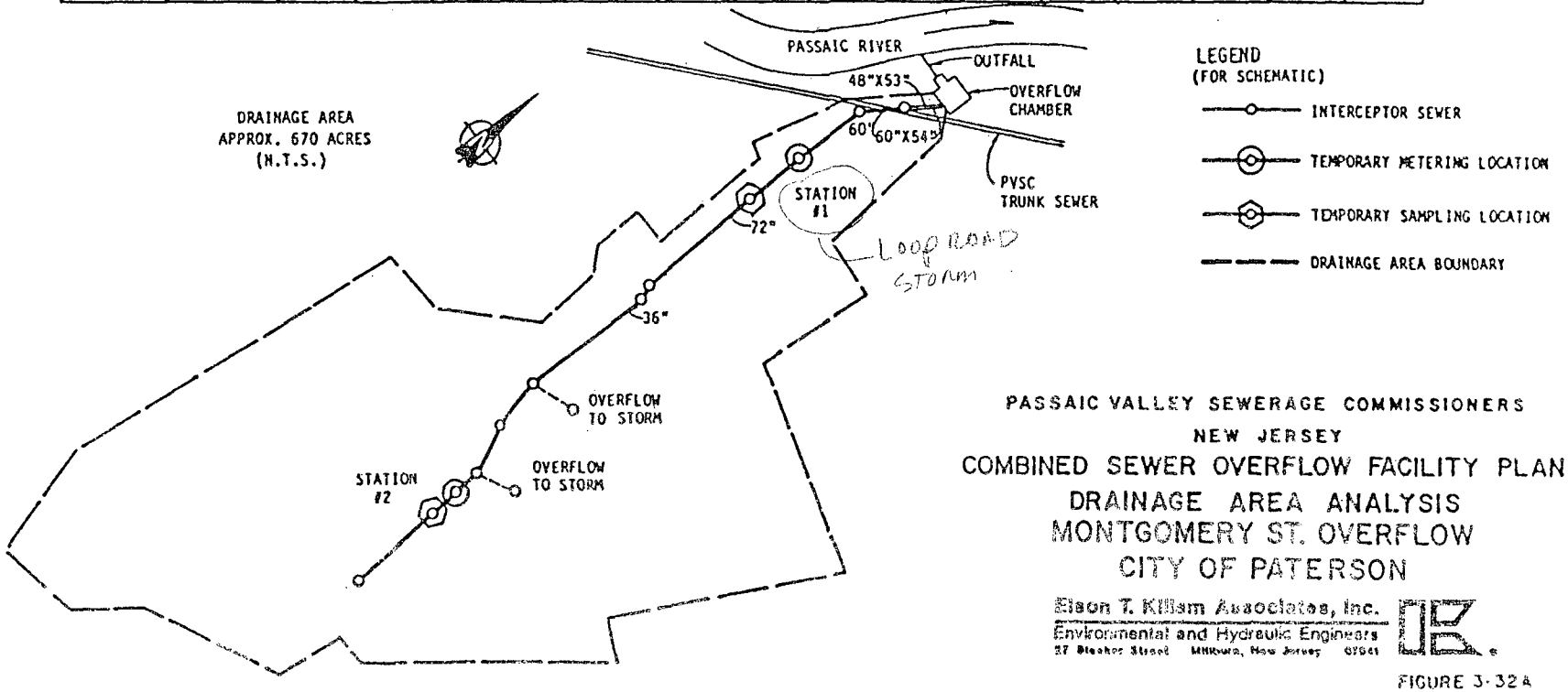
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
31 Step Street Millburn, New Jersey 07041

FIGURE 3-31C

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	1	3.11	5.46	4.06	50	100	32	120	36	140	0.01	0.13	0.10	0.76	2.86	8.09
	2	2.82	3.12	3.06	50	140	60	112	62	128	0.03	0.10	0.01	0.58	2.80	11.1
3-16-82	1	2.01	6.79	3.57	69	90	30	50	40	70	0.05	0.11	0.29	0.57	4.60	9.74
	2	2.84	5.89	4.17	68	102	30	90	50	150	0.07	0.14	0.40	0.61	2.87	9.74
4-3-82	1	-	-	-	42	140	28	204	104	288	0.01	1.12	0.00	3.42	1.87	15.9
	2	2.12	4.51	3.36	56	140	30	290	70	435	0.00	2.38	0.00	0.91	0.96	23.3

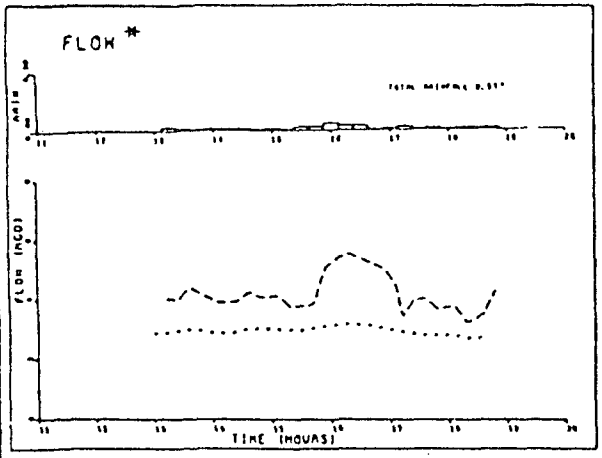


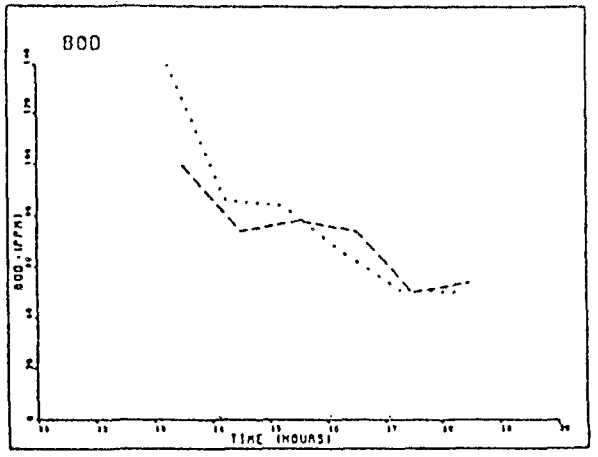
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
MONTGOMERY ST. OVERFLOW
CITY OF PATERSON

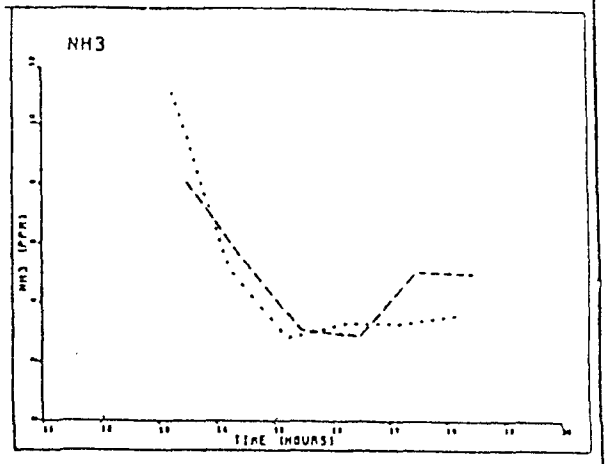
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

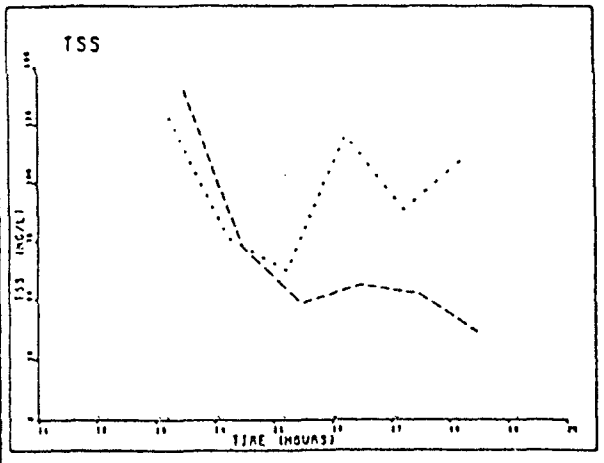
FIGURE 3-32A

946510117









LEGEND

---------- (STA. 1)

- - - - - - - - - (STA. 2)

* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 10/23/81

MONTGOMERY ST. OVERFLOW

CITY OF PATERSON

946510118

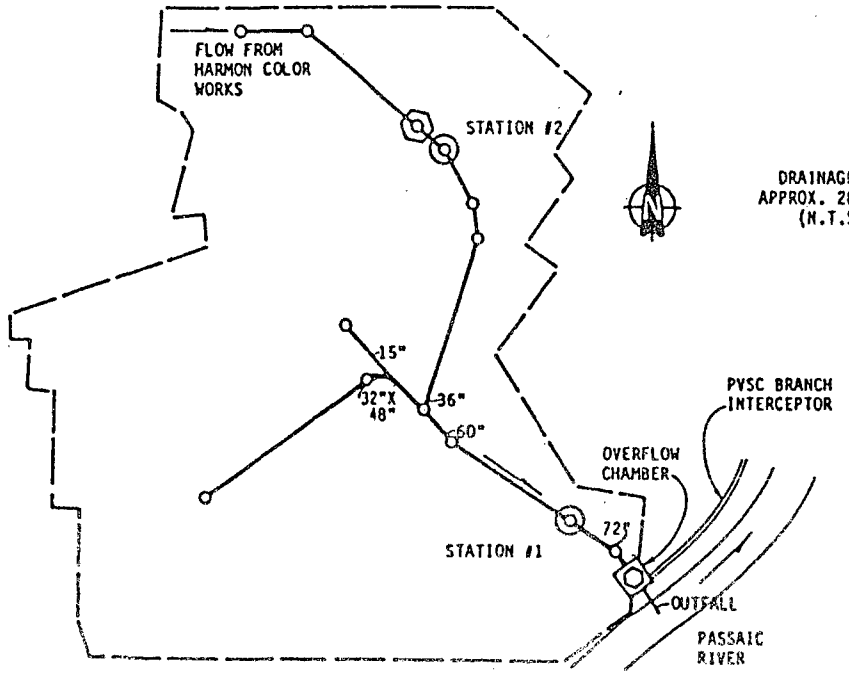
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 3-32B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	1	1.18	2.44	1.60	84	230	36	200	40	360	0.01	0.07	0.04	0.29	32.4	77.5
	2	0.73	1.68	1.04	220	390	40	180	50	630	0.01	0.03	0.07	0.25	108.	234.
3-16-82	1	1.06	2.49	1.38	105	278	20	40	60	70	0.01	0.01	0.12	0.39	58.8	107.
	2	0.59	1.23	0.88	510	510	20	20	40	40	0.01	0.01	0.19	0.19	237.	237.
4-3-82	1	0.97	3.04	1.39	33	270	60	270	130	470	0.00	0.57	0.00	0.96	1.35	22.9
	2	0.89	2.02	1.29	57	320	30	90	40	140	0.00	0.73	0.00	0.53	1.78	11.8
4-26-82	1	1.19	3.67	2.14	44	250	20	130	56	200	0.01	0.31	0.03	0.70	3.72	50.8
	2	0.15	1.08	0.50	57	885	20	190	30	350	0.01	0.14	0.07	0.70	10.5	158.



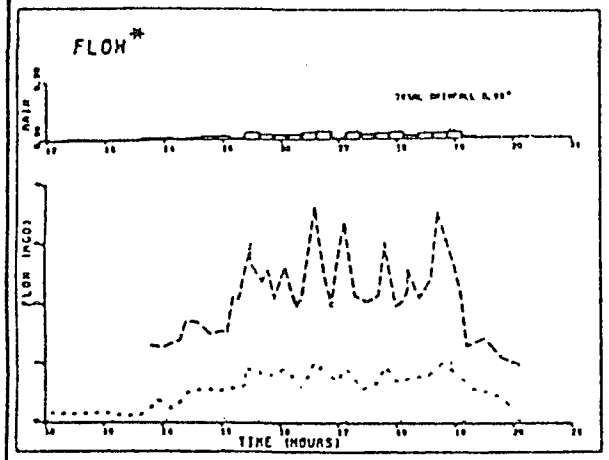
LEGEND
(FOR SCHEMATIC)
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

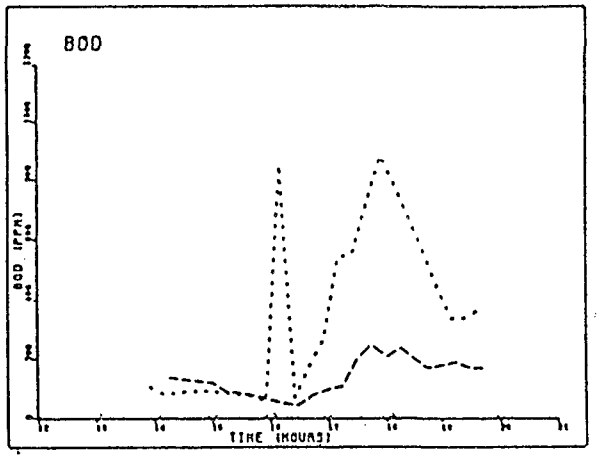
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
NORTHWEST STREET OVERFLOW
CITY OF PATERSON

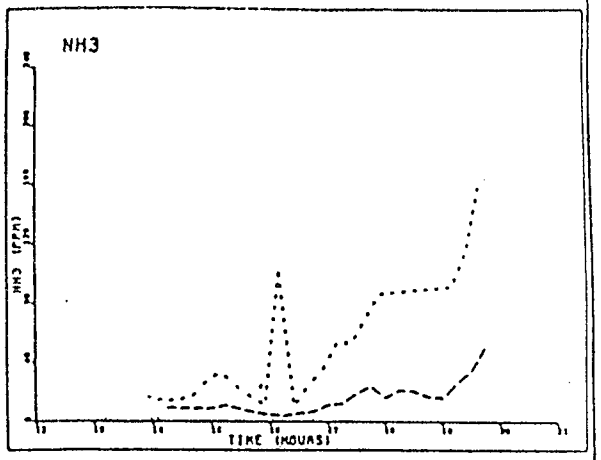
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
Millburn, New Jersey

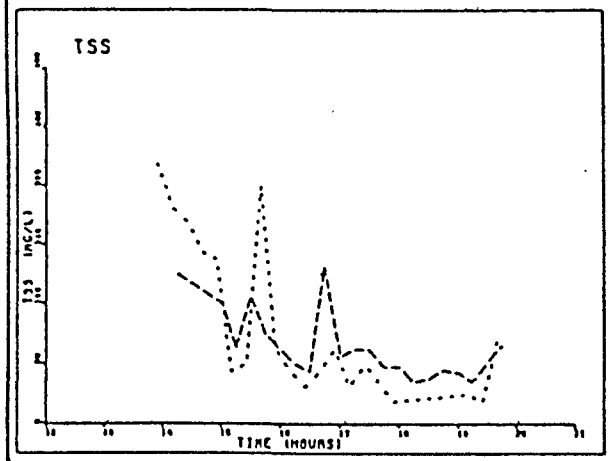
FIGURE 3-33A

946510119









LEGEND

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* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 4/26/82

NORTHWEST STREET OVERFLOW
CITY OF PATERSON

946510120

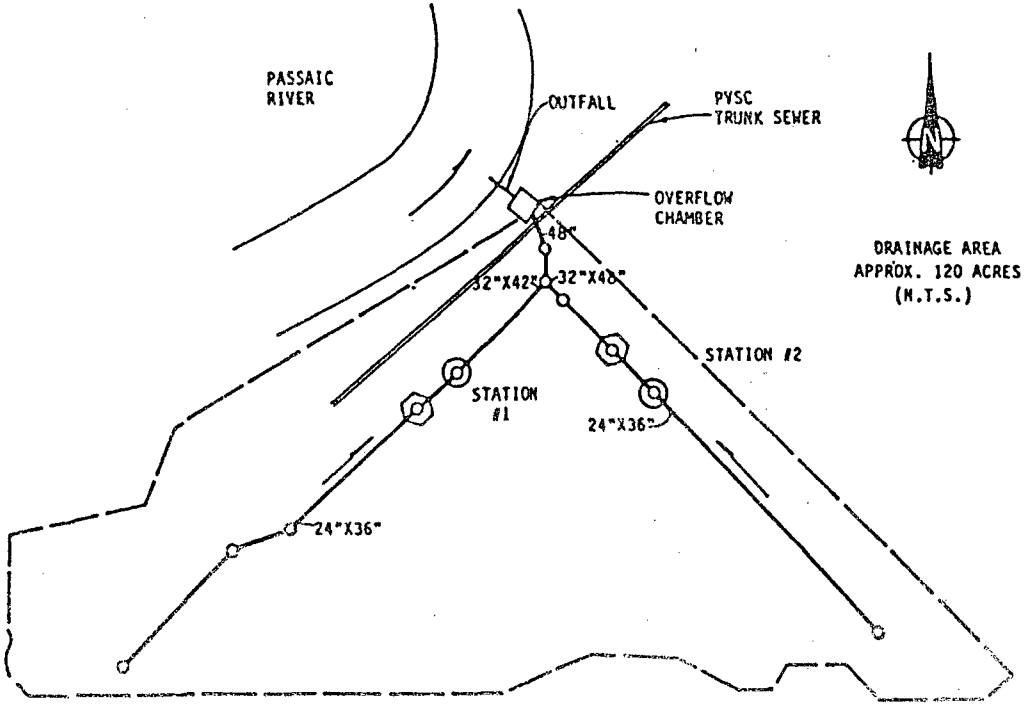
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

FIGURE 3-33B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	1	1.31	2.43	1.85	100	150	40	80	76	96	0.02	0.21	0.04	0.91	2.86	12.9
	2	0.17	0.35	0.22	45	62	8	60	44	100	0.04	0.09	0.28	0.77	1.66	5.74
3-16-82	1	-	-	-	75	90	90	90	180	180	0.05	0.06	0.42	0.49	3.83	4.17
	2	0.08	0.29	0.21	98	232	200	200	240	240	0.12	0.23	0.51	0.77	4.31	11.8
4-3-82	1	0.29	2.08	0.84	48	280	32	180	100	312	0.00	0.33	0.00	0.64	1.40	17.1
	2	0.09	0.48	0.17	32	220	24	188	96	408	0.00	0.50	0.00	1.36	0.53	12.1
6-16-82	1	0.29	11.49	1.29	108	180	56	116	64	116	0.01	0.04	0.01	0.52	3.49	14.4
	2	0.06	1.97	0.16	90	220	60	187	88	967	0.01	0.01	0.01	0.11	0.06	9.64



DRAINAGE AREA APPROX. 120 ACRES (M.T.S.)

LEGEND
(FOR SCHEMATIC)

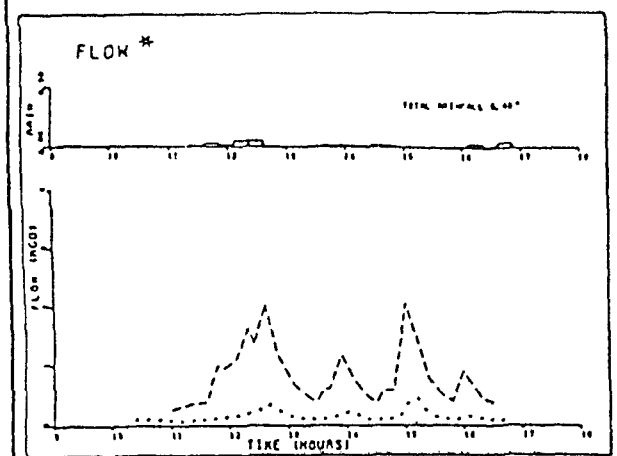
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

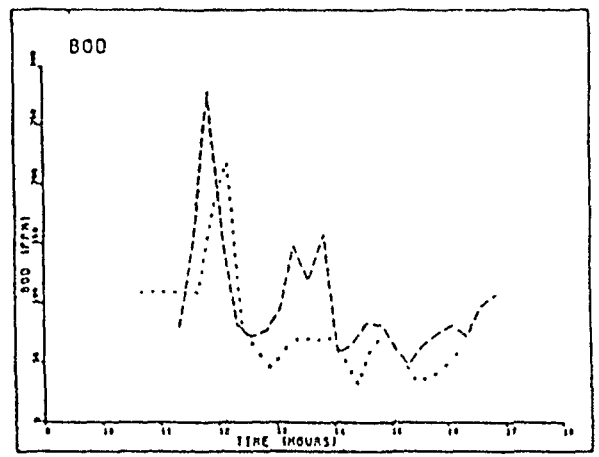
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
STRAIGHT STREET OVERFLOW
CITY OF PATERSON

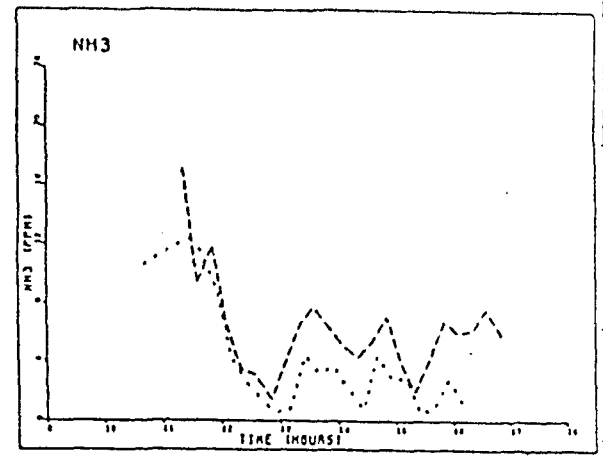
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

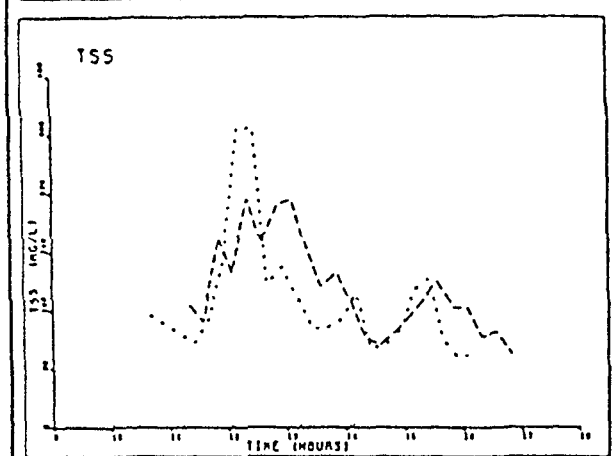
FIGURE 3-34A

946510121









LEGEND

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* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 4/3/82

STRAIGHT STREET OVERFLOW

CITY OF PATERSON

946510122

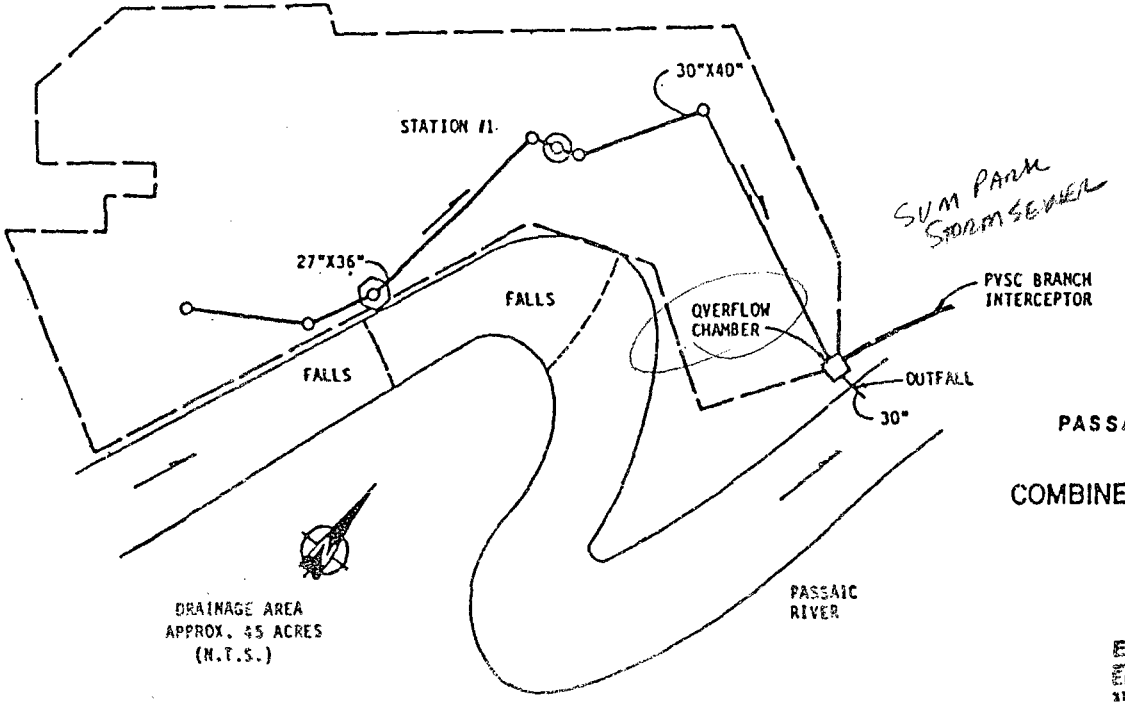
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Bleeker Street Millburn, New Jersey 07041

FIGURE 3-34B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
10-23-81	1	0.09	0.38	0.18	70	93	36	56	56	72	0.01	0.58	0.07	1.05	3.72	6.16
3-16-82	1	0.05	0.29	0.09	80	405	56	360	84	470	0.06	0.08	0.27	0.82	5.10	10.1
4-3-82	1	-	-	-	40	130	10	110	20	180	0.00	0.27	0.00	0.16	5.30	16.9
9-2-82	1	0.06	3.24	0.23	27	260	4	452	12	636	0.02	0.14	0.02	0.57	0.37	15.3



LEGEND
(FOR SCHEMATIC)

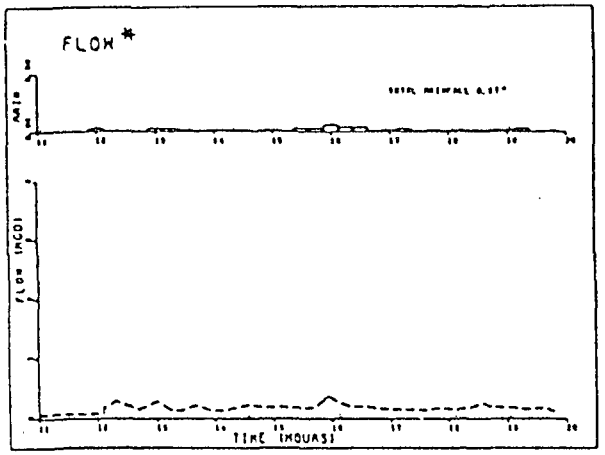
- INTERCEPTOR SEWER
- TEMPORARY METERING LOCATION
- TEMPORARY SAMPLING LOCATION
- DRAINAGE AREA BOUNDARY

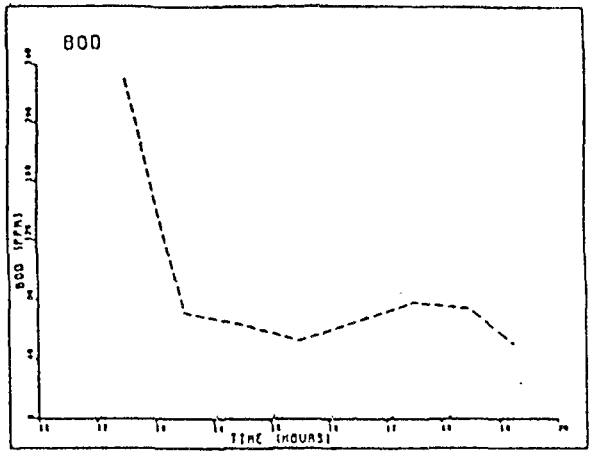
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
S.U.M. OVERFLOW
CITY OF PATERSON

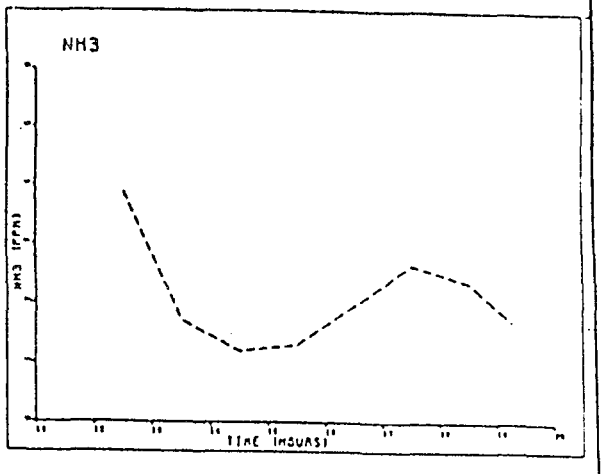
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
37 Skyline Street Millburn, New Jersey 07041

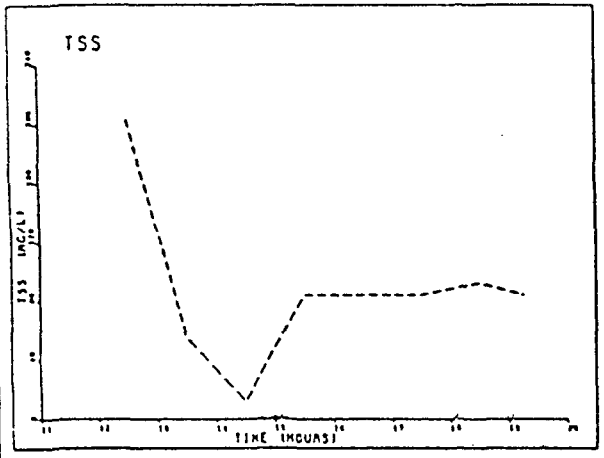
FIGURE 3-35A

946510123









LEGEND

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* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
RAINFALL OF 10/23/81

S.U.M. PARK OVERFLOW
CITY OF PATERSON

946510124

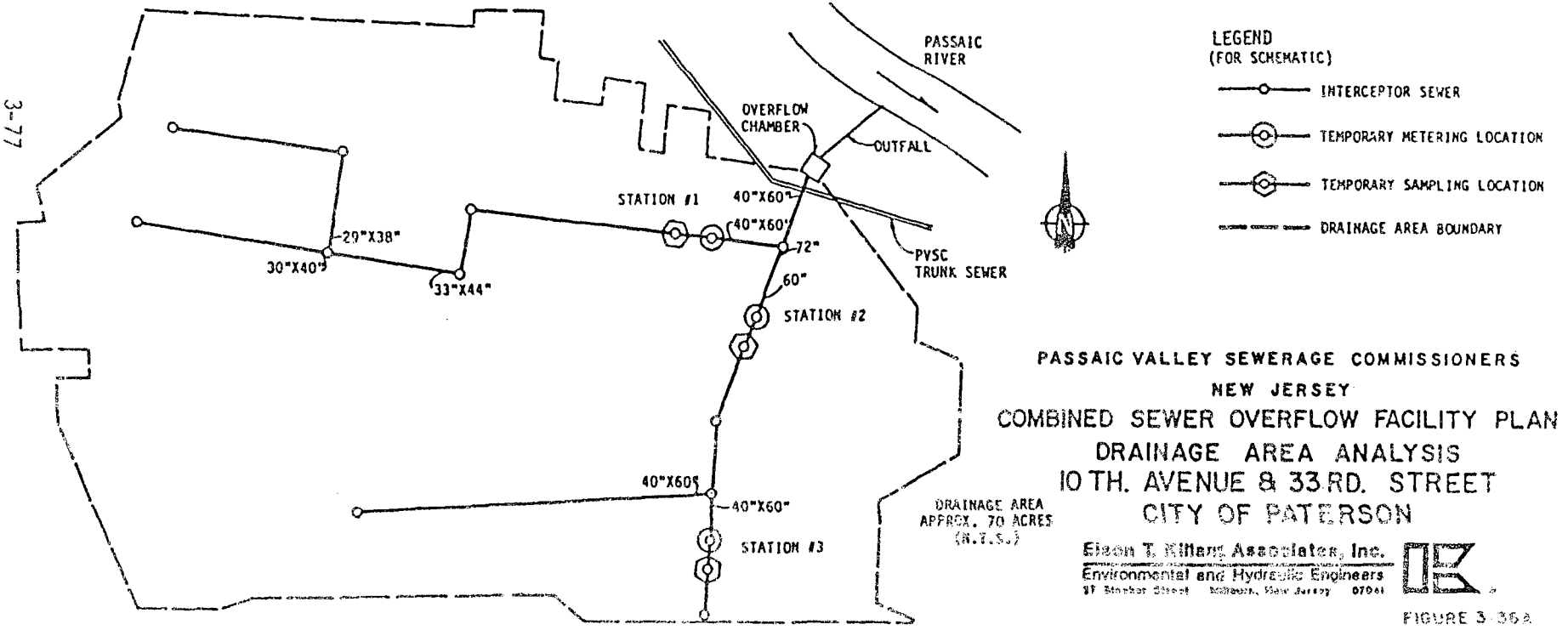
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 3-35B

NOTE:
A.D.F. = AVERAGE DAILY FLOW
MIN. = MINIMUM
MAX. = MAXIMUM

SUMMARY OF INTERCEPTOR MONITORING

DATE	STATION NO.	FLOW (MGD)			BOD (MG/L)		TVSS (MG/L)		TSS (MG/L)		NO_2-N (MG/L)		NO_3-N (MG/L)		NH_3-N (MG/L)	
		MIN.	MAX.	ADF.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
4-26-82	1	3.31	7.87	6.28	28	222	0	190	60	520	0.01	1.14	0.01	0.52	1.51	11.8
	2	4.39	19.43	10.61	27	198	10	210	39	370	0.01	0.03	0.01	0.65	0.49	6.36
	3	0.52	14.07	3.95	33	180	0	240	10	310	0.01	0.08	0.01	0.58	0.38	3.48
6-16-82	1	1.99	11.23	3.12	80	450	76	410	84	1140	0.01	0.22	0.01	0.08	1.52	21.6
	2	2.03	27.93	5.33	62	210	72	355	80	600	0.01	0.02	0.01	0.20	0.29	11.0
	3	0.34	17.85	2.62	15	210	32	230	56	440	0.01	0.03	0.01	0.25	0.40	11.2
7-27-82	1	1.55	12.75	2.85	20	84	16	136	18	328	0.02	0.48	0.02	1.07	0.52	21.0
	2	1.33	42.67	4.67	36	36	28	32	36	44	0.02	0.08	0.02	0.06	6.28	6.36
	3	0.14	34.89	2.49	30	72	28	108	32	264	0.02	0.29	0.04	1.66	0.36	7.56



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
DRAINAGE AREA ANALYSIS
10TH. AVENUE & 33RD. STREET
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
FIGURE 3-36A

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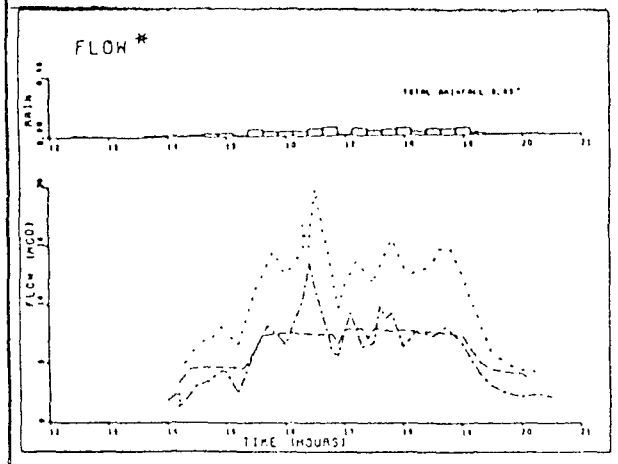

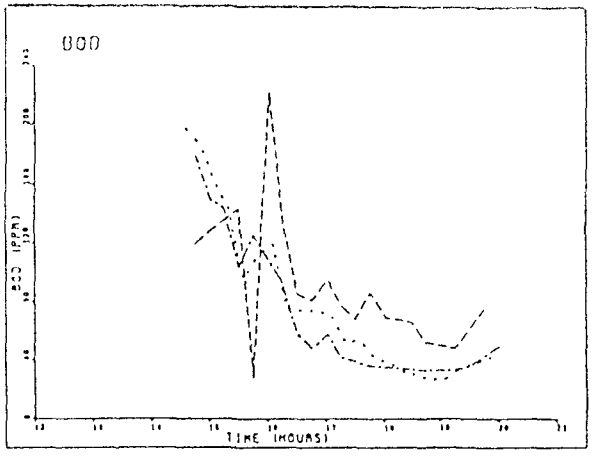

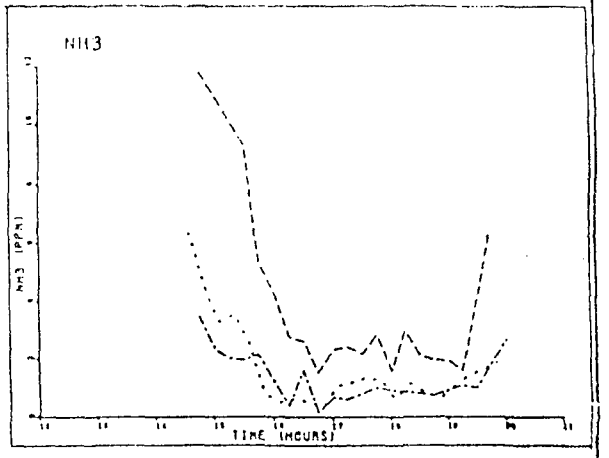

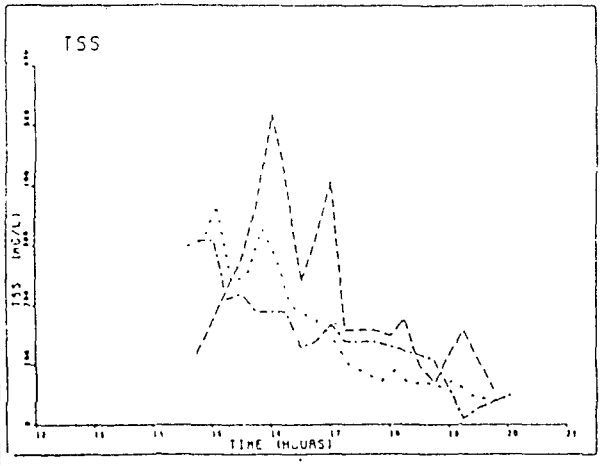

LEGEND

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* NOTE: FLOW SHOWN IS FOR SAMPLING PERIOD ONLY.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

DRAINAGE AREA ANALYSIS
RAINFALL OF 4/26/82

10TH. AVE. & 33RD. ST. OVERFLOW

CITY OF PATERSON

946510126

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 3-36B

4. ALTERNATIVE ANALYSIS

4. ALTERNATIVE ANALYSIS

Control alternatives to continued combined sewer overflow discharges are usually classified into three groups: (a) capital intensive alternatives, (b) minimal-structural alternatives, and (c) non-structural alternatives. Current thinking on CSO control alternatives has moved away from capital intensive controls and towards those that would provide a more cost-effective approach to the problem. Accordingly, throughout the various stages of the alternative analysis, minimal and non-structural alternatives have been given primary consideration with capital intensive alternatives only considered as a last resort.

The control alternatives within the lower Passaic River have been formulated in conjunction with the long and short term analysis upon the impacts of combined sewer overflow discharge upon the lower Passaic River and other known factors. The analysis of pollutional loadings to the lower Passaic River has shown that combined sewer overflow discharges within the PVSC District are only marginally responsible for the pollutional loadings and subsequent low dissolved oxygen content within the river (See Volume 2). The analysis completed upon the CSOs impact within this phase of the study was based upon concentration variations in C-BOD, N-BOD and DO within the study area. It did not evaluate the impacts on other water quality parameters (heavy metals, grease and oil, solids, phosphorus, coliforms, etc.); therefore conclusions drawn from the analysis should not be extended to parameters outside of the original scope of work.

In an aquatic environment, pollution is first perceived by various conditions that offend our natural senses of sight and smell. Debris and floating material in addition to obnoxious odors produced under anaerobic

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conditions are parameters that produce negative responses and are therefore, objectionable in nature. The lower Passaic River is polluted in the sense that when viewed under conditons not abnormal within this region, the perception of pollution is evident. This is especially true within the estuary region due to tidal fluctuations and increased residence times for pollutants. The fact that measured pollutional loadings have shown that CSO discharges do not have a major impact on "water quality" for the parameters investigated, does not diminish or eliminate the perception of pollution. As a whole the total pollutional load reaching lower areas is significant. The total pollutional load from upper drainage areas, storm sewers, benthos and CSO discharges, does have a substantial impact on water quality and the biological communities within the lower Passaic River. Significant differences exist within the variety and diversity of biological communities (See Volume 3) as one progresses from Little Falls to Newark Bay.

Vast quantities of suspended and floatable solids are discharged from both combined sewer overflows, bypasses, and separate storm sewers throughout the basin. Improper disposal of solid wastes (tires, shopping carts, crates, etc.), sunken boats, barges, deteriorating docks and bulkheads located along the estuary, and to a lesser extent the river portion, all contribute to the pollution within the lower Passaic River. This material is aesthetically objectionable and thus impairs the recreational use by destroying the allure of the river. The alternative analysis has therefore concentrated on alternative controls which would improve the aesthetics of the river by limiting the amount of solid material being discharged from both combined and non-combined areas.

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The following list represents control alternatives which have been considered and evaluated under the alternative analysis of the facility plan:

a) Best Management Practices

b) Minor Structural Modifications

c) Inline Storage

d) Structural Improvements

e) Aesthetic Improvements

f) Regional Planning

g) Change in State Water Quality Classification

h) No action

Each will be discussed in detail within the following sections.

a. Best Management Practices

A Best Management Practice (BMP) program is a series of individual controls that focus on the sources of pollutants and their means of conveyance within the system. It provides a means of decreasing the total annual load of contaminants discharged to the receiving water without the enormous costs of capital-intensive construction programs. Furthermore, a BMP Program can be initiated within a relatively short time period, thereby providing some pollution abatement while other long term solutions are evaluated and implemented.

Generally, BMP control methods are divided into source management and collection system management. Source management involves the application of control measures specifically designed to reduce the pollutional load by reducing the surface contaminants/runoff prior to its entering the conveyance system. Control measures within source management include restrictions on chemical usage, surface flow attenuation techniques, land

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and road maintenance, and improved sanitary practices including trash removal and street cleaning. Collection system management deals with improved maintenance and control of the sewer system. Control measures included within collection system management include infiltration/inflow control, improved system regulation, and scheduled maintenance such as catchbasin and sewer cleaning. Together these control measures are capable of reducing that portion of the pollutional load contributed by urban runoff. Most of these control methods are equally applicable within both combined and non-combined sewer areas.

Source Management

Pollutants washed from an area by stormwater originate from sources found within all urban environments. It is therefore important to plan and implement control measures that will be effective on a regional basis. Control chemicals such as pesticides, herbicides and fertilizers are found and utilized throughout the PVSC Service District. Accordingly, to be truly effective, source management must be implemented within all areas of the service district, regardless of the nature of the stormwater collection system.

Litter is perhaps one of the largest and hardest to control pollutants within the urban environment. It is the primary constituent of floating solids within stormwater runoff and must therefore be effectively removed by street sweeping or prevented from occurring.

Methods utilized within litter control are greatly dependent upon public acceptance and cooperation. Even street sweeping effectiveness is conditioned on the willingness of the public to accept the inconvenience of parking restrictions so necessary for an effective program. Public awareness and anti-littering programs need strong citizen support to

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succeed. Business groups, school system organizations, service organizations, church and labor unions must all be made part of the overall organization.

Even if a strong anti-littering campaign is successful, established street sweeping operations will still be a requirement of source management. The results of various studies on street sweeping have shown that on the average, two or three passes per week would be capable of removing 25 percent of the initial street surface loading. More important from the aesthetic viewpoint, is the fact that a reliable street sweeping program would be instrumental in limiting the quantity of litter present in both the urban and aquatic environments.

Street sweeping effectiveness is a function of equipment utilized, pavement conditions, return interval and public acceptance. Conventional sweepers are most effective at removing large contamination materials while vacuum and air blasting vehicles are capable of removing the smaller pollutants. While the vacuum equipment is more effective in removing pollutants, it rapidly loses its effectiveness when pavements are wet and has experienced difficulties with clogged air hoses and filters when exposed to clay sized particles. Recommendations as to the type of sweeper best suited for each muncipality would need to be based upon cost factors and existing street/litter conditions.

Pavement conditions have a direct impact on the amount of pollutants found on the street surface. Rougher road conditions would tend to shake more particulate matter off vehicles in addition to producing particulates due to surface deterioration. Overall, conventional sweepers would not be as effective in areas of poor street maintenance due to the smaller size and distribution of particles upon the street surface.

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An efficient street sweeping operation is only possible when complete curb access is available within the service area. Opposite side of the street parking or parking restrictions during specific hours must be enforced to insure proper removal rates from all street sweeping operations. Overall effectiveness of pollutant removal is directly related to the curb area available for sweeping with removal rates decreasing significantly as curb access is restricted.

Cost factors for street sweeping ranged from $6.40 to $24.48 per curb mile (ENR = 4,000) and were highly dependent upon the region of the country reporting. Data review has shown that street sweeping is not effective in removing the smallest of particles and therefore is not capable of meeting complete source control. A higher percentage of pollutant removal rates would be obtainable by implementing street sweeping within non-CSO areas, since the total loading there is derived from street related pollution. However, other benefits including improved air quality, aesthetic conditions, public health would warrant implementation or continued use within all areas.

Surveys conducted within the combined sewer areas of the PVSC District have shown that budgetary restrictions have had a drastic effect upon street sweeping operations within most municipalities. The City of Newark maintains a street sweeping operation only within the central business district. Streets within the central business district area are swept on a daily basis, while other areas of the city are swept infrequently. Similar conditions exist in the City of Paterson where only the central business area is swept daily with other areas infrequent or based upon citizen complaints. Only the Towns of Harrison and Kearny have a regular street sweeping operation throughout the municipality and maintain parking restrictions to facilitate the removal of curb material.

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A preliminary survey upon street sweeping operations has been completed within most municipalities within the PVSC District (Table 4.1). Overall, most municipalities have established street sweeping operations within the commercial areas of the municipality, and to a lesser extent within residential areas. However, the Survey indicates that most do not follow schedules and procedures which have been shown to optimize removal of pollutants. Additional work is necessary within this area; however, at this time, it appears that optimization of street sweeping operation within all municipalities could have a substantial impact upon the water quality and floatable solids from both combined and non-combined areas.

Collection System Management

Collection system management consists of a series of programs designed to remove or eliminate the pollutant from the collection system prior to discharge into the receiving waters. Its major objective is to maintain the system so as to provide peak carrying capacity while providing for the control removal of extraneous solids and debris. It depends upon regular and systematic maintenance of catchbasins and collector sewers in addition to improved system regulations and optimized control. Non-structural alternatives such as cleaning of catchbasins and sewer collectors will be discussed presently while structural alternatives will be discussed within future sections.

All combined collection sewer systems within the PVSC Service District maintain catchbasins for the admission of surface water to the sewer. A catchbasin is a device usually built at the curb line of the street which includes at its base a sediment sump designed to retain grit and other solids below the point of overflow. Catchbasins are different from storm inlets in that storm inlets do not have sumps and as a result are not designed to retain sediment.

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TABLE 4.1

SUMMARY OF STREET SWEEPING OPERATIONS
WITHIN THE PVSC SERVICE DISTRICT
(NON-COMBINED AREAS)

MUNICIPALITY	ESTABLISHED PROGRAM	FREQUENCY OF SWEEPING		PARKING RESTRICTIONS
		RESIDENTIAL	COMMERCIAL	
BELLEVILLE	Yes	Once/wk	Once/wk	Alternate Side Parking Restrictions
BLOOMFIELD	Yes	Once/wk	5 Times/wk	65% of Town-Restricted Parking
CLIFTON	No	Unknown	Unknown	Restrictions on Narrow and Commercial Streets
EAST ORANGE	Yes	Unknown	5 Times/wk	4 Hr. Prohibited Parking Daily
E. RUTHERFORD	No	Once/2 wks	2 Times/wk	2 Hr. Restricted Parking Daily
ELMWOOD PARK	No	Once/1.5 wks	Once/wk	4 Hr. Restricted Parking in Some Areas
FAIR LAWN	Yes	Once/4 wks	Once/wk	None
GARFIELD	Yes	Once/wk	Once/wk	4 Hr. Restricted Parking
GLEN RIDGE	No	-	-	None
GLEN ROCK	Yes	Once/wk	Once/wk	None
HALEDON	Yes	Once/wk	Once/wk	Some Areas
HAWTHORNE	Yes	Once/2 wks	Once/2 wks	None
LODI	Yes	Unknown	Unknown	Alternate Side Parking Restrictions
LYNDHURST	Yes	Once/2 wks	2 Times/wk	2 Hr. Restricted Parking Daily
NUTLEY	Yes	Once/4 wks	Once/wk	Some Areas Posted Ahead of Cleaning
ORANGE	Yes	2-3 Times/wk	2-3 Times/wk	Alternate Side Parking Restrictions
PASSAIC	Yes	Once/wk	5 Times/wk	Alternate Side Parking Restrictions

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From a pollution abatement standpoint, the benefits of catchbasin cleaning appear somewhat limited based upon a recent analysis. The net removal of BOD_5 from a well designed and maintained system of catchbasins is expected to be in the range of 5 to 10 percent of the applied load. The main reason for this relatively low removal rate is the displacement of the high BOD_5 liquid contained within the sump by rainfall of very low intensity. It has been estimated that the load displaced within a catchbasin by rain of as little as 0.02 inches per hour lasting 4 hours is equivalent to the waste discharged by one person a day. This high pollutional load purged from catchbasins during a storm is one reason for first flush loadings usually associated with combined sewer areas.

In contrast to the poor BOD_5 removal by catchbasins is the fact that properly maintained catchbasins remove approximately 40 to 75 percent of the total solids entering them on an annual basis. Removal efficiencies do not vary substantially until 50% of the sump is filled. Under further loading, the removal rates drop dramatically with negative efficiency experienced before 60% of the sump is filled. Total removal rates of pollutants have varied considerably and have been hard to establish with any confidence from past studies. However, if properly maintained, catchbasins will retain solids within the sump of the catchbasin, thereby limiting the aesthetic problems associated with CSO and stormwater discharge.

Studies have shown that in order to maintain the effectiveness of catch basins for pollutant removal, a cleaning frequency of at least twice per year is required. Cost factors for cleaning range from $11.80 to $15.20 per catch basin (ENR = 4,000), if performed semi-annually by municipal employees, and is somewhat dependent upon the methodology

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utilized within the cleaning effort. Cleaning methods for catchbasin maintenance fall into four main categories: hand cleaning, bucket cleaning, eductor cleaning, and vacuum cleaning.

Overall, the vacuum cleaning method appears to be the most economical method for cleaning catchbasins. The vacuum cleaning method utilizes an air blower to create the vacuum with air/solid/liquid separation accomplished in the unit by gravity separation baffles. Usually large pieces of debris can be removed easily from catchbasins with a vacuum unit more so than with any other method. As with the eductor, the vacuum method is economical and efficient while not creating a nuisance with unsanitary and unsightly removal. It should be considered one of the major methods of catchbasin cleaning and should be incorporated in any future program of catchbasin maintenance.

In conjunction with maintenance of catchbasins, maintenance of the collection system is an important factor in collection system management. The basic parts of a maintenance program include: (1) regular inspection of the system; (2) cleaning of sewer deposits and flushing of pipes; and (3) control of infiltration and inflow sources. All of these items are important in the struggle to maintain maximum capacity, minimize overflows, and to provide reliable removal of stormwater runoff.

Cleaning methods and costs vary considerably depending upon the particular type of obstructions encountered as well as the physical configuration of the system. Costs can vary from less than $1.00/linear foot for smaller diameter pipe to over $20/linear foot for large diameter pipe with heavy deposits. Total costs would depend on numerous factors which are site specific and cannot be estimated at the present time.

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The deposition of solids in both combined and storm sewer systems during dry weather is a major contributor to high solids loadings during wet weather runoff periods. Elimination or reduction of these solids could improve the aesthetic quality of the lower Passaic River.

Internal automatic flushing devices have been developed for sewer systems; however, they are effective only within relatively short runs (less than 1000 feet) even in small to medium diameter sewers. Normal maintenance procedures such as portable flushers used in conjunction with vacuum units have been much more effective since solid material is removed rather than just transported downstream. An established cleaning program within known problem areas and to a lesser extent within all municipal sewers, has been shown to have many positive effects including fewer complaints and emergency calls, improved sewer capacity, and reduction of street flooding.

Although combined sewers' deposition during dry weather flow is a known reason for organic and solids loading during storm events, no known studies have ever been completed upon deposition and the possible impact of such within separate storm sewers. Storm sewers do not have the constant loading and flows of combined sewers, they do have potential for substantial organic loading especially during certain months of the year. Many storm inlets receive pollutants through deliberate dumping of waste oil, leaves, grass clippings, paper, bottles and cans. Although this problem may not be as severe as within combined sewer areas, there is a potential for the reduction in total pollutants/solids discharged from separate storm sewer systems. Additional work is needed to substantiate the facts, however consideration should be given to storm sewer or special street maintenance programs, i.e. leaf pickup, especially during periods of potentially high organic loading (summer and fall months).

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Street sweeping, catchbasin cleaning, and sewer flushing if implemented under the proper conditions should provide a substantial decrease in the total loadings discharged within both combined and non-combined areas. While significant reductions in C-BOD may not be attainable by implementa- tion of best management practices, a considerable reduction of suspended and floatable material is possible through proper maintenance.

A major problem at this stage of the facility planning is that a suspended solids transport model has not been developed for the lower Passaic River. Reason would suggest that removal of solids from within the collection system should decrease the floatable solids found within the river. Reason however cannot replace a comprehensive modeling effort designed to first determine the sources of floatable material within the lower Passaic, second to determine what percentage of that material is originating within stormwater runoff, and last of all to predict what impact alternative control measures would have in improving the aesthetics of the lower Passaic River.

The original design for the modeling effort utilized within this facility plan was based upon federal and state requirements for water quality in addition to previous studies showing CSO discharge was a major reason for contravened water quality standards. It could not be foreseen that CSO discharge would be a relatively minor source for C-BOD, N-BOD and subsequent low dissolved oxygen levels. In the same way it could not be anticipated that control alternatives within the lower Passaic River would be primarily for aesthetic reasons at the present time. Accordingly, unless a suspended solids transport model is developed within future phases of the facility plan, a benefits vs. cost analysis upon aesthetic improvements cannot be completed.

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b. Minor Regulator Reconstruction

All combined sewer overflows under the jurisdiction of the Passaic Valley Sewerage Commissioners contain a regulatory chamber wherein the amount of flow discharged to the trunk sewer is restricted during rainfall periods. Each regulator chamber was originally designed to limit and finally eliminate flow to the PVSC Trunk as flow levels within the tributary municipal sewers increased. This was done to prevent surcharging of the trunk and interceptor systems during periods of intense rainfall. Most regulator chambers within the district, except for those recently constructed in Newark, do not function properly due to age and the corrosive nature of flows within this heavily industrialized area. As a result, surcharging of the PVSC trunk sewer is a persistent problem within specific areas of the service district.

The general configuration of overflow structures within the PVSC district is illustrated within Figure 4.1. Normal dry weather flow enters the sandcatcher wherein the flow is diverted by the stop log (overflow weir) through the regulator valve and subsequently into the PVSC Trunk Sewer System. During storm periods excessive combined flows could overflow the stop logs and discharge into the Passaic River.

Overflows at the overflow chambers are controlled not only by the regulator orifice and stop log elevations, but in many cases by the tide gates and river elevation downstream of the overflow chamber. Tide gates are structures utilized to prevent the normal daily high tide or stream flow from entering the collection system. During periods of high tide or stream flow, the system hydraulics can prevent or restrict flow through the tide gates and into the receiving water. Thus regulator performance is totally dependent upon overall system hydraulics.

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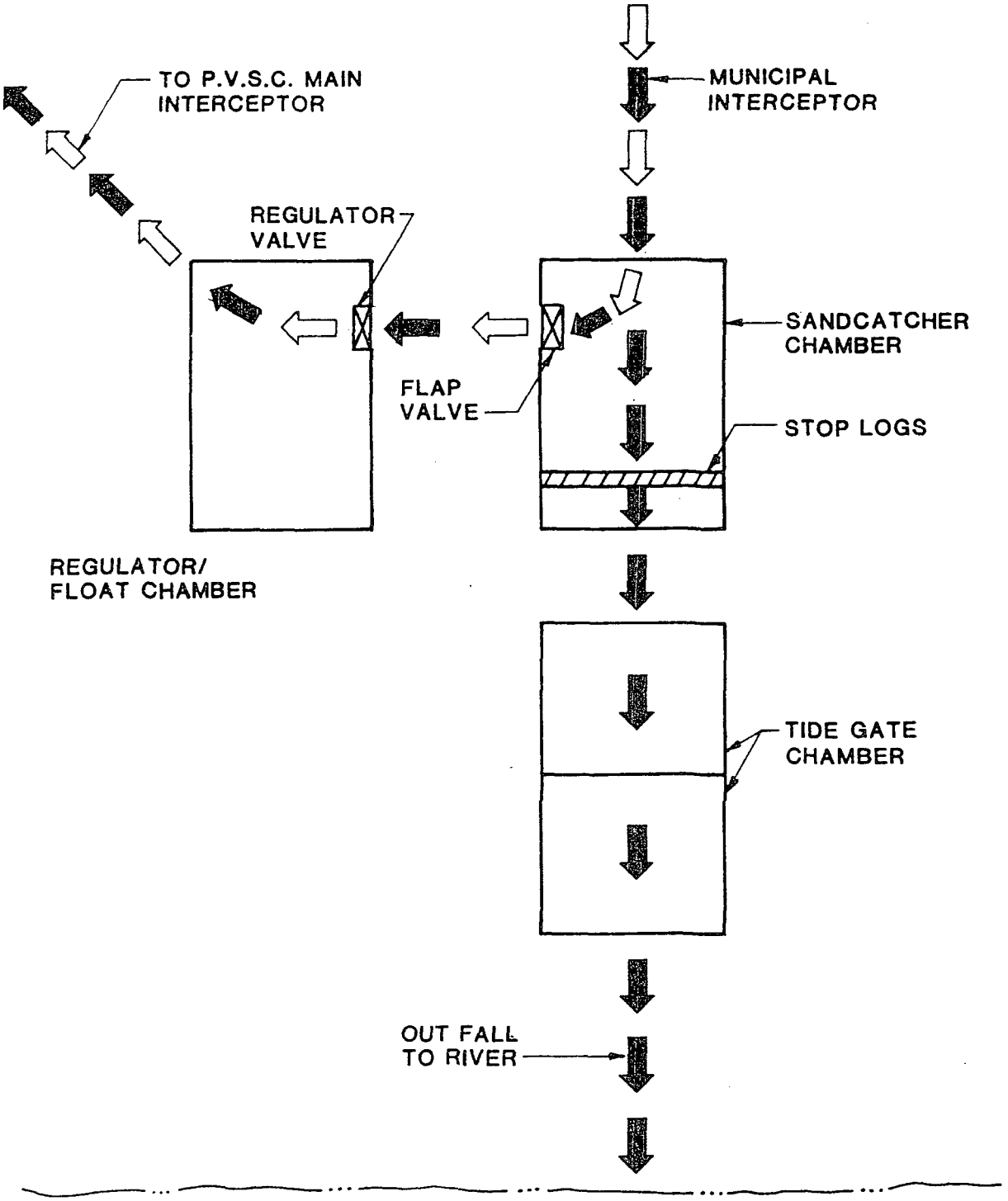

LEGEND

DRY WEATHER FLOW

STORM FLOW/OVERFLOW

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

TYPICAL OVERFLOW CHAMBER SCHEMATIC

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946510141

FIGURE 4-1

Perhaps the simplest measure to prevent or minimize overflows from the combined sewer systems would be to raise the existing stop log/weirs structure to minimize or decrease the amount of discharge to the Passaic River (see Figure 4.2). In addition to preventing or limiting the overflow of combined sewage, the raising of the existing stop logs would cause a backwater effect on the incoming combined sewer. This backwater effect would temporarily store a portion of the overflow volume within the municipal sewer thereby attenuating the flow to both the PVSC trunk sewer and the Passaic River. Depending upon hydraulic gradients and system characteristics it is theoretically feasible to produce a substantial amount of inline storage and therefore produce a substantial decrease in the total flow discharged to the river.

Raising of the overflow weir would prevent or limit the occurrence of discharge through the overflow structure. Since changing the weir elevation has no effect on the total volume of runoff from a specific rainfall, changes in the flow pattern of the overflow chamber must occur. Additional flow must enter the regulator and subsequently the trunk system and/or storage of the flow volume previously discharged to the river must occur within the system. Since present conditions within most of the district would limit additional discharge to the PVSC trunk the initial feasibility screening was conducted upon the potential for inline storage. This potential for inline storage is essential for balanced flow conditions and proper utilization of the PVSC trunk system.

A screening process was established whereby only those sites which passed initial feasibility tests were included in detailed flow analyses. Potential inline storage is directly influenced by pipe size and system characteristics (i.e. depth, slope, etc.). An initial evaluation was

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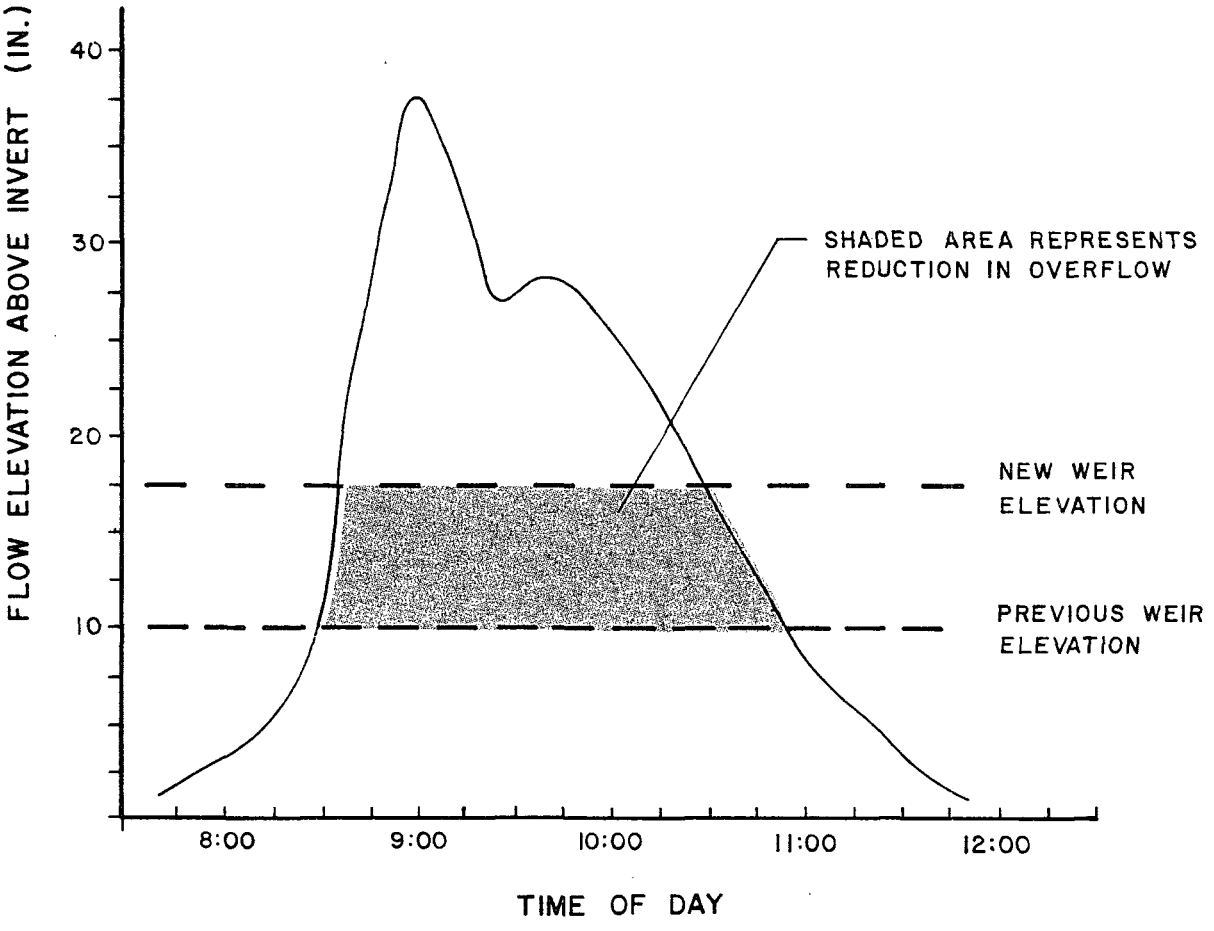

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

EXAMPLE OF OVERFLOW REDUCTION BY RAISING OF WEIR ELEVATION

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FIGURE 4·2

therefore conducted on all 65 PVSC overflows to determine which sites could be eliminated due to storage limitations. In addition, the screening process involved a general knowledge of the system tributary to each CSO. Areas wherein system problems such as surcharging or backups were known to occur were eliminated from further consideration.

The results of the preliminary screening and analysis showed that only 18 of the original 65 PVSC overflow sites showed a potential for storage. The eighteen CSOs requiring further flow analysis for inline storage were:

MUNICIPALITY	OVERFLOW	DRAINAGE AREA (Acres)	PRELIMINARY RANKING AS PER TABLE 3.2
City of Paterson	Market St.	1500	Major *
	10th Ave. & 33rd St.	700	Major *
	Montgomery St.	670	Major *
	Northwest St.	280	Major *
	Straight St.	120	Moderate
	E. 11th St.	105	Moderate
	Warren St.	80	Moderate
	3rd Ave.	75	Moderate
City of Newark	Clay St.	1600	Major *
	City Dock	380	Major *
	Verona Ave.	370	Major *
	Saybrook Place	310	Major *
	Herbert Place	300	Major *
	Fourth Ave.	225	Moderate
	Polk St.	200	Moderate
Town of Harrison	Harrison Ave.	65	Moderate
Town of Kearny	Ivy St.	610	Major *
	Johnston Ave.	210	Major *

* Systems monitored during calibration/verification of DNM & SWMM

Understandably all of the overflows included for detailed analysis for inline storage fall into the major and moderate classifications as established within section 3. Smaller overflow systems would not have sufficient storage volume for inflow storage and if utilized would not substantially change the overflow volume discharged to the river for a specific storm.

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The second phase of the screening involved a detailed hydraulic analysis of the above CSOs including the municipal interceptors tributary to each. This analysis involved the use of the HEC-2 Water Surface Profiles computer program written at the Hydrologic Engineering Center (a division of the U. S. Army Corps of Engineers). The HEC-2 program can compute water surface profiles given input data such as cross-section, flow rate, roughness coefficient, etc., under open channel or pressure flow conditions. It had the advantage of accurately accounting for and calculating backwater curves which were an essential determination for this analysis.

The computer analysis was conducted under the arbitrary requirement that under no condition shall the sewer surcharge to a level wherein the difference between the depth from the water surface to the ground surface was less than five (5) feet. This requirement was utilized as a preliminary parameter to compensate for service connections and to prevent surcharge or backup into residential or commercial buildings. Failure to meet this requirement resulted in the CSO being eliminated from further inline storage analysis.

Flow rates for the analysis were developed using a combination of monitored overflows and known system hydraulics obtained during the initial phases of the facility plan. Prior to the HEC-2 computer analysis, a secondary screening was utilized wherein maximum overflow events recorded (from both Phase I Analysis and current measurements) were compared to design capacities within the tributary interceptor sewer. Any sites wherein the municipal interceptor design capacities were exceeded by a relatively minor storm event (return period < 0.5 years for intensity) were eliminated from further analysis. These sites could not provide any reasonable storage volume and as such did not warrant further consideration.

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Those overflow sites eliminated through the secondary screening process were:

Municipality	Overflow	Reason
City of Paterson	Montgomery	Water surface to road <5'
	Straight St.	Design capacity exceeded.
	E. 11th St.	Design capacity exceeded.
	Warren St.	Design capacity exceeded.
	3rd Ave.	Design capacity exceeded.
City of Newark	Verona Ave.	Design capacity exceeded.
Town of Kearny	Johnston Ave.	Design capacity exceeded.

In addition to the concept of raising the existing weirs, consideration was given to the installation of inline weir structures. These structures would be installed within a pipe section or at a manhole and would consist of an inflatable rubber membrane which would remain deflated during normal flow (non-storm) conditions. During storm events, the inflatable dam (i.e. Fabridam, a trademark of the N. H. Imberton Co.) could be pressurized to create an impoundment and store water within the pipeline. The Fabridam may also be equipped with instrumentation to provide for automatic operation to adjust for surcharges and to prevent overloading of the system. The instrumentation would be programmed such that with a given head differential the dam would automatically deflate, thereby relieving the upstream system.

The HEC-2 analysis was performed for those CSO sites which were not eliminated during the initial and secondary screening. The goal of this analysis was to determine the maximum allowable surcharge level at the overflow weir such that the previously established five foot limit (from ground surface to water surface) would not be violated upstream. Those cases wherein the interceptor sewer would be slightly over capacity would not necessarily create a problem provided there was adequate cover over the sewer. The surcharging of the sewer would build up a greater

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hydraulic head which would provide for a greater flow through the regulator orifice then would occur under existing conditions.

The initial HEC-2 analysis was conducted utilizing the maximum overflow event recorded for each overflow site under investigation. Since only overflow flow quantities were recorded during these events, system hydraulics were utilized to calculate the total flow entering the chamber. This flow in conjunction with several assumed water surface levels was utilized to determine a specific water surface elevation which would not present system problems upstream.

The initial HEC-2 analysis showed that several areas had a potential for raising of the overflow weir and subsequent inline storage. Feasibility was analyzed either at the overflow chamber or at some point upstream with the following results:

Overflow Site	Weir Location	Est. Increase In Storage Volume (MG)
City of Paterson		
Northwest St.	Overflow chamber	0.01
10th Ave. & 33rd St.	Overflow chamber	0.01
Market St.	Overflow chamber	0.10
City of Newark		
Herbert Place	Overflow chamber	0.04
Fourth Ave.	Overflow chamber	
Clay Street	Inline weir	0.33
Saybrook Place	Inline weir	0.64
Polk St.	Overflow chamber	0.18
Town of Kearny		
Ivy Street	Overflow chamber	negligible

In most areas the amount of inline storage available is insignificant compared to recorded flows during storm events. The only areas of substantial storage volume are within municipal interceptors, not at the PVSC Overflow regulators. Raising of the weir elevation at the regulator would only prevent or reduce an overflow by an amount approximately equal to the

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additional discharge to the PVSC trunk. Essentially, the raising of the weir would retain a small amount of flow (perhaps the first flush) which would otherwise overflow to the river.

Using known system hydraulics, a maximum new weir elevation had been determined within those overflows showing some potential of inline storage. An analysis was conducted to determine the quantity of flow which could be retained before overflow occurs at present and under proposed new weir elevations. Inline weirs not at the overflow chamber were not included within the analysis since they would not change regulator hydraulics. In addition, those areas wherein tidal elevations exert a strong affect upon system hydraulics were also not included. The results of this investigation are as follows:

Location	Change in Flow Before Overflow Occurs (MGD)	Percent of Total Tributary to PVSC Trunk		Percent Increase In Trunk Flow	Storage Volume (MG)
		Existing	Proposed		
Paterson:					
Northwest St.	3.0	17.6	20.3	2.7	0.01
10th Ave. & 33rd St.	8.8	14.7	25.7	11.0	0.01
Market St.	12.2	28.3	34.7	6.4	0.10
Newark:					
Herbert Pl.	7.1	15.8	21.0	5.2	0.04

Following initial formulation of system modifications, a meeting was held with the respective municipal engineers to discuss the potential changes to several overflow structures. The municipal engineers have a good operational understanding of the tributary sewers and as such would be aware of any potential problems associated with raising of the weirs. As a result of these discussions, two overflow sites were eliminated from further evaluation based upon known surcharging and/or structural problems within the municipal interceptors. These were:

City of Paterson - 10th Ave. & 33rd Street Overflow

City of Newark - Polk Street Overflow

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Analysis of the Presidential Boulevard Branch Trunk Sewer in Paterson has shown that modification of the Northwest Street Overflow weir would not be effective in reducing overflows. The present flow capacity of this branch sewer is less than the regulated flow under present conditions. As such, the trunk capacity and not the orifice capacity is the limiting factor within this overflow structure. Any modifications of the overflow chamber at present would not appreciably change overflow frequencies or volumes.

The results of the preliminary analysis of inline storage/weir raising potential is summarized within Table 4.2. As per this table, the following locations should be considered for detailed analysis under Phase II of the Facility Plan:

City of Paterson - Market Street Overflow

City of Newark - Clay Street (Inline)
Saybrook Place (Inline)
Herbert Place
Fourth Avenue

The detailed analysis recommended under Phase II would require: (1) an intensive modeling analysis utilizing SWMM to determine acceptable limits and potential water quality improvements; (2) an investigation into the structural integrity of the municipal interceptors including rehabilitation/improvements which may be necessary prior to implementation; and (3) an evaluation as to what impact these improvements in conjunction with other control alternatives would have on water quality within the receiving stream as well as the total operation of the PVSC Regulator/Trunk System.

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TABLE 4.2
RESULTS OF PRELIMINARY INVESTIGATIONS INTO
WEIR RAISING/INLINE STORAGE

MUNICIPALITY	OVERFLOW	RESULTS OF ANALYSIS
Paterson	Market St.	Recommended Detailed Analysis
	10th Ave. & 33rd St.	Eliminated As Per Municipal Engineer
	Montgomery St.	Interceptor Too Close To Ground Surface
	Northwest St.	Insufficient Trunk Capacity
	Straight St.	Insufficient Interceptor Capacity
	E. 11th St.	Insufficient Interceptor Capacity
	Warren St.	Insufficient Interceptor Capacity
	3rd Avenue	Insufficient Interceptor Capacity
Newark	Clay Street	Recommend Detailed Analysis For Inline Storage
	City Dock	Interceptor Too Close To Ground Surface
	Verona Ave.	Insufficient Interceptor Capacity
	Saybrook Pl.	Recommend Detailed Analysis For Inline Storage
	Herbert Pl.	Recommend Detailed Analysis
	Fourth Ave.	Recommend Detailed Analysis
	Polk St.	Eliminated As Per Municipal Engineer
Harrison	Harrison Ave.	Interceptor Too Close To Ground Surface
Kearny	Ivy St.	Interceptor Too Close To Ground Surface
	Johnson St.	Insufficient Interceptor Capacity

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The preliminary investigations discussed so far have shown that minor regulator modifications within the PVSC Service District do not have a significant potential in the reduction and/or elimination of Combined Sewer Overflows. This analysis was conducted on the expectation that adjusted weir elevations would be modified by the addition of a permanent structure (i.e. additional weir boards). System restrictions which develop during significant rainfall events have resulted in the elimination of a number of overflows from further consideration. These restrictions however would not be significant during the more frequent, low intensity storms which commonly occur within the PVSC Service District.

A secondary approach to the problem of frequent Combined Sewer Overflows would be the implementation of a automatic dynamic or integrated regulator operation wherein weir and regulator orifice elevations would not be fixed. By instituting an adjustable weir/orifice system within the regulator, discharge load reductions are possible for more frequent low intensity storms.

An improvement over the present system of perpendicular weirs and static regulators is the dynamic regulator system illustrated within Figure 4.3. Sensors monitor the flow levels within the overflow chambers, trunk sewer and outfall. These sensors provide input data for a computerized system analysis. Gate and weir locations are automatically controlled to provide maximum capture of stormwater while minimizing surcharging problems within both the interceptor and trunk systems. A diagram illustrating the operations of a dynamic regulator is shown on Figure 4.4.

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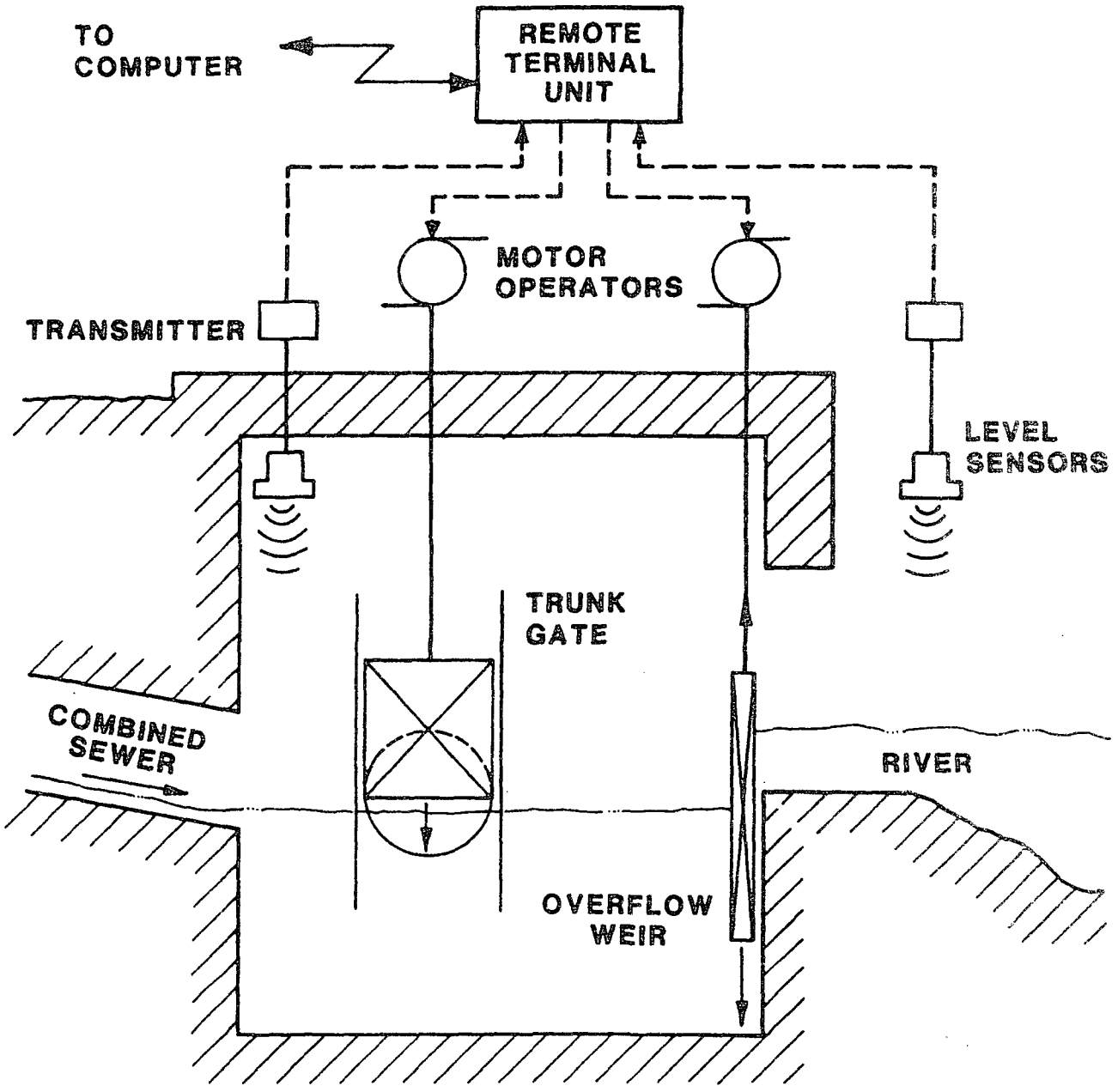

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

AUTOMATIC DYNAMIC REGULATOR

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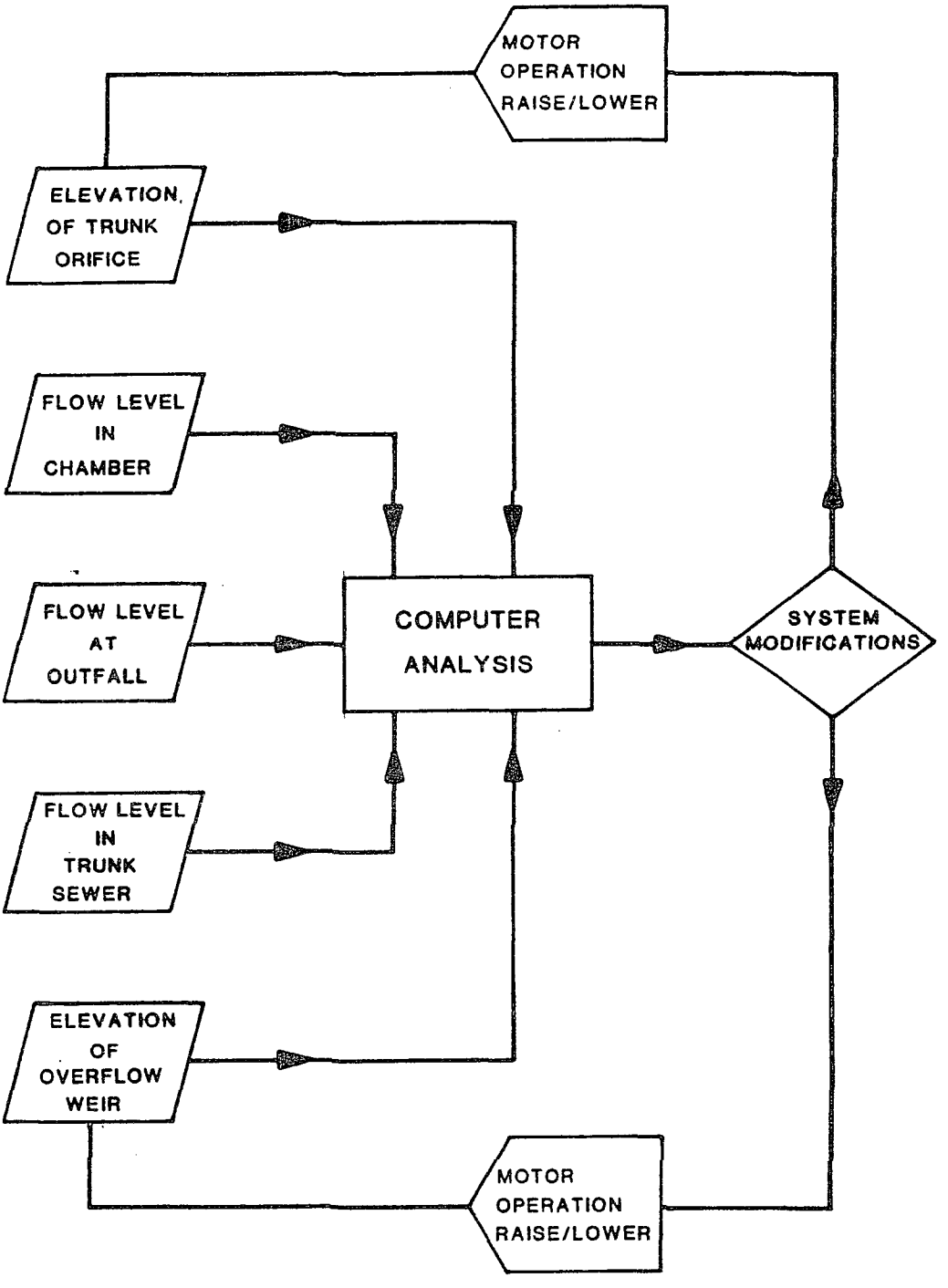
FIGURE 4·3



PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

AUTOMATIC DYNAMIC REGULATOR OPERATIONAL SCHEMATIC

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946510153

FIGURE 4-4

A major limitation of the dynamic regulator is that orifice/weir gates are not responsive enough for sudden changes in stormwater input. Since the system only monitors flow levels within the immediate area, it can not react to changes within other overflows or sudden increases in rainfall intensity. A system which attempts to overcome this limitation is the integrated regulator system wherein computer modeling is utilized to unify operation of all overflows.

Studies have shown that where little or no inline or other system storage is available (1) a means of predicting expected flowrates to the interceptor must be available, and (2) an operational bias must be implemented which either minimizes overflows from specific interceptors or favors the timing of the overflow event. Without these capabilities, an integrated regulator system has no advantage over local automatic-dynamic regulators.

Modeling conducted within this phase of the Facility Plan has shown the predictive capabilities of SWMM (Storm Water Management Model), calibrated and verified within the PVSC District. Information and experience gained through this phase should allow for flowrate prediction within an integrated regulator operation. Additional input in the form of automatic rainfall measurements and/or predictions would be necessary to complete the system. Recent developments in storm tracking, rainfall measurement and predictive capabilities have improved the feasibility of an integrated regulator system. Although reduction of "first flush" is probably not possible throughout the system without offline storage, significant improvement may develop by the reductions possible at designated (high pollutional loading) outfalls.

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Significant differences have been observed within the pollutional loadings discharged by Combined Sewer Overflows within the PVSC District. Water quality and quantity measurements made during the 1981 storm monitoring program have shown that several overflows accounted for most of the ultimate C-BOD load discharged from CSOs during each storm period. Table 4.3 illustrates the ultimate C-BOD loadings from each of the major overflows monitored. In some cases, equipment failures did not allow compilation of flow quantity/quality data. These account for the absence of data within two of the storm periods.

The compiled information indicates that C-BOD loadings are not necessarily related to overflow volume. Industrial areas have a much higher C-BOD loading factor due to industrial discharge. In fact, C-BOD values measured during the December 1st storm at Ivy Street overflow were in excess of 1000 mg/l at peak flow. Although this type of loading is intermittent, a substantial impact is possible when occurrence coincides with stormwater discharges as in the December 1st storm.

The C-BOD loadings shown in Table 4.3 are not meant to indicate a ranking of the major CSOs. Although similar loadings are possible for other storm periods, the total load discharged is dependent upon a number of factors. The sanitary and industrial discharges at the time of overflow do have an impact, however in industrial areas these can vary substantially. The Ivy Street overflow showed the highest C-BOD loading measured during the three monitored storm events. This was primarily due to an extremely high C-BOD discharge within the sub-area at the time of peak rainfall intensity. This event was only evident during the December 1st storm and may or may not be repeated during other storm events not monitored.

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TABLE 4.3
ULTIMATE C-BOD LOADING DISCHARGED
FROM MAJOR COMBINED SEWER OVERFLOWS

MUNICIPALITY	OVERFLOW	APRIL 14, 1981 C-BOD (lbs)	APRIL 14, 1981 FLOW VOLUME (MG)	SEPT. 15, 1981 C-BOD (lbs)	SEPT. 15, 1981 FLOW VOLUME (MG)	DEC. 1, 1981 C-BOD (lbs)	DEC. 1, 1981 FLOW VOLUME (MG)
Newark	City Dock	-	-	107	0.16	8,500	16.47
	Saybrook Pl.	393	0.96	-	-	577	0.47
	Clay St.	10,000	9.58	8,850	11.50	47,300	62.83
	Herbert Pl.	-	-	-	-	2,060	4.01
	Verona Ave.	64	0.10	-	-	12,100	3.53
	Union Outlet*	22,700	8.2	NO	BYPASS	14,700	8.27
Kearny	Johnston Ave.	104	0.15	-	-	2,720	6.85
	Ivy St.	4,770	9.0	460	3.30	65,700	10.38
Paterson	Market St.	2,880	4.0	4,140	2.93	15,400	11.91
	10th Ave. & 33rd St.	196	0.36	506	1.36	3,320	7.09
	Montgomery Pl.	290	0.41	175	0.53	600	1.04
	Curtis Pl.	157	0.03	540	0.12	1,550	0.45
	Northwest Ave.	600	0.60	23	0.06	1,650	2.66
	Hudson St.	-	-	-	-	495	0.47

* Sanitary Sewer Bypass

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Automatic control of orifice and overflow weir structures show a substantial potential for the reduction of pollutional loads discharged during frequent low intensity storms. Higher load reductions per unit overflow volume are obtainable by formulating and applying a bias on the operational mode of the regulators. This operational bias would be based upon anticipated loadings in addition to the hydraulic characteristics of each overflow chamber.

A preliminary ranking of the major Combined Sewer Overflows has been completed and is shown in Table 4.4 This ranking was based upon two factors: (1) the ultimate C-BOD loading per unit volume discharged (pounds/million gallons) as measured during the 1981 monitoring of CSOs; and (2) the average C-BOD values measured during the initial Phase I Analysis completed in 1976. This ranking outlines those areas wherein the highest C-BOD unit loadings (lbs/MG) are expected. It cannot however be viewed as an absolute ranking for all storm events. As previously stated, the actual loading within many of the CSOs is very dependent upon random industrial discharges. It is therefore not surprising that those overflows within the upper section of the ranking are generally those within large industrial areas.

The Union Outlet Bypass was not included within the ranking on Table 4.4 since it is not a combined sewer overflow. This bypass was frequently activated during the monitoring period as a means of regulating flow into the lower PVSC trunk sewer during storm events. Although technically not an overflow, this bypass has been shown to be a major source of C-BOD during the events monitored (see Table 4.3). A more efficient operation of regulators and treatment plant pumping capacity should provide the flexibility necessary to eliminate the need to bypass this major source of C-BOD.

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TABLE 4.4
RANKING OF MAJOR COMBINED SEWER OVERFLOWS
BASED UPON C-BOD LOADING PER UNIT VOLUME
DISCHARGED TO RECEIVING WATERS

RANKING NUMBER	OVERFLOW	MUNICIPALITY	RANGE C-BOD LOAD DISCHARGED 1981 MONITORING PERIOD (lbs/MG)
1	Curtis Place	Paterson	3450-5620
2	Market Street	Paterson	700-1410
3	Verona Avenue	Newark	590-3460
4	Clay Street	Newark	750-1050
5	Hudson Street	Paterson	900
6	Ivy Street	Kearny	190-6320
7	Montgomery St.	Paterson	330- 960
8	Northwest St.	Paterson	530-1000
9	10th Ave. & 33rd Street	Paterson	375- 720
10	City Dock	Newark	515
11	Herbert Place	Newark	500
12	Johnston Avenue	Kearny	400- 690
13	Saybrook Place	Newark	400-1150

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Cost factors involved within integrated regulator systems include: (1) modification or reconstruction of regulator chambers; (2) installation of the computer and peripheral control equipment including telemetry, control interfacing, and systematic flow survelliance instrumentation; (3) weather radar and rainfall monitoring systems; and (4) operation and maintenance costs including parts, materials, labor and utilities. Based upon similar installations around the country it is estimated that all cost factors within 1, 2, and 3 above would average $680,000 per site (ENR=4000) if only the fifteen largest overflows are included.

Implementation of a weather radar and rainfall monitoring system would provide greater operational flexibility at the treatment plant. Available pumping capacity could be better utilized if sufficient time is available for pumpdown of the PVSC Trunk System. An early warning system would provide the time needed for pumpdown. This would provide additional storage capacity for stormwater flows which normally require discharge into the receiving waters. A complete and automatic flow surveillance system within the trunk system would provide the systems operator the information needed to minimize system problems while making full utilization of trunk and treatment plant capacity. Better utilization of existing facilities could eliminate the necessity for bypassing both separate and combined sewer systems.

Actual cost factors would depend upon the size of the overflow and the amount of reconstruction necessary. Accordingly, a detailed analysis of each individual overflow would be required to determine which overflows would prove to be the most cost-effective. A substantial cost within the initial development of an integrated regulator system would be involved within the development and verification of the several computer models

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necessary for proper operation. Accordingly, once the initial programs are developed and tested, a significant reduction should be possible for extension of the integrated system to other CSOs.

Integrated regulator control cannot provide a complete solution in and of itself. The inline storage analysis of regulator chambers has shown that most key areas have negligible storage volume available. System restrictions within specific areas would require the implementation of additional control measures in conjunction with an integrated regulator system. An analysis of other control alternatives required within specific areas will be discussed in detail within subsequent sections of the Facility Plan.

c. Inline Storage

Inline storage involves the utilization of excess sewer capacity to attentuate flow within combined sewer areas. Initial design storms for most major storm sewers are usually within the 5 to 10 year return period. Theoretically, typical storm events would underutilize the existing storm system since stormwater flows should be much lower than the design capacity. This would allow for inline storage during storm events not exceeding the design storm.

Most combined sewer systems within the PVSC district were constructed during the period 1880-1920. Land development, changes within land use, and changes within sewer utilization over the past 80-100 years, have all impacted the flow characteristics within many areas. Several areas within the PVSC Service District have combined sewer systems which do not have sufficient capacity for even a 6 month or 12 month storm. This problem appears to be especially acute within the City of Paterson where four of the eight CSOs analyzed for regulator modifications were eliminated due to insufficient design capacity.

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The feasibility analysis for inline storage was identical to the analysis utilized within the minor regulator modification discussed within section 4b. A screening process was established wherein system characteristics (i.e. depth, slope, pipe size, etc.) were utilized to determine those locations requiring a detailed HEC-2 analysis. The HEC-2 analysis was conducted to determine the maximum allowable flow elevation (surcharge level) possible at an inline weir such that the water surface elevation would not exceed an arbitrary level 5' from the ground surface.

Inline storage would be possible by the installation of an inline weir structure or flow regulator within a pipe section or at a manhole. The weir structure would consist of an inflatable rubberized fabric dam which could be utilized with a bypass for dry weather flows. Under storm conditions the inflatable dam would be pressurized to create an impoundment and thus create inline storage. Other flow regulators which could be utilized are Hydrobrakes® or automatically controlled sluice gates. Instrumentation would be provided for automatic control to prevent overloading the system. The instrumentation would be programmed such that at a given head upstream the system would adjust itself, thereby preventing surcharge and backup problems under severe conditions.

Final feasibility and storage potential will need to be determined through a detailed system modeling (SWMM) so that the analysis could be completed using the full range of expected flow rates. The process utilized herein was only a preliminary investigation to determine the potential for inline storage and to determine those areas requiring detailed analysis.

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Figures 4.5 thru 4.11 illustrate the areas wherein inline storage of combined flows showed some potential based upon the preliminary screening (pipe size, slope, measured flows, etc.). Five of these areas were within the Clay Street Overflow drainage basin, one within the Saybrook Place Overflow drainage basin and one within the Ivy Street Overflow drainage basin. The initial screening process eliminated most areas because of limited storage capacity due to pipe size, slope, or design flow capacity. The fact that only seven areas survived the initial screening process emphasizes the limited capacity of most of the combined sewer systems within the PVSC District.

Volume estimates for inline storage were first made by determining the difference between anticipated flow depth and maximum water elevation as determined through the HEC-2 analysis (Figure 4.12). Flow rates utilized were based upon the maximum flow rate measured during system monitoring. As such, the volume determination through the HEC-2 analysis would be valid only at the specified flow. Since the water surface elevation cannot increase beyond that set and analyzed, any increase in flow would produce a corresponding reduction in storage volume. This type of analysis is valid as a means of determining the dynamic storage capacity anticipated and provides a means of selecting the weir elevation and corresponding storage capacity anticipated within each region.

A second analysis was conducted to determine the minimum storage capacity anticipated within each area. Figure 4.12 illustrates the concept of static water surface utilized within the analysis. A conservative determination of storage volume could be made by utilizing the volume of flow actually contained within the pipe section by the weir structure. The storage calculated through this determination is valid for

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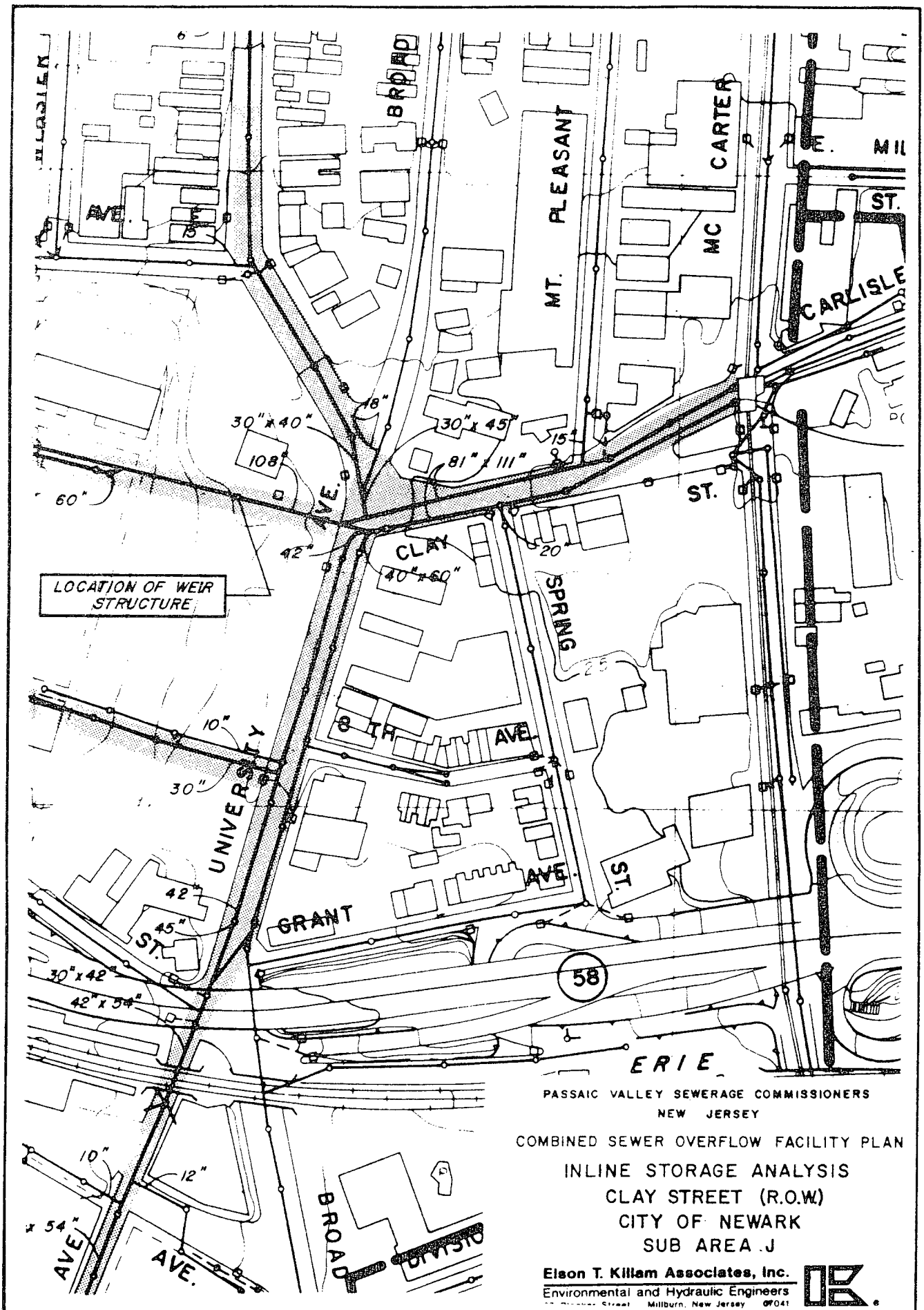


PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

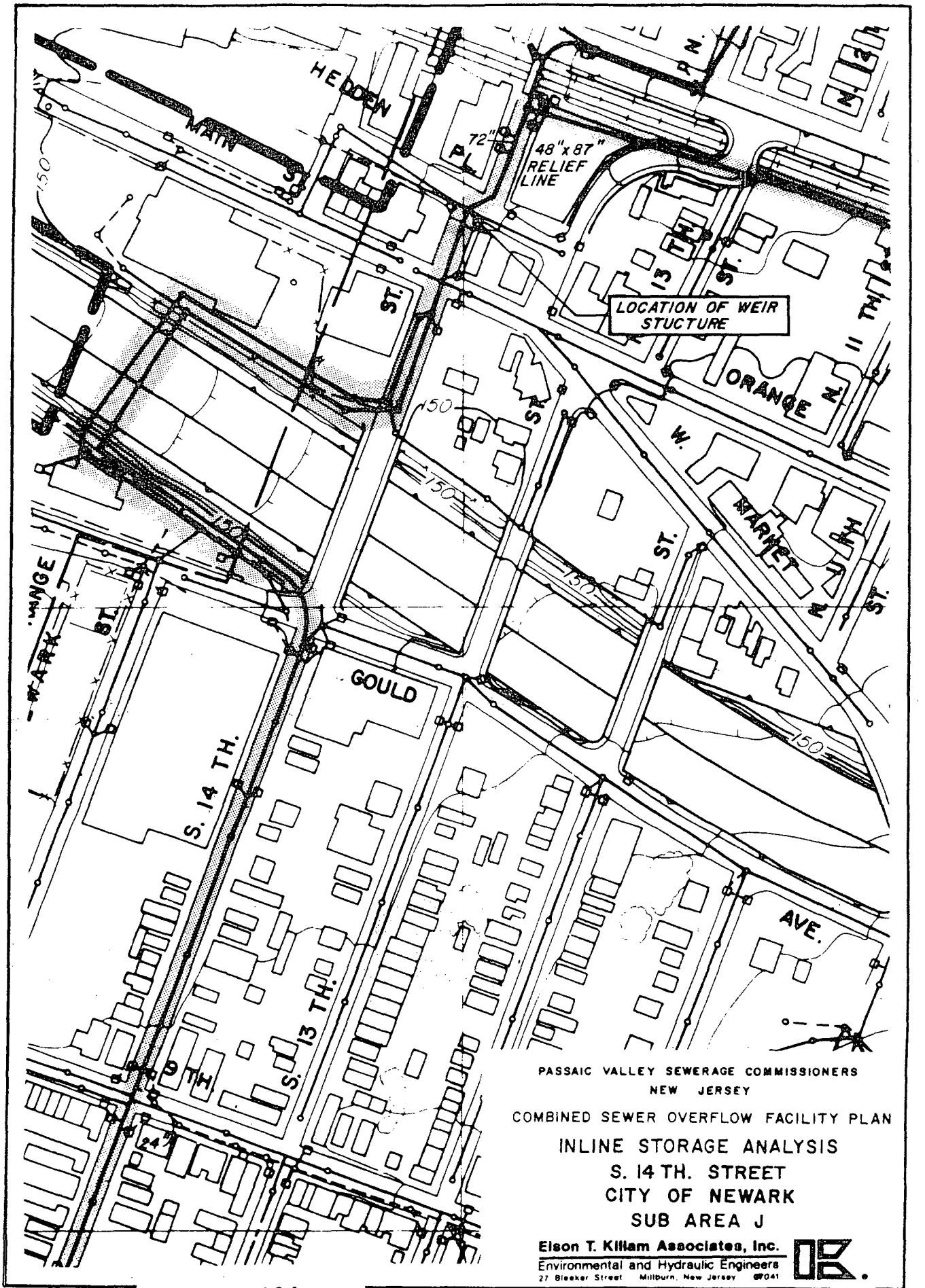
COMBINED SEWER OVERFLOW FACILITY PLAN

INLINE STORAGE ANALYSIS
CLAY STREET (R.O.W.)
CITY OF NEWARK
SUB AREA J

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
Millburn, New Jersey 07041

946510163

FIGURE 4-5



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

INLINE STORAGE ANALYSIS
S. 14 TH. STREET
CITY OF NEWARK
SUB AREA J

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 4-6

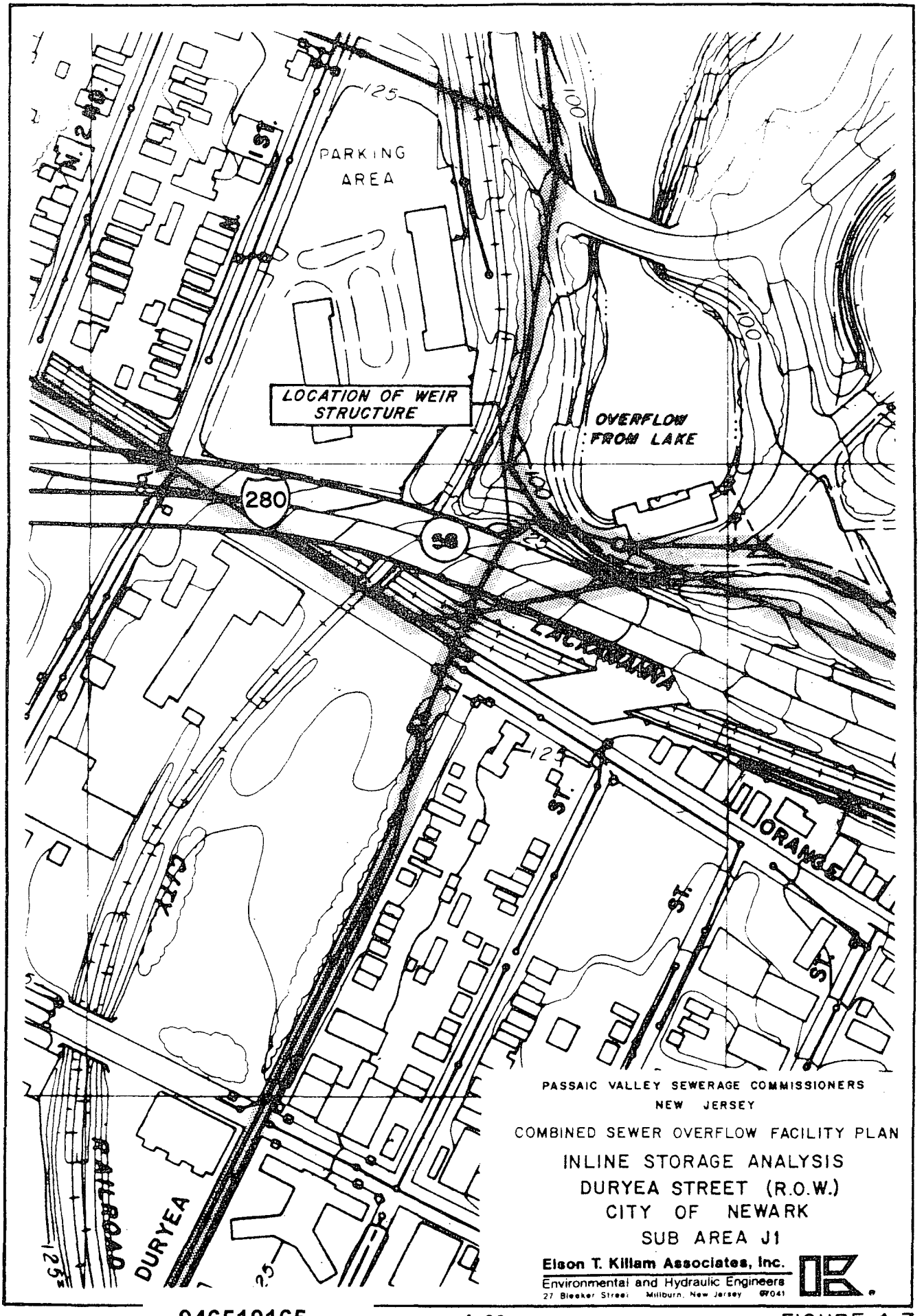
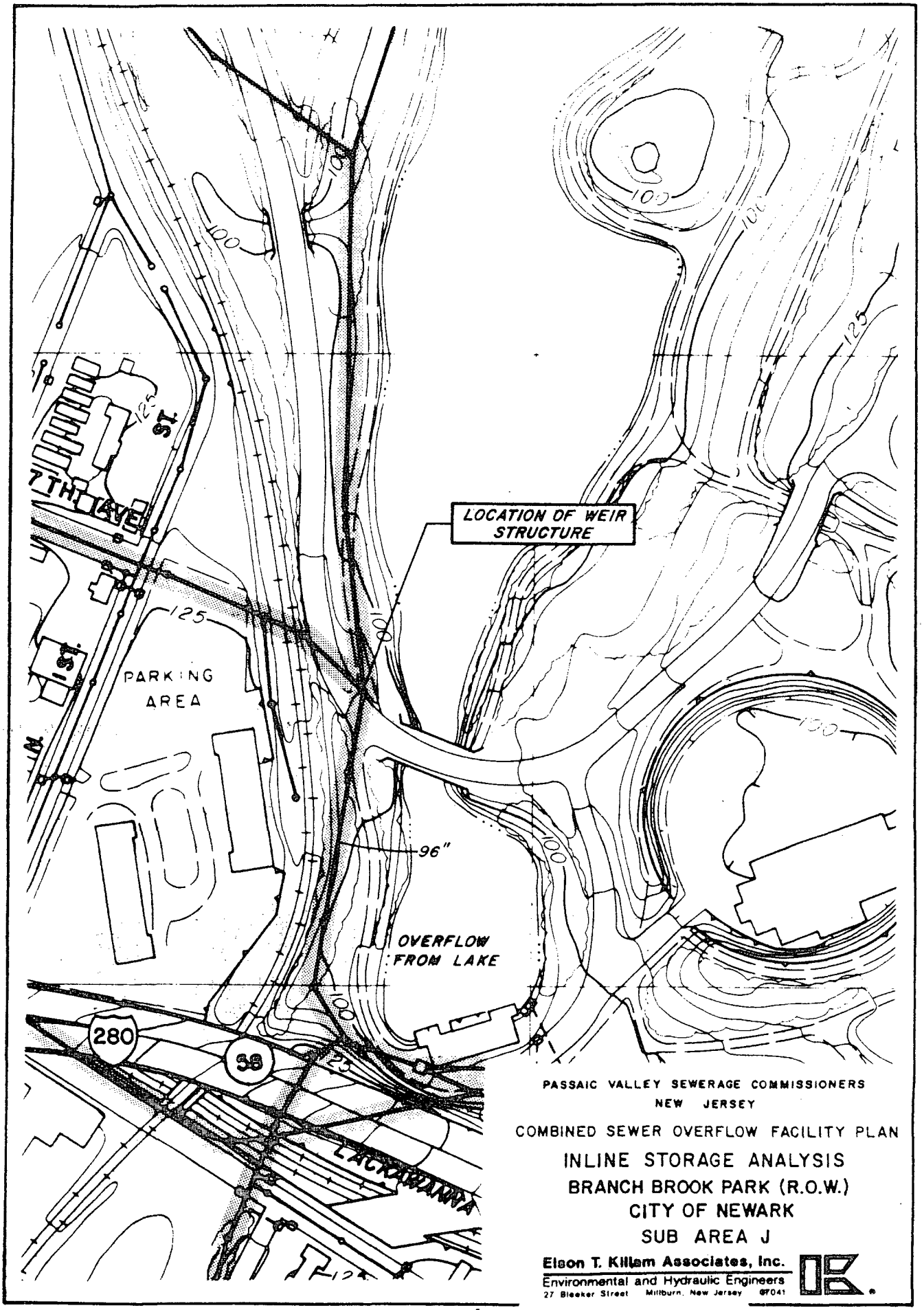

PARKING AREA
LOCATION OF WEIR STRUCTURE
OVERFLOW FROM LAKE
280
98
LACKAWANNA
ORANGE
ST.
CITY
RAILROAD
DURYEA
125
100
PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN
INLINE STORAGE ANALYSIS
DURYEA STREET (R.O.W.)
CITY OF NEWARK
SUB AREA J1
Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 4·7



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

INLINE STORAGE ANALYSIS
BRANCH BROOK PARK (R.O.W.)
CITY OF NEWARK
SUB AREA J

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Environmental and Hydraulic Engineers
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FIGURE 4·8

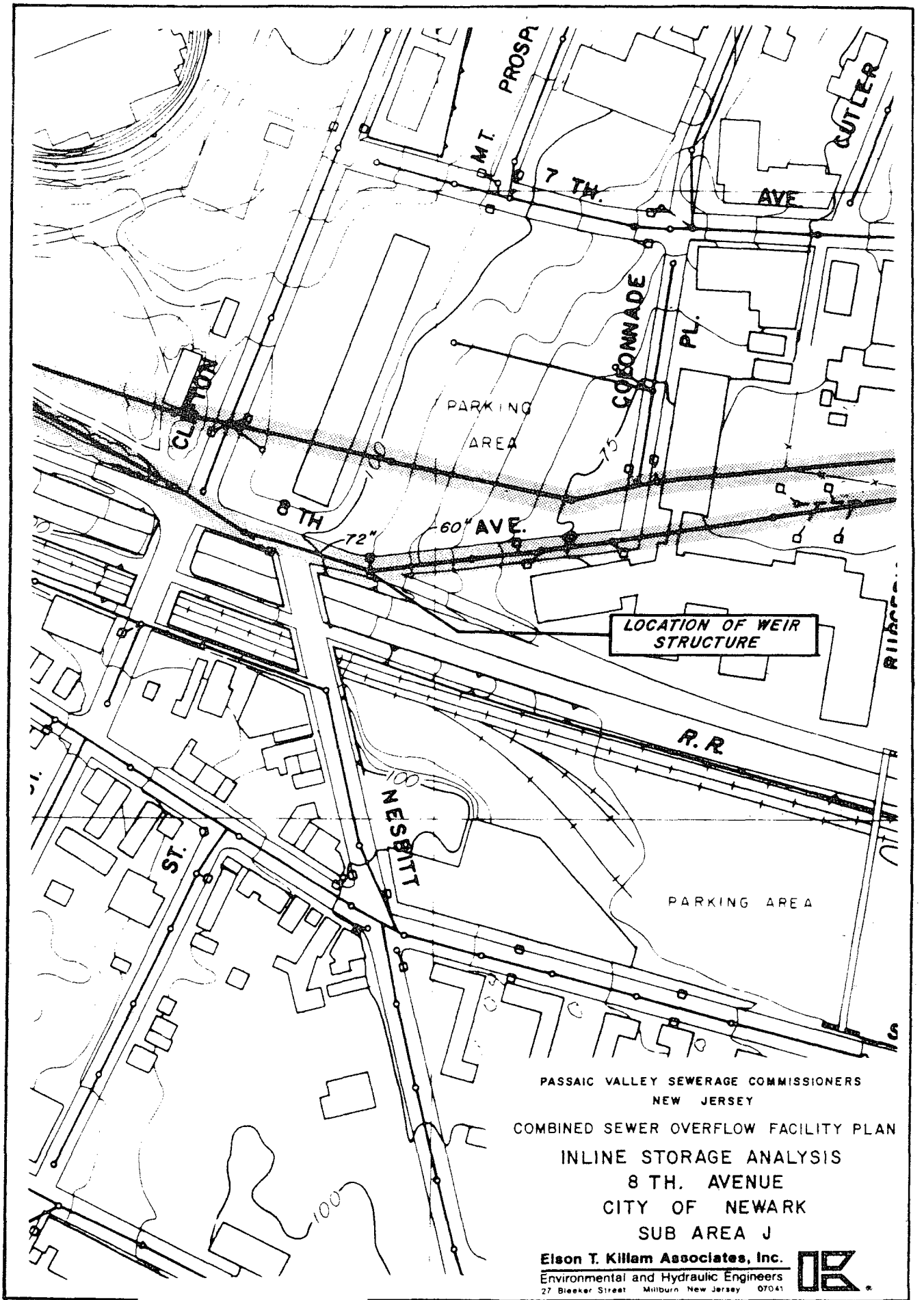

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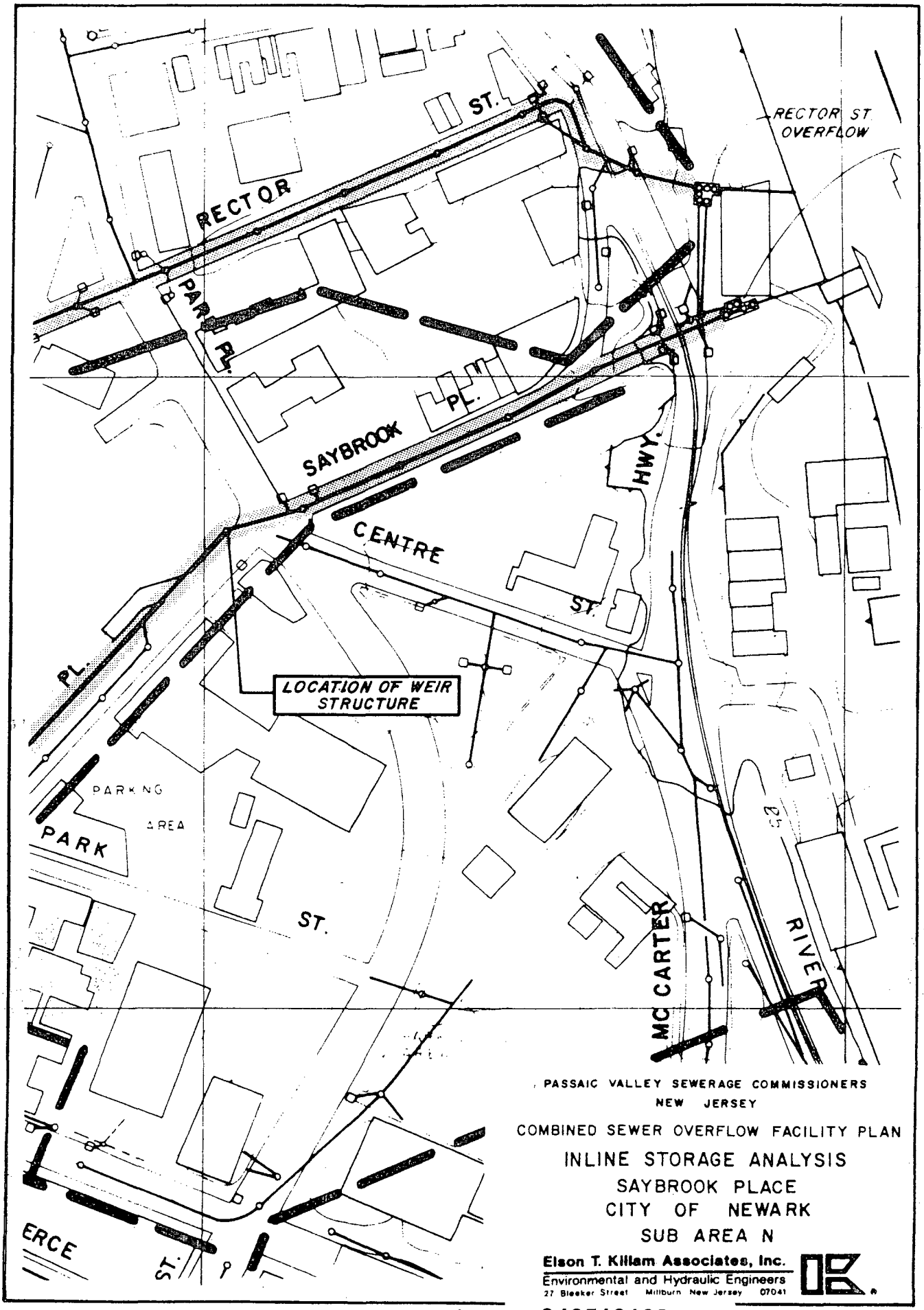
FIGURE 4·9



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

INLINE STORAGE ANALYSIS
SAYBROOK PLACE
CITY OF NEWARK
SUB AREA N

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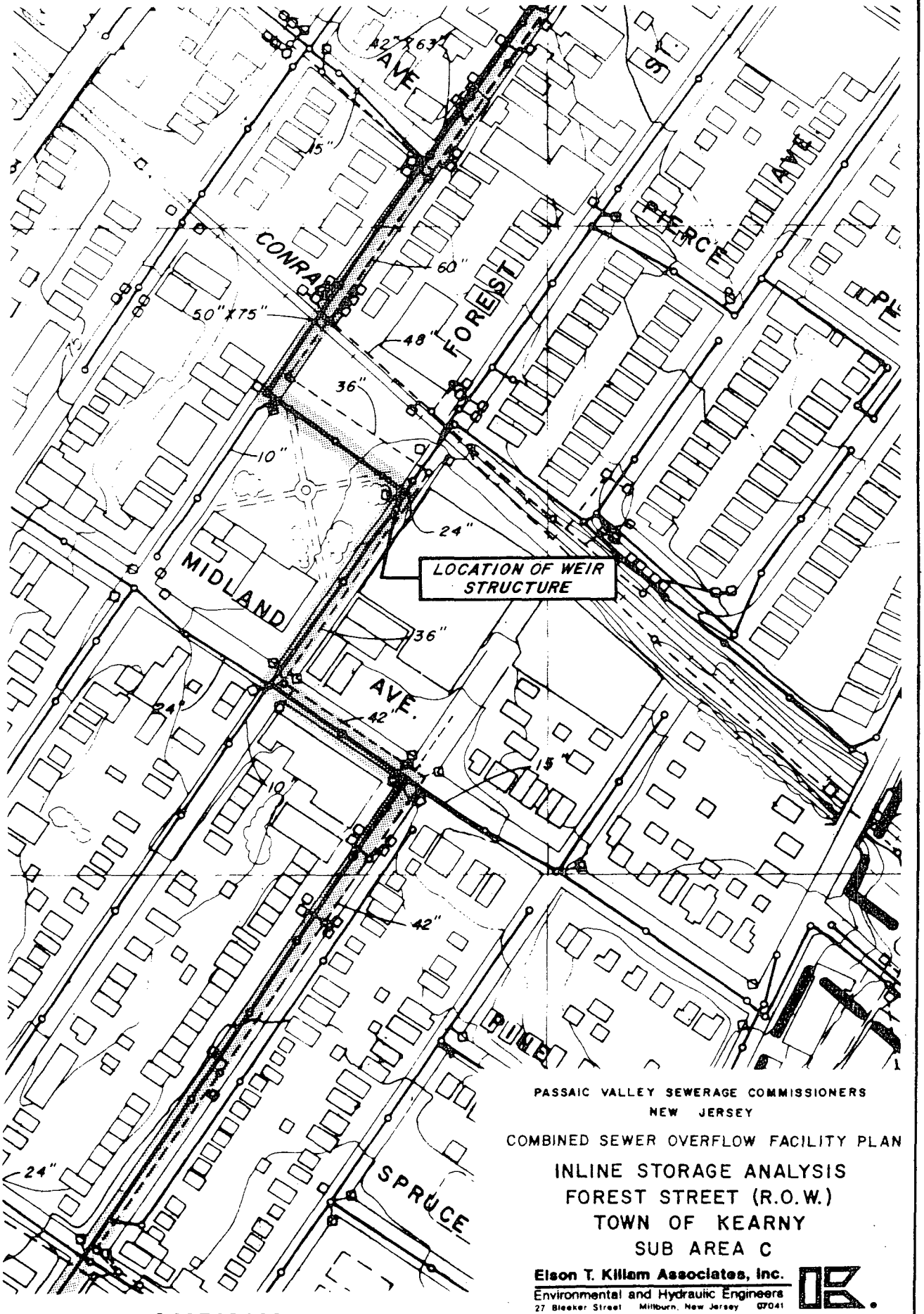
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn New Jersey 07041

946510168

FIGURE 4·10



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

INLINE STORAGE ANALYSIS
FOREST STREET (R.O.W.)
TOWN OF KEARNY
SUB AREA C

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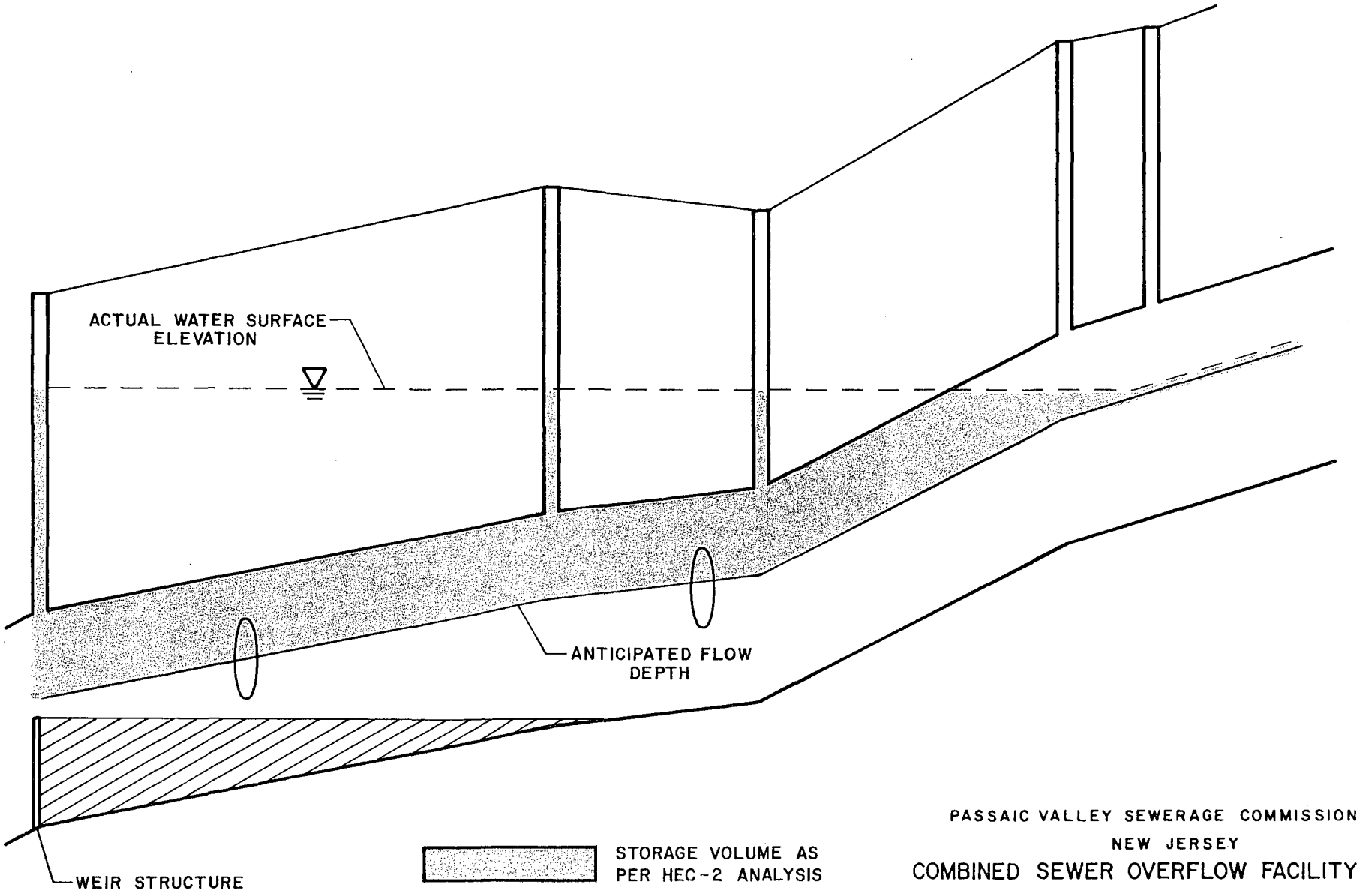
FIGURE 4-11



PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC OF STORAGE VOLUME ANALYSIS

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946510170

FIGURE 4-12

all flow rates wherein the weir structure is maintained at maximum elevation. It therefore provides an estimate of the minimum storage capacity available under a wide variety of flow rates.

A summary has been prepared showing the results of the inline storage analysis. Table 4.5, Inline Storage Analysis - Upstream Areas shows that storage volume determinations ranged from approximately 1.2 - 1.6 MG. Only two areas, Branch Brook Park Easement and Saybrook Place, both within the City of Newark, had any significant static or dynamic storage. Storage however is only one facet of the total picture. Industrial discharges are not homogeneous throughout the area. As such, the pollutional load retained within each storage area is dependent not only upon volume but also on pollutional loads discharged within the area.

Monitoring of flow quantity and quality has been completed within each of the major overflow areas. (Section 3.b) An analysis of pollutional loads retained within each of the storage areas has been compiled and is summarized in Table 4.6, Inline Storage Analysis - Ultimate C-BOD Retained. C-BOD values used within each analysis were based upon values actually monitored at each site or were based upon values obtained from contributing or surrounding areas. Since the pollutional loading factors utilized represented maximum C-BOD's recorded, actual reductions could be substantially less. The analysis does however provide some insight as to those areas wherein the potential exists for substantial storage of C-BOD.

The one area which showed a substantial potential for C-BOD storage was S. 14th Street in the City of Newark. C-BOD values obtained from contributing areas showed a consistently high load factor ranging from the minimum C-BOD recorded of 98 mg/l to the maximum of 1830 mg/l. This area receives sanitary wastes from the City of East Orange in addition to

TABLE 4.5
INLINE STORAGE ANALYSIS
UPSTREAM AREAS

LOCATION	FIGURE NO.	HEC-2 ANALYSIS RETURN PERIOD PEAK INTENSITY(In/Hr)	HEC-2 ANALYSIS STORAGE (MG)	STATIC WATER ANALYSIS-STORAGE (MG)
Clay Street, Newark	4.5	*	0.176	0.054
S 14th Street, Newark	4.6	1.1 yr	0.241	0.186
Duryea Street, Newark	4.7	1.1 yr	0.123	0.027
Branch Brook (ROW), Newark	4.8	5.8 yr	0.407	0.440
8th Avenue, Newark	4.9	*	-	0.110
Saybrook Place, Newark	4.10	2.9 yr	0.640	0.340
Forest Street, Kearny	4.11	5.8 yr	0.003	<0.003
TOTAL			1.590MG	1.160MG

* Actual flow measurements not made at these locations - Analysis based upon expected flow values.

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TABLE 4.6
INLINE STORAGE ANALYSIS
ULTIMATE C-BOD RETAINED

LOCATION	FIGURE NO.	STORAGE CAPACITY RANGE (MG) MIN.	MAX.	MAX. C-BOD RECORDED WITHIN AREA* (mg/l)	ULTIMATE C-BOD RETAINED (LBS) MIN.	MAX.
Clay Street, Newark	4.5	0.054	0.176	310	23	73
S. 14th Street, Newark	4.6	0.186	0.241	1830	450	587
Duryea Street, Newark	4.7	0.027	0.123	98	4	16
Branch Brook (ROW), Newark	4.8	0.407	0.440	102	55	60
8th Avenue, Newark	4.9	0.100	0.200	100	13	26
Saybrook Place, Newark	4.10	0.340	0.640	210	95	180

* If quality determinations were not available within the storage area, quality determinations were based upon flow contributed or quality values obtained within the surrounding area.

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combined flow from the southwestern section of the Clay Street drainage area. Since flow quantity and measurements were not obtained within the actual storage area, a detailed modeling analysis would be required to determine the full potential of storage at this site.

d. Attenuation of Stormwater

Over the years, capacity limitations or new construction within the combined sewer systems have required the separation of sanitary and stormwater flows within specific areas. Depending upon the severity of the problem, areas may have been completely separated, providing for a separate stormwater outlet to the Passaic River, or may have been separated only within local areas. The latter was utilized where sufficient capacity was available within downstream areas but wherein system restrictions or bottlenecks resulted or would result in frequent, local backups or surface flooding. These areas currently have separate storm sewers which discharge to the combined sewer system (see Figure 4.13). Utilization of excess capacity within these separate storm systems may provide some attenuation of peak flow and subsequently diminish the flow volume discharged through the combined sewer overflows.

A review of system mapping has shown that the drainage areas tributary to those separate storm sewers discharging to the combined sewer system varies from less than one acres to approximately 45 acres. Table 4.7 lists those areas wherein the drainage area was found to be equal to or greater than 4 acres. Listed within the table are the location, sub-area, approximate drainage area, pipe size, and runoff characteristics for each area listed. Although the potential for inline storage within these areas does not appear to be substantial, the relatively small cost involved in system modifications does make it attractive from a cost

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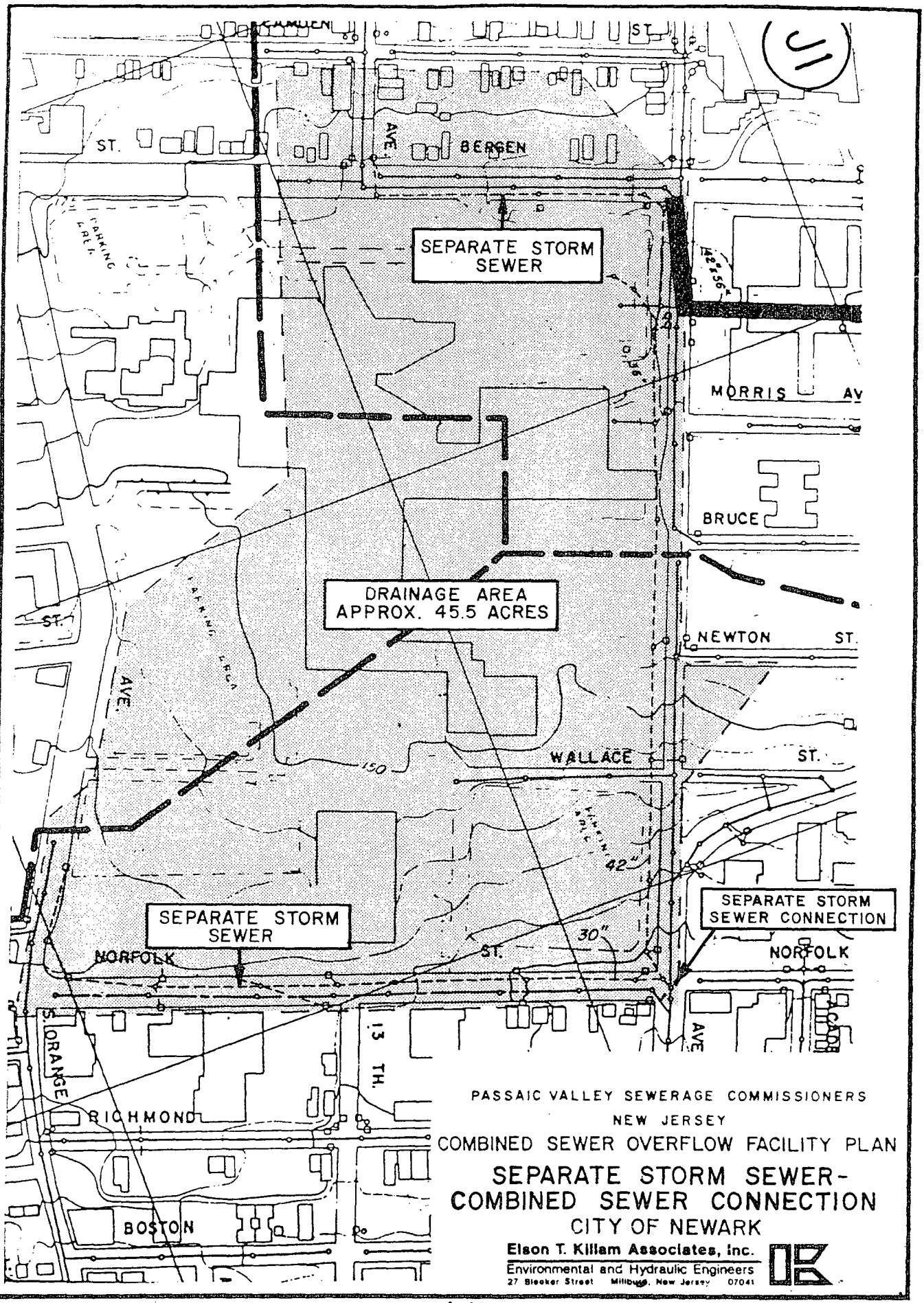

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SEPARATE STORM SEWER-COMBINED SEWER CONNECTION

CITY OF NEWARK

Elson T. Killam Associates, Inc.

Environmental and Hydraulic Engineers

27 Bleeker Street Millburn, New Jersey 07041

BRUNING 44-142 32466

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FIGURE 4-13

TABLE 4.7
SEPARATE STORM SEWERS DISCHARGING
TO COMBINED SEWER SYSTEMS

LOCATION OF ENTRY TO COMBINED SEWER	SUB-AREA	DRAINAGE AREA (ACRES)	PIPE SIZE AT COMBINED SEWER (IN.)	PERCENT IMPERVIOUS	LAND USE
City of Newark					
#1) 12th Avenue & Norfolk St.	J1	45	42"	75	Commercial
#2) Broadway & Crittenden St.	J	8	18"	64	Industrial
#3) Duryea & Dickenson St.	J1	8	21"	60	Industrial/ Residential
#4) S. 14th St. & 9th Avenue	J	17	24"	61	Residential
#5) Broadway & Grafton Avenue	D	22	27"	52	Residential/ Commercial
#6) Mt. Prospect	I	18	36"	54	Residential
Town of Kearny					
#7) Ivy St. & King St.	C	26	42"	49	Residential
#8) Bergen Ave. & Ivy St.	C	10	24"	49	Residential
City of Paterson					
#9) E. 28th St. & 19th Avenue	V2	5	15"	67	Industrial
#10) E. 34th St. & 19th Avenue	V2	4	15"	58	Residential
#11) 20th Ave. & Lewis St.	V2	25	36"	64	Commercial
#12) Fulton St. & Summer St.	G1,G2	11	24"	55	Residential
#13) Lawrence St. & Summer St.	G1,G2	9	15"	55	Residential
#14) Montgomery St. near Summer.	G1,G2	7	15"	55	Residential

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viewpoint. In addition many of these storm systems drain parking lots and other high runoff areas therein representing a potential for attenuation of stormwater runoff within these areas.

As with any inline storage analysis the evaluation of benefit cannot be limited to just an assessment of volume. Other potential system improvements may be possible through the use of flow control or regulation. The following outlines several items which must be considered in any analysis within this area:

(1) Location #4, S. 14th Street & 9th Avenue within the City of Newark is tributary to that area considered for inline storage under section 4.c. This area has been shown to have a very high pollutional load and as such could represent a substantial reduction or attenuation in total pollutional loading from this area.

(2) Location #7, Ivy Street & King Street within the Town of Kearny is tributary to the Ivy Street Overflow. Significant industrial pollutional discharges have been recorded within this area. As such, flow restriction within this area could represent a substantial reduction or attenuation in total pollutional loading discharged to the Passaic River.

(3) Locations #12, 13 & 14, all located on or near Summer Street within the City of Paterson are all tributary to the Straight Street Overflow. Detailed system analysis under section 4b has shown that major municipal interceptors within this area do not have sufficient capacity for even a one year storm. Total drainage areas for separate storm sewers represent over 20% of the total drainage area. As such, significant reduction in system surcharging is possible through flow restrictions within these areas.

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System modifications which would reduce the discharge rate at the outlet of these storm sewer systems can be accomplished at a minimum cost by utilization of Hydro-Brakes. A Hydro-Brake is a flow controlling device which utilizes a swirl to dissipate energy and retard flow. This flow regulator was invented in Denmark about 15 years ago and is marketed by Hydro Storm Sewage Corporation. It is maintenance free, requires no energy consumption, self cleaning, clog and jam resistant and is extremely easy to install.

Hydrobrakes® have been used for both inlet and outlet control. Although stormwater inlet control could result in a greater level of surface flooding, an analysis may show that stormwater temporarily detained in the streets will result in fewer and less severe problems than sewer surcharge and downstream flooding. When utilized as an outlet control, sufficient inline storage is required or desirable to minimize surface flooding. Where inline storage is not available large holding tanks, which are simply lengths of sewer pipes sealed at both ends and buried beneath the pavement, have been utilized for inline storage. (See Figure 4.14).

A detailed modeling within these areas is required to determine the full potential for flow attentuation and reduced overflow. Profiles of all related storm sewer systems would be required in addition to a modeling analysis of runoff. Those storm sewers without sufficient inline storage should be evaluated for installation of holding tanks as illustrated in Figure 4.14. Only when the above analysis is completed, can a realistic cost figure be assessed for this alternative.

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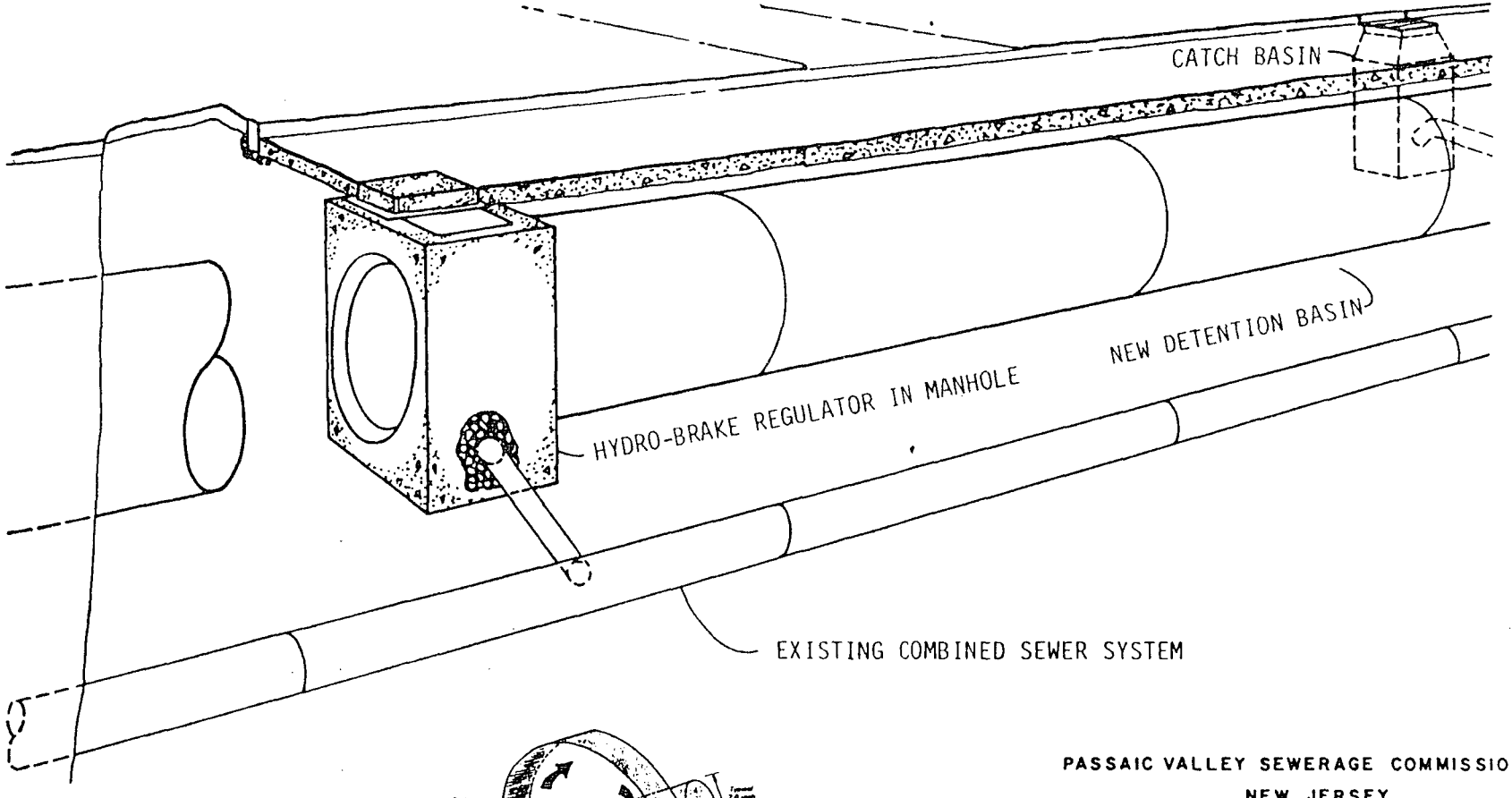

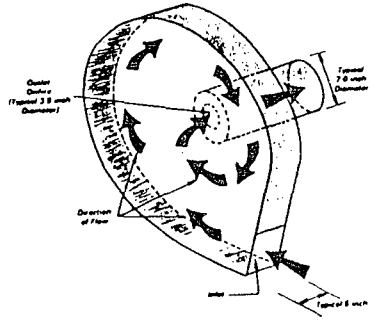

Schematic of hydro-brake regulator.

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC HYDRO – BRAKE REGULATOR WITH AREA DETENTION (TYPICAL)

Elson T. Killam Associates, Inc.
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27 Bleeker Street Millburn, New Jersey 07041

FIGURE 4-14

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e. Initial Screening Process

Prior to the analysis of more costly control alternatives, an initial screening process was conducted to determine those CSO areas warranting further consideration. The screening utilized available data compiled during the Phase I Overflow Analysis conducted by Elson T. Killam Associates, Inc., in 1976. The analysis was completed only upon the moderate and minor overflows as listed on Table 3.2. Major overflows have been shown to discharge substantial pollutional loads and as such were automatically included within the alternative control screening process.

A statistical analysis has been conducted for the Newark and Little Falls (NOAA) rain gaging stations for the period 1950-1979. This analysis upon rainfall intensity, volume, and duration has provided a means of determining and classifying various storms experienced within these regions. This information was utilized within the screening process.

A hydraulic analysis of each CSO area has provided an estimate of the rainfall intensity required to produce an overflow within each CSO chamber. This rainfall intensity was compared to flow data obtained during the Phase I Analysis (1976) as well as to the statistical analysis to substantiate the calculated value and to obtain information as to the relative size storm required and an estimate of the yearly occurrence.

Table 4.8, Results of Initial Screening of Moderate and Minor Overflows, shows the results of this initial analysis. Included within this table are the location of each overflow, its approximate drainage area, the estimate rainfall intensity required to produce an overflow, the estimated number of overflows expected within a typical year, and the classification of the storm intensity required. The classification of storm intensity indicates the percentage of all storm hourly intensity

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TABLE 4.8
RESULTS OF INITIAL SCREENING
MODERATE AND MINOR OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	APPROXIMATE DRAINAGE AREA (ACRES)	EST. RAINFALL INTENSITY REQUIRED FOR OVERFLOW (Inch/Hour)	EST. NUMBER OF OVERFLOWS PER YEAR	INTENSITY STORM PERCENTILE	RECOMMENDATIONS
Newark					
Fourth Ave.	225	0.17	6	95.1	
Polk St.	200	0.08	24	82.0	
Rector St.	180	0.09	20	85.0	
Freeman St.	150	0.20	5	96.5	
Delavan Ave.	90	NO OVERFLOWS OBSERVED		99.9	No further analysis
Jackson St.	67	0.21	5	96.9	
Passaic St.	30	0.29	2	98.4	No further analysis
Orange St.	15	0.80	<1	99.9	No further analysis
Bridge St.	10	1.45	<1	99.9	No further analysis
Third St.	10	0.70	<1	99.8	No further analysis
Paterson					
Straight St.	120	0.13	10	92.1	
E. 11th St.	105	0.08	23	82.0	
20th St.	95	0.17	6	95.1	No further analysis
Warren St.	80	0.08	23	82.0	
Third Ave.	75	0.19	5	96.1	No further analysis
Bridge St.	60	0.30	2	98.5	No further analysis
Sixth Ave.	50	0.65	<1	99.8	No further analysis
S.U.M. Park	45	0.40	1	99.3	No further analysis
2nd Ave.	45	0.41	1	99.3	No further analysis
Arch St.	32	0.12	10	91.1	
Short St.	30	0.25	3	98.1	No further analysis
12th St. & 4th Ave.	20	1.00	<1	99.9	No further analysis
Keen St.	10	0.64	<1	99.8	No further analysis
Bergen St.	10	1.54	<1	99.9	No further analysis
E. 5th St. & 5th Ave.	10	0.78	<1	99.9	No further analysis
West Broadway	5	1.10	<1	99.9	No further analysis
Mulberry St.	5	0.90	<1	99.9	No further analysis
Bank St.	5	>1.75	<1	99.9	No further analysis
Franklin St.	5	>1.75	<1	99.9	No further analysis

946510181

TABLE 4.8
RESULTS OF INITIAL SCREENING
MODERATE AND MINOR OVERFLOWS
(Continued)

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	APPROXIMATE DRAINAGE AREA (ACRES)	EST. RAINFALL INTENSITY REQUIRED FOR OVERFLOW (Inch/Hour)	EST. NUMBER OF OVERFLOWS PER YEAR	INTENSITY STORM PERCENTILE	RECOMMENDATIONS
Kearny					
Nairn	175	0.14	9	92.8	
Bergan Ave. (East)	110	0.14	9	92.8	
Washington Ave.	37	0.11	13	89.6	
Tappan St.	35	0.08	23	82.0	
Stewart Ave.	34	0.22	5	97.4	No further analysis
Dukes St.	25	0.16	7	94.4	
Marshall St.	25	0.16	7	94.4	
Bergan Ave. (West)	10	0.16	7	94.4	
Harrison					
Harrison Ave.	65	0.13	12	92.1	
Middlesex St.	38	0.11	13	89.6	
Hamilton St. (New)	30	0.33	2	98.5	No further analysis
Cleveland Ave.	10	0.20	5	96.5	No further analysis
Dey St.	5	0.85	1	99.9	No further analysis
Worthington Ave.	180	OUTFALL FULL OF DEBRIS			No further analysis
Bergan St.	70	0.06	34	> 2.8	
East Newark					
Central Ave.	26	0.18	6	95.8	No further analysis

946510182

values, recorded over the 30 year analysis period, which equaled or fell below the indicated value. That is, a 95 percentile storm intensity has been equaled or exceeded only by 5 percent of all the hourly intensities recorded during the 30 year analysis period. The estimated number of overflows occurring within any year was based upon expected return periods for intensities equal to or exceeding the calculated value.

This analysis has shown that 60 percent of the moderate and minor overflows within the PVSC district would be expected to overflow less than six times per year, requiring greater than a 95 percentile storm. In addition, review of the Phase I Overflow Analysis has shown that the maximum overflow volume recorded at each of these sites during the monitoring period averaged less than 0.3 MG per inch of rainfall (unless the overflow was caused by system restrictions within the PVSC trunk). It was determined that, unless other conditions proved otherwise, these areas would not warrant the expenditures required for control alternatives and as such should be eliminated from further analysis. These include:

CITY OF PATERSON

20th Ave.
Third Ave.
Bridge St.
Sixth Ave.
S.U.M. Park
2nd Ave.
Short St.
12th St. & 4th Ave.
Keen St.
Bergen St.
E. 5th St. & 5th Ave.
West Broadway
Mulberry St.
Bank St.
Franklin St.

CITY OF NEWARK

Delavan Ave.
Passaic St.
Bridge St.
Orange St.
Third St.

TOWN OF KEARNY

Stewart Ave.

TOWN OF HARRISON

New St. (Hamilton)
Cleveland Ave.
Dey St.
Worthington Ave.

BOROUGH OF EAST NEWARK

Central Ave.

946510183

f. Offline Storage

Analyses reported upon within previous sections have shown that there is not a significant amount of inline storage available within the PVSC District. Total inline storage available within all areas is less than two million gallons. Of this approximately three quarters to one millon gallons of storage is available within the Clay Street Drainage Area and half a million gallons of storage is available within the Saybrook Place Drainage Area, both within the City of Newark. This means that eighty five percent (85%) of the major overflows previously listed within Table 3.2 have insignificant or no potential for inline storage of combined flows.

The construction of offline storage reservoirs would provide additional storage volume to retain the combined sewer overflows caused by the storm. Once sufficient capacity is available within the PVSC Interceptor, the stored wastewater would be discharged/ pumped back into the sewerage system for conveyance to the PVSC Treatment Plant.

The schematic of a typical storage reservoir is shown in Figure 4.15. Each reservoir would be equipped with bar screens, a system for flushing sediment from the reservoir bottom, odor control systems, a ventilation system, and pumps for returning wastewater or accumulated sludge back into the system. The number of compartments used during any storm would depend on the rainfall intensity and subsequent overflow volume.

Although most unit processes have been eliminated from consideration due to the minor pollutional impact of CSO discharges, those control alternatives which would reduce the floatable material discharged to the Passaic River have been evaluated from an aesthetic viewpoint. By reducing the frequency and volume of CSO discharge an improvement in

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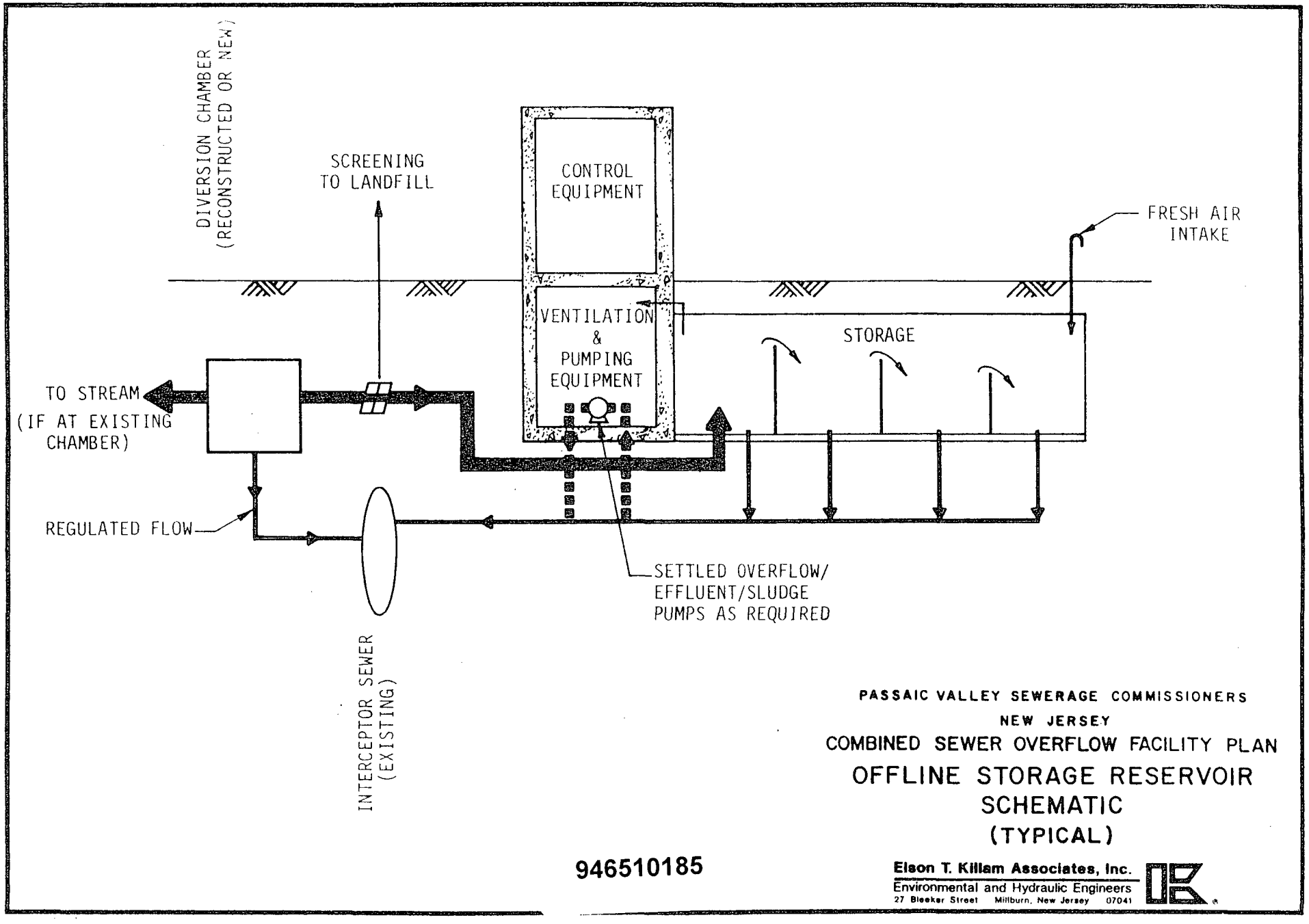

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

OFFLINE STORAGE RESERVOIR
SCHEMATIC
(TYPICAL)

946510185

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27 Bleeker Street Millburn, New Jersey 07041

FIGURE 4-15

aesthetics is possible. It must be remembered however that all the analyses conducted within this section are preliminary, since solids transport was neither considered or modeled within the current study. A detailed sampling and modeling analysis would be required to determine the relative impact of CSO discharge upon the aesthetics of the lower Passaic River. This would be an essential part of the cost-benefit analysis and must be completed prior to the final consideration of all the alternatives currently under investigation.

Although a relatively expensive method for the reduction or elimination of discharge from combined sewer overflows, storage or flow equalization is a fundamental part of most unit processes utilized for the control of stormwater pollution. Storage is necessary because the high volume and variability associated with storm and combined sewer overflows cannot be adquately provided for in the design of most unit processes. Storage therefore would reduce the size, number and costs associated with other unit processes considered for control or treatment of both combined and separate stormwater discharges. In addition, storage with the resulting sedimentation that occurs due to increased detention times, can also be considered a treatment process.

Offline storage would be an integral part of an integrated or dynamic regulator system installed within the combined sewer areas of the PVSC District. Although storage is not required per se, it would provide the flexibility required for maximum utilization of the regulator capabilities under a full range of flow conditions. Accordingly, an investigation was conducted as to the preliminary site selection for offline storage.

A feasibility analysis of offline storage was initialized using information obtained during the corridor inventory conducted at the outset

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of the facility plan. The corridor inventory, reported upon within Volume 3, was instituted to compile a list of potential sites for combined sewer overflow facilities. It was conducted, through field observations and review of aerial photos and land use reports, upon those areas adjacent to major municipal interceptors and along the Passaic River. The sites compiled through the Corridor Inventory were thus the major source of potential offline storage sites utilized within the screening process.

The investigations conducted under this portion of the facility plan are preliminary; that is, final analysis of these alternatives and sites will not be conducted until Phase II of the plan. A detailed modeling analysis of each drainage area would be required in order to determine the most cost-effective alternative in addition to determining the level of storage/treatment necessary. As a preliminary indication as to the size and cost projected for each storage facility, each site was evaluated on the basis of available information and most sites sized for approximately an 80-85 percentile storm. (80-85% of all storms that occur have a total volume equal to or less than this design storm).

The offline storage screening process was based upon primary factors important in the preliminary evaluation of each CSO area. Each CSO was evaluated for: sufficient overflow volume to warrant the expense and associated operation and maintenance costs involved with offline storage, the availability of land within the immediate area of the combined sewer overflow regulator and/or municipal interceptor; and for sufficient available head between the CSO, storage facility and discharge point to eliminate the need for pumping facilities if possible. Wherein sufficient volume and/or adjacent land area was not available the site was evaluated for regional storage.

946510187

Due to the congested and urban nature of most combined sewer overflow locations, all storage facilities were assumed to be covered reinforced concrete reservoirs equipped with facilities for screening, sludge removal, odor control, pumping (if needed) and chlorination. In addition, cost factors provided for each site include allowances for piping modifications, site work, etc., which may be necessary. Operation and maintenance costs will be discussed subsequently and were not evaluated on a per site basis.

The combined sewer overflow areas which have survived the initial offline storage screening process are illustrated within Figures 4.16 thru 4.28. These figures show open areas wherein the construction of offline storage facilities appears to be feasible. Detailed site investigations would be required within all locations to determine limiting factors such as utilitites, poor soil conditions, etc., which may impact construction. In addition, both the Cities of Newark and Paterson are in a state of flux wherein new construction has or will be planned for open areas. It is therefore important that all areas be investigated in detail to determine the true availability of sites currently under investigation. (See Volume 3)

All of the locations wherein the preliminary analysis has shown offline storage to be feasible are listed in Table 4.9. Included within this table are the locations of each CSO involved, the figure number wherein the area of interest is illustrated, the storage volume analyzed, and the estimated construction cost (ENR=4000) determined for each site. Those locations wherein several CSOs are indicated with only one storage volume have been evaluated for regional storage.

946510188

TABLE 4.9
SITES FEASIBLE FOR OFFLINE STORAGE
PRELIMINARY ANALYSIS

MUNICIPALITY	OVERFLOW	FIGURE NO.	STORAGE VOLUME (MG)	ESTIMATED CONSTRUCTION COSTS (1)
Paterson	Northwest St.	4.16	1.0	$1,885,000
	(2) Straight St.	4.17	0.5	990,000
	(2) Montgomery St.	4.17	1.0	1,820,000
	(3) Curtis Pl.			
	(3) Mulberry St.	4.16	2.2	3,290,000
	(3) W. Broadway			
Newark	Clay Street	4.21	3.5	4,940,000
		4.22	6.2	7,800,000
	City Dock	4.24	1.6	3,025,000
	Verona Ave.	4.18	1.3	2,380,000
	Saybrook Pl.	4.23	0.8	1,560,000
	Herbert Pl.	4.19	0.6	1,235,000
	Fourth Ave.	4.20	0.5	990,000
	Rector St.	4.23	0.8	1,560,000
	Jackson St.	4.25	0.6	1,235,000
Kearny	Marshall St.	4.27	0.8	1,625,000
	Johnston Ave.	4.27	2.8	4,290,000
	Tappan St.	4.26	0.6	1,235,000
	Dukes			
Harrison	Hamilton St.	4.28	0.8	1,625,000
	Cleveland Ave.			
	Harrison St.			
	TOTAL		25.6	$41,495,000

(1) Construction costs do not include land acquisition.

(2) Response from the City of Paterson indicates future redevelopment plans within this area.

(3) Response from the City of Paterson indicates recent redevelopment within this area.

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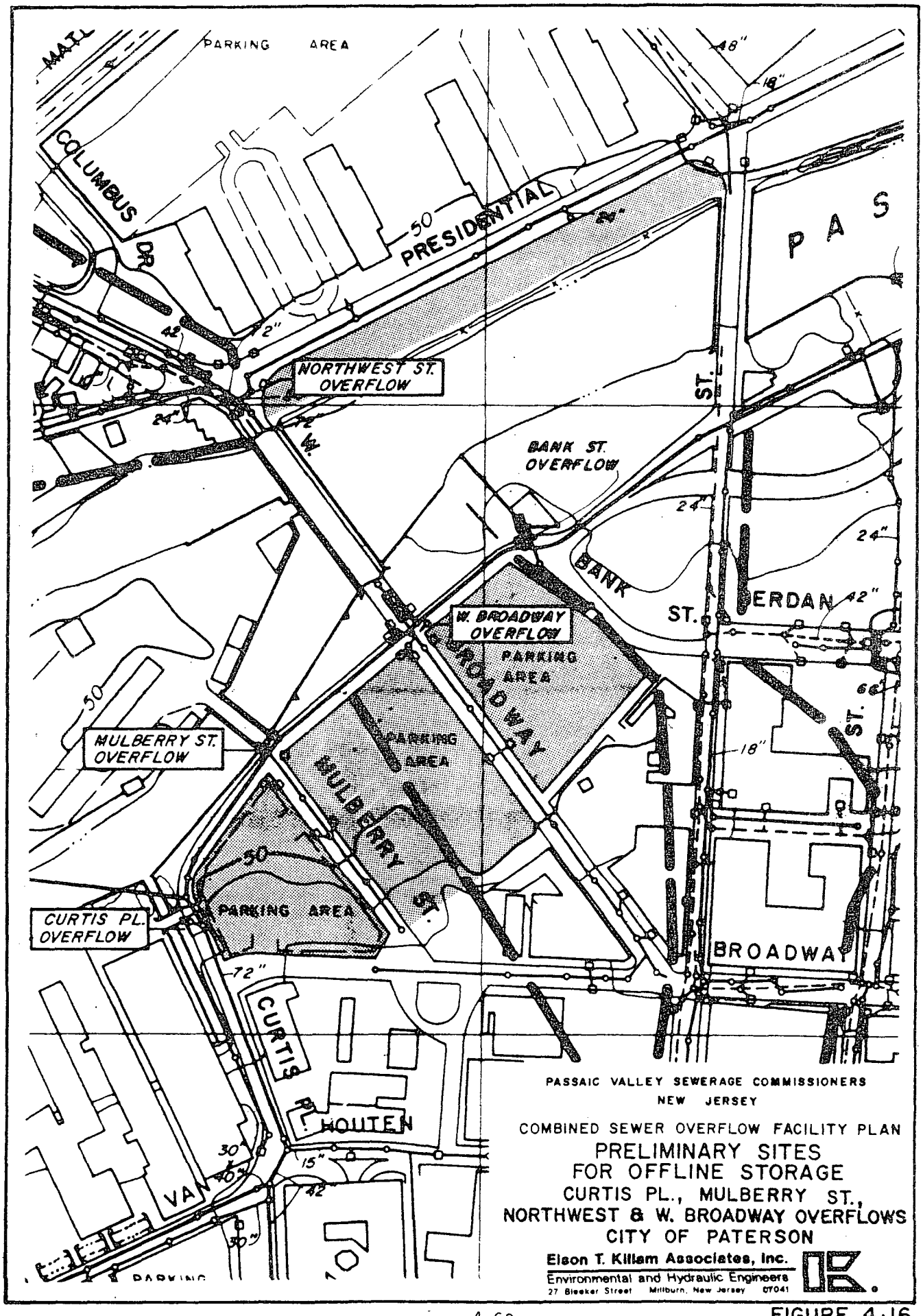


FIGURE 4·16

946510190

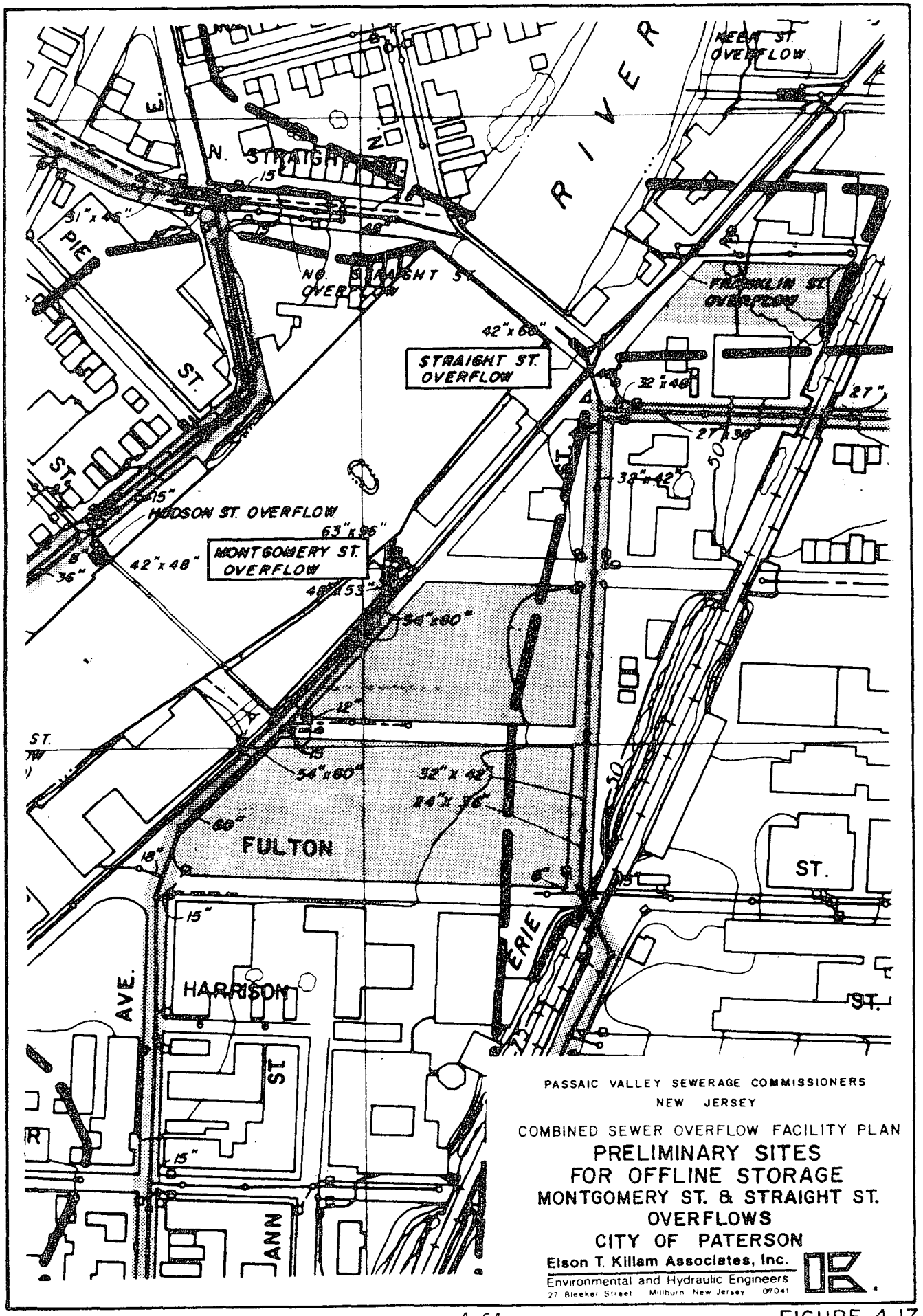
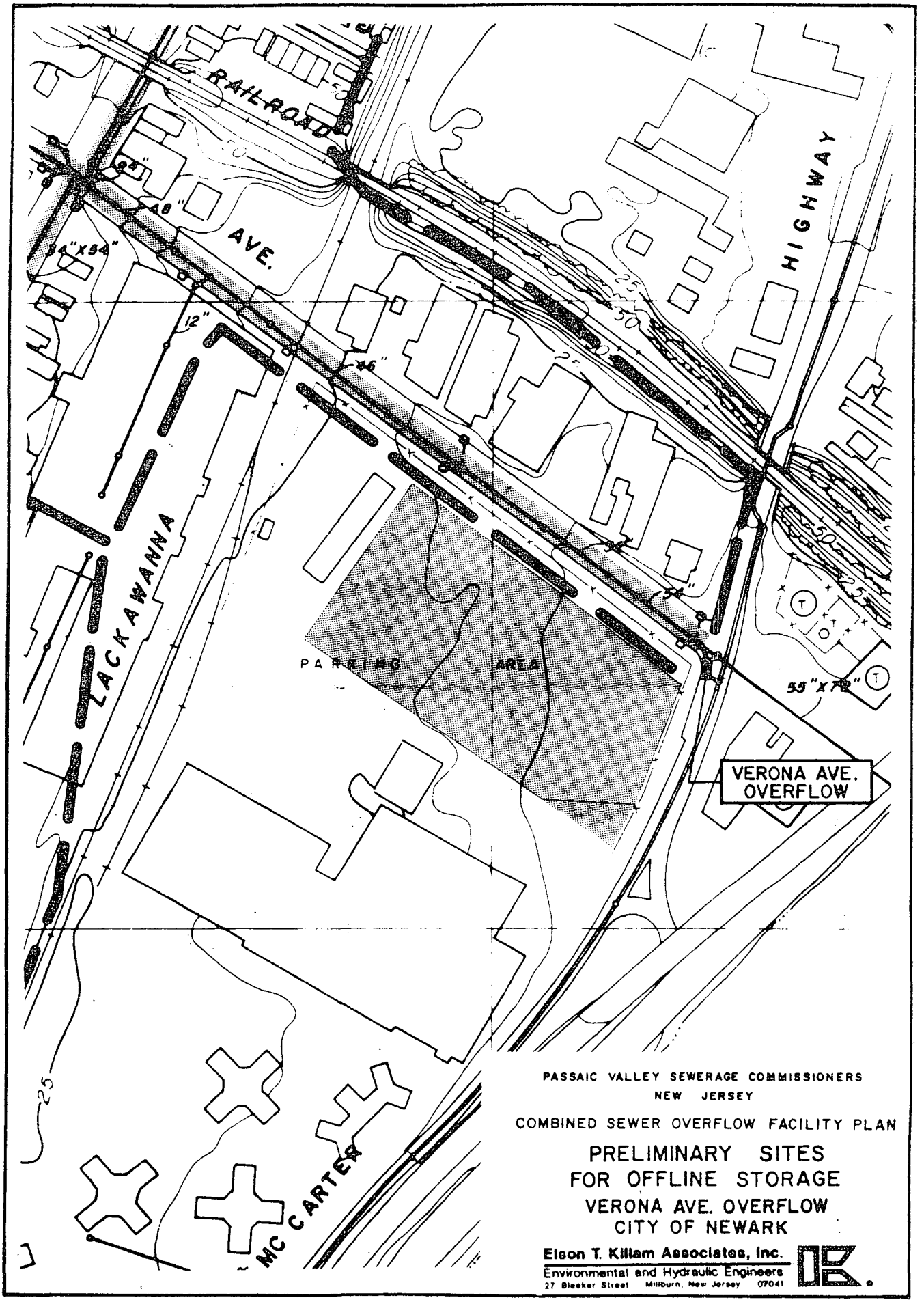


FIGURE 4-17

946510191



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

PRELIMINARY SITES
FOR OFFLINE STORAGE
VERONA AVE. OVERFLOW
CITY OF NEWARK

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27 Bleeker Street Millburn, New Jersey 07041

FIGURE 4-18

946510192

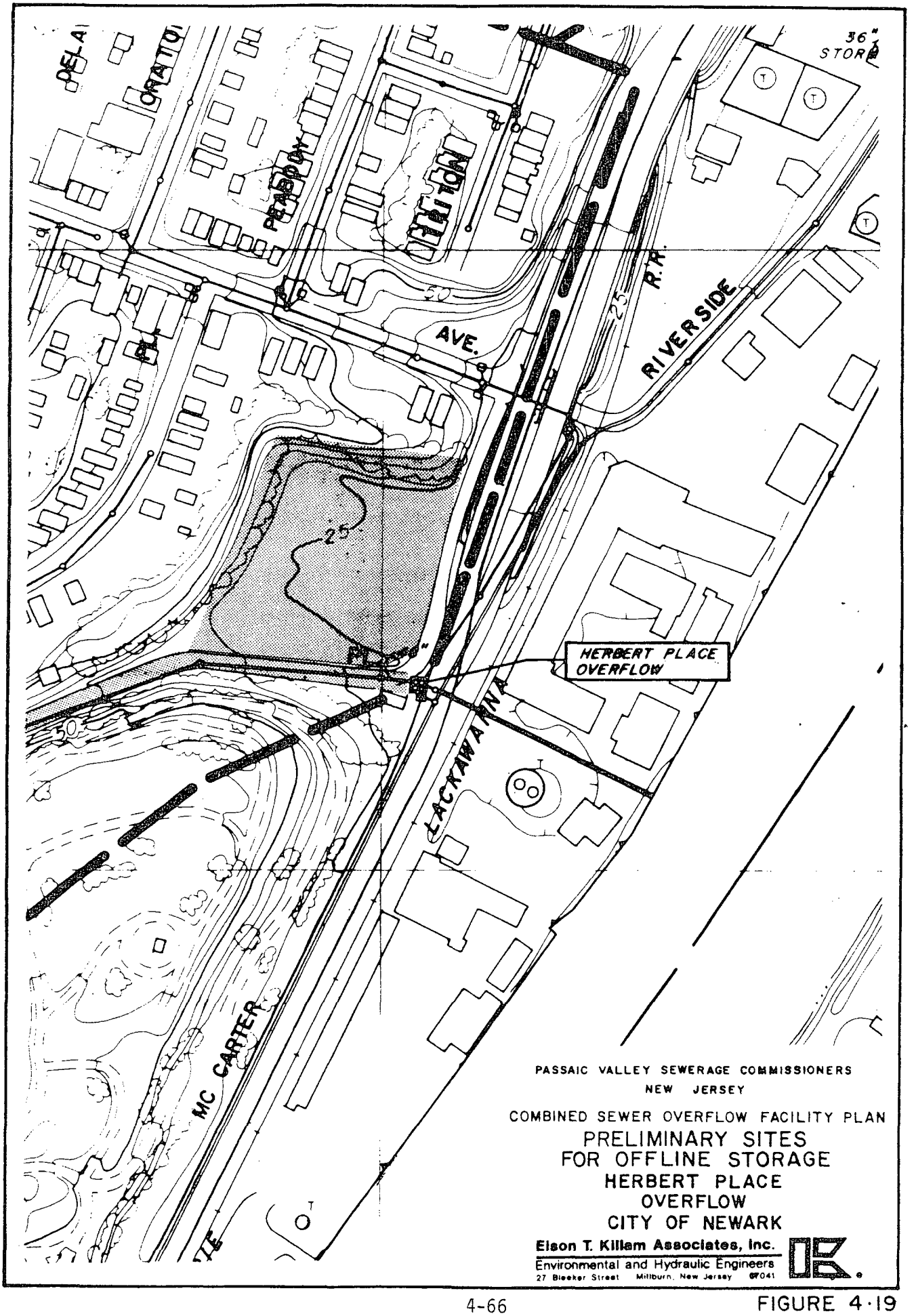

FIGURE 4·19

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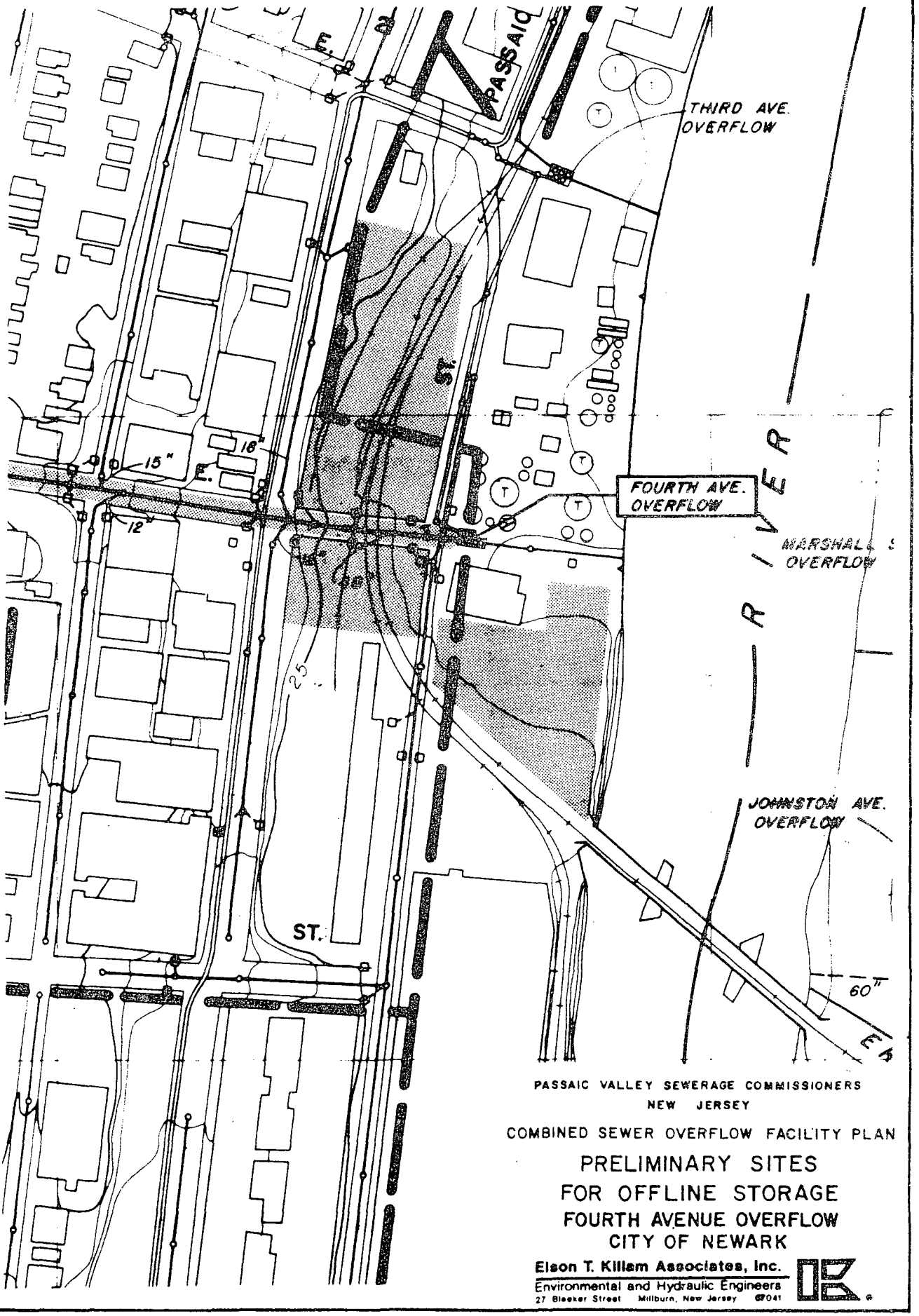

FIGURE 4-20

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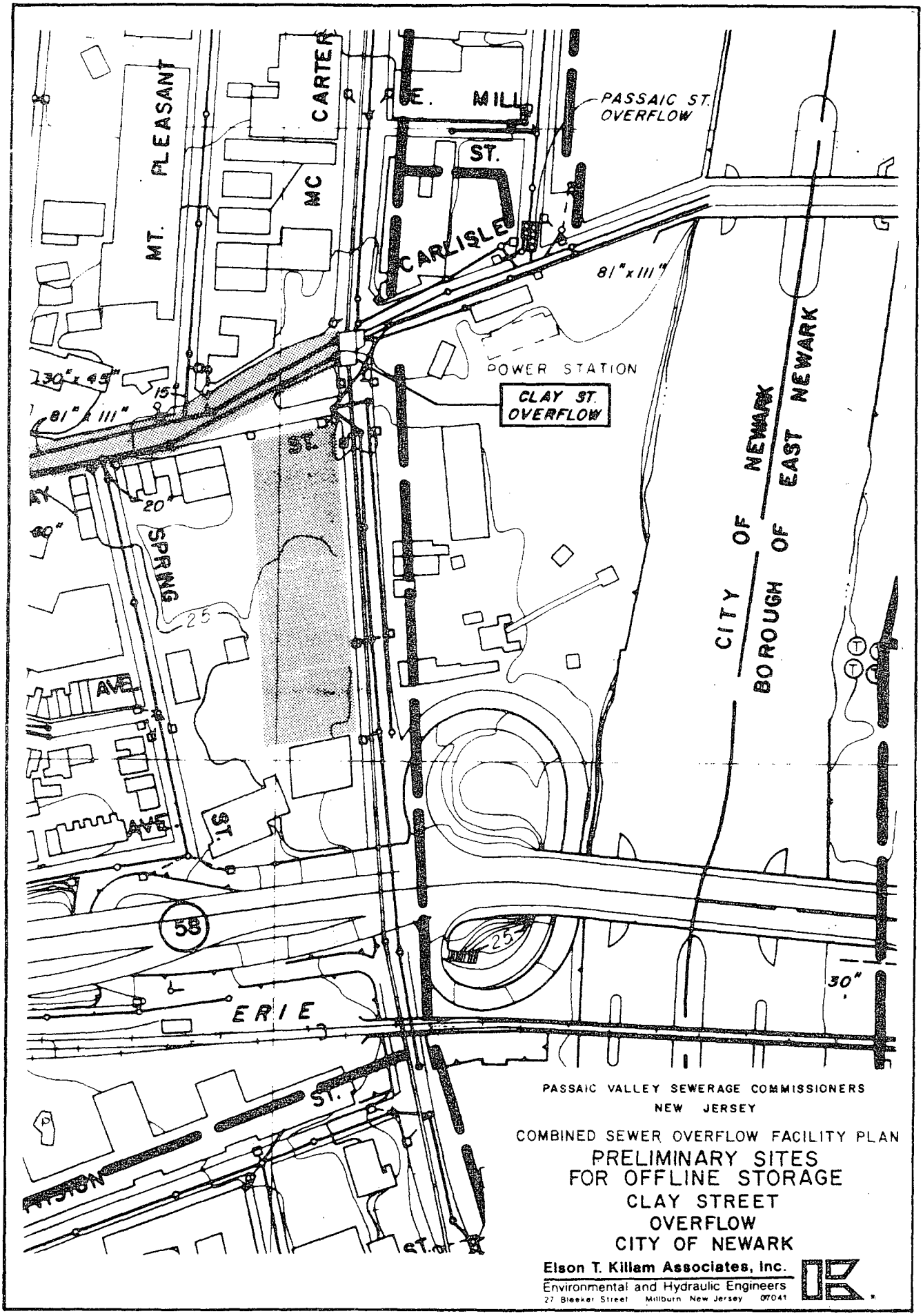

FIGURE 4-21

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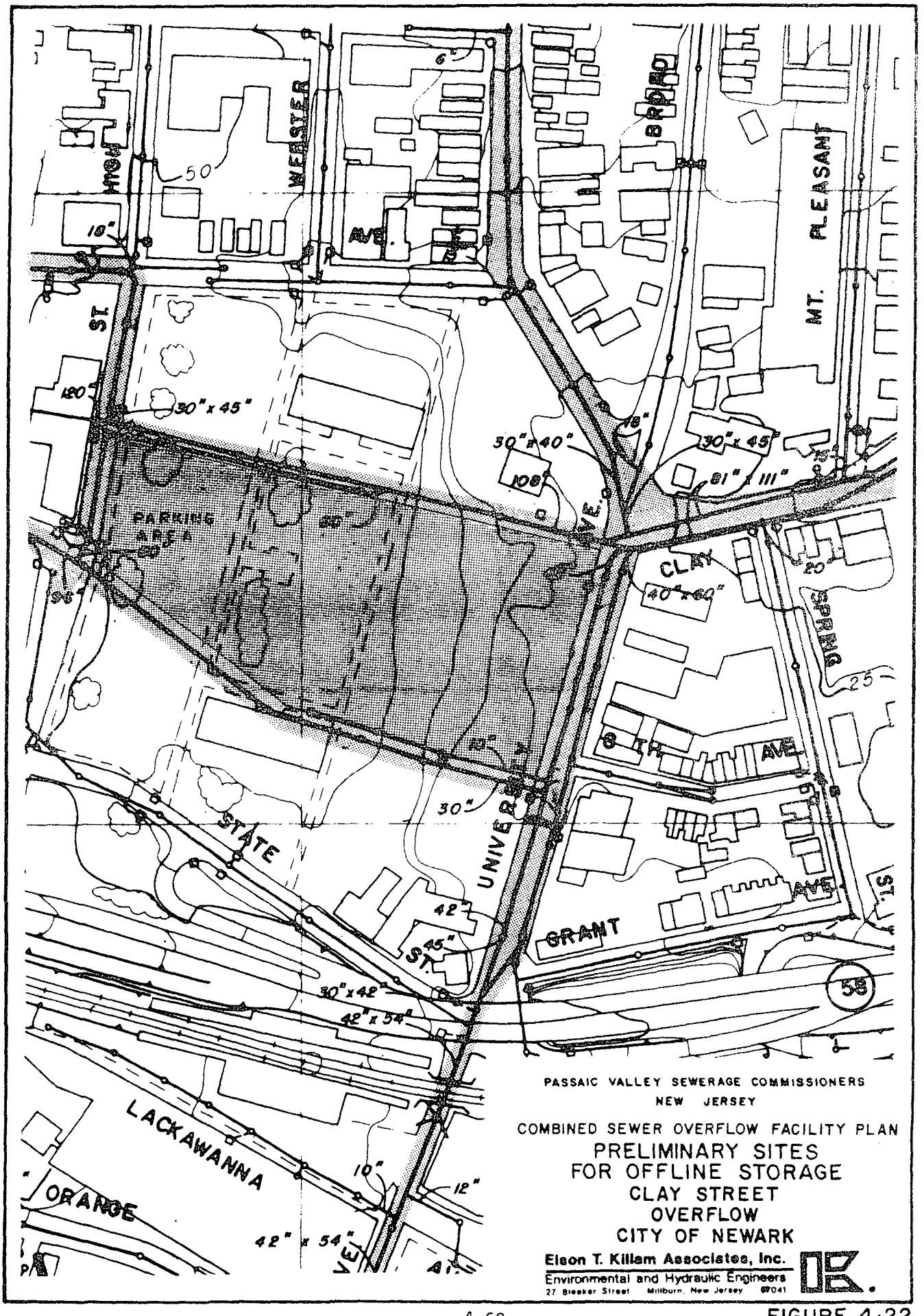

FIGURE 4-22

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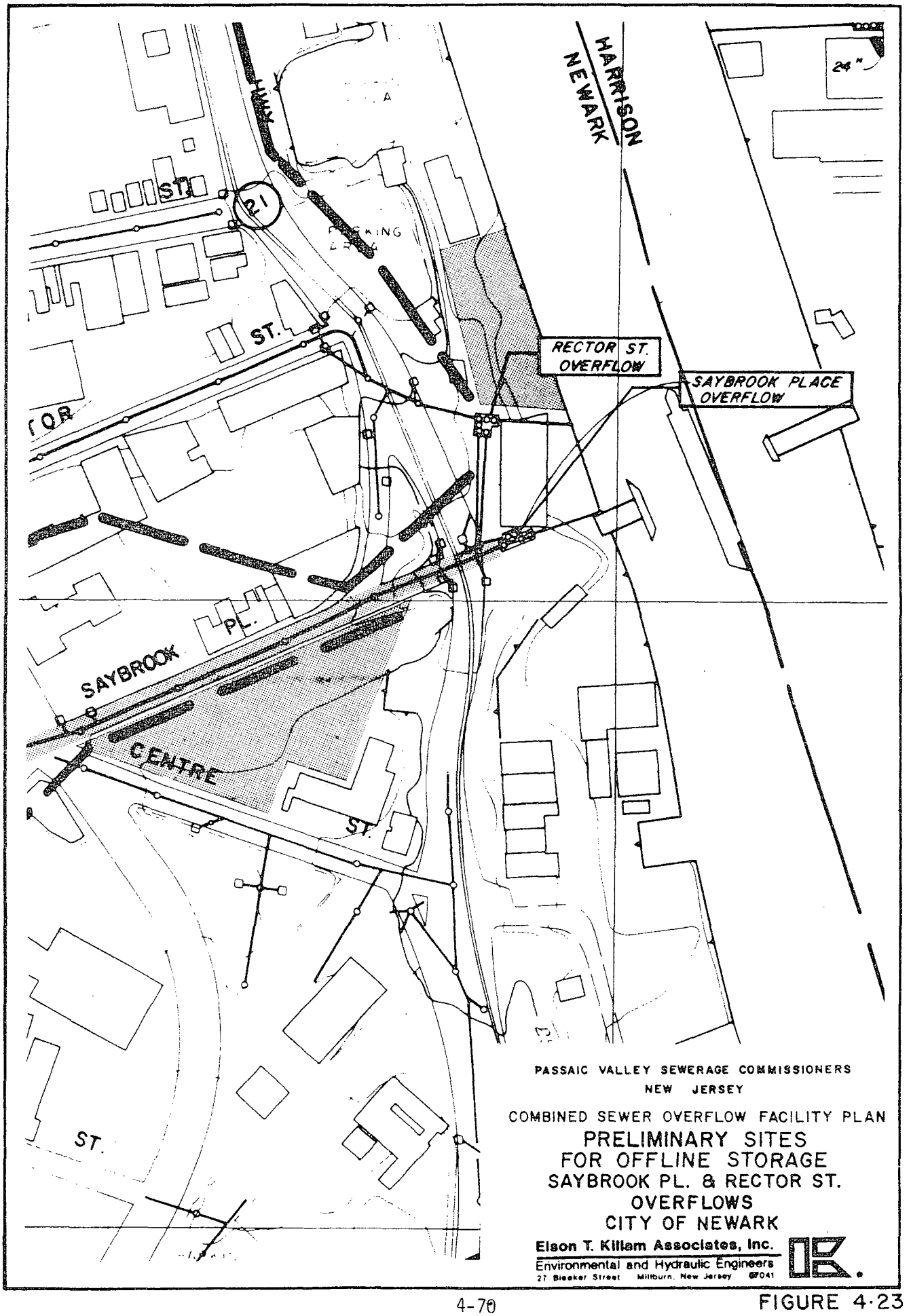

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

PRELIMINARY SITES FOR OFFLINE STORAGE SAYBROOK PL. & RECTOR ST. OVERFLOWS CITY OF NEWARK

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FIGURE 4-23

946510197

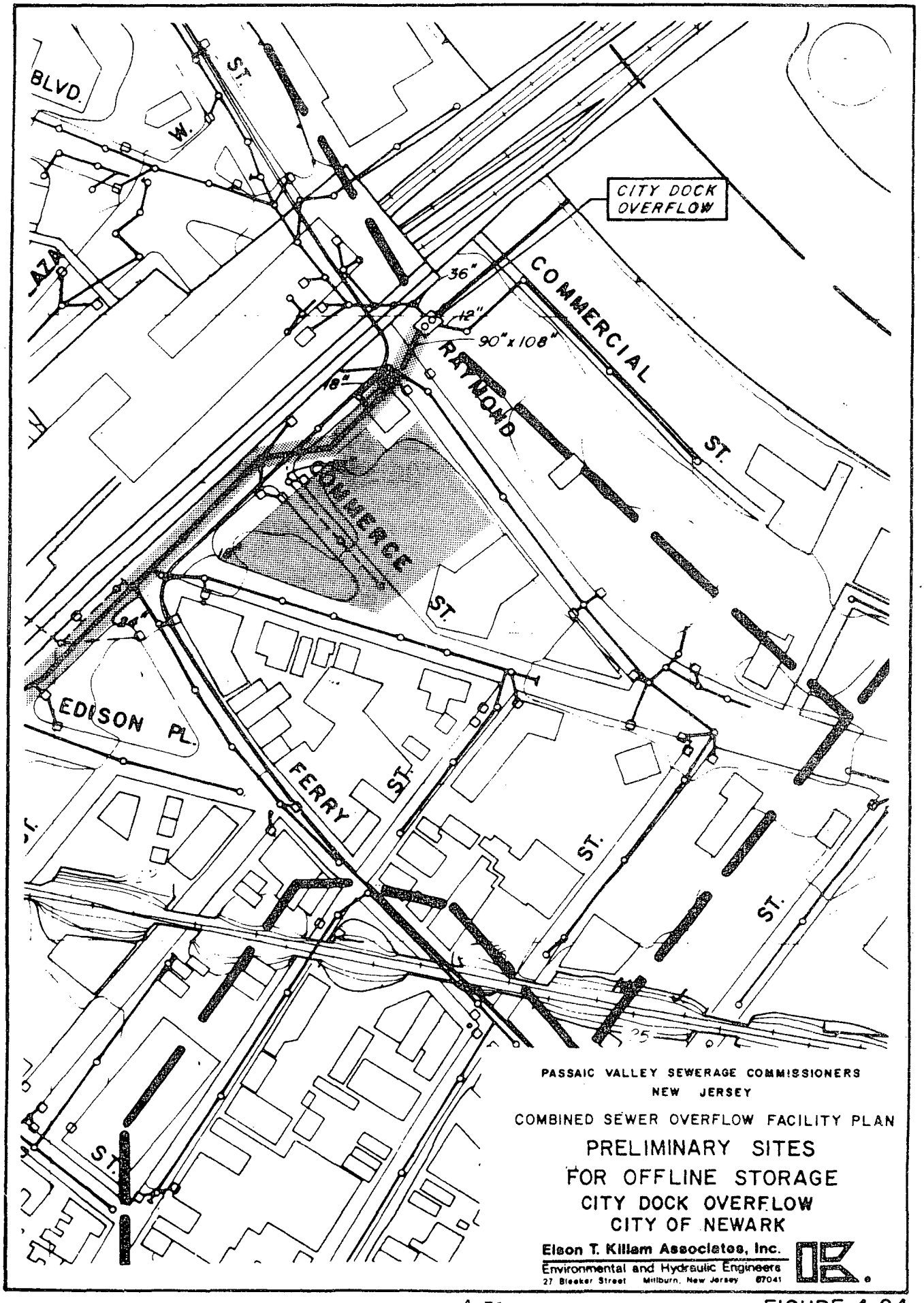

FIGURE 4-24

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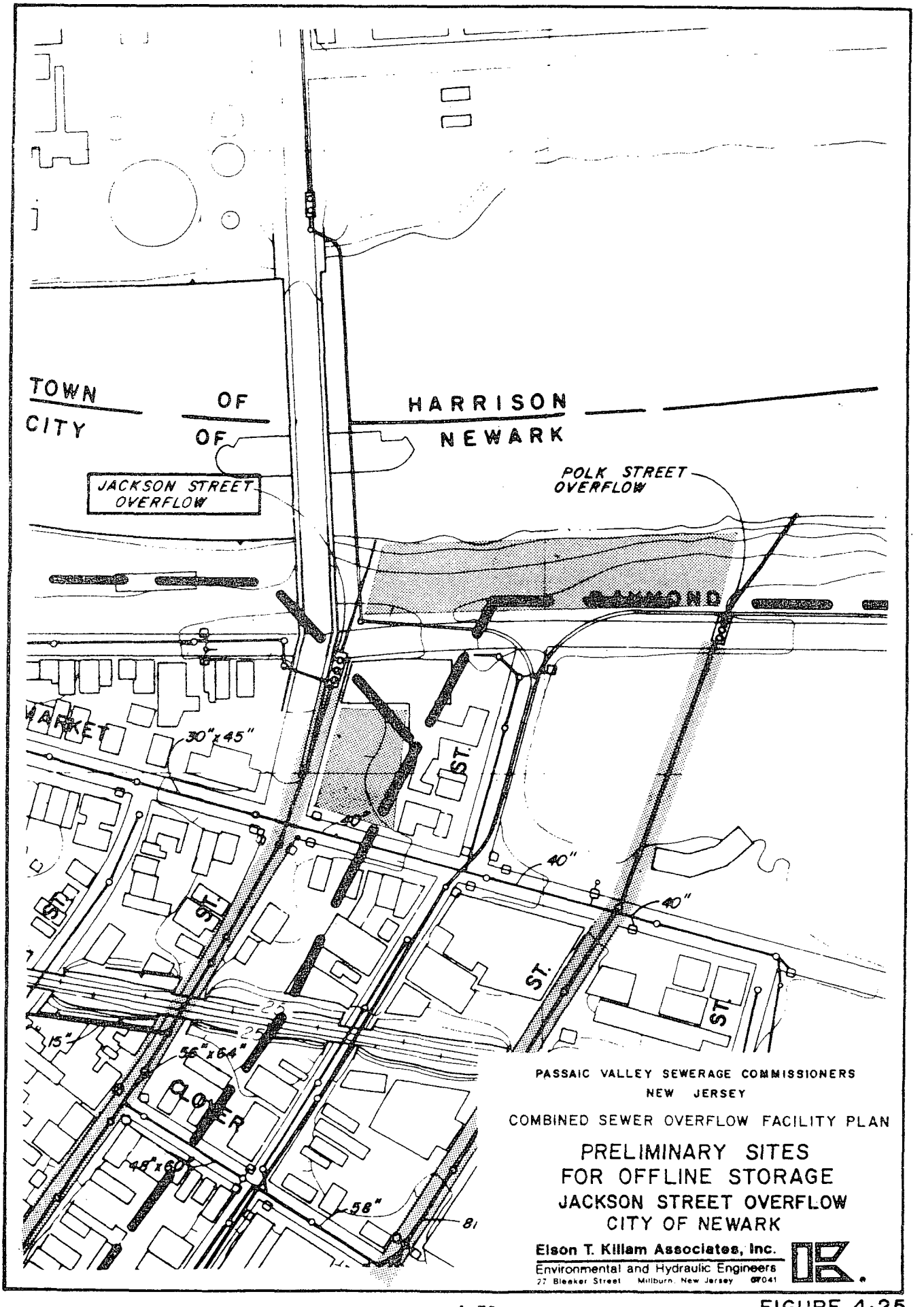

FIGURE 4·25

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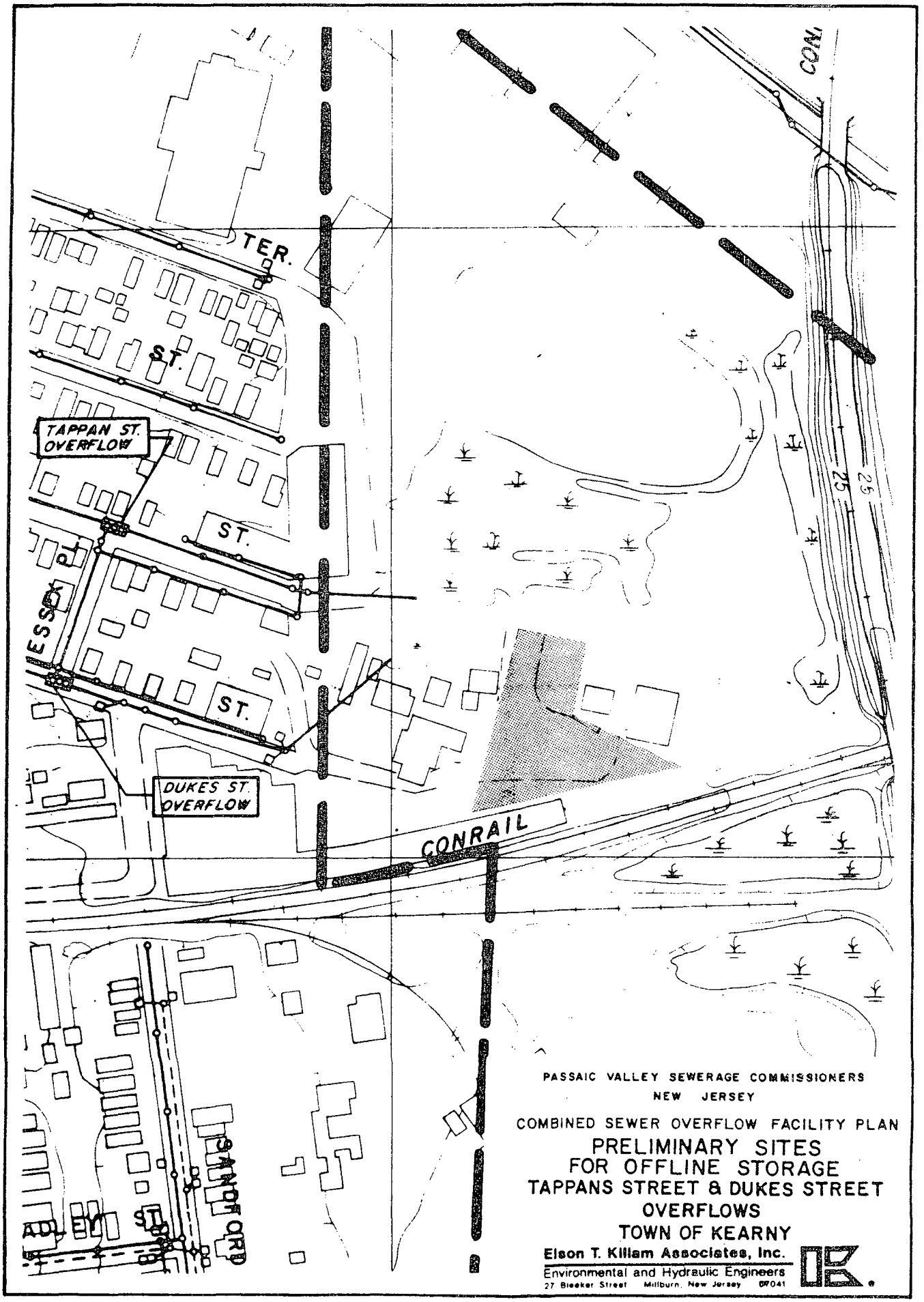

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

PRELIMINARY SITES
FOR OFFLINE STORAGE
TAPPANS STREET & DUKES STREET
OVERFLOWS
TOWN OF KEARNY

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FIGURE 4-26

946510200

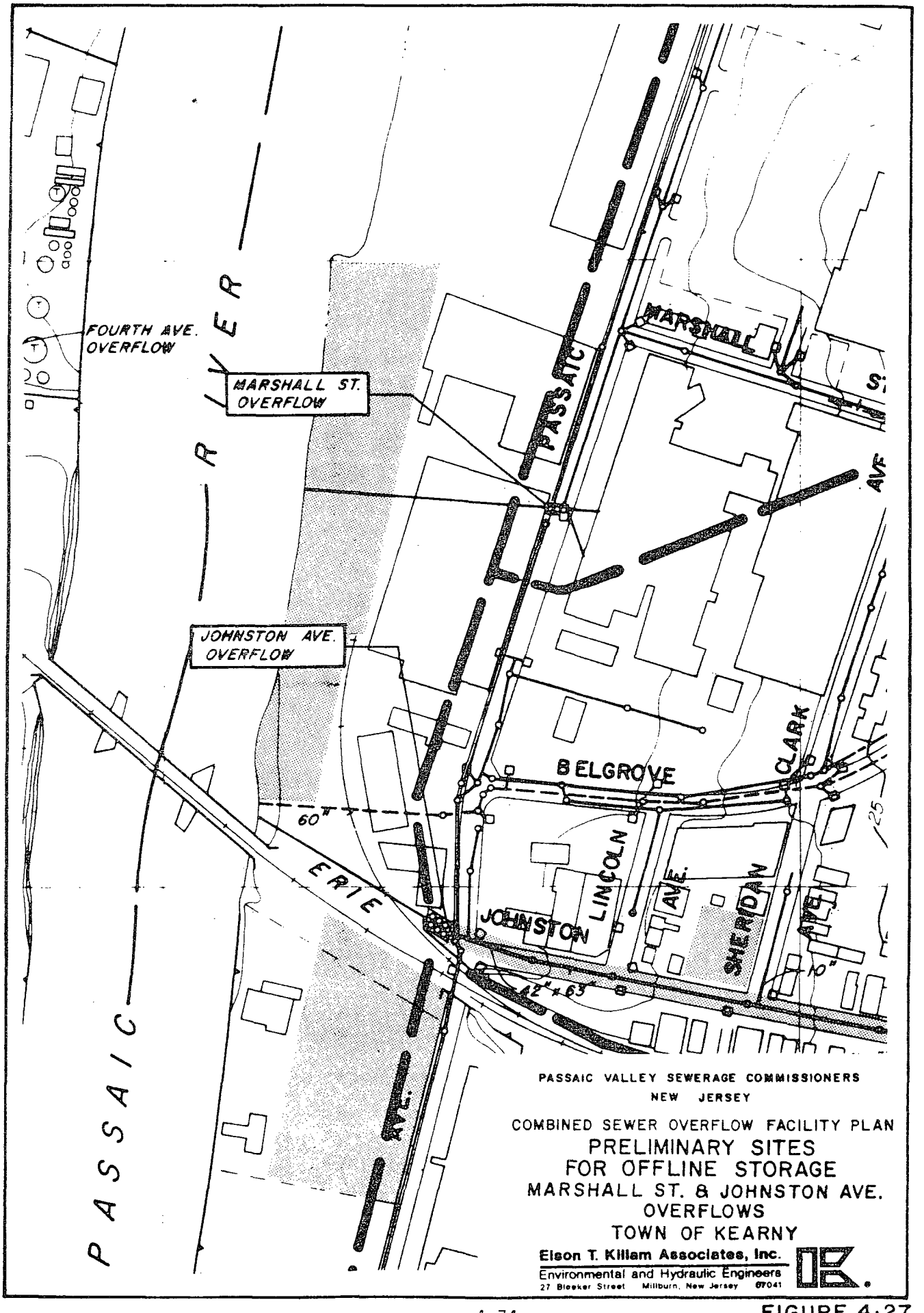

FIGURE 4-27

946510201

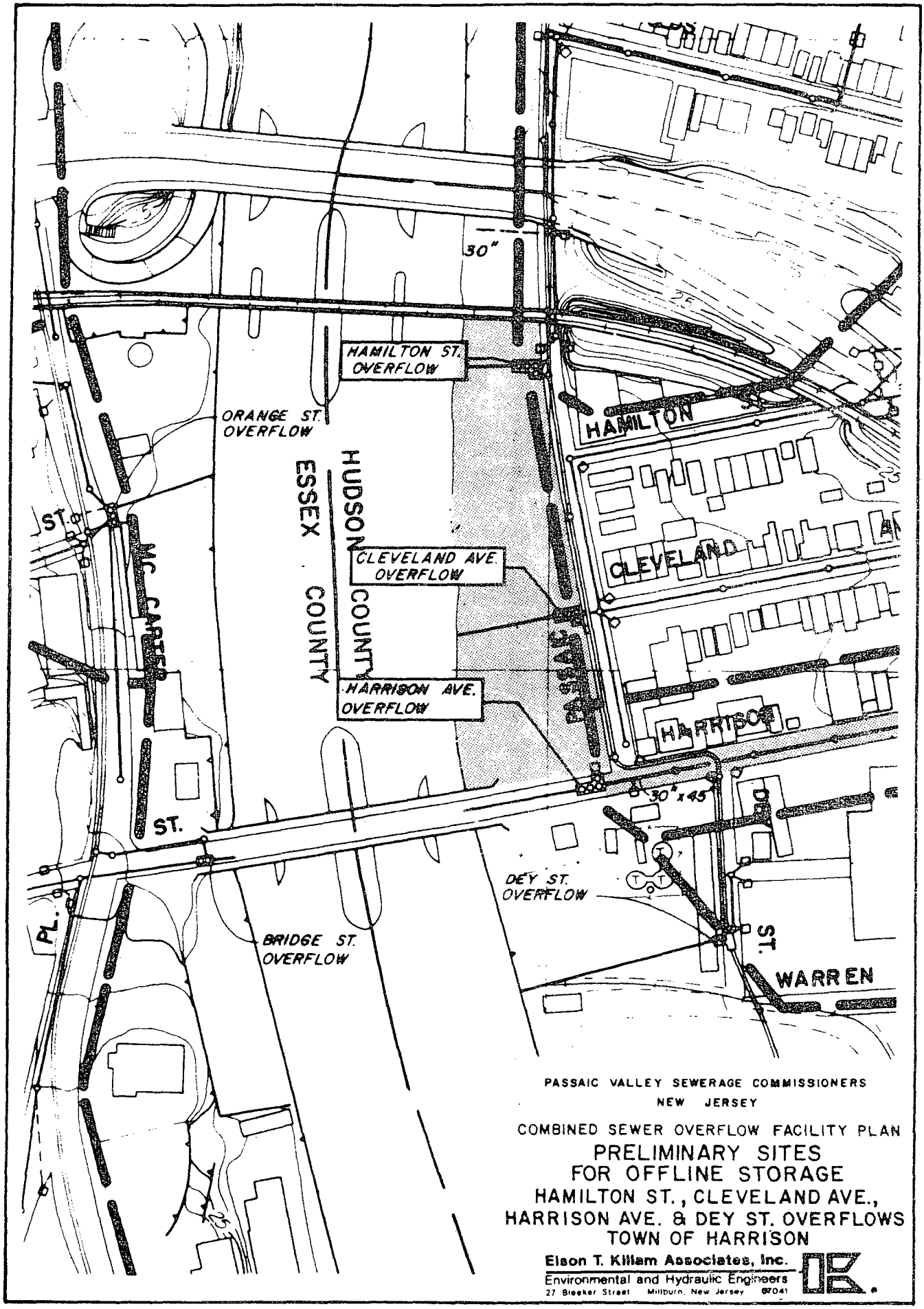

FIGURE 4·28

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All offline storage areas under consideration are at or near the existing overflow chambers with the exception of the 6.2 MG storage area for Clay Street. (Figure 4.22). A detailed modeling analysis in addition to some inline system modifications (control of split flows upstream) would be needed to provide reasonable control at this location. In addition, the control structure or diversion chamber would need to be correlated to the flow within the overflow chamber and would require computerized predictive capabilities and control to provide maximum potential.

g. Physical Treatment

Physical treatment control methods are primarily utilized for removal of settleable and suspended solids and floatable material. Physical treatment processes that have been utilized on a pilot or prototype scale include: dissolved floatation, sedimentation and chemical clarification, high rate filtration, magnetic separation and solid concentration and flow regulation. The principal disadvantage of these systems relates to the relatively long periods during which the equipment sits idle. For this reason, and because the modeling analysis has shown that CSO discharges are not significant in terms of water quality, most physical treatment alternatives have been eliminated from consideration.

Specific physical treatment alternatives have been analyzed as a means of improving the aesthetic quality of the lower Passaic River. Offline storage facilities discussed within the previous section can be considered a form of physical treatment. Sedimentation which occurs during detention periods would reduce the solids loading for storms exceeding the design capacity. In addition, storage facilities would include prescreening, removal of floatables, and disinfection, all of which are considered forms of physical treatment.

946510203

Swirl and Helical Bend Regulators

The Passaic Valley Sewerage Commissioners' overflow regulators within many of the areas under consideration, do not operate properly or do not operate at all. To provide greater control and flexibility within the system, all of the PVSC-CSO regulator chambers within the City of Newark have been recently reconstructed. It seems reasonable to believe that similar reconstruction of PVSC overflow chambers will be conducted within the other combined sewer areas as monies become available. The practice of designing regulators exclusively for flow control or diversion of excess flows to receiving waters should be reevaluated. If the Commissioners do undertake the reconstruction of existing CSO's, consideration should be given to the construction of new swirl or helical bend regulators where feasible.

Swirl and helical regulators provide for solid/liquid separation by secondary fluid motions attained by imparting a rotational motion to the flow. By introducing long path geometric flow patterns, inertial separation of liquids and solids is produced by centrifugal and other induced forces. These regulators can thus provide control of flow rates to the interceptor sewer while imparting solids removal prior to discharge of excess flows to the receiving waters.

The swirl regulator/separator for combined sewer overflows is an annular-shaped regulator which contains no moving parts (See Figure 4.29). Dry weather flows enter the chamber and travel along the floor gutter to the foul sewer. Under high flow storm conditions the rotary motion utilized within the regulator for solids concentration is induced by the kinetic energy of the incoming sewage. The concentrated flow is deflected and discharged through the foul sewer located at the bottom of the

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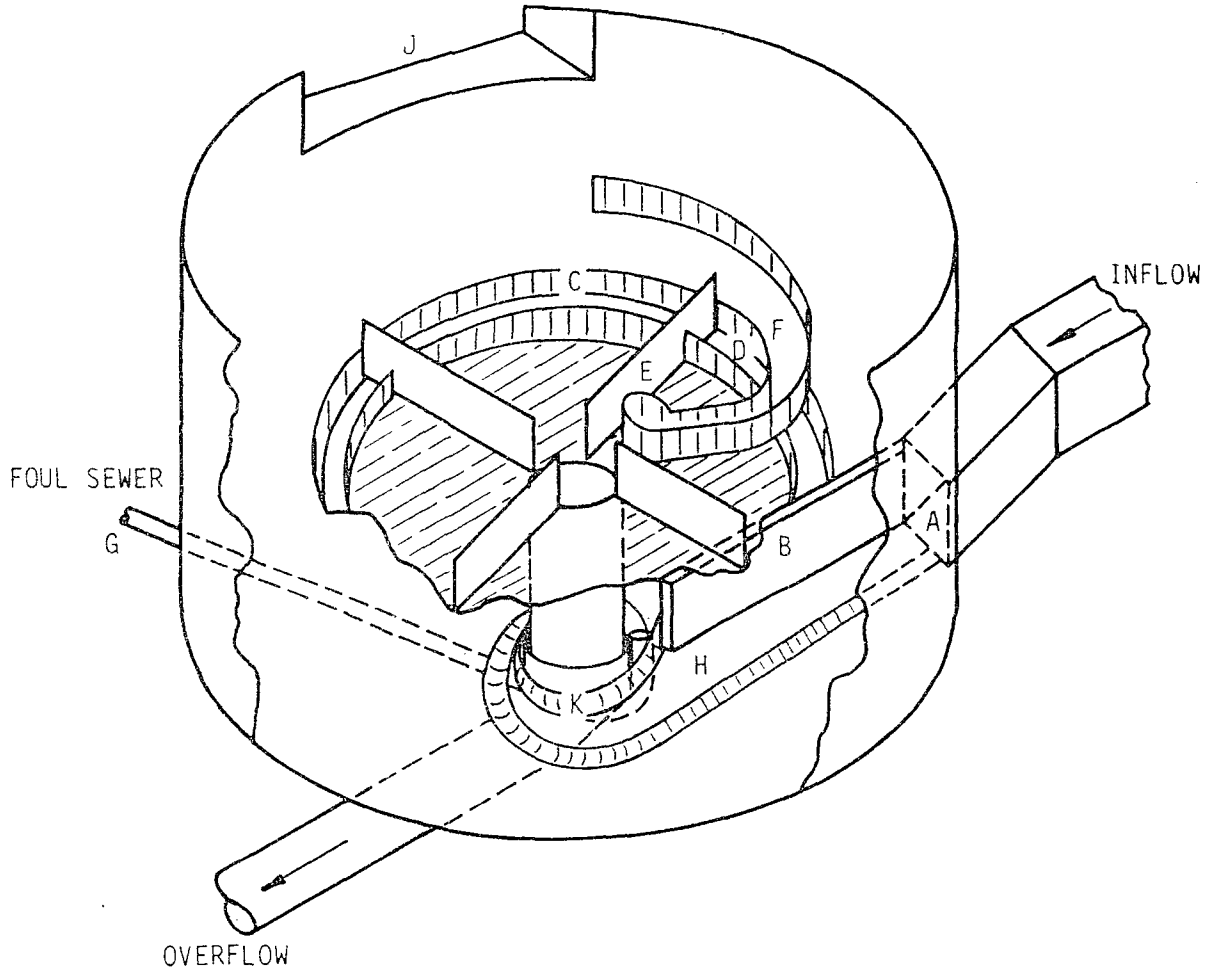

A INLET RAMP
B FLOW DEFLECTOR
C SCUM RING
D OVERFLOW WEIR AND WEIR PLATE
E SPOILERS
F FLOATABLES TRAP
G FOUL SEWER OUTLET
H FLOOR GUTTERS
I DOWNSHAFT
J SECONDARY OVERFLOW WEIR
K SECONDARY GUTTER

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

ISOMETRIC VIEW OF A SWIRL COMBINED SEWER OVERFLOW REGULATOR

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946510205

FIGURE 4-29

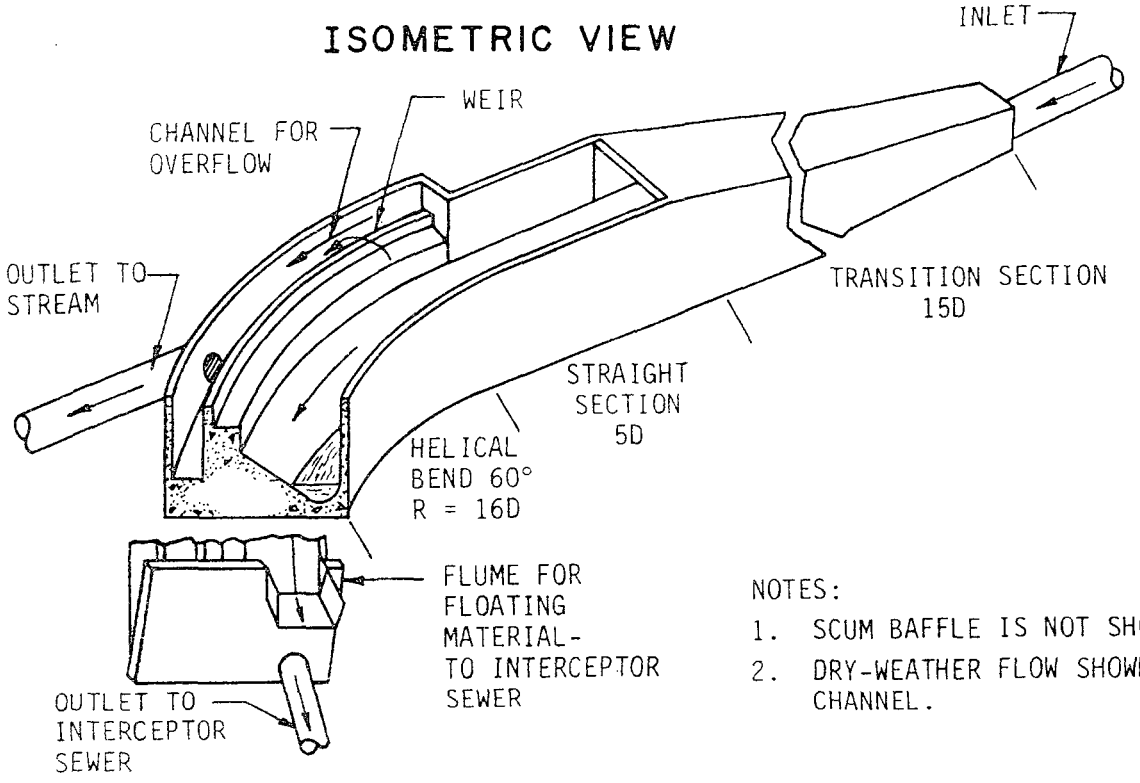
chamber. Excessive stormwater flows are discharged over a circular weir located at the center of the tank and are conveyed to offline storage or the receiving waters.

The concept behind the swirl is that the rotary motion causes combined flows introduced at the bottom to follow a long spiral path through the annular chambers. The flow deflector prevents the mixing of flow at the inlet and thus dissipates some energy and induces a gentle swirl. This causes water entering the chamber from the inlet to slow down and to diffuse with very little turbulence. Solids are spread over the full cross-section of the channel and settle rapidly. There they are entrained along the bottom channel and concentrated at the foul sewer orifice. Floatables are trapped by a surface flow deflector and directed to a vertical vortex cylinder where they are drawn down by the vortex and dispersed into the foul sewer. To prevent asymmetrical flow patterns within the unit, a secondary overflow weir is provided. This secondary weir is designed to help dissipate flows exceeding the design capacity of the unit.

The helical bend combined sewer overflow regulator consists of a curved channel which acts as a solids and floatable trap by developing helical secondary motions within the flow. The device which consists of an enlarged section of the sewer (Figure 4.30) has no mechanical or moving parts. The imparted helical motion is very effective in capturing particles which have a greater settling velocity than the upward velocity of the helical motion. The settled particles are removed by relatively high velocities achieved within the chamber at the end of the storm inlet. Thus most removed solids are held within the channel during overflow occurencies.

946510206

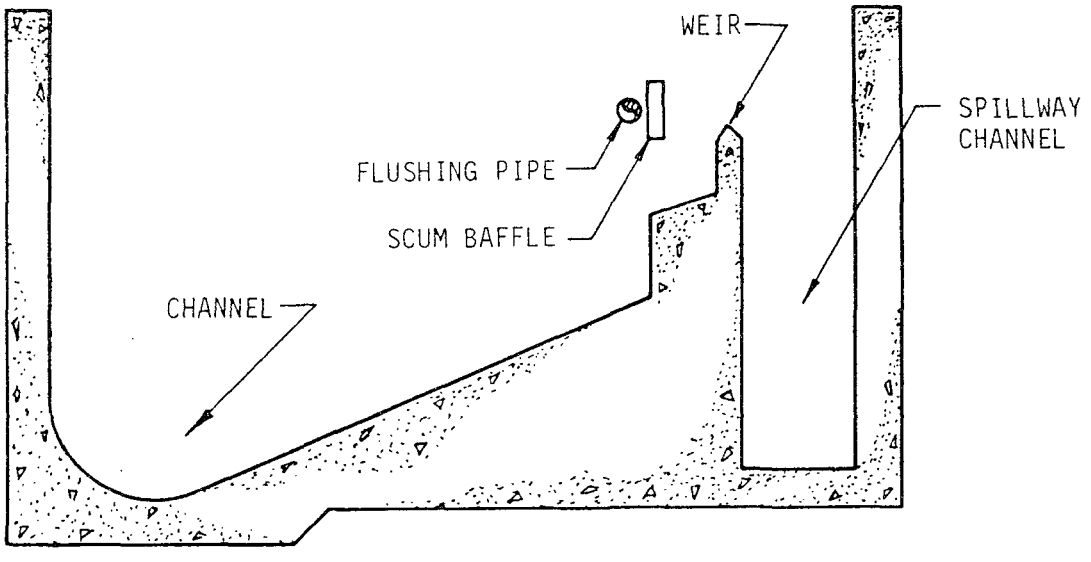
ISOMETRIC VIEW



NOTES:

1. SCUM BAFFLE IS NOT SHOWN.
2. DRY-WEATHER FLOW SHOWN IN CHANNEL.

CROSS-SECTIONAL VIEW



PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC

HELICAL BEND COMBINED SEWER OVERFLOW REGULATOR

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946510207

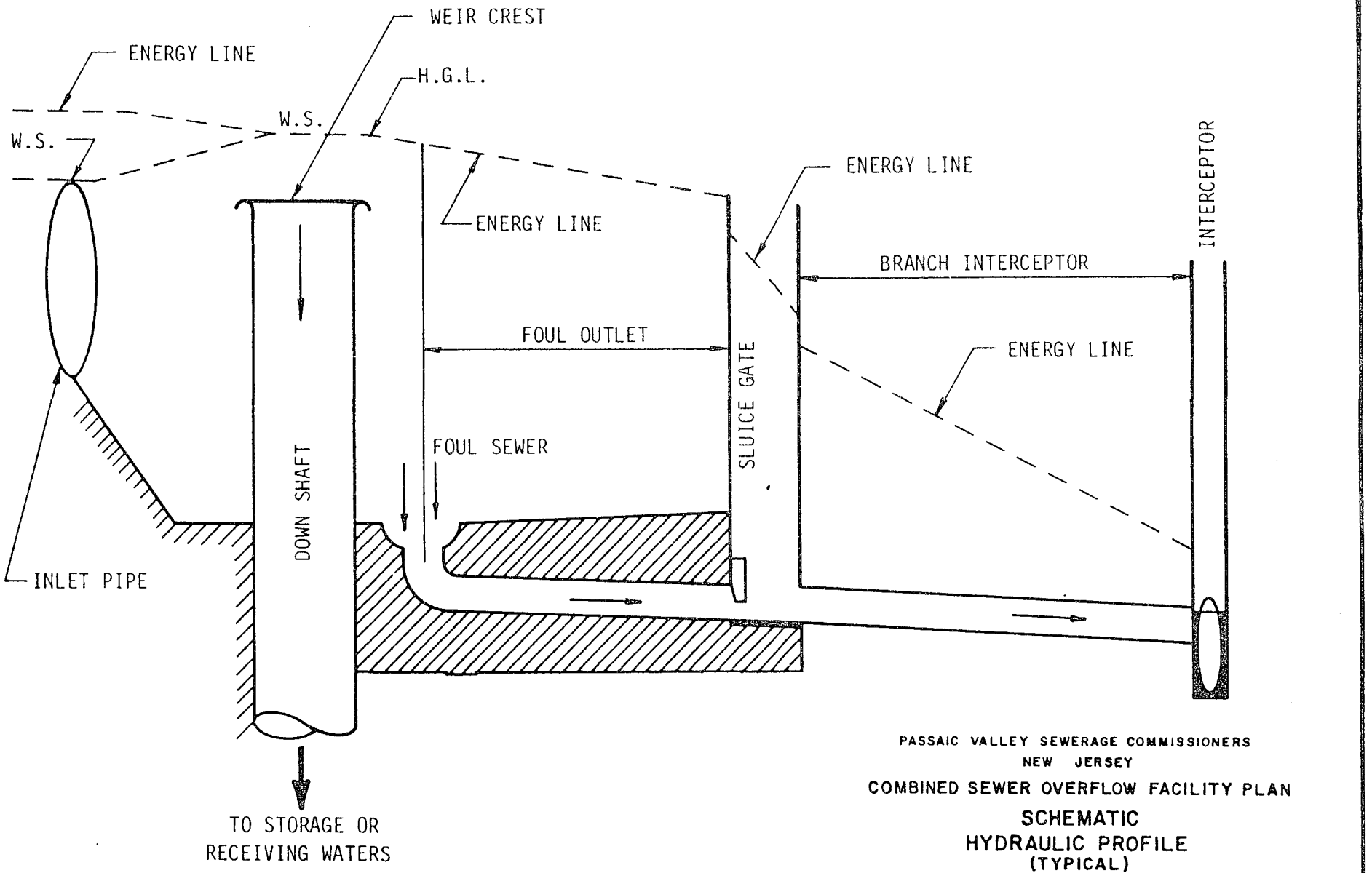
FIGURE 4-30

Major design restraints exist within both the swirl and helical bend regulators. The feasibility of a swirl regulator is largely dependent upon having sufficient available head between the combined sewer, the interceptor sewer, and the receiving waters. Sufficient head is required to compensate for the height of flow over the weir, the chamber depth, and losses due to outlet gates, the connecting sewer and the flow through the chamber. (See Figure 4.31). Economic restraints would eliminate from consideration any area wherein sufficient head is not available to operate the foul sewer by gravity.

Within the helical bend regulator the major design constraints are the available head and the considerable space required for construction. As illustrated on the isometric view of the helical regulator shown on Figure 4.30, the regulator consists of three distinctive parts: the transition section, the straight section, and the 60° helical bend section. The total length of the regulator is approximately equal to 37 times the inlet diameter which is a function of the design flow.

Each section of the helical bend regulator has a specific function and design length. The transition section which is 15 pipe diameters in length, is utilized to expand the width of the chamber to three times the inlet diameter and to improve flow lines within the section. The straight section, which is 5 pipe diameters in length allows for the development of a less turbulent flow field and provides for the development of the bottom cross-section. The 60° helical bend section, which has a radius of 16 pipe diameters uses the outside edge of the curve an an overflow weir and develops secondary forces which cause the liquid-solids separation within the section. To prevent loss of floatable solids, the overflow weir along the bend is baffled. The baffle traps floatable solids which are sub-

946510208



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC
HYDRAULIC PROFILE
(TYPICAL)
SWIRL COMBINED SEWER
OVERFLOW REGULATOR

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946510209

FIGURE 4-31

sequently discharged to the outlet pipe leading to the main interceptor sewer.

All major and several moderate CSO's with the exception of those within the City of Newark and those eliminated within section 4e, were analyzed for possible construction of the swirl or helical bend regulator. The City of Newark was not included within this analysis for two reasons. First, the Passaic Valley Sewerage Commissioners have recently reconstructed all of their overflow chambers within the City of Newark, and secondly, because all CSO's within the City of Newark are tidal influenced and as such would not provide sufficient head for utilization of either of these regulators. Design parameters utilized within the initial screening of these regulators were the total head requirements of the respective regulator and the total land/space available for construction.

The initial step in the screening process was to determine the design flow rate and the amount of suspended solids to be removed. Both of these considerations influence the size of the unit. In general, larger units provide a higher degree of treatment, especially at flow rates less than design flow. However, the hydraulic and site requirements are also directly related to these parameters and as such must be considered in the selection process.

All sites were evaluated for 90% removal or separation of settleable solids of a "typical" mixture of combined sewage. Design flow rate were established utilizing a statistical analysis of area rainfall and existing data from both the 1974 Overflow Analysis and currently monitoring. A return period of 6 months for peak intensity was initally utilized to determine the design flow rate for the regulator chamber. If system restrictions existed upstream of the chamber, the design flow rate was modified to pass the maximum flow anticipated.

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A statistical analysis of rainfall records over the past 30 years has shown that the chosen values of 0.26"/hr. for the City of Paterson and 0.30"/hr. for the City of Newark (and surrounding areas) are both 98 percentile storm intensities. That is, less than 2% of all hourly storm intensities recorded over the previous 30 year period were equal to or greater than these values. This means that the amount of time the flow rate will exceed the design flow will be approximately 14 hours per year. A secondary analysis was conducted to assure that intensities beyond those chosen could be sufficiently handled through the regulator without causing significant problems upstream.

Once the design flow rate was determined each CSO site was evaluated for sufficient head, available construction sites and any other restrictions which may affect construction or proper utilization of the regulator. Typical head loss formulas established through modeling analysis were utilized within the initial screening. In general, a helical bend regulator would cost approximately 2.5-3.0 times the cost of an equivalent swirl regulator. Therefore, each site was initially evaluated for the swirl regulator prior to consideration of the helical bend unit.

The results of the initial screening process are summarized on Table 4.10, Results of Initial Feasibility Screening for Helical Bend and Swirl Regulators. In all only seven CSO sites passed for either unit; with four of the seven having possible site restrictions due to available construction area being less than that recommended. Most sites which failed did so because of insufficient head between the regulator and the PVSC trunk sewer. Initially each site was evaluated for construction of the regulator at the existing overflow chamber; however, most areas

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TABLE 4.10
RESULTS OF INITIAL FEASIBILITY SCREENING
FOR HELICAL BEND & SWIRL REGULATORS

OVERFLOW DESCRIPTION LOCATION	APPROXIMATE DRAINAGE AREA (ACRES)	RECORDED PEAK OVERFLOW TO RIVER (CFS)	INITIAL SCREENING RESULTS SWIRL REGULATOR ANALYSIS	INITIAL SCREENING RESULTS HELICAL BEND REGULATOR ANALYSIS	DESIGN FLOW (CFS)	COMMENTS
Paterson						
Market St.	1500	146	Passed	Insufficient space	150	Possible site restrictions
Curtis Place	970	36	Insufficient head	Insufficient head	-	
10th Ave. & 33rd St.	700	142	Passed	Insufficient space	100	
Montgomery St.	670	68	Insufficient head	Insufficient head	-	
Hudson St.	450	28	Insufficient space	Insufficient space	-	
Northwest St.	280	140	Insufficient head	Passed	70	
Straight St.	120	88	Insufficient head	Passed	40	Possible site restrictions
E. 11th St.	105	70	Passed	Insufficient space	40	Possible site restrictions
Warren St.	80	17	Passed	Passed	40	
Arch St.	32	15	Insufficient head	Insufficient space	-	
Newark	NO SITES CONSIDERED DUE TO RECENT RECONSTRUCTION & TIDAL INFLUENCE					
Kearny						
Ivy St.	610	378	Insufficient head	Insufficient head	-	
Johnston St.	210	352	Insufficient head	Insufficient head	-	Tidal influence
Nairn Ave.	175	5			-	Insignificant overflow volume
Bergen Ave. (East)	110	45	Insufficient head	Passed	20	Possible site restrictions
Washington Ave.	37	8			-	Insignificant overflow volume
Tappan St.	35	14	System restrictions	System restrictions	-	Insufficient trunk capacity
Dukes St.	25	9	System restrictions	System restrictions	-	Insufficient trunk capacity
Marshall St.	25	8	Insufficient head	Insufficient head	-	Tidal influence
Bergan Ave. (West)	10	3				Insignificant overflow volume
Harrison						
Harrison Ave.	65	30	Insufficient head	Insufficient head	-	Tidal influence
Middlesex St.	60	20	Insufficient head	Insufficient head	-	Tidal influence
Bergan St.	70	26	Insufficient head	Insufficient head	-	Tidal influence

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required that the new units be constructed on adjacent vacant areas to provide sufficient area and minimal piping changes.

Each of the seven CSO's which passed the initial screening were subsequently evaluated in detail through a preliminary design procedure. Utilizing available information, each unit was designed for peak dry-weather flow, design flow, and the maximum flow likely to occur within the chamber. Each unit was sized to provide the desired removal efficiencies and design flow rate and analyzed for head losses and hydraulic requirements. If system restrictions developed, alternative designs were considered and evaluated. All CSO's were evaluated to the degree necessary to establish the feasibility of the appropriate regulator unit based upon currently available information.

The results of the secondary screening process are summarized on Table 4.11, Results of Feasibility Screening for Helical Bend and Swirl Regulators. Four of the seven sites appear to be feasible for the swirl or helical bend regulators. It must be remembered that the overall impact of these units upon the aesthetic quality of the Passaic River must be determined within the next Phase of the Facility Plan. Only then can a economic analysis determine whether the units are cost-effective. In addition, detailed site investigations must be completed to assess utilities and other site factors which may impact construction. Easement rights will need to be obtained within several areas since two of the new regulators would be located within private domain.

The four sites which passed the feasibility screening are:

City of Paterson - Straight Street
E. 11th Street
Warren Street
Town of Kearny - Bergan Ave. (East)

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TABLE 4.11
RESULTS OF FEASIBILITY SCREENING FOR
HELICAL BEND AND SWIRL REGULATORS

OVERFLOW DESCRIPTION LOCATION	DESIGN FLOW (CFS)	UNIT UNDER CONSIDERATION	RESULTS	CONCLUSIONS
Paterson				
Market Street	150	Swirl	When regulator was designed to meet existing combined sewer sufficient head was not available to allow discharge of 300 CGS to the River.	Unit not feasible
10th Ave. & 33rd St.	100	Swirl	When regulator was designed to meet existing combined sewer sufficient head was not available to allow discharge of 200 CFS to the River.	Unit not feasible.
E. 11th Street	40	Swirl	Sufficient head is available for both the swirl and outfall flow rates. Potential problems include deep excavation for both swirl and trunk connections.	Swirl appears feasible. Proceed with detailed analysis and final design if cost-effective.
Warren Street	40	Swirl	Sufficient head is available for both the swirl and outfall flowrates.	Swirl appears feasible. Proceed with detailed analysis and final design if cost-effective.
Straight Street	40	Helical bend	Sufficient head is available. Potential problems include construction within major intersection and possible problems upstream due to hydraulic grade.	Helical bend appears feasible. Proceed with detailed modeling analysis to determine if any restrictions exist upstream. Proceed with detailed analysis and final design if cost-effective.
Northwest	70	Helical bend	Detailed analysis showed hydraulic grade requirements too great for site.	Unit not feasible.
Kearny				
Bergan Ave. (East)	40	Helical bend	Sufficient head is available. Possible site restrictions due due to location.	Helical bend appears feasible. Proceed with detailed analysis and final design if cost-effective.

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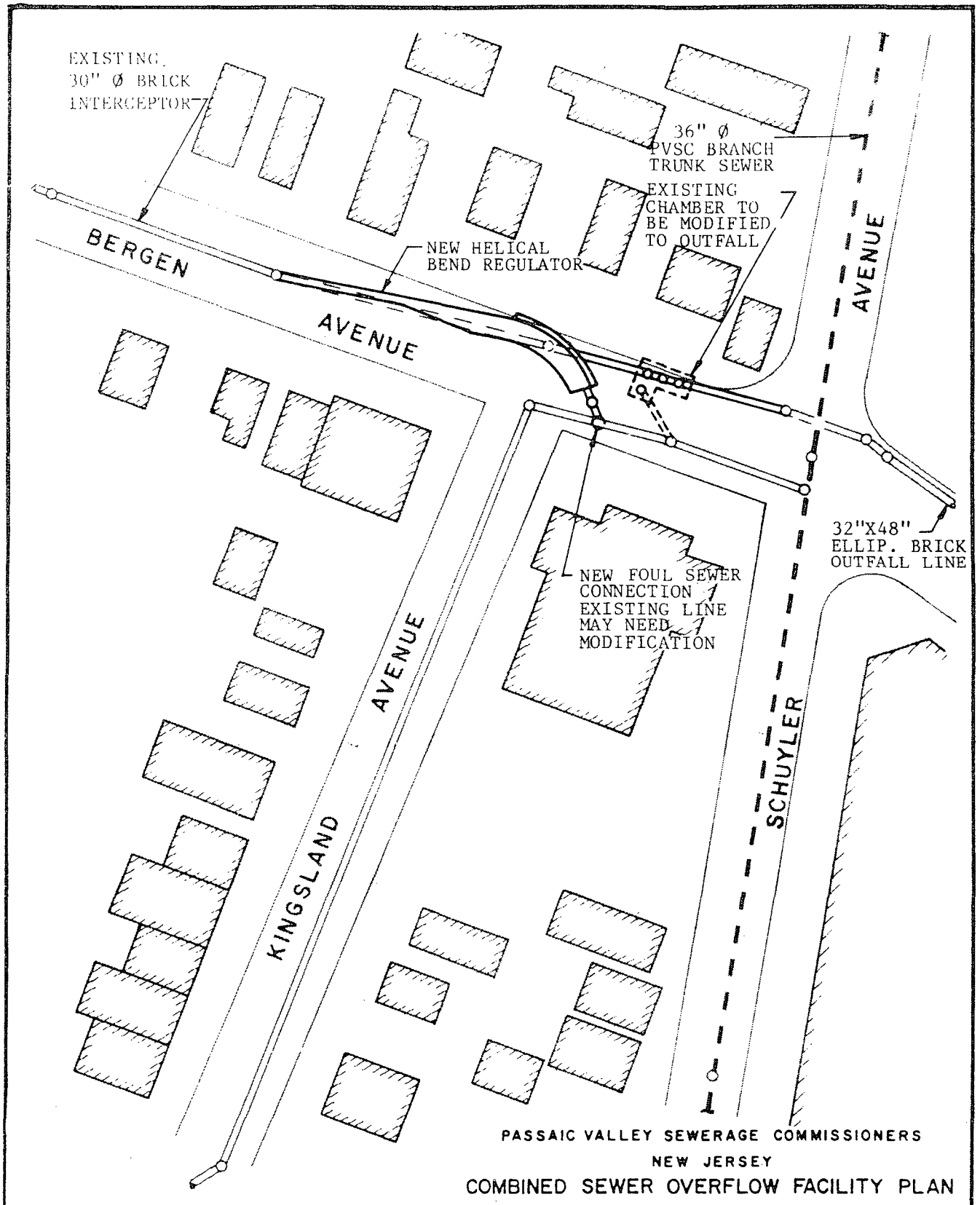

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC

HELICAL BEND REGULATOR

BERGEN AVE. (EAST) OVERFLOW

TOWN OF KEARNY

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

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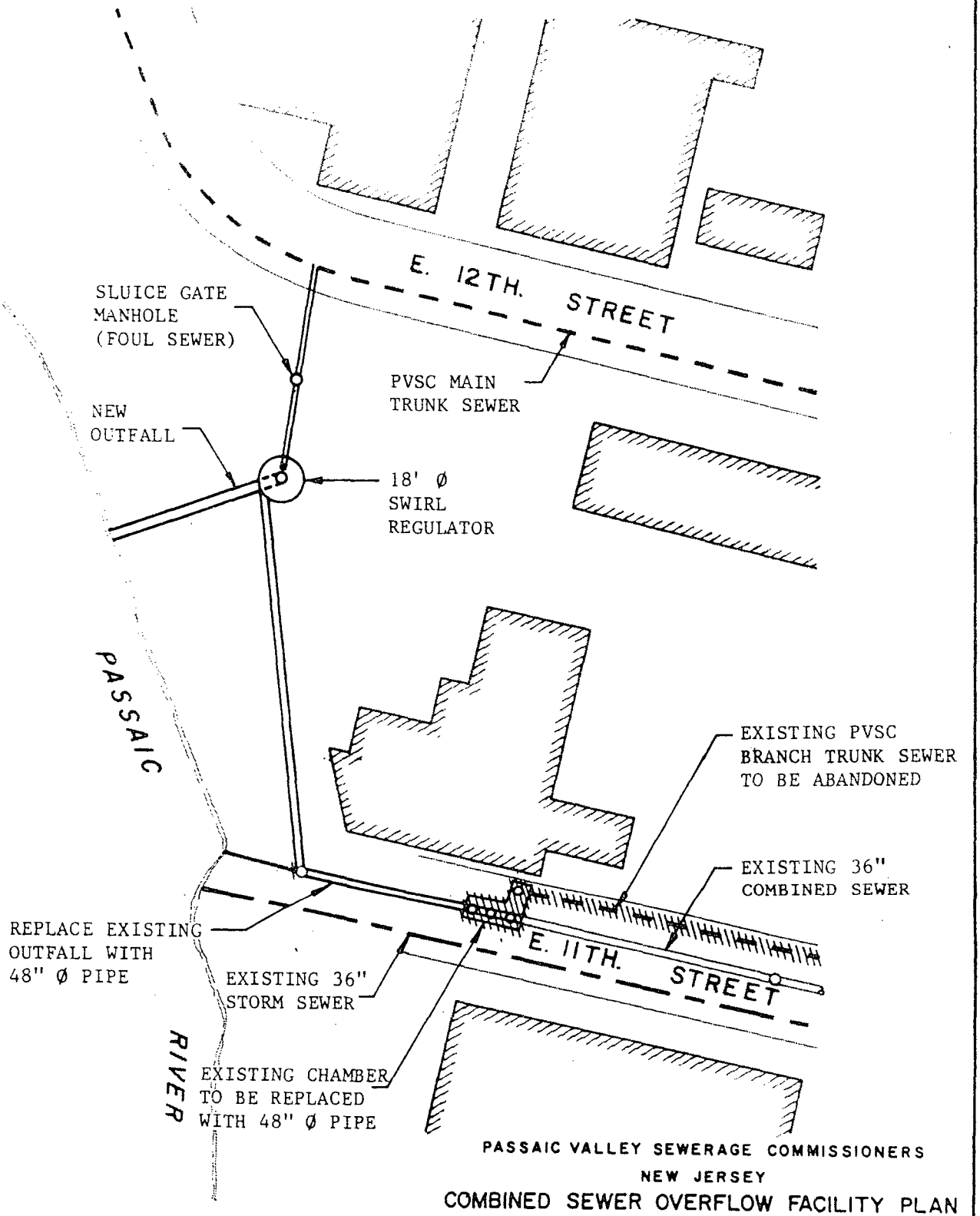
FIGURE 4·32



PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC SWIRL REGULATOR E. 11TH. ST. OVERFLOW CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

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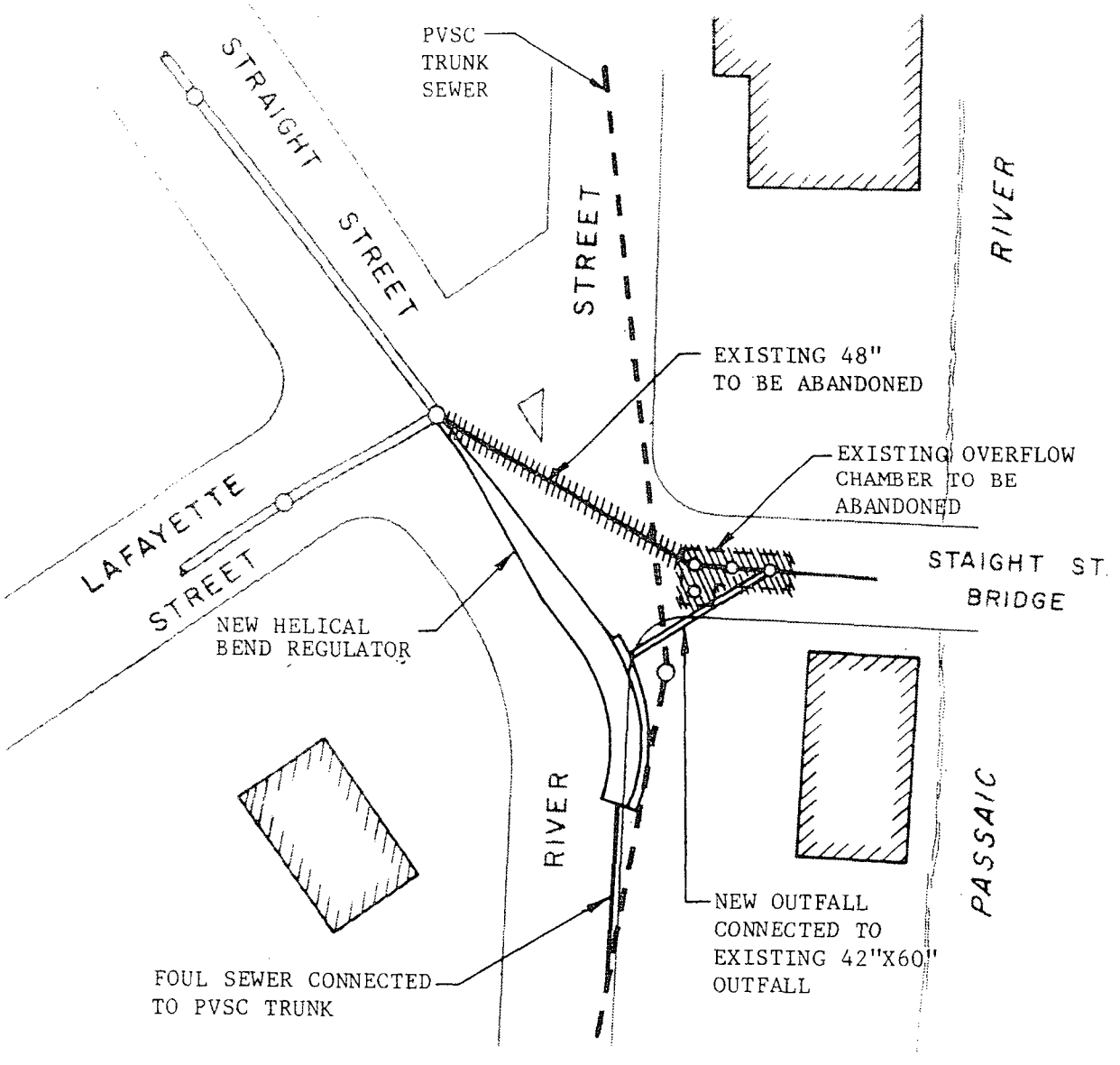
FIGURE 4-33



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PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC
HELICAL BEND REGULATOR
STRAIGHT ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

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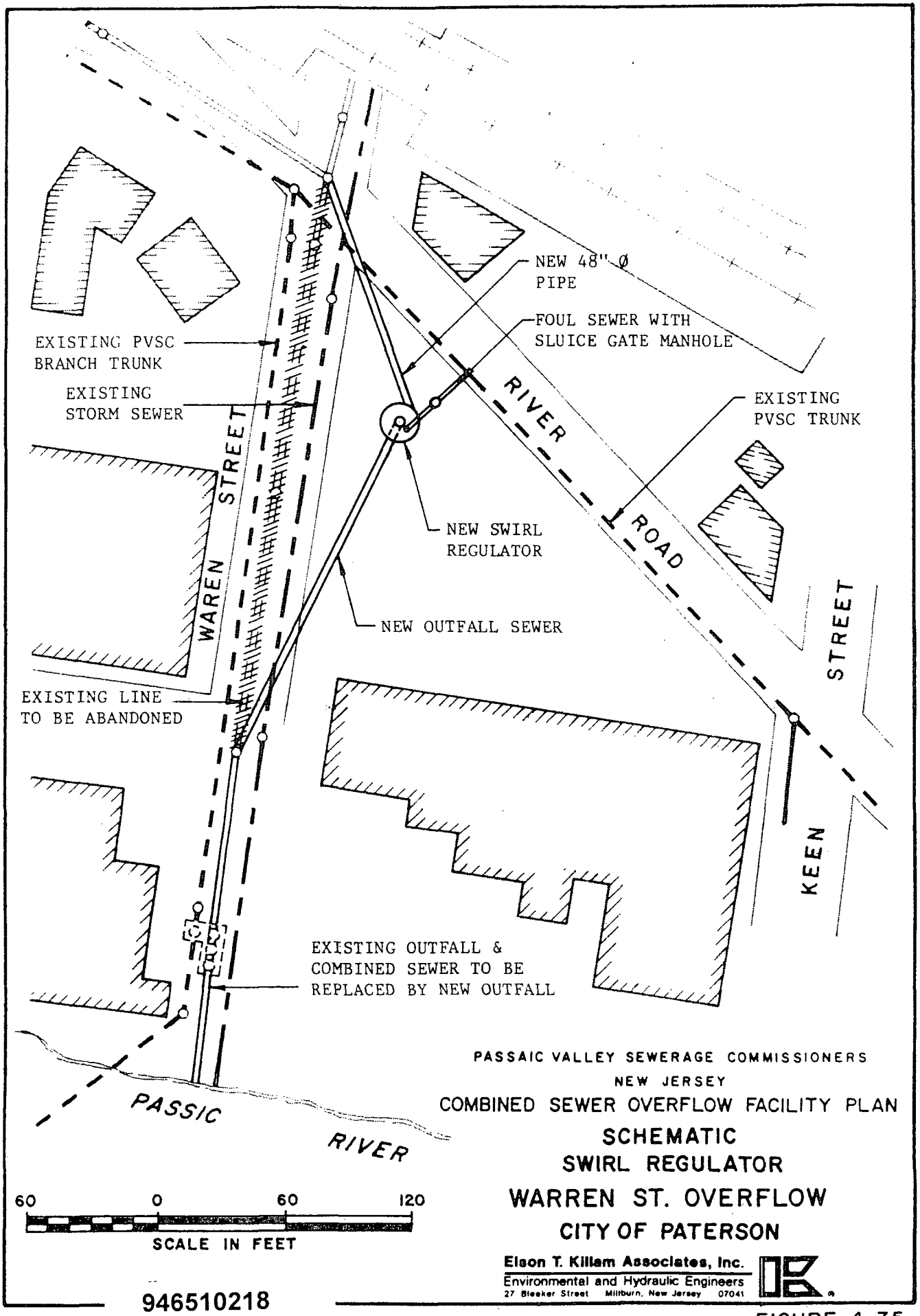
FIGURE 4-34



PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC
SWIRL REGULATOR
WARREN ST. OVERFLOW
CITY OF PATERSON

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

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FIGURE 4-35

The feasibility of each site was based upon available information and as such would need to be reevaluated once site specific information is obtained. The four sites are illustrated in Figures 4.32 to 4.35. Each figure shows the general area of construction in addition to the estimated layout of inlet and outlet piping. Preliminary cost estimates indicate that each swirl would cost approximately $340,000 per site while the helical bend units would cost approximately $568,000 per site (ENR4100). These costs are based upon other units constructed within recent years and are all based upon a 40 CFS Design Flow.

Coarse Screening

The primary reason for the consideration of physical treatment within CSO drainage areas is the need to improve the aesthetic quality of the lower Passaic River. Storm systems within both combined and separate sewered areas become depositories for all variations of solid waste through natural and man-made contributions. This material may become suspended and flushed out of the system during significant rainfalls thereby adding to the solids pollutional load discharged to the river. It is desirable to remove, at a minimum, the coarse solids and floatable material so as not to degrade the aesthetic quality of the receiving waters. This removal would probably be required not only within combined sewer areas but also within separate storm sewers in order to be an effective mechanism for solids removal and aesthetic improvement.

A preliminary analysis for the feasibility of coarse solids removal was conducted for all CSOs within the PVSC service district. Separate storm sewer systems were not included in that analysis due to a lack of background data in these areas. The initial screening process was conducted on the hydraulic head and space requirements of a screening

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facility as well as adequate potential for the use of this facility.

With the exception of static screens, operational and control problems associated with screening have been experienced at most demonstration facilities. Mechanical problems have been experienced with drum screens and microstrainers in addition to screen blinding due to oil and grease buildup and biological growth on the screen panels. Rotary screens were unacceptable in several installations due to limited screen life, solids breakup and backwashing requirements. The operational and maintenance requirements of most screening methods, as determined through these demonstrative projects, would make them undesirable for use within the PVSC service district.

One method of screening which has been found, during pilot projects, to be an effective means for the removal of coarse solid debris is the Bauer Hydrosieve (registered trademark). The Bauer unit is a fixed, vertical side hill hydraulic sieve which produces a semi-dry solid residue that can be easily removed for disposal. As with all screening methods the pollutant removal rate for suspended solids, BOD, COD and nutrients has been found to be minimal, however the Bauer unit makes an excellent screening device for the removal of solid debris such as wood pieces, metals, plastics, leaves and twigs. These units do have hydraulic limitations and are therefore limited in their potential use without pumping.

The hydraulic head requirements of the Bauer unit (7 feet) has eliminated its utilization within the PVSC District. Analysis of all CSOs has indicated that only four CSO areas had sufficient hydraulic head available: Keen Street, Warren Street, E. 11th Street, and S.U.M. Park, all of which are located within the City of Paterson. Two of these CSOs

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(Keen Street and S.U.M. Park) have infrequent and/or low volume overflows which would not warrant the expense associated with physical treatment while the other two are sites feasible for swirl regulators. It is estimated that the cost associated within a swirl regulator would be approximately half the cost of the Bauer hydrosieve of equal capacity and as such would be more cost-effective (The Bauer Hydrosieve unit costs approximately $80,000 per 10 MGD capacity not including construction or installation).

Although not as effective for solids removal, a mechanically cleaned bar screen would be capable of removal large coarse solids and floatables from outfalls prior to discharge. Design parameters for such a screening facility present special problems and restrictions which must be considered. Normally screening facilities are designed for known flow rates within a fairly narrow flow range. Within the overflow chambers, the experienced flow rate fluctuates considerably depending upon the rainfall intensity.

Outfalls for most of the CSOs have theoretical flow velocities in the eight to ten feet per second (FPS) range. In order to adequately treat or provide for solids removal the maximum velocities through the screen should fall within the 3-4 FPS range. It is therefore necessary to increase the cross-sectional area through the screening chamber to decrease the velocity to acceptable limits. One problem with decreasing the velocity within the channel is that scour velocity (>2 FPS) will not be obtained until significant flow is provided. Decreased velocities through the screening channel could prove inadequate during intense storm periods thereby resulting in possible sewer backups upstream. These considerations have been evaluated and have been adequately provided for within the preliminary design for such a screening facility.

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Figure 4.36 illustrates a typical screening chamber utilized within the analysis. Each chamber, where feasible, would consist of two or three mechanical screening units set on a step channel pattern. That is, each channel would be set at an elevation that would insure scour velocity within one channel prior to the flow being diverted to the subsequent channel(s). Velocities through the screens would be in the 4-5 FPS range at maximum flow rates assuring adequate removal rates. Emergency flow relief would be provided during extreme storm periods by a side weir overflow and an automatically operated sluice gate. These provisions would assure that problems associated with extremely intense storm periods and/or mechanical failure of the screen would not impact upstream areas.

Each mechanical bar screen would be protected from damage by large objects by the utilization of a trash rack. The trash rack could be of a mechanical or manual cleaning mode and would be located just upstream of each bar screen. Handling and disposal of screenings would be accomplished automatically wherever feasible. Screenings would be shredded and directed to the PVSC-Trunk system or would be stored for manual pickup. Special facilities would be required for stored material to minimize odor problems within the surrounding areas.

An initial feasibility analysis on static screening has been completed on all CSOs within the PVSC district and is summarized on Table 4.12, Results of Initial Feasibility Analysis For Screening by Mechanical Bar Screens. The investigation was conducted to determine which CSOs required a detailed analysis and was based upon space (both horizontal and vertical) considerations, hydraulic restrictions, and adequate overflow volume and frequency to warrant the facility.

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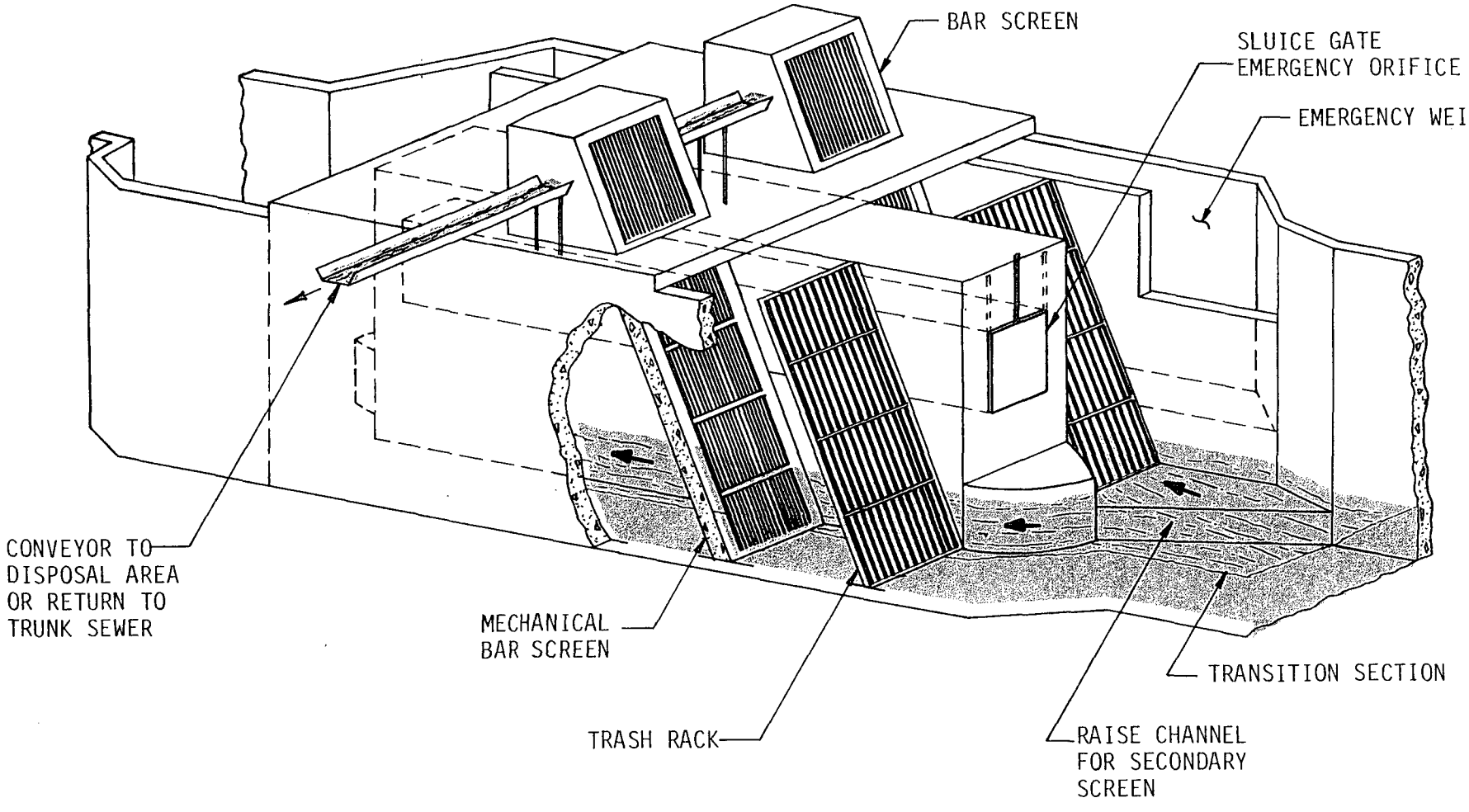

PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

ISOMETRIC VIEW OF A COARSE SCREENING FACILITY (TYPICAL)

Elson T. Killam Associates, Inc.
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946510223

FIGURE 4·36

TABLE 4.12
RESULTS OF INITIAL FEASIBILITY ANALYSIS
FOR COARSE SCREENING WITH MECHANICAL BAR SCREENS

MAJOR OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	INADEQUATE SPACE	INSUFFICIENT OVERFLOW VOL/FREQ.	REQUIRES ADDITIONAL ANALYSIS
Clay St. - Newark	X		
Market St. - Paterson	X		
Curtis Pl. - Paterson	X		
10th Ave. & 33rd St.-Paterson	X		
Montgomery St. - Paterson	X		
Ivy St. - Kearny	X		
Hudson St. - Paterson (1)			X
City Dock - Newark	X		
Verona Ave. - Newark			X
Saybrook Pl. - Newark			X
Herbert Pl. - Newark			X
Northwest St. - Paterson	X		
Johnston Ave. - Kearny			X

MODERATE OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	INADEQUATE SPACE	INSUFFICIENT OVERFLOW VOL/FREQ.	REQUIRES ADDITIONAL ANALYSIS
Fourth Ave. - Newark	X		
Polk St. - Newark			X
Rector St. - Newark	X		
Worthington Ave - Harrison	X	X	
Wairn Ave. - Kearny		X	
Freeman St. - Newark			X
Straight St. - Paterson	X		
Bergen Ave. - Kearny	X	X	
E. 11th St. - Paterson	X		
20th Ave. - Paterson	X	X	
Delavan Ave. - Newark		X	
Jackson St. - Newark	X		
Warren St. - Paterson	X		
Third Ave. - Paterson	X		
Bergen St. - Harrison		X	
Harrison Ave. - Harrison	X		
Bridge St. - Paterson		X	
Middlesex St. - Harrison		X	
Sixth Ave. - Paterson	X	X	
S.U.M. Park - Paterson		X	
Second Ave. - Paterson		X	

MINOR OVERFLOWS

OVERFLOW DESCRIPTION LOCATION/MUNICIPALITY	INADEQUATE SPACE	INSUFFICIENT OVERFLOW VOL/FREQ.	REQUIRES ADDITIONAL ANALYSIS
Washington Ave. - Kearny		X	
Tappan St. - Kearny	X		
Stewart Ave. - Kearny		X	
Arch St. - Paterson	X		
Short St. - Paterson		X	
Hamilton St. - Harrison		X	
Passaic St. - Newark	X	X	
Central Ave. - East Newark	X	X	
Dukes St.- Kearny	X		
Marshall St. - Kearny		X	
12th St. & 4th Ave. - Paterson		X	
Orange St. - Newark	X	X	
Bergen Ave. - Kearny		X	
Cleveland Ave. - Harrison		X	
Keen St. - Paterson		X	
Bergen St. - Paterson	X	X	
Bridge St. - Newark	X	X	
E. 5th St. & 5th Ave. - Paterson		X	
Third Ave. - Newark		X	
West Broadway - Paterson	X	X	
Dey St. - Harrison		X	
Mulberry St. - Paterson	X	X	
Bank St. - Paterson	X	X	
Franklin St. - Paterson		X	

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The analysis showed that 27 of the 58 active PVSC-CSOs have sufficient space (both horizontal and vertical) for construction of the screening chamber. Further consideration showed however, that only 7 of the 27 sites had sufficient overflow volume and frequency to warrant construction. Those CSO areas which were eliminated from further consideration due to inadequate space availability were either too shallow or too close to the river. Although CSO sites located within existing roadways were considered, only those sites with sufficient easements along the river were deemed feasible. Operating mechanisms for automatic cleaning of the racks require considerable vertical space and as such were feasible only where above ground construction was possible. In addition, velocities through the screening mechanism must be maintained in the 2-4 FPS range necessitating a much greater horizontal cross-section than is presently available. Transitional sections which would provide for the controlled change in cross-section and velocity were in cases greater than the available area between the present regulator chamber and outfall. In these areas the overflow was eliminated from any further investigation.

The seven CSOs which passed the initial analysis for coarse screening were:

Hudson Street, Paterson
Verona Avenue, Newark
Saybrook Place, Newark
Herbert Place, Newark
Polk Street, Newark
Freeman Street, Newark
Johnson Avenue, Kearny

All seven locations require above ground construction within existing easements. Table 4.13, Preliminary Coarse Screening Analysis indicates the locations, the projected number and size of the screening units, and the estimated Construction Costs including construction of the screening chambers and installation of each unit and control mechanisms.

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TABLE 4.13
PRELIMINARY COARSE SCREENING ANALYSIS

OVERFLOW DESCRIPTION/LOCATION	NO. SCREENS REQUIRED	SCREEN SIZE (FT)	ESTIMATED CONSTRUCTION COST*
Hudson Street-Paterson	1	3.5	115,000
Verona Avenue-Newark	2	2.0	255,000
Saybrook Place-Newark	2	3.0	319,000
Herbert Place-Newark	2	2.0	337,000
Polk Street-Newark	3	3.0	494,000
Freeman Street-Newark	2	2.0	231,000
Johnston Avenue-Kearny	2	8.0	445,000
TOTAL			$2,196,000

(*) ENR-4100

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The cost-effectiveness and the cost to benefit ratio cannot be determined for these units without additional sampling and a new modeling analysis. Solids transport was not considered within the initial modeling and as such, the existing model must be expanded. Detailed information both qualitative and quantitative would be required within each of the major storm sewer areas to assess the contributions of solids from both separate and combined sewered areas. Only then can a realistic evaluation be conducted on the effectiveness of aesthetic control mechanisms.

Deep Rock Tunnel

The modeling analysis conducted under this phase of the Facility Plan has indicated that the major pollutional impacts, as measured by C-BOD, N-BOD, and D.O., are being contributed by the Upper Passaic River Basin. Although the dissolved oxygen impact of CSOs at the present time is marginal, future improvements within the water quality from the Upper Passaic River may modify their (CSO) relative contribution. Under these conditions, CSO discharges may become a significant loading factor and may require control methods to further improve the water quality of the lower Passaic River.

Although the control alternatives considered under this phase of the Facility Plan were for aesthetic improvements, many of the system restrictions identified through the analysis would be applicable to control alternatives for reduction of pollutional loadings. These system restrictions include:

(1) Inline storage capabilities within the PVSC District are restricted to a few areas with insignificant volume available under severe storm conditions.

(2) Most areas encompassing CSO regulator chambers are congested and as such leave insufficient land for offline storage or treatment facilities.

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(3) Hydraulic and land restrictions limit the use of swirl and helical bend regulators except within a few of the combined sewer areas.

(4) Best management practices are localized programs and therefore depend heavily on municipal budgeting and the availability of municipal manpower.

These restrictions would greatly limit the number of control alternatives feasible for reduction of the pollutional loading from CSOs. Although some improvement may be possible for less severe storms, an alternative approach would be required under severe storm conditions.

The Overflow Analysis completed by Elson T. Killam Associates, Inc., in 1976 discussed several possible alternatives to continued CSO discharge into the Passaic River. Among these were the storage and eventual treatment of CSO discharges within deep rock tunnels located far below the existing surface. Although extremely expensive, the deep rock tunnel would be one alternative which would be capable of eliminating or substantially reducing the CSO pollutional loading even under severe storm conditions. This alternative, however, should only be considered if and when water quality improvements within the upper Passaic River make CSO discharges a significant portion of the overall pollutional load discharged to the lower Passaic River.

The deep rock tunnel offline storage facility would consist of:

(1) Deep underground tunnels, roughly paralleling the route of the existing PVSC interceptors within the City of Paterson, the City of Newark and the Towns of Kearny and Harrison. The tunnel would be continuous from Paterson to Newark Bay or could be designed as satellite facilities for regional storage with separate pumping facilities to return the stored flows during non-storm periods.

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(2) A total storage capacity of approximately 120 MG which should provide sufficient capacity of a two year storm.

(3) Vertical drain shafts at all CSOs to convey the CSO overflow down into the deep tunnel.

(4) Aeration blowers-mixers to ventilate the deep underground tunnels and to prevent septicity and the settling of troublesome solids within the tunnel.

Projected cost estimates for satellite storage within deep rock tunnels range from 350-450 million dollars. (ENR 4100) In addition to the extremely large construction costs it is estimated that pumping costs would run approximately $200 per MG assuming that all flow would be returned to the system within a 24 hour period. Additional operation and maintenance costs would make this an extremely costly alternative and accordingly, one which should only be considered if considerable benefits or improvement of water quality is possible.

Instream Aeration

The traditional approach to improving water quality within our nation's streams and rivers has been to control or improve the quality of point source discharges (sewage treatment plants, industrial wastewater discharge, etc.). Sewers, storage and regional treatment facilities have been constructed with the belief that area water quality would improve to acceptable levels. Although control and improvement of point source effluents have provided some improvement within our nation's waterways, it is becoming increasingly apparent that non-point sources (sources of water pollution which do not enter receiving waters as regular flow) and instream characteristics may preclude attainment of established water quality standards within specific areas.

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The modeling analysis conducted as part of this facility plan (Volume 2) has shown that most of the pollutional loads entering the lower Passaic River are discharged from the Saddle and Upper Passaic Rivers. This analysis was based upon flow quantity and quality measurements made at upstream boundary stations and as such was not related to any assessment or characterization of the contributing sources.

A preliminary assessment of the loading characteristics for the entire Passaic River basin has been conducted by the State of New Jersey as part of its Northeast New Jersey Water Quality Management Plan (NJDEP, 1979). This modeling analysis predicted average annual loadings using the USEPA Storm Water Management Model and nationally averaged loading parameters based upon land use, population densities, sewer system types, and street sweeping frequency. The use of non-point source loading rates based upon national averages does produce limitations within the utilization of this data. Storm Water Management Model analysis within the PVSC District, completed as part of this facility plan (Volume 2), has shown that actual loading parameters may be four to five times greater than national averages when based upon site specific water quality data. Accordingly, the information obtained from the New Jersey modeling analysis must be viewed as a preliminary assessment of the expected loadings with the expectation that actual loading factors can be quite different.

Data obtained from the Northeast New Jersey Water Quality Management Plan is provided within Volume 3 of the facility plan. Information obtained from NJDEP shows that C-BOD_5 loadings from point sources within the Passaic River basin are estimated at 4,968,000 pounds per year, while the non-point loadings within the same area are estimated at 7,752,000 pounds per year. Non-point sources by the State's estimate represent over

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60% of the total yearly C-BOD load theoretically discharged to the Passaic River. Even if the actual loading is somewhat smaller, it appears that a substantial improvement in water quality will not be possible unless both point and non-point sources are controlled or a reliable alternative system is implemented which can assist the self purification process within the receiving water.

Oxygen is an essential ingredient in the lives of all living organisms. In general, the more dissolved oxygen present within an aquatic system - the more complex and diversified the biological community.

The biochemical breakdown of organic matter utilizes dissolved oxygen within the system and thereby depresses the dissolved oxygen levels within the receiving waters. Most organisms have minimum dissolved oxygen levels below which the organism cannot sustain itself and dies. The periodic depression of dissolved oxygen levels may lead to the elimination of less tolerant organisms and the degradation of the biological communities.

The biocommunities inventory conducted as part of this facility plan (See Volume 3) shows that the study area is subject to environmental stress with conditions deteriorating in a downstream direction. All stations showed biological species which displayed tendencies to withstand reduced dissolved oxygen conditions with only extremely tolerate species located within the extreme downstream areas.

Information which had been compiled from the long term modeling analysis (See Volume 2) is illustrated in the graphic display on Figure 4.37. Statistical analysis of the dissolved oxygen profiles compiled at each location have resulted in the compilation of the percentage of time during which the dissolved oxygen levels fell below established NJDEP

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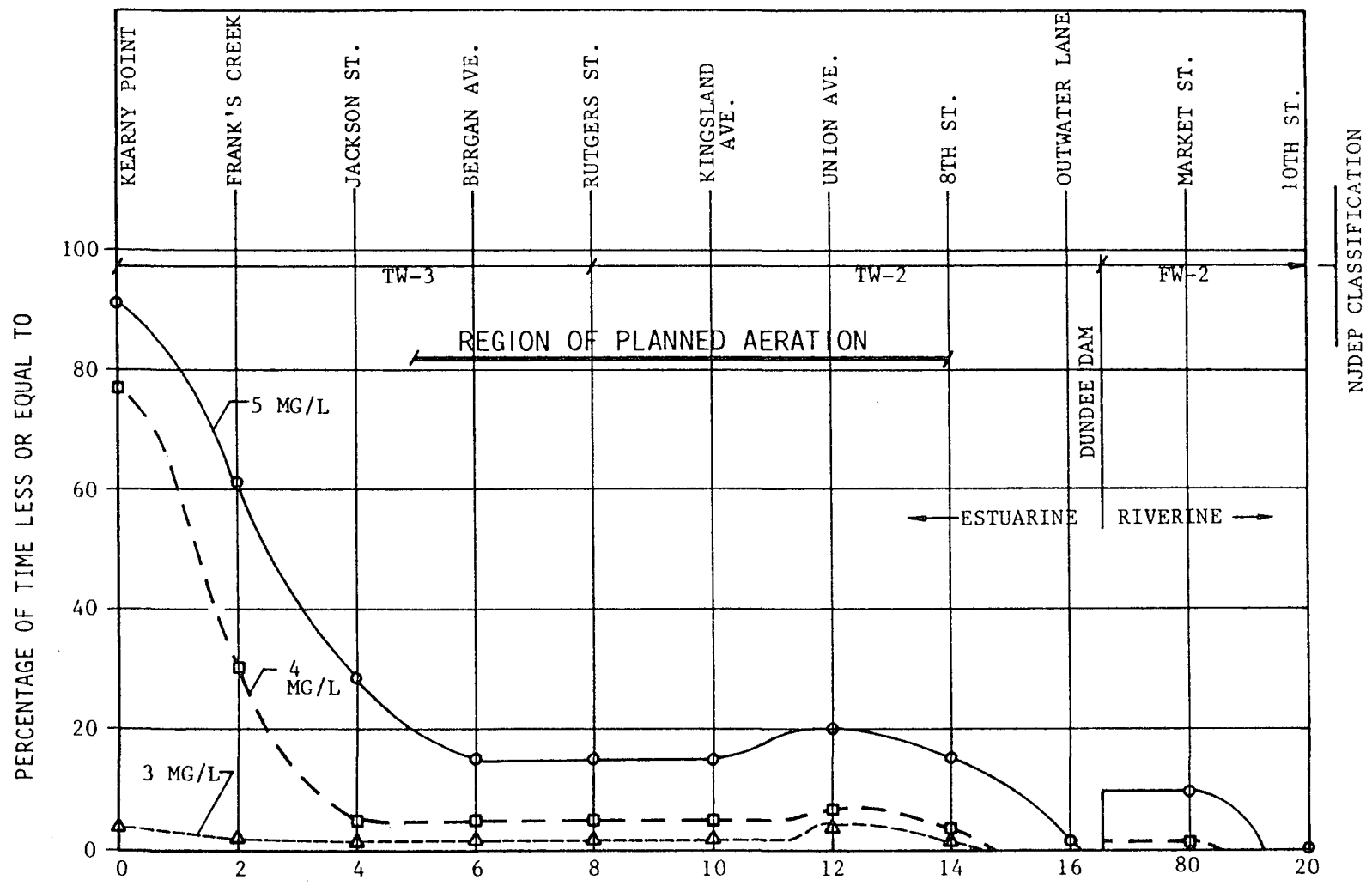

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN
LONG TERM ANALYSIS · SUMMER 1981
DISSOLVED OXYGEN PROFILE

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 4-37

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standards. The lower Passaic River above the dam is classified by NJDEP as FW-2 non-trout waters for which DO standards are not less than 5.0 milligrams per liter, 24 hour average, and not less than 4 milligrams per liter at any time. The reach from the the head of the tide at Dundee Dam to the confluence of the Second River is classified TW-2 which has a DO standard of not less than 4.0 milligrams per liter at any time. The Passaic River main stem at the Second River confluence to Newark Bay is classified TW-3 and has a DO standard of not less than 3.0 milligrams per liter at any time.

Review of Figure 4.37 indicates that dissolved oxygen standards are not being met at all times within the study area. Illustrated within this figure are the three oxygen standards (3, 4, and 5 milligrams per liter) established at various locations and the percentage of time during the 1981 simulation that dissolved oxygen levels were less than or equal to the established quantity. Also illustrated within Figure 4.37 is that section of the lower Passaic River considered for instream aeration to reestablish minimum dissolved oxygen requirements. Tidal cycles within the lower Passaic River should help establish acceptable dissolved oxygen levels within areas both upstream and downstream of the planned aeration stations.

Various methods of aeration have been studied as part of the feasibility analysis for this alternative. Experimental uses of instream aeration have been conducted throughout the years and are reported upon within the literature. Very little has been completed within the non-experimental use of instream aeration. Presently there is one project at completion in Chicago wherein reaeration is being utilized to reestablish minimum dissolved oxygen levels within the receiving waters. In addition, there is a study currently being conducted upon the Fox River in Wisconsin

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wherein instream aeration would be utilized to minimize the impact of point and non-point inputs.

Comparisons have been made on both mechanical aeration and fine bubble aerators to determine which system would prove most beneficial within the lower Passaic River. Due to the cross sectional depth within the study area, the overall efficiency of mechanical or fine bubble aeration would be essentially equal. The final analysis showed that the possibility of problems with vandalism, clogging by river debris, and the aesthetic quality, made subsurface diffuser aerators more desirable than surface mechanical aerators.

A preliminary analysis has been completed to determine the quantity of oxygen required as well as potential sites based on cross-sectional profiles. An Air-Aqua aeration system has been investigated for use within the Passaic River. Preliminary design analysis has shown the need for seven separate and independent units, each capable of introducing 1,000 cubic feet per minute of air under standard conditions. Figures 4.38 and 4.39 illustrate typical aeration units currently under investigation. Each aeration unit will consist of a blower structure wherein two positive displacement blowers will be located. Galvanized feeder pipe would then transfer the compressed air to stream aeration modules in series or parallel upon the river bed. The modules would contain weighted Air-Aqua tubing either on 1 foot or 1-1/2 foot centers depending upon the geometry of the stream cross section at the appropriate location. Each module would contain 1,350 to 2,000 feet of weighted Air-Aqua tubing, depending upon whether it contains 1 foot or 1-1/2 foot centers. In total, each station would contain approximately 27,000 feet of aeration tubing and would require two 40 horsepower motors to provide the necessary compressed air.

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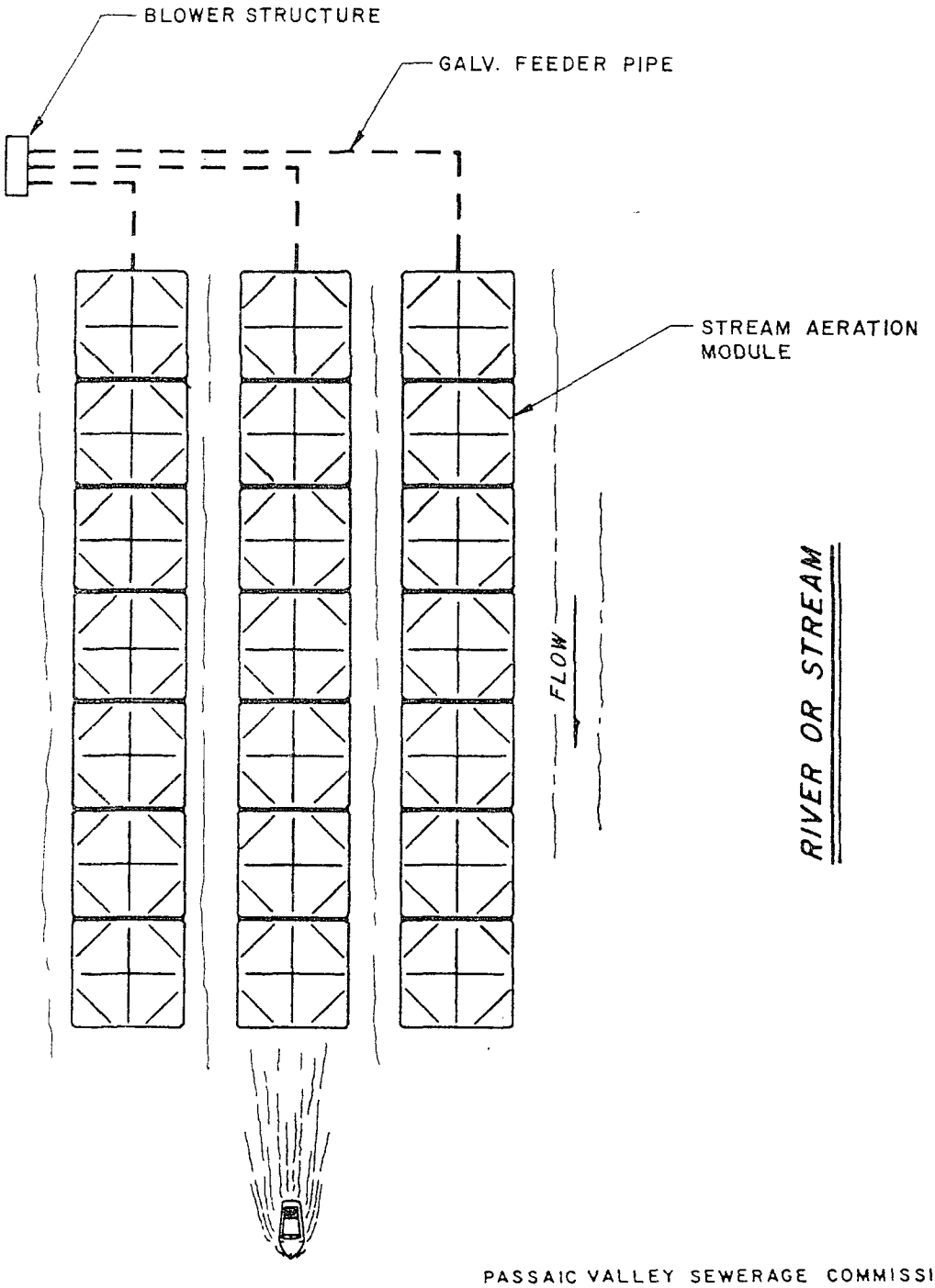


PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

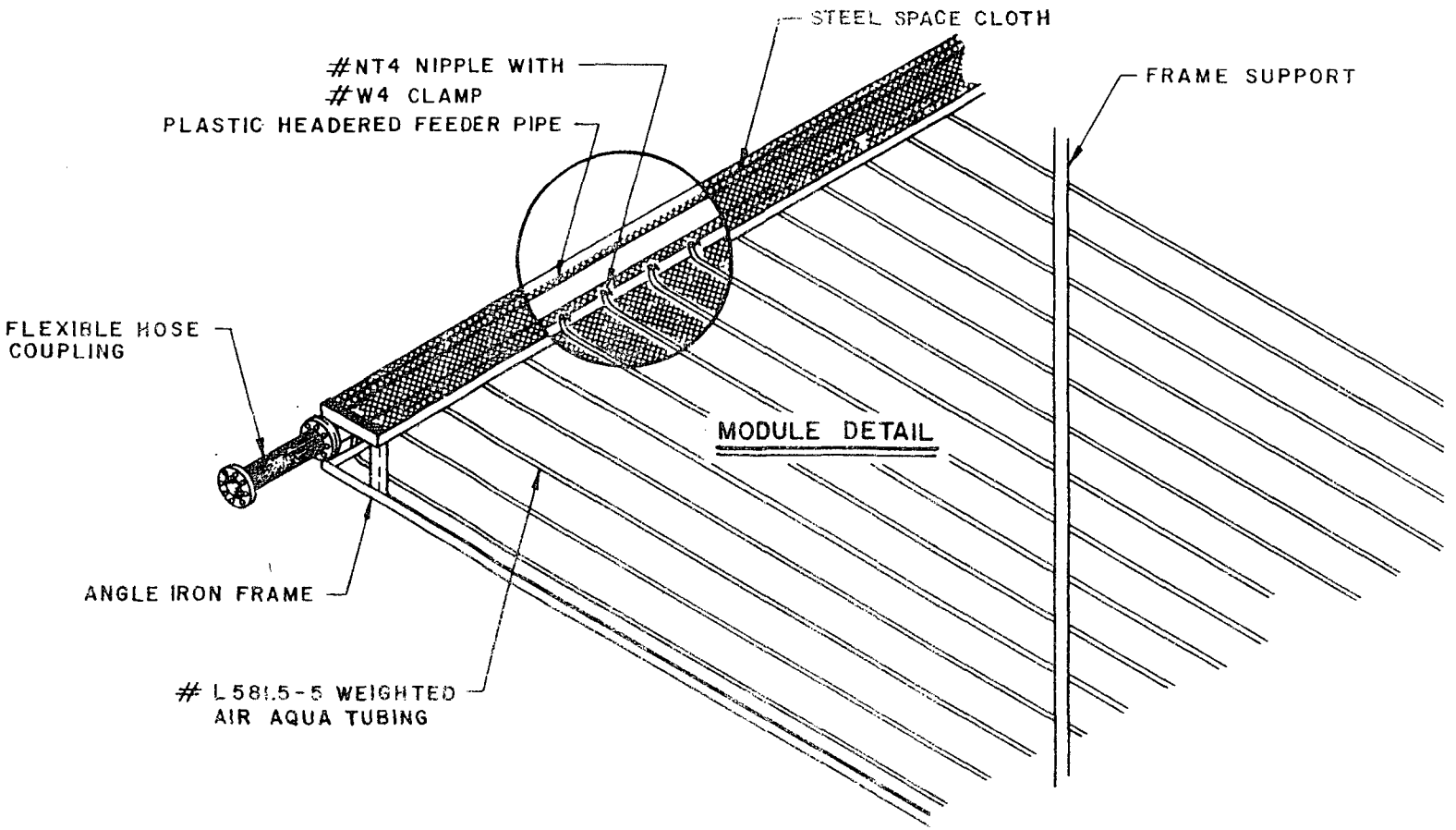
COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC

AIR-AQUA AERATION STATION FOR UTILIZATION WITHIN THE LOWER PASSAIC RIVER

(TYPICAL)

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041



PASSAIC VALLEY SEWERAGE COMMISSIONERS

NEW JERSEY

COMBINED SEWER OVERFLOW FACILITY PLAN

SCHEMATIC

AIR-AQUA AERATION SYSTEM

MODULE DETAIL

(TYPICAL)

Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
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FIGURE 4-39

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This preliminary design for instream aeration was based upon available river cross sections and estimates of dissolved oxygen utilization. Actual design parameters would be based upon a detailed model analysis to determine the ultimate location of aeration stations as well as the total volume of compressed air required to establish acceptable dissolved oxygen levels within the lower Passaic River. Emphasis has been placed upon establishing acceptable levels within the section of the river extending from River Mile 05 to River Mile 15. This areas encompasses the area from about the Saddle River confluence to approximately Clay Street within the City of Newark. Establishment of acceptable dissolved oxygen levels within the area downstream of Clay Street would require considerably more effort due to the tidal influx from both the Hackensack River and Newark Bay.

The need for instream aeration has been established through the modeling analysis. Higher dissolved oxygen levels within the receiving water would allow the stream to absorb more organic waste and provide for a more diversified biological community. Preliminary estimates have indicated that equipment installation of the seven substations would cost approximately 1 to 1.5 million dollars. In addition to the construction and operating costs associated with this alternative, the responsible agency would be required to direct construction and to provide the necessary construction and operating funds. Although this section of the river is currently under the responsibility of the Passaic Valley Sewerage Commissioners, it is unreasonable to believe that this public agency would be capable of rectifying a basin wide problem. For this reason, special consideration would need to be given by the State of New Jersey for the establishment and the operation of the proposed aeration stations.

h. Other Considerations

The modeling analysis conducted as part of this facility plan has shown that the pollutional load exerted by the upper regions of the Passaic River and Saddle River basins has a detrimental effect upon the water quality within the lower Passaic River. The pollutant contributions of the upper Passaic River and Saddle River originate from two types of sources - point and non-point. An evaluation of all known point sources has been conducted by the State of New Jersey and is reported upon within Volume 3. In addition, the State of New Jersey has made a preliminary assessment of the pollutional load contributed by non-point sources within the entire Passaic River basin. The State assessment in conjunction with results of modeling analysis suggests that a regional rather than a local perspective is needed to design better control alternatives. A regional approach would have the advantage of providing a wider range of options with more cost-effective controls and would provide for control of point and non-point sources independent of local boundaries and jurisdictions.

By expanding the engineering tool developed within this phase of the facility plan, it would be possible to formulate comprehensive water resource planning and water quality control alternatives for the entire Passaic River basin. A regional facility plan would provide for more cost-effective controls since all improvements (including treatment plant upgrading) could be incorporated into the model to assess the overall impact prior to implementation. As such, a regional approach would prove a valuable tool to obtaining the most benefit within the limited funds available. In addition to expanding the engineering tool to upstream areas, it must incorporate all the essential components of the complex

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network consisting of the Newark Bay, the Kills, the Hackensack and Passaic estuaries. Only through a concerted effort involving all the local and governmental agencies, would it be possible to formulate a comprehensive water resource management plan and water quality control alternatives for the entire region. The reduction of discharges within the lower Passaic River basin alone would do little or nothing for the water quality within this region.

The only alternative independent of the regional approach is the instream aeration recommended within the estuary portion of the lower Passaic River. Here too, potential problems exist in the regional nature of pollutional loadings and their localized impact within the PVSC Service District. Although the effect is experienced locally, the cause is regional in nature. Therefore, any control alternative of this nature (i.e. stream aeration), should be implemented and funded on a regional basis or through state implementation.

It is possible that, if conducted, the final analysis of a regional study and feasibility analysis would show that the cost of reducing the pollutional loads from the entire Passaic River Basin may be more than is economically feasible. Under these conditions, perhaps the state and federal government would need to reevaluate their present water quality requirements and goals and accept the fact that certain rivers or portions thereof are not reclaimable at a reasonable cost. It is therefore vitally important that a complete and systematic assessment of all pollutional loadings and impacts be conducted to determine whether regional control facilities will be capable of substantially improving water quality within this region. Only then can an intelligent, realistic evaluation be conducted upon the fate of the lower Passaic River.

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5. AESTHETIC IMPROVEMENTS

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5. AESTHETIC IMPROVEMENTS TO THE LOWER PASSAIC RIVER

The following portion of this report has been included to emphasize the importance of aesthetics in a riverine environment. Funding and implementation of suggested methods for aesthetic improvements are not the responsibility of the Passaic Valley Sewerage Commissioners. A section has been included to list various agencies from which funding may be obtained while the vehicle for implementation must be determined through the regulatory agencies.

a. Introduction

Since the 1950's there has been a growing concern for recreation, open space, conservation, pollution abatement and protection of the environment. The general public has become increasingly aware of problems stemming from urbanization and over-population. We have also become better educated in the ways to protect and beautify the environment in which we live. Through legislative action, agencies have evolved which supply funding to help subsidize the often phenomenal costs associated with pollution clean-ups and urban beautification projects. On a whole, towns and communities are seeking to restore what has been lost due to rapid industrial and urban growth and to preserve those natural and sensitive areas which could fall into despair in the years to come.

The lower Passaic River Basin is one of these "lost" areas which is in dire need of a cosmetic face lift. This area holds the proper ingredients needed to stimulate new life, however public interest and support are vital components which must be developed. The recent surge of waterfront rehabilitation projects going on throughout the country is a clear indication that support from local communities can have significant

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impacts upon the direction and success of the project. There are many areas within the PVSC District where vacant lots or abandoned buildings could be revamped to create a pleasant, functioning river front community, capable of generating new interest within this area.

Convenient and pleasant recreational facilities are an important need for the urban dweller. Leaving the area can be costly and time consuming if one just wishes to escape for a few short hours. A need then develops to have facilities close at hand to be utilized whenever and as often as needed.

With the proper planning and design, various enclaves can be created right in the heart of the urban community. With the right amount of creativity, the lands along the Passaic can be transformed from an overgrown, debris laden eyesore to attractive parklands or wharf areas which could support bustling new business communities.

Of course a project of this scope is no easy task and would require a lot of research and planning. An involved and aware community base is one of the most important aspects needed when organizing a project of this nature. If one were to look at the benefits incurred, it is definitely a worthwhile investment. If the waterfront areas were made attractive again, it may become a selling point to attract new business to the communities. This would generate an increase in tax revenues and could possibly increase the cash flow to the existing businesses in these areas. Attractively designed parkland and well controlled open space would create appealing environments which could draw homeowners back to these urban areas. Other attractive incentives which could be implemented, would include boating facilities, exercise courses, and quiet sitting areas for relaxation.

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To effectively implement this type of project a great deal of community involvement is needed. Since the area of concern transgresses municipal boundaries it would require the support of all communities who would benefit from the project. Total support and commitment is necessary, from the input of ideas to funding the project.

There are a total of twenty communities which border the Passaic River from Newark Bay upstream to Paterson's Great Falls. These have been broken down into two sub groups, the communities below Dundee Dam or the estuarine communities and those above Dundee Dam or the riverine communities. The following is a listing of the communities under their prospective sub group:

Estuarine Communities	Riverine Communities
Newark	Garfield
Harrison	Clifton
E. Newark	Elmwood Park
Kearny	Fair Lawn
N. Arlington	Hawthorne
Belleville	Prospect Park
Nutley	Paterson
Lyndhurst	Haledon
Rutherford	
E. Rutherford	
Wallington	
Passaic	

b. Passaic River Restoration Project

In 1969 an environmental affairs group, the Passaic River Coalition, was formed to battle the ongoing deterioration of the Passaic River Basin. Located in Basking Ridge, the coalition has developed a master plan for the protection and restoration of the lower Passaic River Basin. The communities of Rutherford, Lyndhurst, North Arlington and Kearny are the main backing for the project. These communities were assisted in the development of a master plan by receiving a $35,000 planning grant from the New Jersey Department of Environmental Protection, Division of Coastal Resources.

The coalition proposes to develop a trail which would interconnect all communities between the Borough of Rutherford and the Town of Kearny. The trail would meander along the river and traverse existing parkland as well as proposed facilities. Besides open space, a theater barge, a restaurant, a parcourse facility and boating marinas are planned. The map on the succeeding page represents the study area with the planned facilities at their respective locations. Further information can be obtained from the Passaic River Restoration Master Plan or by contacting the coalition at their Basking Ridge headquarters.

c. Alternative Strategies

In addition to the proposed master plan, consideration should be given to other methods of improving the river basin. The following are feasible alternatives which should be carefully considered for addition to any adopted plan for the Passaic River Basin.

Dredging

Bottom dredging is an important aspect of river maintenance which should be considered. The Army Corps of Engineers maintains the navigational channel but does not remove the deposition of material on the river's edge. A private contractor must be hired if this material is to be removed. The estuarine portion of the river, being tidal, is very susceptible to sedimentation, especially along the long bends in the flats. This in conjunction with solid wastes has made these areas aesthetically objectionable.

In the past, dredge spoil has been disposed of by open water dumping; as close to harbors as possible but far enough away as not to interfere with water use facilities. This was practiced mostly to minimize the often exorbitant costs of transporting dredged material to an appropriate dump site. Then in the late 1960's and early 1970's the general public

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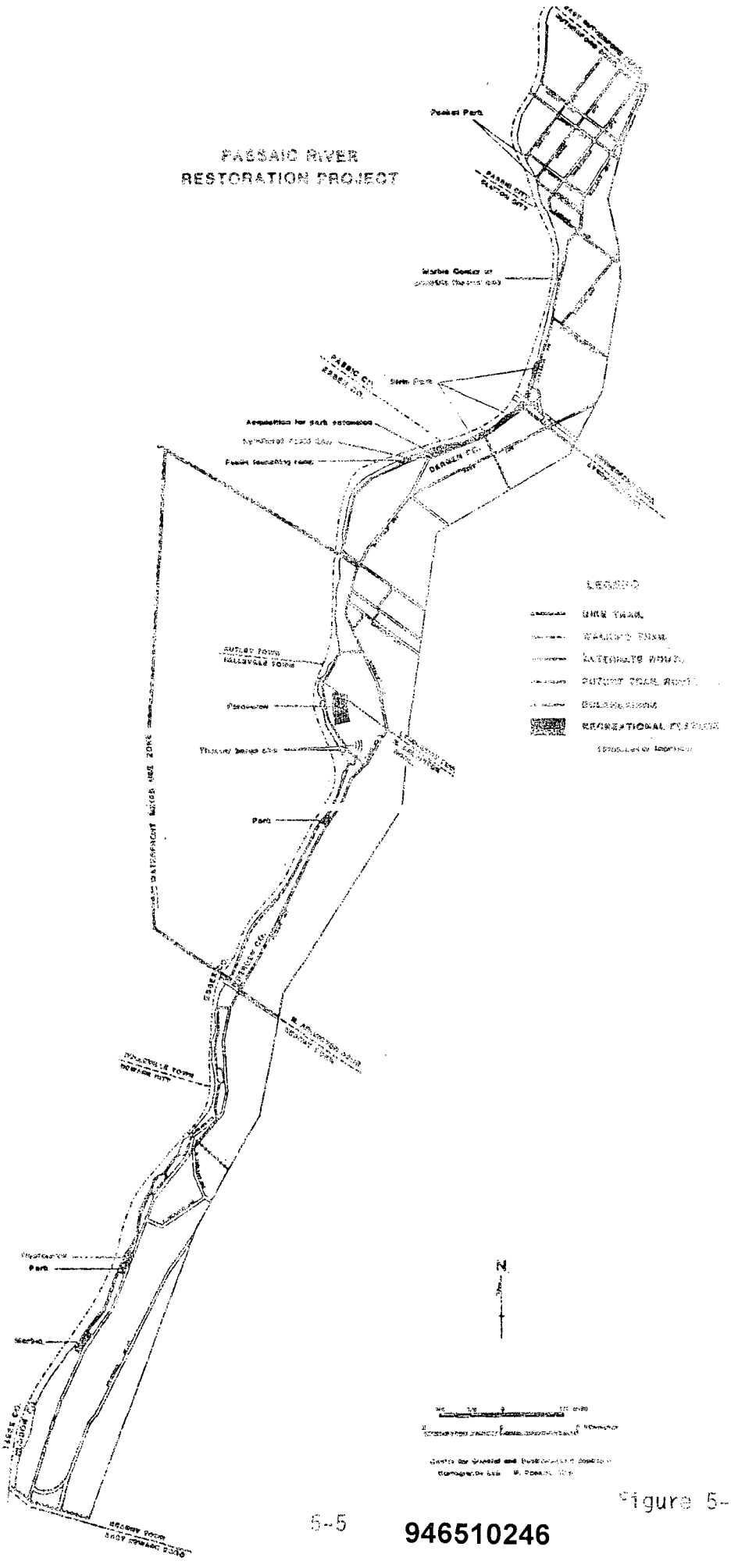

Figure 5-1

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became concerned with the pollutional content of these sediments and the effects upon the inlets and harbors. Thus, certain criteria for the disposal of dredge spoil was developed and enforced by the Environmental Protection Agency. An acceptable disposal practice which has evolved is containing the spoil in dike containment areas. This practice has proved to be quite effective in restricting pollutional sediment from reaching open water. Although diked containments are rather expensive, they appear more feasible than other methods of disposal, except deposition in open waters.

In relation to the Passaic River Basin, especially in the estuarine areas, we find long stretches of the river banks where the sediment build up is a major problem. Not only is the sediment encroaching the main channel, but it entraps discarded automobile tires, shopping carts, plastic containers and many other unsightly objects. This problem is predominant in, but not restricted to County Park North in Lyndhurst. There, the river flows south making a wide bend to the left which causes slower movement of flow on the east shore, causing material such as suspended solids, bottles and other debris to settle out and be deposited in the mud sediment. During periods of low tide whatever garbage has been left there is clearly visible to persons in the park, and more so to travelers on Highway 21 (McCarter Highway) opposite the east bank.

A dredging program should be incorporated into the master plan for the areas of high deposition. A private contractor with a dredge would be needed. A rough cost estimate obtained from the Army Corps of Engineers is $3 per cu.yd. for material removed. This includes the cost of transporting the material to a dump site, although prices may vary with different disposal methods. Routine maintenance would be required, and

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costs can be minimized by using community volunteers in a river bank clean-up program.

The removal rates for dredges vary considerably, depending on the size and type of equipment used. For a Cutter-Suction dredge, material is normally piped through a semi-flexible pipeline to a disposal area which is near the deposit. The distance for piping will vary due to the consistency of the material. Assuming the dredged material is of a finer consistency the following capacities can be utilized as guides:

Small Dredge 200 cy. per hr = 1,400 cy. per day

Medium Dredge 400 cy. per hr = 2,800 cy. per day

Large Dredge 1,500 cy. per hr = 10,500 cy. per day

For a general rule of thumb, the larger the dredge the lower the cost for the same distance of transport; whereas with a smaller dredge one can expect a higher unit cost per cubic yard of material moved. The largest dredges, hopper dredges, are almost all owned and operated by the Army Corps of Engineers. With the larger dredges, greater amounts of material must be retrieved to keep the cost low. Another method to reduce cost is to keep an operation active 24 hours a day.

Erosion Control

Erosion caused by stormwater runoff and bank deterioration from high flows add considerable amounts of sediment to the stream bottom. The results are unsightly and possibly dangerous conditions along the channel bank. Where planned or existing facilities are located, retaining walls or stabilization should be incorporated. The Passaic River Coalition has proposed two pocket parks at locations where the slope is extremely steep to the river's edge; these locations will require a retaining structure

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and fill to expand on the amount of space and to prevent further erosion from taking place.

Bank stabilization can be accomplished utilizing a number of methods. One device is the use of gabions. These are large rectangular boxes made from wire mesh which are filled with stone and abuted together to form a man-made channel bank. Although gabions are used in many applications, their purpose is for stabilization. Stabilization of this nature will best be placed on bends in the river where the force of the stream is directed against the outside bank causing extreme erosion at the bend.

Along the straights of the river the banks have been deteriorated by high flood waters over the years. Preservation of the bank by enhancing their vegetative cover would prevent further degradation. Plantings with dense, fibrous root systems, such as grasses, sedges and woody shrubs are best suited for these areas. Where steep slopes are problems, it may be necessary to flatten the slopes and establish a vegetative cover.

Other erosion control devices which are available are rip rap and Fabriform®. These structures would be best at points of heavy erosion.

For bank stabilization, gabions of 1 foot thickness would be required. Costs are based on the size of the job; the larger the area to be covered the lesser the unit cost of the gabions. (Unit costs are per square yard of surface area). (ENR = 4100).

10 square yards	$36.00
100 square yards	$20.00
1000 square yards	$16.00

Fabriform® or flexible erosion control mats are more expensive, although installation of the mats can be used where gabions may not be needed.

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Costs are based on a channel 25 feet wide and 0.25 miles long (i.e. 33,000 square feet).

Total cost	$53,300
Unit cost per square yard	14.60

Removal of Floatables

Floatables upon a water surface can be of many forms. Liquids such as oil and grease are possibly the most damaging while being less visible than solids such as cans and bottles. They also originate from a variety of sources. When dealing with the removal of floatables there have not been many technological advancements for river improvement. There are stormwater management programs being incorporated to combat non-point sources that involve both nonstructural and structural practices. Examples of nonstructural practices are:

1. Street cleaning
   a. Broom
   b. Advanced sweeping (broom and vacuum)
2. Street and catch basin flushing
3. Solid waste management
4. Infiltration/Inflow studies
5. Deicing control (limited use of salt on roadways)
6. Leaf collection

Examples of structural practices are:

1. Detention basins
2. Diversion for seepage or recharge (retention)
3. Physical treatment (microstrainers, filtration, D.O. floatation)
4. Trash catchers or bar screens

The elimination of debris carried by excess runoff before it reaches the river is the most practical solution. Of course this practice will not totally amend the problem of floating debris for it is virtually impossible to clean up all existing debris generated daily.

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Aside from the non-point stormwater management practices, we still must confront the floating materials which do and have reached the river. One feasible alternative is to utilize a machine designed to control aquatic vegetation. A Swiss company, Rolba, has a weed harvester which doubles as a surface skimmer for removal of floating materials. As a weed harvester it will cut all sorts of surface plants up to a depth of 4 feet below water level. The weeds are transported up a conveyor to another conveyor which then places the material into a boat.

When doubling as a surface skimmer a set of booms are attached to each side of the machine causing a funneling of floating material to the first conveyor, then to the second, and finally to the boat. The process is the same as for weed removal.

The cost of the equipment varies with the type of machine purchased. The range is between $115,000 to $158,000 per unit which does not include the addition of freight and duty costs estimated to be 3-5% of the machine's base price.

A large portion of the river's floatables can be attributed to aging structures on the banks of the river or on the main stream itself. Pylons where piers had once stood are presently a source of the floating wood. Some can be found on both banks of the river at the Belleville Turnpike bridge and on the opposite shore of the Magullian Oil Company in Kearny. Abandoned barges are also a prime contributor. Three are beached on the mud flats along Passaic Avenue in Kearny which are adding to the wood splinters on the water's surface.

The Passaic River Coalition has compiled an inventory of abandoned structures and is preparing a program to eliminate them. It is recommended to expand on this by requiring private residences and

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businesses to tidy up their properties which are adjoining the river and are accumulating debris.

Funding

Funding for a project of this nature will come from a variety of sources. Local communities who will benefit from the plan should contribute a major portion. Planning and improvement grants are available through the Environmental Protection Agency and other government agencies.

The following is a summary of several programs and acts which could be utilized to conserve, acquire and/or develop open space or recreation in the Passaic River Basin.

1. Self help programs.
2. Federal Land and Water Conservation Fund.
3. Agricultural Land Preservation Act.
4. Coastal Zone Management Program.
5. Wetlands Protection Act.
6. Inland Wetlands Restriction Act.
7. Scenic Rivers Act.
8. Conservation Restriction Act.
9. Floodplain and Wetland Zoning.
10. National Historic Preservation Act.
11. Green Acres Funding

It is the sole responsibility of the communities involved to seek and obtain funding from any and all available resources.

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6. CONCLUSIONS AND RECOMMENDATIONS

6. CONCLUSIONS AND RECOMMENDATIONS

The modeling analysis conducted within this phase of the facility plan, and reported upon within Volume 2, has suggested that CSO discharges from the PVSC service district have only marginal impacts upon the lower Passaic River water quality. The results of this analysis furthermore shows that CSO impacts are transient in nature and of short duration, and that the relative CSO pollutional loadings are small compared to total pollutant sources within the basin, see Figure 6.1. Water quality parameters utilized within this study are stream C-BOD and dissolved oxygen concentration variations. Inferences on CSO impacts regarding other variables based on the results of the present investigation must be avoided. The conclusions reached must remain limited only to those variables investigated.

Consideration of water quality control alternatives within the lower Passaic River have been formulated with due consideration of the findings of this study. Large expenditures of monies for CSO control alternatives would not be warranted based upon water quality parameters utilized within this analysis. There does however, exist an acute aesthetic problem within the lower Passaic River basin. The existing degree of floating material often observed within the Passaic River provides for the perception of a polluted waterway and makes the river an undesirable source of recreational use.

The control alternative analysis conducted within the Facility Plan has concentrated on methods of decreasing solids loadings to the receiving water from both combined and non-combined areas. It should be emphasized that solids transport was not part of the original study, and as such is currently not available within the existing Passaic River model. Additional field investigations and a new model calibration would be required

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to provide a final analysis of the contributors and modes of elimination of solid debris within this region.

Control alternatives considered within the facility plan have been mostly restricted to the combined sewer areas of the PVSC district. Although control mechanisms may well be required within separate storm systems, the lack of sufficient hydraulic and water quality data within this area necessitated the postponement of these analyses. Detailed information would be required upon all major storm sewer systems within the Basin prior to the consideration of any control alternatives. In addition, an assessment must be made as to the solids contributions of areas outside the PVSC district (the upper Passaic River, Saddle River, and Newark Bay).

Best management practices have been analyzed and exhibit a realistic potential for reduction of solids loading within both combined and non-combined areas. Best management practice control methods involved both source and collection system management. Control measures within source management include restrictions on chemical usage, land and road maintenance, and improved sanitary practices including trash removal and street cleaning. Collection system management deals with improved maintenance and control of both the combined and separated storm sewer systems. Together these control measures are capable of reducing that portion of the pollutional load contributed by urban runoff. As such, best management practices are equally applicable within both combined and non-combined sewer areas.

Acceptance of best management practices depends on the willingness of the public to accept the inconveniences and expenses necessary for an effective program. Litter is perhaps one of the largest and hardest to

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POLLUTANT LOADINGS TO THE LOWER PASSAIC RIVER DURING THE SUMMER OF 1981

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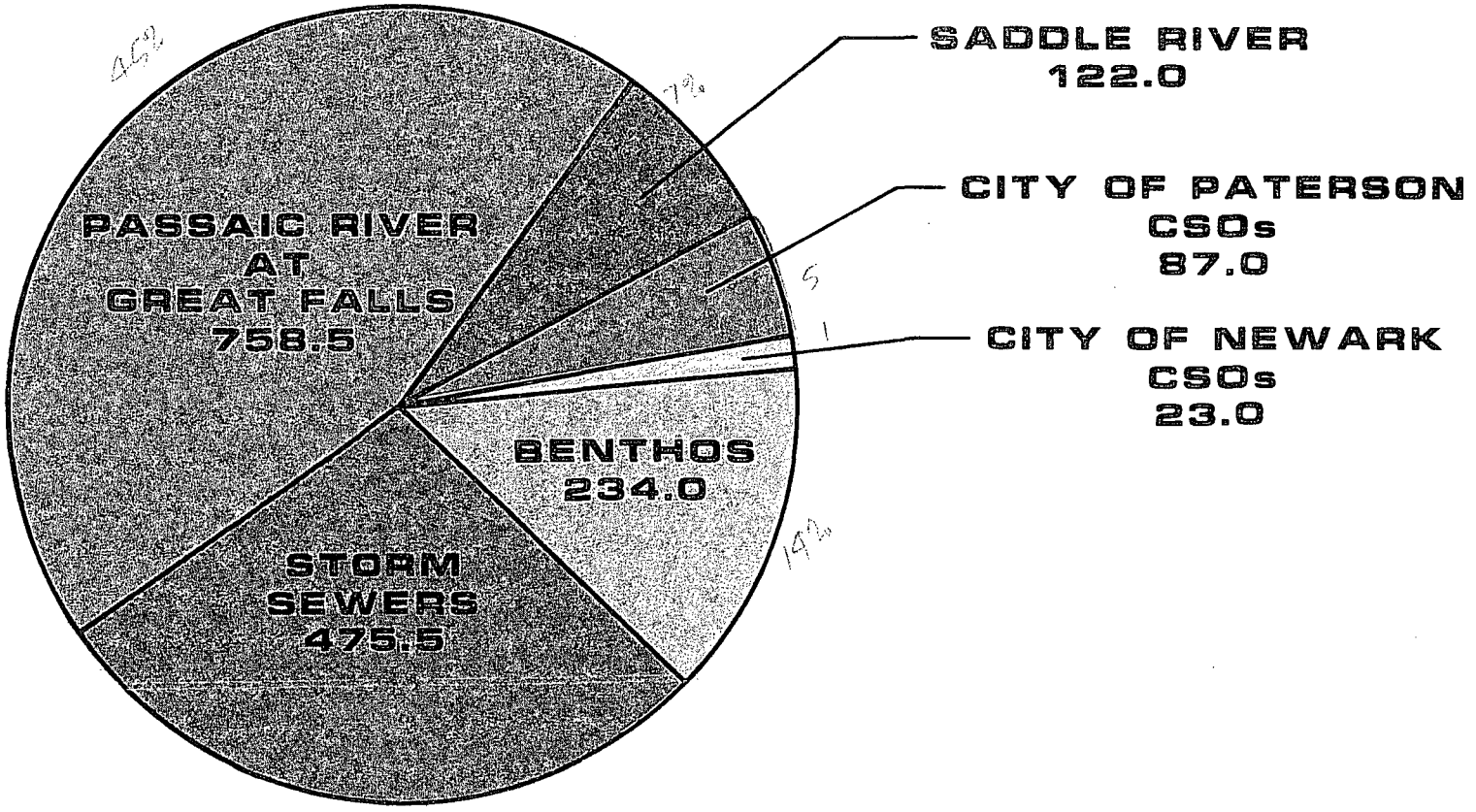

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FIGURE 6-2

control pollutants within the urban environment. Even if a strong anti-littering compaign is successful, established street sweeping operations would still be required as a method of source management and solids control.

Street sweeping effectiveness is a function of the equipment utilized, pavement or surface conditions, return interval, parking characteristics, population density, and public acceptance. Effective parking restrictions and other control mechanisms together with street maintenance and maintenance of the storm water collection system are all necessary components of a best management plan. Although very labor intensive, street sweeping and other best management practices do provide other benefits including improved air quality, aesthetic conditions, and reduction in street flooding and sewer backups.

The pollutional removal rates associated with street sweeping are affected by a number of separate parameters. It is therefore necessary to establish pilot studies capable of gauging the effectiveness of street sweeping in the various sections of the PVSC district. Only then can a plan of action be established to determine the effectiveness and the logistics involved within the street sweeping program. A survey conducted within the entire PVSC district has shown that although street sweeping is practiced within most municipalities, the established programs do not optimize the utilization of this control alternative for pollution reduction.

In conjunction with street sweeping, an established catchbasin and sewer maintenance program must be implemented within the PVSC district to optimize removal of floatable and solid materials prior to discharge to the receiving waters. This control mechanism must be considered and

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implemented within both combined sewer areas and separate storm sewer areas in order to be an effective means of reducing the total solids discharged to the Passaic River.

Other control mechanisms have been reviewed for implementation within the PVSC district. Although minor regulator modifications have been studied, it has been found that in general there is very little inline storage within the municipal collector system and little additional capacity within the PVSC trunk system during significant rainfall periods. Many of the combined sewer systems within the PVSC district, especially within the City of Paterson have very limited hydraulic capabilities and therefore would not provide sufficient capacity for even a one year storm. Changing the weir elevations within the existing PVSC regulators would, in most cases, induce undesirable conditions within upstream areas. It is therefore not feasible to substantially reduce the overflow volumes entering the Passaic River by minor modifications of PVSC regulator chambers.

An improvement over the present system of perpendicular weirs and static regulators could be implemented by the utilization of an automatic dynamic regulator system. A dynamic system would utilize moveable weirs and sluice gates to control the discharge of combined flows to both the receiving waters and the PVSC trunk system. By instituting an adjustable weir/orifice system within the regulator, discharge load reductions are possible for more frequent low intensity storms while provisions are made for hydraulic capacities required under severe storm conditions.

A dynamic regulator system could be integrated into a computer operated capability utilizing predictive or monitored rainfall intensities. An operational bias would be utilized to minimize overflow

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from specific "high load" interceptors or to favor the timing of the overflow event (allows for the capture of "first flush"). Recent developments in storm tracking, rainfall measurement and predictive capabilities have improved the feasibility of an integrated regulator system. Due to the lack of inline storage capabilities, this alternative would need to be supplemented by offline storage to achieve maximum utilization.

Costs involved within an integrated regulator system include reconstruction of regulator chambers, installation of control interfacing, system flow surveillance equipment, and rainfall monitoring stations and/or weather radar. It is estimated the total cost of implementation within the major overflows would be approximately $13,800,000 (ENR=4100) if implemented within the seventeen largest overflows. These would include, in preliminary priority order:

City of Paterson:	Market Street (2 sites) 10th Ave. & 33rd St. Northwest Ave. Curtis Place Hudson St. Montgomery Place
Town of Kearny:	Ivy St. Johnston Ave.
City of Newark:	Clay Street City Dock Verona Ave. Saybrook Place Herbert Place Fourth Ave. Polk St. Rector St.

A detailed cost analysis and priority ranking would be accomplished during Phase II of the Facility Plan once the cost-benefit analysis and expansion of the computer model is completed.

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An initial screening process of the 58 Combined Sewer Overflows (CSOs) within the PVSC District showed that 26 of the CSOs exhibited infrequent and/or low volume overflows. It was therefore determined that unless site specific conditions prevailed, control alternatives within these overflow areas would not be warranted based upon the present modeling analysis. Drainage areas within these 26 CSOs ranged from 95 acres to less than 5 acres and were mostly within the smallest of the combined sewer overflow drainage areas.

Due to the limited availability of inline storage an analysis was conducted upon the feasibility of offline storage within the PVSC District. An analysis was conducted upon each drainage area based upon overflow volume, the availability of land for construction, and hydraulic considerations. Storage volumes were initially set for a 80-85 percentile storm and were designed for intermediate storms with the potential for first flush capture under severe storm conditions. Final design parameters would need to be set through the detailed modeling analysis proposed under Phase II of the Facility Plan.

Initial site selection within the City of Paterson revealed four potential site locations for offline storage. These preliminary sites, in addition to those from the other municipalities, were submitted to each municipality to determine whether any redevelopment plans were currently being considered. Three of the four sites within the City of Paterson have been or are currently planned for redevelopment within the future. The CSO sites affected by the redevelopment are Curtis Place, Mulberry St., West Broadway, Montgomery St., and Straight Street. The only site which received initial approval from the City of Paterson was the Northwest Overflow storage facility off Presidential Blvd. Consequently,

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offline storage facilities within the City of Paterson would need to be satellite storage utilizing hydrobrakes within the drainage areas. Responses received from the other combined sewer municipalities has indicated that present redevelopment plans do not interfere with preliminary offline storage facility sites.

The preliminary analysis for offline storage has indicated a need for a combined storage volume of 25.6 million gallons and an estimated construction cost of $41,495,000. These estimates include local the three offline storage locations within the City of Paterson which have been or are planned for future development. These areas would require regional Hydrobrake® storage within the drainage areas and consequently will need a modeling analysis to determine the ideal site locations. All offline storage areas under consideration are at or near the existing overflow chambers with the exception of a 6.2 million gallon storage area located within upstream areas of the Clay Street overflow. The cost to benefit analysis cannot be completed until the current Passaic River model is expanded to account for solids transport within the study area.

In addition to offline storage, other physical treatment alternatives have been considered within various sections of the PVSC combined sewer district. Included within these were the swirl and helical bend regulators, coarse screening facilities and regional storage/sedimentation of combined flow discharges. The latter alternative was considered only as a solution of combined sewer overflow discharges should water quality improvements be instituted within upstream and non-combined areas.

Swirl and helical bend regulators provide for solid/liquid separation by secondary fluid motions attained by imparting a rotational motion to the flow. Site inspections conducted during the 1976 Overflow Analysis

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have shown that many of the overflow regulators within the PVSC district do not operate properly. Therefore, if reconstruction of PVSC overflow chambers is to be conducted within the future, consideration should be given to construction of new swirl or helical bend regulators where feasible.

Major design restraints exist within the construction of both the swirl and helical bend regulators. The feasibility of both these control mechanisms is largely dependent upon having sufficient available head between the combined sewer, interceptor sewer, and the receiving waters. In addition, the helical bend regulator requires considerable space for construction and has a total length approximately equal to 37 times the inlet diameter. This translates to overall lengths usually between 100 and 200 feet in length.

Major and moderate CSOs with the exception of those within the City of Newark were analyzed for possible construction of swirl or helical bend regulators. The CSOs within the City of Newark were not included within this analysis due to their recent reconstruction by the Passaic Valley Sewerage Commissioners.

The screening analysis conducted upon the swirl and helical bend regulators show that only four of the combined sewer overflows within the Passaic Valley District had sufficient head for implementation of these alternatives. The four sites which passed the screening are: within the City of Paterson - Straight Street, East 11th Street, Warren Street, and in the Town of Kearny - Bergen Avenue (East). Bergen Avenue East and Straight Street were found to be feasible for helical bend regulators while East 11th Street and Warren Street overflows were found to be feasible for construction of swirl regulators. Preliminary cost estimates based on previous construction indicate that each swirl regulator would

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cost approximately $340,000 per site, while the helical bend regulator would cost approximately $568,000 per site (ENR=4100). Due to the much higher cost of the helical bend regulator, all sites were initially evaluated for construction of the swirl regulator.

A preliminary analysis for the feasibility of coarse solids removal was conducted for all CSOs within the PVSC service district. Previous studies have indicated that with the exception of static screens, operation and control problems associated with screening (i.e. drum screens, micro screens and rotary screens) make them undesirable for solids control within CSO discharge. Although the Bauer Hydrosieve® has shown itself as an excellent screening device for removal of solid debris, the hydraulic head requirements of this unit has eliminated its utilization within the PVSC district.

Preliminary design parameters have been established for a mechanical bar screen facility. Although not as effective for solids removal, such a facility would be capable of removing large coarse solids and floatables from outfalls prior to discharge. Each facility would consist of two or more mechanical screen units, an emergency overflow weir, and an automatically operated sluice gate orifice to provide hydraulic relief during extreme storm periods. Each mechanical bar screen would be protected from damage by large objects by the utilization of a trash rack. Screenings from this facility would be shredded and directed to the PVSC trunk system or would be stored for manual pickup. Special facilities would be required for stored materials to minimize odor problems within the surrounding areas.

Coarse screen analysis showed that at least 7 of the 58 active PVSC CSOs have sufficient horizontal and vertical space and sufficient overflow

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volume and frequency to warrant construction The 7 CSOs which passed the initial analysis for coarse screening were:

Hudson Street - Paterson
Verona Avenue - Newark
Saybrook Place- Newark
Herbert Place - Newark
Polk Street - Newark
Freeman Street- Newark
Johnston Ave. - Kearny

All seven locations require above ground construction within existing or expanded easements. Total cost projections for the seven screening facilities would be approximately 2.2 million dollars. The cost-effectiveness (the cost to benefit ratio) can not be determined for these units without additional sampling and a new modeling analysis. Solids transport was not considered within this phase of the facility plan and as such the existing model would need to be expanded to provide a realistic evaluation of the effectiveness of these units.

Several conclusions were reached during the alternative control analysis for combined sewer overflow alternatives. Among these are: (1) Many combined sewers within the PVSC service district have insufficient hydraulic capacity for even a one year storm event. (2) Inline storage capabilities within the PVSC district are restricted to a relatively few areas with insignificant total volume available under severe storm conditions. Inline storage analysis determined that more than 95% of the combined sewer overflow drainage areas did not have sufficient capacity for inline storage; and (3) Insufficient land for treatment facilities and hydraulic considerations within the combined sewer areas have limited the feasibility of offline storage or the construction of other control facilities. These restrictions would greatly limit the number of control alternatives feasible for reduction of

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the pollutional loading from CSOs should water quality improvements within the upper Passaic River make CSO discharges a significant portion of the overall pollutional load discharged to the lower Passaic River.

The overall analysis completed by Elson T. Killam Associates, Inc., in 1976 discussed the possibility of storage and eventual treatment of CSO discharges within deep rock tunnels located far below the existing surface. Although extremely expensive, this is one of the few alternatives which would be capable of eliminating or substantially reducing the CSO pollutional loading under severe storm conditions. One type of regional storage would consist of deep underground tunnels paralleling the route of the existing PVSC interceptors with vertical down shafts at all existing CSOs to convey the combined sewer overflow to the storage facilities. Projected cost estimates for regional storage within the deep rock tunnels range from 350 to 450 million dollars (ENR=4100). A newer, and perhaps more cost-effective method of large volume storage would be satellite storage facilities controlled by Hydro-brakes®. Cost estimates for this type of storage would required detailed, site specific information for realistic evaluation.

Although the alternative control analysis has concentrated on mechanisms of reducing the solids loading to the Passaic River, a substantial effort would be required to remove existing material and to improve the present aesthetic quality of the lower Passaic River. The major contributors to the perception of pollution within this area are the floating and partially buried materials found in abundance throughout the estuary regions. Tidal variations expose a large variety of materials within the bottom mud deposits, including many man-made objects. In addition, tidal flows deposit a vast quantity of floating debris along

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the banks. This material is aesthetically objectionable and should be removed.

Aesthetic improvements within the lower Passaic River would require a combination of methods and solutions to clean up and eliminate the present material and to maintain the improved conditions. Any program to clean up the river would need to include possible dredging of tidal mud flats, removal of all debris along the banks and a maintenance program designed to remove floatable material from the surface of the water. Although this program is feasible, it relies upon public education and improved solid waste management to maintain the area once improvements are made.

Several park areas have been established along the Passaic River in both the estuarine and riverine portions. Improvement in the present parks and development of new parks are currently under consideration. Bulk-heading and dredging of the areas adjacent to the Passaic River would provide a more aesthetically pleasing environment and would remove the objectionable nature of the current mud flats located within many of these areas.

The Passaic River Coalition has been actively involved in improving the water quality and aesthetics within the lower Passaic River. This environmental group has recently completed a master plan wherein specific recommendations were made for redevelopment of the area adjacent to the Passaic River. Recently, the group has completed a survey of the river banks. Whereas, they are currently seeking Federal grants for the cleanup of the tidal flats and river banks. Public support generated by environmental groups is an important consideration in the success of a project of this nature. We have outlined within Section 5 additional areas where we feel improvements are warranted.

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In addition to improving conditions in and around the area of the lower Passaic River, it may become necessary to provide some type of instream aeration to increase the dissolved oxygen (DO) content of the water and therefore minimize the associated problems of low DO. The regional nature of the pollutional load requires the evaluation of alternatives, not designed to eliminate the pollutional discharge, but to minimize their impact within specific areas. Non-point sources by the State's estimate of pollutional loads within the Passaic River Basin represent over 60% of the total yearly C-BOD load theoretically discharged to the Passaic River. Even if point source controls and programs are implemented within the future, non-point source pollution may still produce dissolved oxygen levels below the established minimum standards.

Various methods of aeration have been studied as part of the feasibility analysis for this alternative. Very little has been completed within the non-experimental use of instream aeration to reestablish minimum dissolved oxygen levels within receiving waters. Presently, there is only one project, at or near completion, in Chicago wherein aeration is being utilized as a means of treating the large organic loads discharged from regional sewage treatment plants.

A preliminary analysis of instream aeration has shown this to be a feasible method of improving dissolved oxygen levels within the lower Passaic River. The analysis has shown that because of vandalism, clogging by river debris and aesthetic quality considerations, subsurface diffused aerators were found to be more desirable than surface mechanical aerators. The preliminary design analysis has shown a need for seven separate and independent units, each capable of introducing 1,000 cubic feet per minute of air under standard conditions. Each station would contain approxi-

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mately 27,000 feet of aeration tubing and would require 2-40 horsepower motors to provide the compressed air necessary. Actual design parameters would be based upon a detailed modeling analysis to determine the ultimate location of aeration stations as well as the total volume of compressed air required to establish acceptable dissolved oxygen levels within this region. Preliminary estimates have indicated that equipment installation of the seven sub-stations would cost approximately 1 to 1.5 million dollars.

Although monitoring of water quality within this section of the river is currently the responsibility of the Passaic Valley Sewerage Commissioners, it is unreasonable to believe that this public agency should be responsible for rectifying a basin wide problem. The effect of large pollutional loads is experienced locally; however, the cause is of a regional nature. Any control alternative of this type should be implemented and funded on a regional basis or through State implementation.

The modeling analysis conducted as part of this facility plan has shown that the combined sewer overflow discharges have a marginal impact upon water quality (as measured by BOD and DO) within the lower Passaic River. The pollutant contributions of the upper Passaic River and Saddle River represent a major portion of the C-BOD loadings within the Basin (see Volume 2). The State assessment of point and non-point source pollutional contributions (see Volume 3) within the Passaic River Basin, in conjunction of the results of the modeling analysis, suggest that a regional rather than a local perspective is needed to provide better and more desirable alternatives. A regional approach would have the advantage of providing a wider range of control alternatives and a systematic evaluation of all pollutional contributions.

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A regional facility plan would provide far more cost-effective controls since all improvements could be incorporated and modeled on a continuous basis. By expanding the engineering tool developed within this facility plan, it would be possible to formulate a comprehensive water source management plan for water quality control within the entire Passaic River Basin. The reduction of discharges or the application of control alternatives within the lower Passaic River Basin alone would do little or nothing for the water quality within the region. Only a comprehensive water quality master plan could hope to succeed in the final determination of the feasibility of improved water quality within the lower Passaic River.

The studies reported herein demonstrate that an engineering tool has been successfully developed and applied in assessing the impacts of specific source of pollutants on the water quality of the receiving water. This engineering tool has provided valuable information upon the various pollutional sources and has been instrumental within the conclusions made during this facility plan. It is possible to extend this tool to provide information upon the solids loadings within local and regional areas as well as to extend the water quality analysis to a regional basis. The expanded tool however, must incorporate all the essential components of the complex network consisting of Newark Bay, the Kills, the Hackensack and Passaic estuaries. Through a concerted effort involving all the local and governmental agencies, it will be possible to formulate a comprehensive water management plan for water quality control and control alternatives for the environmental concern here. Such an endeavor would help delineate the uses of the regional water sources within a set of socio-economic constraints. The end result of this effort would provide

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the scientific basis for establishing clean water quality standards that are commensurate with the designated usage of the receiving stream and the bay.

It is recommended that a study with seven phases, outlined in Figure 6.1, be designed to address these issues to designate uses and the water quality of the receiving water.

The first phase of the study would be the acquisition and documentation of point sources of pollution discharging into the complex network. This task would create a master inventory of all industrial and municipal wastewater treatment facilities describing their levels of treatment, modes of operation and long and short term quality and quantity variations in discharge.

The second phase of the study should be related to the preliminary assessment of all non-point sources contributing to the system. Here two types of sources must be considered: (a)- direct storm runoff from both sewered and unsewered areas into the receiving waters and (b)- contribution of pollutants to the waters from groundwater seepage and benthic exchanges. No new field data is necessary for this preliminary assessment. Available models of rainfall runoff will be used to evaluate the long-term quantity and quality of non-point pollution contribution. For this assessment, model simulations will be made with realistic rates and wherever possible with observed values within the domain of interest. The intent here is to develop a field for a comparative magnitude of the contribution of pollutants from point and non-point sources.

The third phase of the study should consist of extending the receiving water quality and hydrodynamic models to incorporate the Kills, Newark Bay and the two estuaries. The model must then be used with the

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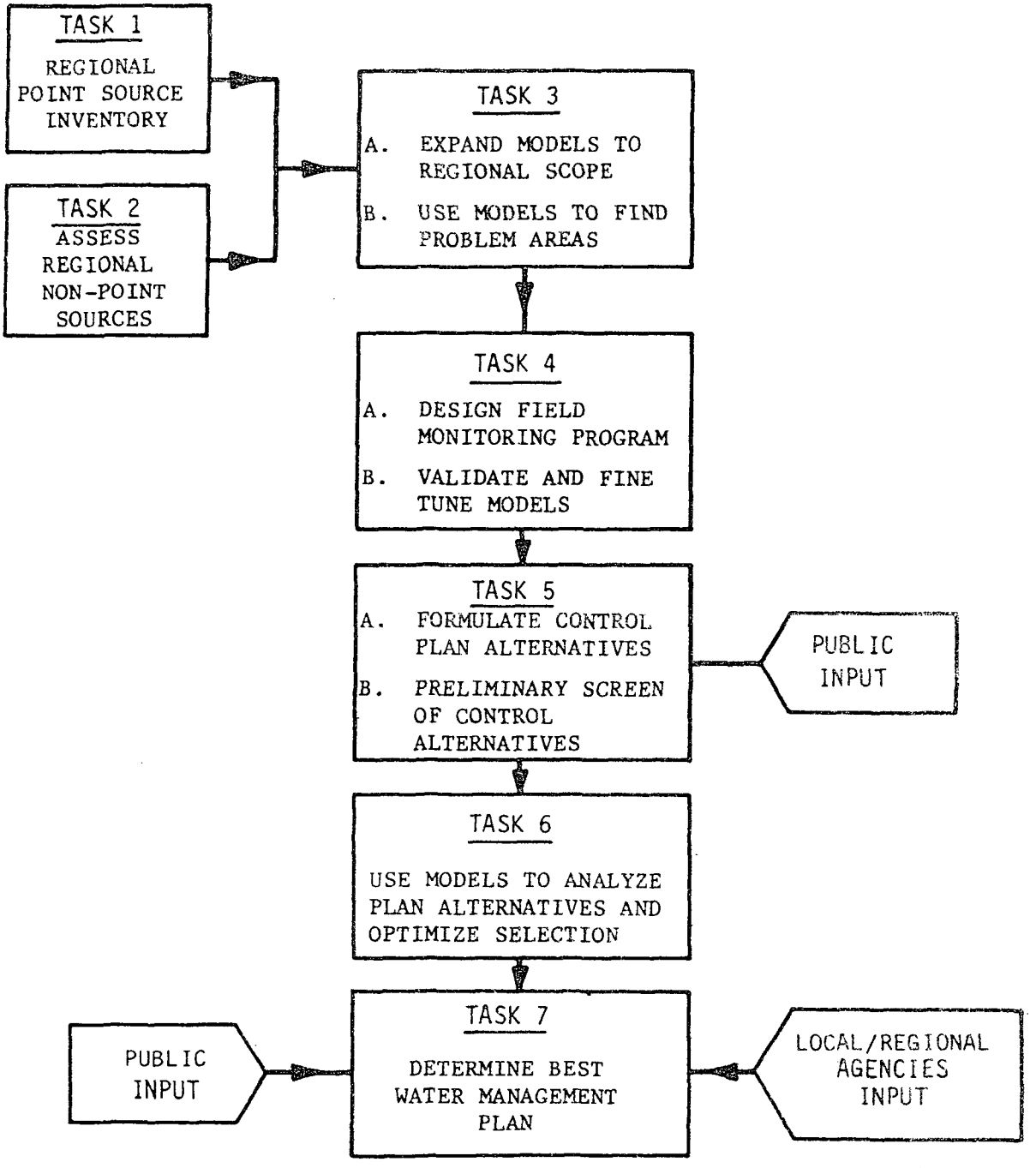

PASSAIC VALLEY SEWERAGE COMMISSIONERS
NEW JERSEY
COMBINED SEWER OVERFLOW FACILITY PLAN

PROPOSED
REGIONAL WATER MANAGEMENT
PLANNING PROCESS
FLOW SCHEMATIC

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Elson T. Killam Associates, Inc.
Environmental and Hydraulic Engineers
27 Bleeker Street Millburn, New Jersey 07041

FIGURE 6.1

generated information in Phase I and Phase II to simulate realistic conditions within the network. This exercise should provide the needed insight to delineate those reaches within the network where severe pollution problems are liable to occur.

The fourth phase of the study will consist of designing an efficient and consistent field monitoring program commensurate with the spatial and temporal scales characteristic of transport processes within the network. Design of field experiments will be based on the results of the simulation discussed in the preceding phase. This phase will also include post-auditing of model results. What is intended here is to reexamine the model performance and validate its results by comparing them with field observed conditions. This endeavor will help fine tune the model and make it more accurate for use in decision making processes.

The fifth phase must deal with formulation of control alternatives which satisfy institutional, social, and economic constraints. These alternatives must first be chosen based on the engineering feasibility. They should then be presented to government agencies for their revisions and recommendations. Finally, an effort must be made to present the available control options to concerned citizens which will be directly affected by plan alterations. This phase will constitute preliminary screening of the conceived controlled alternatives.

The sixth phase will consist of analyzing the expected improvements in water quality as a result of implementing each of the variable control alternatives. This analysis will be made using the model developed specifically for the system of concern. It is expected that during this phase the cost benefit function will be developed which would constitute the basis of selecting the optimum control alternative.

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The seventh phase of the study will consist of presenting the results of the sensitivity analysis described in the preceding phase to local regional agencies responsible for the environmental protection of the Passaic River and Newark Bay complex. Planned formal meetings will provide the forum for engineers, planners and concerned citizens. It is expected that through consultation among various groups involved, the single best water source and water quality management plan can be selected which would best suit and best satisfy the socio-economic restraints of the region.

Control alternatives within the PVSC district have been developed and analyzed to the extent possible. This phase of the facility plan has shown that conditions within many of the combined sewer areas provide for inadequate conveyance of combined flows, and as such require maintenance and alternative measures designed to minimize system problems. In addition to problems within the municipal interceptors, the PVSC combined sewer overflows and trunk system provide inadequate regulation and control of combined flows within many areas.

Except for the newly constructed combined sewer overflows within the City of Newark, the PVSC regulator system is inoperable within many areas of the district. Age and corrosion has required the elimination of many control units, with regulation of combined flows conducted by the manual operation of flap valves where available. The reconstruction of these regulators and implementation of a dynamic or integrated system would provide additional flexibility for control of combined sewer overflows within these areas. Where feasible, construction of swirl or helical bend regulators would provide for better flow control, in addition to implementing physical treatment of combined flows prior to discharge into the receiving waters.

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Capacity problems within the Paterson main line interceptor have been aggravated by the accumulation of debris within the lower portion of the trunk sewer. Estimates obtained from PVSC show that there is a buildup of 24 to 30 inches of hard packed gravel and rocks with an estimated volume of 50 cubic yards downstream from the Market Street regulator chamber. The Passaic Valley Sewerage Commissioners had instituted a contract in 1976 for the removal and cleaning of this material; however, the contractor abandoned this project due to system difficulties. Elimination of the debris from the Paterson main line interceptor (estimated to be approximately 1,500 cubic yards) would provide additional capacity and inline storage for combined flows and such, should be considered for implementation under this facility plan.

The work conducted under Phase I of the facility plan and reported upon herein is preliminary and requires additional analysis. It is therefore imperative that the second phase of the facility plan be implemented upon the review and approval of all regulatory agencies.

All alternative considerations developed under this phase will be discussed and analyzed in detail under the second and final phase of the facility plan. This analysis will be directed towards economic and environmental constraints and will in conjunction with implementation considerations and the views of public interests form the basis for a multi-disciplined evaluation.

Alternative evaluation during the final phase of the facility plan includes the analysis of the selected alternatives developed during Phase I utilizing the calibrated verified model of the lower Passaic River system. Quality and quantity determinations for feasible alternatives will be input to the model, which would then generate the relative impacts

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on the water system. Local and regional alternative schemes will be considered separately so as to develop a full understanding of the relative impact of various alternatives upon the river system. The output from the computer analysis will form direct input to the process of ranking alternatives and the final plan selection.

The cost-effective analysis will be completed in accordance with applicable federal guidelines and will include appropriate operational maintenance costs as well as replacement costs for an alternative plan for a 20 year period. Capital costs for proposed facilities will include estimates of construction costs as well as other related engineering and project costs. The cost-effective analysis will be based on total present worth and will not include an allowance for federal and state grants which may or may not be available at the time of project implementation.

The environmental impacts associated with each local and/or regional system alternative will be evaluated. The environmental impact analysis previously prepared for each component for the overall alternative system will be consolidated and organized into a comprehensive impact discussion. Supplementary analyis required as a result of alternative modifications will be prepared. Beneficial as well as adverse impacts will be described in detail including long-term, short-term, primary and secondary impacts if appropriate.

Additional consideration of economic and socio-environmental issues will be considered during the final phase. Implementation of the proposed plan will be dependent upon various public agencies in addition to input from public and concerned interests involved within the facility plan. Possible effects on the project implementation and time tables of these agencies will be assessed to the extent possible.

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Utilizing all information developed, all alternatives will be evaluated and a final ranking prepared. The final facility plan will include a recommended plan of action that will be both cost-effective and environmentally acceptable to the entire facility planning area. The final facility plan will include the reasoning process involved in the final selection in addition to the possible phases for implementation of the recommended plan.

Phase I of the Passaic Valley Sewerage Commissioners Combined Sewer Overflow Facility Plan has been completed and reported upon herein. Expansion of its scope or implementation of the recommendations and control alternatives proposed requires the review and approval of state and federal agencies. It is recommended that due consideration be given to all recommendations so as to provide for the needs and requirements of the PVSC District.

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APPENDIX

Water Quality Data

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APPENDIX

PASSAIC RIVER WATER QUALITY DATA

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Baseline Sampling
March 1981

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BASELINE

KEARNY

PØINT

3-10/3-20-81

1/3 DEPTH

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BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1/3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	830	8.5	1	A	7.45	6.0	3.4	2.080	NA	NA	3.45	0.418	15.58	6.0	8.10	14.3
3	10	1030	10.5	1	A	7.53	5.3	2.2	1.230	NA	NA	NA	NA	6.68	5.0	8.30	17.3
3	10	1230	12.5	1	A	7.54	4.7	2.7	1.520	NA	NA	2.69	0.324	6.31	5.8	8.00	15.5
3	10	1445	14.8	1	A	7.45	5.9	2.1	1.440	0.032	0.714	NA	NA	8.16	5.5	7.90	10.8
3	10	1709	17.1	1	A	7.43	33.0	6.3	1.130	0.042	0.935	1.98	0.340	10.35	5.0	7.50	9.0
3	10	1930	19.5	1	A	7.39	15.0	3.9	1.630	0.037	0.940	NA	NA	8.53	5.0	9.30	14.0
3	10	2125	21.4	1	A	7.52	10.0	3.4	1.470	0.034	0.585	2.34	0.310	8.90	5.5	8.40	17.0
3	10	2255	22.9	1	A	7.55	10.0	2.7	1.170	0.032	0.524	NA	NA	8.53	5.0	9.10	18.0
3	11	45	24.8	1	A	7.44	5.0	2.7	NA	NA	NA	2.62	0.412	NA	5.0	8.20	16.5
3	11	345	27.8	1	A	7.36	6.5	3.4	1.680	0.039	0.791	NA	NA	4.38	5.1	8.00	11.2
3	11	605	30.1	1	A	7.33	8.0	4.8	1.650	0.039	0.896	NA	NA	5.40	5.0	7.70	7.2
3	11	835	32.5	1	A	7.39	15.0	5.8	1.460	0.042	0.759	2.84	0.694	8.76	6.0	7.75	12.5
3	11	1035	34.6	1	A	7.41	6.0	2.0	1.340	0.039	0.721	NA	NA	6.07	5.0	7.40	17.5
3	11	1240	36.7	1	A	7.51	6.2	3.6	0.761	0.018	0.560	1.96	0.251	8.76	4.8	7.10	17.5
3	11	1530	39.5	1	A	7.46	5.4	3.8	1.460	0.039	0.944	1.64	0.274	4.05	5.0	9.70	11.0
3	11	1705	41.1	1	A	7.42	7.0	3.9	1.490	0.039	1.020	NA	NA	6.41	5.9	7.10	11.2
3	11	1910	43.2	1	A	7.44	9.0	3.6	1.730	0.034	1.200	3.72	0.781	4.72	5.0	7.50	8.1
3	11	2100	45.0	1	A	7.45	5.5	2.9	1.430	0.005	0.634	2.51	0.475	1.01	6.0	7.80	14.9
3	11	2240	46.7	1	A	7.41	44.0	17.1	1.140	0.018	0.601	NA	NA	0.67	4.9	8.20	16.5
3	12	35	48.6	1	A	7.54	5.0	3.9	1.340	0.037	0.582	2.42	0.353	6.07	4.5	7.70	19.8
3	12	225	50.3	1	A	7.44	50.0	16.5	0.936	0.029	0.448	NA	NA	14.11	4.9	6.00	19.0
3	12	445	52.8	1	A	7.46	15.0	6.8	1.630	0.031	0.770	3.58	1.160	7.52	5.0	8.10	11.8
3	12	635	54.6	1	A	7.49	35.0	12.3	1.230	0.029	0.529	NA	NA	13.17	5.0	8.20	11.5
3	12	815	56.3	1	A	7.28	15.0	6.4	1.450	0.044	1.020	2.56	0.716	11.80	4.0	8.00	10.0
3	12	935	57.6	1	A	7.20	7.5	5.1	1.420	0.034	0.585	NA	NA	12.14	5.0	7.40	15.0
3	12	1124	59.4	1	A	7.30	4.5	3.9	1.330	0.039	0.559	2.25	0.341	12.14	5.3	7.40	15.3

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BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1X3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	12	1323	61.4	1	A	7.40	6.5	5.2	1.240	0.034	0.524	NA	NA	9.10	4.8	8.00	17.0
3	12	1451	62.9	1	A	7.30	5.5	4.6	1.860	0.042	0.637	2.77	0.460	13.49	5.8	7.50	15.3
3	12	1635	64.6	1	A	7.30	5.5	3.2	NA	NA	NA	NA	NA	9.10	6.0	NA	9.5
3	12	1805	66.1	1	A	7.30	6.0	3.4	1.430	0.044	0.858	NA	NA	8.43	5.5	8.00	12.9
3	12	1935	67.6	1	A	7.30	6.0	4.4	1.550	0.044	0.939	NA	NA	8.77	5.5	8.50	9.8
3	12	2050	68.8	1	A	7.30	6.5	5.7	1.430	0.031	0.790	NA	NA	6.41	5.5	8.20	9.5
3	12	2210	70.2	1	A	7.40	4.5	3.2	1.520	0.044	0.676	3.01	0.467	9.87	5.5	8.80	15.0
3	13	40	72.7	1	A	7.40	25.0	10.5	1.200	0.044	0.676	2.68	0.456	11.29	4.3	8.20	17.0
3	13	140	73.7	1	A	7.40	20.0	7.5	NA	NA	NA	NA	NA	11.29	4.3	8.20	17.0
3	13	240	74.7	1	A	7.30	80.0	24.0	1.140	0.024	0.514	5.35	2.170	13.17	4.5	8.40	16.5
3	13	340	75.7	1	A	7.30	85.0	27.0	0.964	0.034	0.706	NA	NA	18.81	5.0	7.80	14.5
3	13	440	76.7	1	A	7.30	70.0	21.0	1.260	0.008	0.611	2.92	0.920	27.27	5.0	8.00	12.0
3	13	540	77.7	1	A	7.30	5.7	4.3	1.320	0.013	0.727	NA	NA	8.77	5.0	8.00	12.5
3	13	650	78.8	1	A	7.40	15.0	5.8	1.290	0.044	0.737	3.28	0.524	9.44	5.0	7.90	13.1
3	13	756	79.9	1	A	7.00	5.3	2.4	1.430	0.018	0.884	NA	NA	10.12	5.5	7.25	11.8
3	13	855	80.9	1	A	7.30	18.0	8.7	NA	NA	NA	3.54	0.775	12.22	5.5	7.25	9.5
3	13	956	81.9	1	A	7.30	7.0	3.4	1.250	0.044	0.858	NA	NA	9.78	5.5	6.75	11.3
3	13	1057	82.9	1	A	7.40	6.5	3.8	1.430	0.018	0.682	3.54	0.708	11.28	6.3	7.00	13.5
3	13	1155	83.9	1	A	7.40	8.5	6.2	1.200	0.044	0.575	NA	NA	15.04	6.0	7.50	15.0
3	13	1255	84.9	1	A	7.50	5.5	3.8	1.260	0.039	0.539	3.02	0.646	12.81	6.3	7.00	16.0
3	13	1354	85.9	1	A	7.50	8.5	7.1	1.380	0.018	0.601	NA	NA	13.16	7.0	8.25	15.5
3	13	1456	86.9	1	A	7.50	5.0	2.7	1.020	0.016	0.582	3.36	0.962	6.58	7.0	8.25	16.5
3	13	1555	87.9	1	A	7.40	6.3	6.3	1.050	0.039	0.539	NA	NA	11.28	7.0	8.50	17.0
3	13	1650	88.8	1	A	7.40	5.5	2.8	1.370	0.042	0.536	3.46	0.929	6.74	7.1	8.60	13.5
3	13	1750	89.8	1	A	7.40	7.5	5.4	1.790	0.050	0.852	NA	NA	11.31	6.9	8.00	11.8
3	13	1850	90.8	1	A	7.40	23.0	9.8	1.550	0.034	0.706	7.17	2.330	8.46	6.1	7.70	14.0

94651028?

BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	1950	91.8	1	A	7.30	8.5	5.6	NA	NA	NA	NA	NA	13.16	6.0	7.30	14.8
3	13	2050	92.8	1	A	7.40	5.6	2.6	1.460	0.044	0.716	3.07	0.550	11.28	6.2	6.30	14.4
3	13	2150	93.8	1	A	7.40	7.2	3.6	1.370	0.052	0.931	NA	NA	8.43	6.1	7.30	10.5
3	13	2250	94.8	1	A	7.40	6.2	3.8	1.020	0.018	0.560	2.73	0.686	12.81	6.5	7.80	13.1
3	13	2350	95.8	1	A	7.40	17.0	6.0	1.260	0.039	0.762	NA	NA	18.80	6.1	NA	NA
3	14	50	96.8	1	A	7.50	20.0	3.0	1.320	0.013	0.606	4.16	1.310	13.16	5.5	9.20	17.1
3	14	150	97.8	1	A	7.50	33.0	6.9	0.757	0.029	0.485	NA	NA	15.98	5.3	8.70	17.5
3	14	250	98.8	1	A	7.50	27.0	8.7	0.964	0.024	0.534	2.40	0.462	10.34	5.1	7.70	17.9
3	14	350	99.8	1	A	7.50	40.0	8.1	0.964	0.029	0.549	NA	NA	16.92	5.8	8.50	16.9
3	14	450	100.8	1	A	7.40	67.0	14.8	1.320	0.037	0.683	2.38	0.401	10.34	5.9	8.50	15.0
3	14	550	101.8	1	A	7.40	85.0	18.8	1.020	0.026	0.471	NA	NA	17.86	4.8	8.70	17.5
3	14	650	102.8	1	A	7.50	9.0	4.8	0.846	0.024	0.554	2.74	0.521	11.28	5.1	9.70	14.0
3	14	755	103.9	1	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.9	8.10	14.9
3	14	855	104.9	1	A	7.30	7.0	3.8	1.730	0.034	0.828	2.55	0.408	15.51	4.8	9.00	11.5
3	14	955	105.9	1	A	7.30	7.5	3.2	1.730	0.042	0.978	NA	NA	16.52	4.8	8.60	12.0
3	14	1055	106.9	1	A	7.30	7.0	2.8	1.430	0.039	1.020	3.86	1.180	11.80	4.8	8.40	10.3
3	14	1155	107.9	1	A	7.30	8.0	2.8	1.820	0.039	1.190	NA	NA	4.05	4.9	8.20	12.0
3	14	1255	108.9	1	A	7.40	6.8	3.4	1.490	0.047	0.774	3.06	0.528	13.49	6.1	8.70	14.9
3	14	1355	109.9	1	A	7.50	5.7	3.0	1.260	0.039	0.620	NA	NA	11.29	6.0	8.70	17.3
3	14	1455	110.9	1	A	7.50	7.6	4.6	1.320	0.039	0.640	2.32	0.361	16.93	6.5	8.50	16.0
3	14	1555	111.9	1	A	7.50	6.0	3.4	1.200	0.034	0.544	NA	NA	14.16	5.8	8.70	18.0
3	14	1650	112.8	1	A	7.50	5.5	2.6	0.964	NA	NA	NA	NA	9.78	5.9	8.40	13.5
3	14	1750	113.8	1	A	7.40	15.0	5.2	1.670	0.044	0.899	NA	NA	15.17	5.0	9.00	12.0
3	14	1920	115.5	1	A	7.50	5.0	3.2	0.645	0.010	0.588	1.59	0.233	12.48	6.0	8.00	13.0
3	14	2050	116.8	1	A	7.40	6.0	3.0	1.490	0.037	0.663	NA	NA	12.48	5.0	8.50	9.0
3	14	2150	117.8	1	A	7.40	6.2	3.0	1.870	0.050	1.010	3.24	0.370	12.48	5.2	8.00	9.1

946510283

BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O. [PPM]	SAL [PPT]
3	14	2250	118.9	1	A	7.40	7.3	2.9	2.000	0.029	0.873	NA	NA	10.45	5.0	8.50	8.0
3	14	2350	119.9	1	A	7.40	6.0	3.0	1.460	0.044	1.060	2.16	0.354	9.44	5.0	8.20	8.4
3	15	50	120.9	1	A	7.50	6.5	3.6	1.370	0.039	0.620	NA	NA	20.22	5.0	8.20	13.0
3	15	150	121.9	1	A	7.50	5.5	3.2	1.730	0.047	0.734	2.88	0.372	18.81	5.0	8.70	18.0
3	15	250	122.9	1	A	7.50	5.8	3.4	0.786	0.008	0.854	NA	NA	13.15	4.8	8.80	17.5
3	15	350	123.9	1	A	7.50	6.0	3.2	1.020	0.029	0.509	2.41	0.399	14.84	4.5	9.00	17.9
3	15	450	124.9	1	A	7.50	5.8	3.3	1.260	0.008	0.570	NA	NA	14.50	4.9	9.00	17.5
3	15	550	125.9	1	A	7.50	8.2	6.6	0.964	0.034	0.585	NA	NA	13.49	5.1	8.40	17.2
3	15	650	126.9	1	A	7.40	5.2	3.9	1.320	0.042	0.718	1.94	0.238	14.10	5.1	8.80	15.5
3	15	810	128.2	1	A	7.30	5.0	3.4	1.830	0.047	0.993	5.39	1.170	8.53	4.7	9.40	10.5
3	15	905	129.1	1	A	7.40	4.0	2.8	1.830	0.044	0.996	NA	NA	9.64	5.0	9.00	10.0
3	15	1005	130.1	1	A	7.30	6.4	2.8	1.780	0.044	0.976	3.30	0.373	11.38	5.0	9.40	10.0
3	15	1105	131.1	1	A	7.30	8.3	7.6	1.890	0.044	1.060	NA	NA	11.38	5.7	9.20	9.5
3	15	205	132.1	1	A	7.40	6.0	4.8	1.720	0.097	1.250	4.45	1.020	11.50	7.0	8.80	9.5
3	15	1305	133.1	1	A	7.40	6.0	5.2	1.580	0.044	0.777	NA	NA	14.48	7.0	8.50	13.3
3	15	1405	134.1	1	A	7.50	5.0	4.6	1.780	0.052	0.810	3.78	0.483	15.52	6.5	9.30	14.3
3	15	1505	135.1	1	A	7.50	4.8	3.9	1.610	0.076	0.907	NA	NA	16.55	6.5	9.40	14.8
3	15	1600	136.0	1	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.0	9.50	16.5
3	15	1700	137.0	1	A	7.60	4.5	2.8	1.890	0.034	0.544	4.02	0.919	18.62	6.3	10.80	15.0
3	15	1800	138.0	1	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.1	10.60	15.1
3	15	1900	139.	1	A	7.50	6.0	5.1	1.440	0.050	0.771	NA	NA	3.10	6.5	10.10	14.5
3	15	2000	140.0	1	A	7.40	5.5	2.7	1.670	0.039	0.721	3.25	0.340	12.24	6.3	10.30	12.9
3	15	2100	141.0	1	A	7.50	4.8	2.8	1.530	0.039	0.701	NA	NA	14.48	6.2	10.00	12.5
3	15	2200	142.	1	A	7.30	5.7	2.7	0.942	0.024	0.514	3.09	0.368	12.24	6.0	9.90	11.6
3	15	2300	143.0	1	A	7.40	6.5	4.2	1.830	0.047	0.973	NA	NA	10.01	5.9	9.90	11.0
3	16	5	144.1	1	A	7.40	5.2	3.6	NA	NA	NA	NA	NA	13.35	6.0	9.60	12.9

946510284

BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	105	145.1	1	A	7.40	5.5	3.4	1.600	0.044	0.777	NA	NA	22.76	6.0	10.00	14.8
3	16	200	146.0	1	A	7.50	5.6	4.2	1.190	0.044	0.696	3.79	0.556	15.52	6.0	10.00	15.5
3	16	300	147.0	1	A	7.50	4.2	2.8	0.942	0.042	0.698	NA	NA	15.58	5.1	9.40	16.8
3	16	400	148.0	1	A	7.60	6.5	5.1	0.886	0.050	0.792	3.35	0.359	12.61	5.1	9.40	16.9
3	16	500	149.0	1	A	7.50	5.0	3.4	1.830	0.050	0.792	NA	NA	16.55	5.0	8.40	16.9
3	16	600	150.0	1	A	7.60	4.7	2.4	0.802	0.039	0.580	2.93	0.466	11.13	5.0	7.80	17.3
3	16	700	151.0	1	A	7.50	4.5	3.0	1.220	0.044	0.595	NA	NA	1.48	5.8	8.90	16.1
3	16	805	152.1	1	A	7.40	4.3	2.1	1.670	0.050	0.792	NA	NA	12.23	6.0	8.80	13.5
3	16	905	153.1	1	A	7.40	4.7	2.2	1.720	0.050	0.852	2.93	0.343	11.29	6.3	8.80	12.3
3	16	1005	154.1	1	A	7.40	5.4	2.8	1.720	0.044	0.899	NA	NA	8.46	6.0	8.70	11.8
3	16	1105	155.1	1	A	7.40	5.5	2.7	1.830	0.044	0.976	2.98	0.425	10.34	6.0	8.40	11.3
3	16	1205	156.1	1	A	7.40	5.5	2.8	1.780	0.039	0.863	NA	NA	15.05	6.3	8.80	11.0
3	16	1305	157.1	1	A	7.40	5.8	4.2	1.890	0.050	1.050	2.52	0.582	14.11	6.0	8.60	11.5
3	16	1405	158.1	1	A	7.50	5.6	5.6	1.530	0.044	0.737	NA	NA	21.63	6.3	8.80	15.3
3	16	1505	159.1	1	A	7.50	4.4	2.8	1.530	0.044	0.696	2.41	0.453	15.05	5.8	9.20	15.0
3	16	1600	160.0	1	A	7.60	8.2	4.6	1.020	0.008	0.631	NA	NA	15.05	4.5	10.50	18.0
3	16	1700	161.0	1	A	7.60	4.2	2.4	0.551	0.034	0.585	2.48	0.326	15.05	4.5	10.20	17.0
3	16	1800	162.0	1	A	7.60	5.0	2.8	0.964	0.044	0.737	NA	NA	16.93	4.5	9.80	17.3
3	16	1900	163.0	1	A	7.50	4.6	4.2	0.992	0.034	0.747	2.06	0.295	14.11	5.1	9.80	15.8
3	16	2030	164.5	1	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.0	9.80	15.5
3	16	2200	166.0	1	A	7.50	5.4	3.4	NA	NA	NA	NA	NA	15.99	5.0	9.60	14.5
3	17	5	168.1	1	A	7.50	5.0	3.4	0.816	0.034	0.706	2.74	0.403	13.17	4.5	10.00	16.8
3	17	135	169.6	1	A	7.50	6.5	3.3	NA	NA	NA	NA	NA	12.23	4.5	9.20	16.0
3	17	305	171.1	1	A	7.60	5.7	4.4	0.786	0.034	0.605	2.36	0.245	15.99	4.2	9.50	17.0
3	17	435	172.6	1	A	7.60	5.0	4.1	0.964	0.034	0.645	NA	NA	12.23	4.1	9.40	17.0
3	17	615	174.1	1	A	7.60	5.1	3.2	0.727	0.014	0.668	2.90	0.310	8.09	4.0	9.50	17.0

946510285

BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	17	735	175.6	1	A	7.60	4.5	3.0	0.786	0.032	0.608	NA	NA	16.93	4.0	9.20	17.0
3	17	835	176.6	1	A	6.90	4.0	5.4	NA	NA	NA	2.61	0.320	15.99	3.0	9.80	17.3
3	17	935	177.6	1	A	7.50	5.5	2.2	NA	NA	NA	NA	NA	11.29	3.5	9.60	16.0
3	17	1035	178.6	1	A	7.50	7.5	2.6	NA	NA	NA	2.10	0.322	16.93	4.0	9.40	14.3
3	17	1135	179.6	1	A	7.50	8.7	4.6	NA	NA	NA	NA	NA	17.87	4.8	9.20	14.0
3	17	1235	180.6	1	A	7.50	8.4	2.8	NA	NA	NA	2.35	0.364	20.69	4.8	9.00	13.8
3	17	1335	181.6	1	A	7.40	7.7	3.4	NA	NA	NA	NA	NA	14.11	4.8	9.20	13.8
3	17	1435	182.6	1	A	7.40	7.0	5.6	NA	NA	NA	5.92	2.730	16.93	5.3	9.20	14.0
3	17	1535	183.6	1	A	7.50	6.0	6.3	NA	NA	NA	NA	NA	19.75	5.3	9.40	16.3
3	17	1630	184.5	1	A	7.50	7.8	6.6	0.471	0.001	0.026	2.60	0.660	22.57	5.0	9.50	16.2
3	17	1730	185.5	1	A	7.60	7.5	3.8	0.703	0.016	0.372	NA	NA	20.69	4.4	9.50	16.5
3	17	1830	186.5	1	A	7.60	5.7	5.2	0.558	0.011	0.419	2.55	0.460	14.58	4.5	8.80	16.6
3	17	1930	187.5	1	A	7.60	5.0	3.0	0.761	0.019	0.432	NA	NA	13.17	3.9	10.00	16.9
3	17	2030	188.5	1	A	7.60	6.0	3.4	0.529	0.011	0.271	2.25	0.285	14.11	3.9	11.50	17.0
3	17	2130	189.5	1	A	7.50	5.6	2.0	0.878	0.027	0.592	NA	NA	9.41	4.5	11.40	16.0
3	17	2300	191.0	1	A	7.50	7.7	3.0	0.703	0.011	0.335	2.67	0.356	11.29	3.9	12.00	12.9
3	18	35	192.6	1	A	7.40	8.4	2.7	1.400	0.047	0.951	NA	NA	10.35	4.3	NA	12.0
3	18	205	194.1	1	A	7.40	8.4	3.2	1.280	0.042	0.830	2.38	0.375	12.23	4.0	NA	13.0
3	18	335	195.6	1	A	7.60	6.0	3.4	1.750	0.060	0.791	NA	NA	22.57	5.5	NA	14.5
3	18	505	197.1	1	A	7.60	14.0	4.2	0.994	0.034	0.522	2.25	0.317	21.63	4.0	9.90	16.8
3	18	635	198.6	1	A	7.60	5.5	2.4	0.820	0.027	0.592	NA	NA	14.11	3.8	8.70	17.2
3	18	815	200.3	1	A	7.20	8.3	7.6	1.170	0.044	0.680	3.17	0.549	13.49	4.5	9.80	16.1
3	18	915	201.3	1	A	7.50	5.8	3.9	1.010	0.042	0.640	NA	NA	13.15	5.0	9.00	17.5
3	18	1015	202.3	1	A	7.40	7.8	2.6	1.370	0.034	0.859	3.23	0.507	10.82	5.5	9.20	14.0
3	18	1115	203.3	1	A	7.40	7.6	3.0	1.400	0.052	0.841	NA	NA	14.11	4.3	9.30	13.5
3	18	1215	204.3	1	A	7.40	8.0	3.0	1.460	0.047	1.010	3.46	1.090	4.38	5.0	9.00	12.0

946510286

BASE - HIGH RIVER
KEARNY POINT - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	18	1315	205.3	1	A	7.30	17.0	5.6	1.690	0.052	0.988	NA	NA	12.23	6.0	8.60	12.5
3	18	1415	206.3	1	A	7.40	8.3	3.0	1.600	0.052	1.050	3.25	0.516	23.50	6.5	8.60	14.5
3	18	1515	207.3	1	A	7.40	7.5	3.4	1.660	0.047	1.050	NA	NA	13.17	5.5	9.10	15.3
3	18	1600	208.2	1	A	7.60	5.8	2.8	1.520	0.047	0.720	3.06	0.648	15.99	4.6	9.80	16.8
3	18	1700	209.0	1	A	7.60	18.0	8.8	1.170	0.037	0.603	NA	NA	18.81	5.0	10.10	15.0
3	18	1800	210.0	1	A	7.60	5.2	3.0	0.878	0.037	0.561	2.13	0.403	15.05	4.0	10.00	17.8
3	18	1900	211.0	1	A	7.70	13.0	3.6	0.761	0.016	0.540	NA	NA	16.93	3.5	10.30	17.8
3	18	2000	212.0	1	A	7.70	4.7	3.0	1.110	0.042	0.598	2.58	0.365	13.17	3.5	9.50	17.6
3	18	2100	213.0	1	A	7.70	4.0	1.8	0.732	0.037	0.561	NA	NA	8.46	3.5	10.40	16.8
3	18	2200	214.0	1	A	7.60	4.2	10.6	1.110	0.042	0.598	2.42	0.296	13.17	3.8	9.00	15.1
3	18	2300	215.0	1	A	7.60	6.4	3.2	1.230	0.037	0.856	NA	NA	12.23	3.9	9.80	16.0
3	19	5	216.1	1	A	7.50	7.6	2.6	NA	NA	NA	NA	NA	10.34	4.5	8.30	12.0
3	19	105	217.1	1	A	7.50	7.8	2.8	1.460	0.047	0.762	NA	NA	13.17	4.8	9.00	12.2
3	19	205	218.1	1	A	7.40	7.5	3.2	1.860	0.052	0.925	2.55	0.410	12.23	4.8	8.50	11.0
3	19	305	219.1	1	A	7.50	15.0	3.2	1.580	0.037	0.582	NA	NA	15.05	4.1	8.60	14.0
3	19	405	220.1	1	A	7.60	5.6	3.4	1.630	0.042	0.589	1.76	0.244	NA	4.8	9.10	15.9
3	19	505	221.1	1	A	7.60	8.2	3.8	1.310	0.039	0.622	NA	NA	15.05	4.0	9.40	17.2
3	19	605	222.1	1	A	7.70	5.2	2.8	0.994	0.037	0.582	1.94	0.200	13.17	3.8	9.30	17.8
3	19	705	223.1	1	A	7.70	4.5	2.9	0.994	0.037	0.603	NA	NA	14.11	3.5	9.20	17.8
3	19	805	224.1	1	A	7.60	4.6	13.1	0.994	0.037	0.561	1.64	0.163	NA	3.8	8.80	18.3
3	19	905	225.1	1	A	7.60	5.0	4.1	1.050	0.032	0.566	NA	NA	15.05	3.3	8.50	19.0
3	19	1005	226.1	1	A	7.60	5.2	3.6	1.110	0.042	0.682	2.58	0.475	18.81	3.5	9.50	17.8
3	19	1105	227.1	1	A	7.50	5.9	3.6	1.400	0.042	0.640	NA	NA	7.52	5.0	9.00	17.0
3	19	1205	228.1	1	A	7.50	8.4	4.1	1.260	0.044	0.696	2.44	0.379	20.69	4.5	9.00	15.0
3	19	1305	229.1	1	A	7.40	35.0	4.5	1.400	0.047	0.804	NA	NA	13.15	5.0	8.75	13.5
3	19	1405	230.1	1	A	7.40	14.0	3.9	1.460	0.042	0.682	2.32	0.373	1.88	5.5	8.50	12.0

946510287

BASE - HIGH RIVER
KEARNY POINT - LEVEL 4 - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1505	231.1	1	A	7.50	12.0	5.6	1.400	0.042	0.725	2.62	0.421	14.11	4.5	8.50	14.0
3	19	1600	232.1	1	A	7.60	5.2	3.8	0.849	0.037	0.519	2.44	0.405	19.75	5.0	9.50	16.9
3	19	1700	233.1	1	A	7.60	7.3	5.1	1.400	0.037	0.624	NA	NA	17.87	4.8	9.50	16.8
3	19	1800	234.0	1	A	7.70	17.0	7.5	0.732	0.034	0.522	2.14	0.350	13.17	4.0	9.80	17.8
3	19	1900	235.0	1	A	7.70	5.2	3.4	0.878	0.032	0.482	NA	NA	16.93	3.5	9.70	18.5
3	19	2000	236.0	1	A	7.70	6.1	3.6	0.878	0.004	0.531	2.73	0.973	13.17	3.0	9.00	18.5
3	19	2100	237.0	1	A	7.60	4.3	3.4	0.732	0.016	0.456	NA	NA	14.11	3.5	9.60	18.1
3	19	2200	238.0	1	A	7.60	15.0	3.6	0.703	0.022	0.366	1.81	0.258	14.11	3.5	9.60	18.0
3	19	2300	239.0	1	A	7.60	5.4	3.2	0.820	0.011	0.503	NA	NA	16.93	3.8	9.50	17.2
3	20	5	240.1	1	A	7.50	7.1	4.2	NA	NA	NA	NA	NA	13.02	4.1	9.20	14.0
3	20	105	241.1	1	A	7.50	7.0	3.2	1.460	0.047	0.762	NA	NA	22.57	4.5	8.90	14.0
3	20	205	242.1	1	A	7.50	6.6	4.4	0.703	0.022	0.871	NA	NA	15.05	4.3	8.80	13.1
3	20	305	243.1	1	A	7.40	8.6	3.6	1.340	0.042	0.725	NA	NA	12.80	4.2	8.10	14.8
3	20	405	244.1	1	A	7.50	16.0	7.8	1.110	0.042	0.767	2.05	0.421	14.11	4.1	9.40	15.9
3	20	505	245.1	1	A	7.60	5.3	4.2	0.994	0.016	0.414	NA	NA	15.99	5.0	9.60	16.8
3	20	605	246.1	1	A	7.60	5.5	3.6	NA	NA	NA	NA	NA	NA	4.0	9.50	17.2
3	20	705	247.1	1	A	7.70	6.4	4.6	NA	NA	NA	2.08	0.271	15.05	4.0	9.80	17.8
3	20	805	248.1	1	A	7.70	4.0	3.8	0.994	0.032	0.566	2.33	0.361	2.70	3.0	9.10	19.0

946510288

BASELINE

KEARNY

PØINT

3-10/3-20-81

2/3 DEPTH

946510289

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL F - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	10	83[illegible]	6.5	1	[illegible]	7.43	15.0	4.5	1.730	0.039	0.601	2.85	0.294	14.47	5.0	7.40	15.3
3	10	1030	10.5	1	B	7.52	18.0	3.4	1.010	0.022	0.387	NA	NA	14.09	4.5	7.80	18.0
3	10	1230	12.5	1	B	7.55	12.0	2.6	1.120	0.027	0.445	2.30	0.421	7.42	4.4	7.60	17.5
3	10	1445	14.8	1	B	7.44	12.0	3.3	1.730	0.039	0.791	NA	NA	10.01	5.5	7.40	12.5
3	10	1719	17.3	1	B	7.48	20.0	4.6	1.020	0.016	0.372	4.25	2.190	8.16	4.0	7.00	17.0
3	10	1935	19.6	1	B	7.41	17.0	3.8	1.770	0.039	1.020	NA	NA	10.01	4.5	9.00	17.0
3	10	2130	21.5	1	B	7.39	63.0	10.5	1.680	0.032	0.503	2.73	0.425	11.38	5.0	7.60	17.5
3	10	2330	23.8	1	B	7.54	30.0	5.1	1.140	0.032	0.461	NA	NA	10.39	4.5	9.10	18.0
3	11	40	24.7	1	B	7.56	20.0	6.0	NA	NA	NA	NA	NA	NA	4.5	7.60	17.8
3	11	340	27.7	1	B	7.39	30.0	7.1	1.730	0.034	0.461	2.75	0.395	10.12	5.2	8.10	12.5
3	11	600	30.0	1	B	7.34	20.0	10.1	1.610	0.039	0.707	NA	NA	NA	5.3	7.20	13.8
3	11	830	32.5	1	B	7.38	50.0	11.3	1.270	0.036	0.675	2.25	0.387	NA	5.8	7.50	15.3
3	11	1035	34.6	1	B	7.52	30.0	5.8	1.150	0.036	0.596	NA	NA	5.40	4.8	7.75	18.0
3	11	1243	36.7	1	B	7.46	25.0	9.8	0.685	0.023	0.471	1.72	0.376	7.76	4.8	NA	17.8
3	11	1530	39.5	1	B	7.45	5.5	4.1	1.470	0.036	0.833	NA	NA	7.42	5.0	9.00	13.0
3	11	1710	41.2	1	B	7.39	20.0	8.4	0.867	0.023	0.609	2.54	0.634	8.77	5.0	6.00	16.5
3	11	1915	43.3	1	B	7.42	18.0	8.4	1.630	0.041	1.089	NA	NA	6.41	5.0	7.20	16.5
3	11	2110	45.2	1	B	7.45	5.4	4.6	1.440	0.036	0.616	2.22	0.398	7.76	5.5	7.80	15.5
3	11	2250	46.8	1	B	7.50	25.0	6.6	0.942	0.057	0.693	NA	NA	11.28	4.9	8.10	17.0
3	12	30	48.5	1	B	7.49	4.2	3.3	0.891	0.026	0.487	3.01	1.260	7.42	4.3	8.20	18.0
3	12	215	50.3	1	B	7.48	45.0	10.1	1.240	0.026	0.487	NA	NA	13.49	4.2	8.20	19.8
3	12	440	52.7	1	B	7.46	5.5	4.6	1.450	0.041	0.848	2.31	0.408	7.08	5.0	8.30	14.0
3	12	630	54.5	1	B	7.43	35.0	6.3	1.330	0.036	0.695	NA	NA	18.81	4.3	8.10	17.0
3	12	805	56.1	1	B	7.30	20.0	4.3	1.360	0.041	0.947	NA	NA	11.13	4.5	7.50	14.8
3	12	930	57.4	1	B	7.30	15.0	5.1	1.200	0.036	0.635	2.67	0.818	12.14	5.3	7.20	16.3
3	12	1120	59.3	1	B	7.40	15.0	3.8	1.200	0.031	0.561	NA	NA	11.80	4.5	7.20	17.0

946510290

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL B - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	12	1315	61.3	1	B	7.40	6.0	4.3	1.010	0.031	0.482	1.48	0.459	7.08	4.3	7.20	18.0
3	12	1455	62.9	1	B	7.40	7.0	6.6	0.920	0.031	0.482	NA	NA	13.82	5.0	7.10	16.5
3	12	1645	64.9	1	B	7.30	6.5	6.2	1.070	0.036	0.556	2.27	0.403	12.48	6.0	NA	11.5
3	12	1810	66.2	1	B	7.30	6.0	4.2	0.699	0.026	0.487	NA	NA	11.13	4.9	7.40	16.5
3	12	1945	67.8	1	B	7.40	6.5	3.6	1.640	0.041	0.867	2.49	0.547	10.79	5.3	7.00	15.0
3	12	2100	69.0	1	B	7.40	25.0	8.8	1.060	0.036	0.556	NA	NA	15.05	5.0	7.80	15.5
3	12	2220	70.3	1	B	7.40	5.0	4.2	1.190	0.039	0.672	2.37	0.312	12.23	5.0	8.00	16.5
3	13	45	72.8	1	B	7.40	6.5	3.6	0.873	0.031	0.542	1.81	0.388	12.23	4.5	8.20	17.5
3	13	145	73.8	1	B	7.40	22.0	9.4	0.903	0.036	0.635	NA	NA	11.28	5.0	8.40	18.0
3	13	245	74.8	1	B	7.40	30.0	16.8	1.280	0.031	0.522	3.33	1.130	16.93	4.3	8.20	18.0
3	13	345	75.8	1	B	7.40	25.0	10.1	1.070	0.018	0.634	NA	NA	13.17	5.0	7.80	16.2
3	13	445	76.8	1	B	7.40	5.5	4.4	1.140	0.036	0.556	2.50	0.510	10.79	4.3	7.90	17.3
3	13	545	77.8	1	B	7.30	25.0	11.2	1.190	0.020	0.691	NA	NA	10.35	4.5	8.30	16.0
3	13	645	78.8	1	B	7.30	35.0	11.1	0.928	0.020	0.572	5.62	2.460	20.69	4.1	7.40	16.9
3	13	750	79.8	1	B	7.30	4.5	6.6	1.390	0.031	0.621	2.77	0.566	12.22	5.5	6.25	14.5
3	13	850	80.8	1	B	7.20	8.0	12.0	1.340	0.036	0.974	NA	NA	15.04	5.5	6.00	15.3
3	13	950	81.8	1	B	7.20	3.5	7.8	1.730	0.036	0.853	NA	NA	13.16	5.5	6.50	16.0
3	13	1050	82.8	1	B	7.30	4.5	9.6	1.250	0.031	0.601	4.25	1.510	15.98	6.0	6.50	15.8
3	13	1150	83.8	1	B	7.30	30.0	13.8	1.420	0.041	0.670	NA	NA	11.28	6.0	7.50	16.0
3	13	1250	84.9	1	B	7.30	35.0	14.1	1.700	0.031	0.522	2.59	0.651	16.92	5.5	6.75	17.0
3	13	1350	85.8	1	B	7.30	6.5	7.5	1.120	0.031	0.522	NA	NA	15.98	5.8	7.75	15.0
3	13	1450	86.8	1	B	7.40	7.0	12.0	0.908	0.031	0.522	2.49	0.499	18.80	6.0	7.75	17.5
3	13	1550	87.8	1	B	7.40	15.0	14.7	1.190	0.031	0.522	NA	NA	11.28	5.3	8.25	17.8
3	13	1700	89.1	1	B	7.30	20.0	12.9	0.767	0.031	0.601	3.76	1.370	10.45	6.0	7.90	16.0
3	13	1800	90.1	1	B	7.30	6.0	3.6	1.510	0.039	0.790	NA	NA	8.43	5.9	8.00	14.5
3	13	1900	91.0	1	B	7.40	20.0	6.3	1.180	0.041	0.947	2.52	0.569	15.04	5.5	7.20	17.0

946510291

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL A - MAX DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	13	2000	92.0	1	B	7.30	5.0	5.6	1.300	0.039	0.711	NA	NA	12.22	5.9	7.10	16.0
3	13	2100	93.1	1	B	7.40	20.0	18.8	1.150	0.036	0.635	3.04	0.519	11.28	5.2	7.60	17.1
3	13	2200	94.1	1	B	7.40	35.0	17.2	1.060	0.026	0.440	NA	NA	8.46	5.5	7.80	17.1
3	13	2300	95.0	1	B	7.30	5.0	4.5	1.020	0.034	0.519	2.75	0.490	11.12	5.9	8.00	16.0
3	14	0	96.0	1	B	7.30	5.0	4.4	1.250	0.028	0.525	2.17	0.428	14.49	5.9	NA	NA
3	14	55	96.9	1	B	7.40	6.5	13.2	0.966	0.036	0.596	2.87	0.645	11.12	5.3	9.20	17.8
3	14	155	97.9	1	B	7.40	6.0	4.4	0.836	0.020	0.296	NA	NA	11.46	5.0	8.10	18.3
3	14	255	98.9	1	B	7.50	4.0	6.0	0.772	0.034	0.479	1.05	0.251	21.62	4.8	7.60	18.5
3	14	355	99.9	1	B	7.40	4.0	6.6	0.772	0.031	0.443	NA	NA	14.10	4.9	8.60	18.3
3	14	455	100.9	1	B	7.40	4.5	7.5	1.490	0.020	0.442	3.55	0.886	7.52	5.2	8.70	17.0
3	14	555	101.9	1	B	7.50	5.0	5.7	0.785	0.023	0.411	NA	NA	14.16	5.5	8.50	13.0
3	14	655	102.9	1	B	7.40	4.5	3.3	0.558	0.004	0.541	4.83	2.380	9.77	4.0	9.80	18.2
3	14	750	103.8	1	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.8	7.80	18.0
3	14	850	104.8	1	B	7.30	25.0	7.8	1.130	0.031	0.561	2.19	0.512	15.04	4.7	8.10	18.2
3	14	950	105.8	1	B	7.40	3.2	8.8	1.140	0.031	0.522	NA	NA	23.60	4.9	7.90	18.0
3	14	1050	106.8	1	B	7.10	9.0	8.6	1.350	0.034	0.598	3.81	1.740	24.28	4.9	8.00	14.6
3	14	1150	107.8	1	B	7.30	3.6	5.0	1.620	0.041	0.826	NA	NA	11.13	5.3	7.80	16.0
3	14	1250	108.8	1	B	7.30	4.5	4.6	1.300	0.004	0.549	NA	3.870	11.29	5.5	8.10	17.5
3	14	1350	109.8	1	B	7.40	3.0	4.4	1.120	0.031	0.542	NA	NA	11.29	5.7	8.40	17.3
3	14	1450	110.8	1	B	7.40	5.2	6.2	1.060	0.028	0.545	2.26	0.606	11.29	5.7	8.10	18.0
3	14	1550	111.8	1	B	7.50	5.7	10.6	0.844	0.028	0.505	NA	NA	7.08	5.9	8.30	18.0
3	14	1700	113.0	1	B	7.50	6.5	3.6	1.360	0.031	0.858	2.26	0.525	10.45	5.1	8.00	17.2
3	14	1800	114.0	1	B	7.40	37.0	10.0	0.596	0.044	1.030	NA	NA	11.80	5.0	8.00	17.5
3	14	1930	115.5	1	B	7.50	5.0	2.2	0.896	0.020	0.452	2.30	0.385	13.83	5.1	7.50	17.5
3	14	2100	117.0	1	B	7.40	7.0	4.4	1.030	0.023	0.411	NA	NA	15.51	5.5	7.90	12.1
3	14	2200	118.0	1	B	7.40	5.2	3.8	1.330	0.026	0.448	2.29	0.309	11.13	6.0	7.80	11.5

946510292

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL B - PX3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	14	2300	119.[illegible]	1	B	7.30	5.0	7.4	1.370	0.028	0.604	NA	NA	13.83	5.5	7.50	11.0
3	15	[illegible]	120.[illegible]	1	B	7.40	8.4	4.8	NA	NA	NA	NA	NA	11.21	5.1	8.20	13.4
3	15	50	120.[illegible]	1	B	7.50	3.5	3.6	0.735	0.073	0.685	NA	NA	11.29	4.5	8.60	17.9
3	15	150	121.[illegible]	1	B	7.50	4.6	8.0	1.110	0.004	0.572	3.41	1.260	20.69	3.9	8.80	18.5
3	15	250	122.[illegible]	1	B	7.50	8.2	12.8	0.710	0.015	1.020	NA	NA	22.58	4.0	9.40	17.8
3	15	350	123.[illegible]	1	B	7.50	4.7	4.6	1.140	0.015	0.473	2.91	1.030	13.17	3.9	9.50	18.8
3	15	450	124.8	1	B	7.50	6.2	10.0	0.877	0.010	0.568	NA	NA	15.99	4.2	8.70	18.5
3	15	550	125.8	1	B	7.50	9.0	12.6	1.030	0.026	0.552	2.61	0.421	30.10	4.0	8.30	18.1
3	15	650	126.[illegible]	1	B	7.50	12.0	6.0	1.610	0.041	0.874	NA	NA	31.98	4.1	8.90	17.9
3	15	805	128.1	1	B	7.40	25.0	9.3	1.830	0.036	1.010	3.72	0.542	12.24	5.0	8.80	14.0
3	15	900	129.[illegible]	1	B	7.40	7.2	4.4	1.640	0.039	0.991	NA	NA	5.19	5.0	8.60	11.5
3	15	1000	130.0	1	B	7.40	7.0	4.2	1.330	0.028	0.595	3.77	0.759	7.79	4.8	8.60	15.0
3	15	1100	131.[illegible]	1	B	7.40	7.5	4.1	1.220	0.036	0.677	NA	NA	11.13	5.5	8.10	13.5
3	15	1200	132.[illegible]	1	B	7.30	15.0	5.8	1.670	0.036	0.834	4.62	1.140	13.45	6.0	8.20	16.5
3	15	1300	133.0	1	B	7.40	15.0	3.4	1.440	0.028	0.595	NA	NA	12.98	6.8	8.40	15.8
3	15	1400	134.0	1	B	7.50	15.0	5.1	1.470	0.036	0.587	3.25	0.386	16.55	6.0	8.60	15.8
3	15	1500	135.[illegible]	1	B	7.40	40.0	12.0	1.190	0.041	0.650	NA	NA	8.90	5.8	8.90	16.5
3	15	1610	136.2	1	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.5	9.50	17.2
3	15	1710	137.2	1	B	7.60	6.8	7.2	1.160	0.023	0.555	2.69	0.408	15.52	5.5	10.20	16.5
3	15	1810	138.2	1	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.8	10.30	16.1
3	15	1910	139.2	1	B	7.50	5.0	3.6	1.220	0.031	0.637	NA	NA	12.98	6.1	10.00	14.9
3	15	2010	140.2	1	B	7.50	5.2	3.3	1.300	0.036	0.767	3.66	0.445	12.41	6.3	10.20	13.6
3	15	2110	141.2	1	B	7.50	5.5	4.6	1.330	0.031	0.727	NA	NA	17.59	6.0	10.00	14.0
3	15	2210	142.2	1	B	7.50	4.5	3.0	1.580	0.036	0.722	2.99	0.749	17.59	6.0	9.80	13.4
3	15	2310	143.2	1	B	7.40	6.2	3.6	1.440	0.028	0.550	NA	NA	10.76	6.0	9.40	13.4
3	16	[illegible]	144.[illegible]	1	B	7.50	35.0	8.4	NA	NA	NA	NA	NA	7.42	5.8	9.70	16.1

946510293

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL B - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	100	145.1	1	B	7.40	15.0	5.4	1.280	0.031	0.682	NA	NA	7.79	5.9	9.80	15.5
3	16	155	145.9	1	B	7.50	7.0	5.2	1.160	0.036	0.587	3.62	0.488	19.66	5.8	9.80	15.8
3	16	255	146.9	1	B	7.60	8.0	4.5	1.030	0.031	0.502	NA	NA	14.48	5.0	9.50	17.1
3	16	355	147.9	1	B	7.60	4.5	2.8	0.942	0.023	0.510	2.56	0.463	15.52	5.0	9.80	17.8
3	16	455	148.9	1	B	7.60	9.5	4.4	0.691	0.020	0.333	NA	NA	12.41	5.0	8.20	17.9
3	16	555	149.9	1	B	7.60	15.0	6.0	0.718	0.026	0.507	3.41	0.665	17.59	5.0	7.60	17.8
3	16	650	150.8	1	B	7.60	17.0	5.1	0.830	0.031	0.547	NA	NA	17.59	5.0	8.40	17.8
3	16	800	152.1	1	B	7.40	27.0	5.4	1.360	0.036	0.587	NA	NA	28.22	5.8	8.70	15.3
3	16	900	153.1	1	B	7.40	5.5	3.8	1.670	0.031	0.727	3.15	0.732	1.69	6.0	8.60	13.3
3	16	1000	154.0	1	B	7.40	33.0	10.8	1.670	0.002	0.778	NA	NA	14.72	6.0	8.40	15.3
3	16	1100	155.0	1	B	7.50	65.0	14.4	1.220	0.015	0.640	3.25	0.821	NA	6.0	8.00	15.5
3	16	1200	156.1	1	B	7.50	20.0	9.9	1.640	0.040	0.816	NA	NA	19.02	5.5	8.40	16.3
3	16	1300	157.0	1	B	7.50	5.5	3.6	1.160	0.034	0.581	2.70	0.532	15.34	5.5	8.40	15.8
3	16	1400	158.0	1	B	7.50	6.5	3.8	1.280	0.037	0.598	NA	NA	NA	5.5	8.70	16.0
3	16	1500	159.1	1	B	7.60	8.0	3.6	1.110	0.020	0.575	NA	NA	NA	5.3	8.80	16.8
3	16	1610	160.2	1	B	7.60	6.5	4.6	0.982	0.037	0.417	NA	NA	NA	4.5	10.40	18.3
3	16	1710	161.2	1	B	7.60	8.0	4.5	0.864	0.023	0.511	2.47	0.589	18.81	4.3	9.60	18.2
3	16	1810	162.2	1	B	7.60	5.2	3.4	0.781	0.015	0.419	NA	NA	17.87	4.3	9.20	18.2
3	16	1910	163.2	1	B	7.60	5.6	5.4	0.867	0.020	0.474	2.48	0.612	22.57	4.6	9.20	18.0
3	16	2030	164.5	1	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.1	9.20	17.5
3	16	2210	166.2	1	B	7.60	15.0	4.8	0.873	0.018	0.476	NA	NA	17.87	4.5	8.80	18.1
3	17	0	168.0	1	B	7.50	6.7	3.2	0.846	0.012	0.563	NA	NA	9.41	4.0	10.20	19.0
3	17	130	169.5	1	B	7.60	7.2	3.6	1.110	0.026	0.629	NA	NA	13.17	3.6	9.40	17.0
3	17	300	171.0	1	B	7.50	6.0	3.4	0.843	0.009	0.545	2.22	0.592	10.30	3.5	9.70	18.0
3	17	430	172.5	1	B	7.60	15.0	3.0	0.749	0.026	0.569	NA	NA	15.99	3.8	9.00	18.2
3	17	600	174.	1	B	7.60	6.0	3.2	1.080	0.026	0.549	1.97	0.303	11.29	3.0	9.40	18.0

946510294

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL B - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	17	730	175.5	1	B	7.60	5.8	3.4	0.548	0.020	0.534	NA	NA	30.10	3.0	9.60	18.8
3	17	830	176.5	1	B	6.90	20.0	5.1	NA	NA	NA	2.43	0.667	17.87	4.0	9.60	18.0
3	17	930	177.5	1	B	7.50	5.5	2.8	NA	NA	NA	NA	NA	10.35	4.0	9.40	16.0
3	17	1030	178.5	1	B	7.50	35.0	10.4	NA	NA	NA	2.19	0.479	11.29	4.5	9.30	16.0
3	17	1130	179.5	1	B	7.50	15.0	4.4	NA	NA	NA	NA	NA	18.81	5.0	9.00	14.5
3	17	1230	180.5	1	B	7.40	37.0	8.5	NA	NA	NA	3.23	1.370	14.11	5.0	8.60	14.8
3	17	1330	181.5	1	B	7.50	25.0	7.6	NA	NA	NA	NA	NA	8.46	4.8	8.80	15.0
3	17	1430	182.5	1	B	7.40	63.0	13.2	NA	NA	NA	2.37	0.634	13.17	5.0	8.90	15.3
3	17	1530	183.5	1	B	7.60	7.0	5.0	NA	NA	NA	NA	NA	15.99	5.3	9.40	16.5
3	17	1840	186.7	1	B	7.60	6.0	3.0	0.813	0.009	0.365	1.95	0.277	14.11	4.5	8.60	17.5
3	17	1940	187.7	1	B	7.60	6.2	3.0	0.991	0.009	0.284	NA	NA	13.49	4.1	9.70	17.6
3	17	2040	188.7	1	B	7.60	4.7	2.7	0.650	0.002	0.414	2.21	0.521	14.84	4.0	10.50	17.6
3	17	2140	189.7	1	B	7.50	5.0	2.6	1.200	0.026	0.589	NA	NA	9.41	4.5	11.20	16.6
3	17	2310	191.2	1	B	7.50	6.5	3.2	1.480	0.015	0.560	2.51	0.415	13.17	4.5	11.50	13.5
3	18	30	192.5	1	B	7.40	9.0	5.2	1.040	0.004	0.289	NA	NA	12.23	3.5	NA	13.1
3	18	200	194.0	1	B	7.30	17.0	4.6	1.610	0.034	0.903	2.57	0.511	14.11	3.0	NA	16.0
3	18	330	195.5	1	B	7.50	6.7	4.8	1.450	0.031	0.785	NA	NA	31.96	4.5	NA	16.0
3	18	530	197.5	1	B	7.60	7.2	2.7	0.969	0.026	0.549	2.21	0.455	9.44	3.5	10.00	17.6
3	18	630	198.5	1	B	7.60	6.0	3.9	0.871	0.026	0.549	NA	NA	11.46	3.0	9.10	18.0
3	17	1640	232.7	1	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.0	9.20	16.5
3	17	1740	233.7	1	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.5	9.40	17.6
3	18	810	248.2	1	B	7.50	8.7	2.8	1.220	0.028	0.607	3.07	0.921	12.14	4.5	9.40	16.5
3	19	91	249.2	1	B	7.50	25.0	5.8	1.130	0.015	0.459	NA	NA	20.69	4.8	9.40	15.8
3	19	1017	250.3	1	B	7.40	18.0	7.2	1.750	0.037	0.819	2.98	0.604	20.69	5.0	9.10	14.5
3	18	1113	251.2	1	B	7.40	15.0	5.6	1.700	0.037	0.819	NA	NA	16.93	4.5	9.10	14.5
3	18	1210	252.2	1	B	7.40	8.5	3.3	1.810	0.034	0.883	3.11	0.612	23.51	4.5	8.40	15.5

94510295

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL B - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	18	1310	253.2	1	B	7.40	17.0	5.6	1.130	0.042	0.978	NA	NA	7.08	5.0	8.60	16.5
3	18	1410	254.2	1	B	7.40	8.8	3.2	0.917	0.026	0.589	3.19	0.785	15.99	4.5	9.30	18.0
3	18	1510	255.2	1	B	7.50	7.0	2.8	1.800	0.020	1.040	NA	NA	15.05	4.5	9.20	15.8
3	18	1610	256.2	1	B	7.50	18.0	6.0	1.240	0.031	0.664	2.84	0.497	13.46	4.1	9.60	17.5
3	18	1710	257.2	1	B	7.60	20.0	8.1	1.220	0.023	0.552	NA	NA	22.93	4.0	9.80	17.1
3	18	1810	258.2	1	B	7.60	16.0	4.8	0.658	0.026	0.589	2.63	0.553	23.60	3.9	9.80	18.0
3	18	1910	259.2	1	B	7.70	5.7	4.2	0.905	0.026	0.609	NA	NA	16.93	3.5	9.70	18.2
3	18	2010	260.2	1	B	7.70	4.2	3.2	0.520	0.009	0.707	2.70	0.715	15.05	3.5	9.20	18.0
3	18	2110	261.2	1	B	7.70	15.0	5.6	1.180	0.031	0.725	NA	NA	17.87	3.6	9.70	18.0
3	18	2210	262.2	1	B	7.60	4.5	3.4	1.040	0.015	0.640	2.98	0.829	17.87	4.0	8.90	16.9
3	18	2310	263.2	1	B	7.60	6.4	3.4	1.250	0.020	0.555	NA	NA	12.48	4.0	9.70	16.6
3	19	0	264.0	1	B	7.50	27.0	8.8	NA	NA	NA	NA	NA	20.91	4.9	8.60	13.0
3	19	100	265.0	1	B	7.50	17.0	7.1	NA	NA	NA	NA	NA	19.75	4.2	9.00	15.0
3	19	200	266.0	1	B	7.40	8.6	3.6	1.810	0.037	0.859	3.54	0.783	15.05	4.8	8.60	14.9
3	19	300	267.0	1	B	7.40	20.0	5.8	1.350	0.037	0.759	NA	NA	20.23	4.0	9.00	16.0
3	19	400	268.0	1	B	7.60	18.0	6.3	0.669	0.028	0.667	3.03	0.564	20.69	4.3	9.00	16.2
3	19	500	269.0	1	B	7.60	5.3	3.4	1.130	0.026	0.569	NA	NA	11.80	3.9	9.40	17.8
3	19	600	270.0	1	B	7.70	9.0	4.8	0.956	0.026	0.549	2.16	0.355	14.11	3.7	9.10	18.2
3	19	700	271.0	1	B	7.70	15.0	4.7	0.996	0.018	0.436	NA	NA	18.81	3.1	8.70	19.1
3	19	800	272.0	1	B	7.60	6.0	3.2	1.070	0.018	0.516	2.13	0.353	15.99	3.5	8.40	18.5
3	19	900	273.0	1	B	7.60	21.0	8.6	1.160	0.020	0.555	NA	NA	28.22	3.3	8.40	18.5
3	19	1000	274.0	1	B	7.70	5.3	3.8	1.060	0.015	0.439	1.55	0.277	5.73	3.5	9.25	18.0
3	19	1100	275.0	1	B	7.60	4.5	3.8	1.110	0.026	0.508	NA	NA	13.17	4.8	9.00	17.5
3	19	1200	276.0	1	B	7.50	7.7	4.2	1.500	0.031	0.664	2.64	0.527	14.11	4.5	9.00	15.5
3	19	1300	277.0	1	B	7.50	14.0	3.8	1.680	0.037	0.819	NA	NA	15.99	4.5	8.50	14.0
3	19	1400	278.0	1	B	7.40	16.0	6.4	1.620	0.037	0.799	2.34	0.455	15.05	5.0	6.50	13.5

946510296

BASELINE RIVER SAMPLING
KEARNY POINT - LEVEL B - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1500	279.0	1	B	7.60	6.8	4.4	1.720	0.006	0.770	NA	NA	15.05	4.0	8.50	17.0
3	19	1610	280.2	1	B	7.60	20.0	7.2	1.150	0.015	0.399	2.70	0.722	24.45	4.5	9.30	17.5
3	19	1710	281.2	1	B	7.60	22.0	8.6	1.360	0.031	0.584	NA	NA	9.40	4.5	9.40	17.0
3	19	1810	282.2	1	B	7.70	18.0	5.4	1.120	0.039	0.544	2.46	0.554	27.75	4.0	9.50	17.9
3	19	1910	283.2	1	B	7.70	7.5	4.0	0.965	0.020	0.494	NA	NA	12.23	3.9	9.40	18.6
3	19	2010	284.2	1	B	7.70	6.4	4.2	0.981	0.009	0.525	2.17	0.433	17.87	3.5	8.50	18.8
3	19	2110	285.2	1	B	7.70	8.4	4.6	1.190	0.028	0.587	NA	NA	23.51	3.5	8.80	18.8
3	19	2210	286.2	1	B	7.70	7.4	4.8	1.250	0.026	0.549	2.02	0.349	21.63	3.9	9.40	18.2
3	19	2310	287.2	1	B	7.60	5.4	3.8	0.956	0.020	0.474	NA	NA	19.75	4.0	9.40	17.0
3	20	0	288.0	1	B	7.50	6.7	3.6	NA	NA	NA	NA	NA	19.75	3.9	9.50	15.0
3	20	100	289.0	1	B	7.50	6.9	3.4	NA	NA	NA	NA	NA	15.05	4.1	9.10	15.5
3	20	200	290.0	1	B	7.60	6.5	4.2	1.620	0.037	0.779	2.56	0.613	34.80	4.5	8.40	17.0
3	20	300	291.0	1	B	7.40	20.0	3.0	1.590	0.040	0.776	NA	NA	17.87	3.9	9.00	18.0
3	20	400	292.0	1	B	7.60	18.0	6.4	1.770	0.040	0.897	2.80	0.811	13.17	3.8	9.40	17.5
3	20	500	293.0	1	B	7.70	25.0	7.2	1.450	0.031	0.604	NA	NA	27.27	4.5	9.70	17.5
3	20	600	294.0	1	B	7.60	6.3	4.4	NA	NA	NA	NA	NA	33.89	4.0	9.50	17.8
3	20	700	295.0	1	B	7.70	18.0	6.4	NA	NA	NA	NA	NA	41.38	3.9	9.80	18.5
3	20	800	296.0	1	B	7.70	8.4	4.3	0.730	0.015	0.359	1.87	0.402	13.17	2.8	9.60	19.5

946510297

BASELINE

JACKSØN STREET

3-10/3-20-81

1/3 DEPTH

946510298

BASELINE RIVER SAMPLING
JACKSON STREET - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	930	9.5	2	A	7.36	12.0	3.2	1.650	0.051	1.260	1.62	0.305	5.19	5.0	9.60	7.0
3	10	1130	11.5	2	A	7.45	10.0	3.0	1.660	0.051	0.942	NA	NA	5.56	5.5	8.50	8.5
3	10	1330	13.5	2	A	7.40	13.0	2.6	1.700	0.046	0.942	2.93	0.340	10.76	5.0	8.30	6.5
3	10	1535	15.6	2	A	7.43	17.0	3.3	1.680	0.051	1.400	NA	NA	11.38	5.0	8.70	3.0
3	10	1810	18.3	2	A	7.47	17.0	3.3	1.610	0.056	1.670	2.87	0.491	10.35	5.0	8.50	NA
3	10	2025	20.4	2	A	7.43	15.0	2.7	1.650	0.056	1.530	NA	NA	11.38	5.0	9.90	3.0
3	10	2202	22.0	2	A	7.36	40.0	6.6	1.170	0.053	0.606	2.23	0.374	8.28	5.0	9.40	7.5
3	10	2340	23.7	2	A	7.44	10.0	3.0	1.750	0.046	0.711	NA	NA	11.87	6.0	8.00	14.1
3	11	155	25.9	2	A	7.31	6.5	4.4	1.930	0.051	1.120	1.90	0.261	4.05	5.0	8.30	7.8
3	11	455	28.9	2	A	7.36	20.0	3.4	1.620	0.046	1.170	NA	NA	7.08	5.2	9.00	2.8
3	11	730	31.5	2	A	7.43	15.0	2.8	1.810	0.056	1.670	3.03	0.434	5.40	5.5	9.00	1.0
3	11	949	33.7	2	A	7.42	8.5	2.8	1.620	0.043	1.410	2.95	0.362	6.74	5.3	8.60	4.8
3	11	1135	35.6	2	A	7.43	6.5	3.3	1.510	0.043	1.080	NA	NA	8.77	5.3	8.00	10.3
3	11	1405	38.1	2	A	7.42	6.5	2.6	1.050	0.021	0.605	2.86	0.360	10.12	5.5	10.75	8.0
3	11	1615	40.3	2	A	7.46	15.0	2.8	1.650	0.045	1.460	NA	NA	10.34	5.5	7.80	4.0
3	11	1805	42.1	2	A	7.51	17.0	3.2	1.740	0.043	1.440	3.00	0.495	10.34	5.5	9.00	1.9
3	11	2010	44.2	2	A	7.41	20.0	4.1	1.810	0.037	1.300	3.28	0.343	11.29	5.5	11.00	1.5
3	11	2200	46.0	2	A	7.49	7.0	2.2	1.830	0.045	1.400	2.66	0.315	8.77	5.0	NA	12.5
3	11	2335	47.6	2	A	7.46	6.6	2.7	1.550	0.037	0.837	NA	NA	9.10	5.1	8.80	10.9
3	12	130	49.5	2	A	7.49	4.9	2.7	1.400	0.037	0.699	2.85	0.437	10.79	5.3	7.60	12.9
3	12	350	51.8	2	A	7.45	8.8	2.7	1.480	0.043	0.997	NA	NA	12.23	4.9	8.40	6.5
3	12	525	53.4	2	A	7.47	20.0	3.6	1.800	0.045	1.360	3.21	0.558	13.17	5.0	8.90	3.8
3	12	720	55.3	2	A	7.54	15.0	1.7	1.970	0.051	1.680	NA	NA	10.34	5.1	9.10	1.8
3	12	855	56.9	2	A	7.37	8.0	2.7	1.910	0.048	1.620	3.39	0.411	7.76	5.0	9.00	2.0
3	12	1045	58.8	2	A	7.30	7.2	2.2	1.860	0.045	1.400	NA	NA	8.43	5.0	9.00	4.5
3	12	1211	60.2	2	A	7.30	6.8	2.7	1.710	0.043	1.110	3.31	0.445	10.12	5.3	7.75	10.3

946510299

BASELINE RIVER SAMPLING
JACKSON STREET - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	12	1407	62.1	2	A	7.30	6.0	2.8	1.170	0.040	0.862	NA	NA	12.14	6.0	8.25	11.3
3	12	1539	63.6	2	A	7.30	5.8	2.2	1.800	0.045	1.280	2.96	0.367	8.43	5.8	9.00	6.0
3	12	1730	65.5	2	A	7.40	7.2	2.2	1.660	0.043	1.330	NA	NA	8.77	6.0	9.20	3.9
3	12	2020	68.3	2	A	7.40	7.5	2.4	2.110	0.056	1.700	3.20	0.382	8.09	6.0	8.40	3.0
3	12	2310	71.2	2	A	7.30	6.5	2.4	1.920	0.048	1.290	NA	NA	6.41	5.0	8.80	6.0
3	13	217	74.3	2	A	7.30	5.0	3.2	1.300	0.029	0.624	3.04	0.433	10.45	5.0	7.50	12.3
3	13	417	76.3	2	A	7.30	5.5	2.6	0.717	0.011	0.394	NA	NA	7.76	5.0	8.00	7.0
3	13	639	78.6	2	A	7.40	6.5	2.4	1.840	0.045	1.300	2.20	0.264	7.76	5.0	8.80	4.5
3	13	945	81.8	2	A	7.20	25.0	6.0	2.180	0.056	1.670	NA	NA	10.34	5.9	9.40	3.1
3	13	1210	84.2	2	A	7.20	9.0	3.6	2.060	0.051	1.400	4.13	0.555	11.80	6.0	8.60	6.6
3	13	1515	87.3	2	A	7.30	4.5	3.2	1.150	0.027	0.681	NA	NA	9.77	5.8	7.80	11.2
3	13	1745	89.8	2	A	7.20	8.5	1.0	1.910	0.048	1.180	3.70	0.512	10.79	6.0	8.40	7.0
3	13	1959	92.0	2	A	7.40	8.5	2.0	2.180	0.053	1.570	NA	NA	7.75	6.2	8.80	3.5
3	13	2225	94.4	2	A	7.30	7.0	1.6	1.400	0.027	0.764	3.60	0.400	7.76	6.0	9.00	3.0
3	14	41	96.7	2	A	7.30	6.5	1.0	1.390	0.032	0.814	NA	NA	7.76	6.0	8.20	5.0
3	14	338	99.6	2	A	7.30	3.5	1.6	1.590	0.040	0.834	1.50	0.264	13.83	6.0	7.20	14.0
3	14	640	102.7	2	A	7.30	7.5	1.0	1.090	0.019	0.469	NA	NA	7.75	6.0	8.40	6.0
3	14	850	104.8	2	A	7.20	22.0	1.0	2.270	0.059	1.560	3.86	0.411	16.93	6.5	9.60	2.5
3	14	1210	108.2	2	A	7.40	7.0	1.0	2.320	0.059	1.610	NA	NA	12.81	6.5	10.60	2.5
3	14	1530	111.5	2	A	7.30	6.0	2.8	2.100	0.053	1.350	3.63	0.467	11.80	6.5	9.60	6.1
3	14	1830	114.5	2	A	7.40	5.4	2.0	2.110	0.053	1.290	NA	NA	9.10	6.2	8.90	5.0
3	14	2135	117.6	2	A	7.40	7.8	2.8	2.350	0.059	1.560	3.88	0.417	5.21	6.2	9.00	2.2
3	14	2346	119.8	2	A	7.40	8.0	2.4	2.010	0.048	1.180	NA	NA	9.10	6.5	8.60	3.0
3	15	257	122.9	2	A	7.30	4.5	3.2	1.180	0.029	0.597	2.40	0.421	18.81	5.3	8.60	9.0
3	15	559	126.0	2	A	7.30	5.8	3.6	1.920	0.048	1.130	NA	NA	10.34	5.0	8.60	8.0
3	15	830	128.5	2	A	7.30	6.8	3.2	2.060	0.053	1.290	3.59	0.422	12.98	6.0	10.00	6.9

946510300

BASELINE RIVER SAMPLING
JACKSON STREET - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	15	1140	131.7	2	A	7.50	9.4	2.6	2.180	0.051	1.320	NA	NA	8.53	6.2	8.90	2.8
3	15	1445	134.8	2	A	7.40	20.0	4.2	1.720	0.053	1.180	3.80	0.543	14.47	6.5	8.80	7.8
3	15	1707	137.1	2	A	7.40	6.5	3.0	1.600	0.045	0.912	NA	NA	14.47	6.2	8.20	11.0
3	15	2013	140.2	2	A	7.40	5.5	3.2	1.980	0.053	1.180	4.02	0.459	12.93	6.2	8.90	8.0
3	15	2305	143.1	2	A	7.40	6.0	3.4	2.230	0.059	1.500	NA	NA	19.29	6.2	9.10	3.5
3	16	48	144.8	2	A	7.50	8.0	2.4	2.230	0.059	1.450	2.53	0.340	9.64	6.0	9.00	4.0
3	16	342	147.7	2	A	7.40	7.0	3.4	1.110	0.027	0.488	NA	NA	19.66	6.0	8.70	10.0
3	16	641	150.7	2	A	7.40	5.5	2.7	1.450	0.037	0.754	2.13	0.315	19.66	6.0	8.30	10.0
3	16	950	153.8	2	A	7.30	15.0	2.6	2.120	0.056	1.280	NA	NA	15.05	6.2	9.00	5.8
3	16	1250	156.8	2	A	7.40	8.7	2.7	2.220	0.059	1.450	2.98	0.316	14.11	6.5	9.40	3.5
3	16	1540	159.7	2	A	7.40	23.0	5.1	1.940	0.053	1.020	NA	NA	23.51	6.5	9.90	7.5
3	16	1830	162.5	2	A	7.50	15.0	5.6	NA	NA	NA	4.74	0.571	20.69	6.0	10.20	9.5
3	16	2030	164.5	2	A	7.40	6.3	2.6	NA	NA	NA	NA	NA	20.69	6.0	10.00	8.0
3	16	2345	167.8	2	A	7.40	8.2	2.8	NA	NA	NA	3.51	0.339	11.29	5.9	10.60	4.0
3	17	240	170.7	2	A	7.40	7.6	1.8	2.060	0.053	1.180	NA	NA	22.57	5.0	9.80	4.0
3	17	531	173.5	2	A	7.50	5.4	2.6	1.300	0.037	0.644	1.92	0.280	22.57	5.0	9.30	11.0
3	17	845	176.8	2	A	7.40	5.6	2.8	NA	NA	NA	2.76	0.306	9.10	4.4	10.00	12.0
3	17	1215	180.3	2	A	7.30	26.0	4.4	NA	NA	NA	NA	NA	8.77	5.2	8.80	6.2
3	17	1535	183.6	2	A	7.40	40.0	6.6	NA	NA	NA	3.33	0.362	11.13	5.3	9.00	8.2
3	17	1810	186.2	2	A	7.40	6.8	2.8	1.400	0.021	0.632	NA	NA	11.29	5.0	10.75	9.5
3	17	2055	188.9	2	A	7.40	6.0	7.8	0.992	0.013	0.336	2.76	0.325	10.35	5.0	10.00	9.0
3	17	2345	191.8	2	A	7.40	25.0	5.2	1.520	0.019	0.496	NA	NA	12.23	5.0	10.50	4.0
3	18	256	194.9	2	A	7.40	17.0	3.8	1.670	0.035	0.784	3.43	0.458	16.93	4.5	9.80	2.0
3	18	532	197.5	2	A	7.30	20.0	4.8	1.850	0.043	0.831	NA	NA	22.57	4.0	10.00	8.5
3	18	820	200.3	2	A	7.10	32.0	8.2	1.880	0.048	0.936	3.18	0.456	12.81	3.5	12.00	11.0
3	18	1120	203.3	2	A	7.40	17.0	3.6	2.130	0.059	1.280	NA	NA	20.69	4.0	10.40	5.0

946510301

BASELINE RIVER SAMPLING
JACKSON STREET - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	18	1420	206.3	2	A	7.40	15.0	3.6	2.260	0.064	1.450	3.55	0.414	16.93	4.5	9.80	3.0
3	18	1810	210.2	2	A	7.40	7.6	3.6	1.750	0.051	0.959	NA	NA	32.92	5.0	9.00	10.0
3	18	2105	213.1	2	A	7.40	6.5	3.4	1.030	0.016	0.475	2.29	0.340	13.82	4.5	8.75	8.0
3	18	2355	215.9	2	A	7.40	18.0	4.2	2.000	0.031	1.270	NA	NA	15.61	4.5	8.50	5.3
3	19	238	218.6	2	A	7.40	15.0	3.8	1.700	0.041	1.420	3.62	0.473	20.69	4.8	8.80	3.3
3	19	535	221.6	2	A	7.40	15.0	4.0	1.920	0.054	1.460	NA	NA	16.93	4.0	8.80	10.0
3	19	840	224.7	2	A	7.30	8.7	3.8	1.200	0.013	0.063	3.20	0.498	26.33	4.0	9.40	12.5
3	19	1140	227.7	2	A	7.30	17.0	3.9	1.720	0.026	0.573	NA	NA	18.81	4.2	11.20	8.0
3	19	1440	230.7	2	A	7.40	14.0	3.8	1.690	0.036	0.831	3.86	0.407	22.57	4.8	9.20	4.0
3	19	1650	232.8	2	A	7.40	15.0	3.6	1.110	0.031	0.675	NA	NA	26.33	4.5	9.25	7.0
3	19	1945	235.8	2	A	7.50	7.2	3.6	1.140	0.041	0.611	2.09	0.349	23.04	4.0	8.75	8.0
3	19	2235	238.6	2	A	7.40	8.7	3.2	1.890	0.056	1.000	NA	NA	22.57	4.0	8.75	9.3
3	20	220	242.3	2	A	7.40	9.1	3.3	1.100	0.021	0.363	1.99	0.286	13.17	4.0	8.80	4.5
3	20	522	245.4	2	A	7.40	17.0	3.4	2.210	0.062	1.160	NA	NA	15.05	4.0	8.80	5.3

946510302

BASELINE

JACKSON STREET

3-10/3-20-81

2/3 DEPTH

946510303

BASELINE H-RIVER SAMPLING
JACKSON STREET - LEVEL B - 2/3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	10	930	9.5	2	B	7.40	22.0	3.6	1.660	0.035	0.629	3.13	0.598	5.56	4.8	8.70	8.0
3	10	1130	11.5	2	B	7.45	12.0	2.8	1.720	0.051	0.706	NA	NA	10.39	5.5	7.50	13.0
3	10	1330	13.5	2	B	7.40	11.0	2.8	1.710	0.035	0.652	2.71	0.369	9.27	5.0	8.20	7.0
3	10	1535	15.6	2	B	7.41	20.0	3.2	1.740	0.044	0.909	NA	NA	14.48	5.0	8.60	3.3
3	10	1820	18.3	2	B	7.53	17.0	3.4	1.630	0.056	1.620	2.97	0.404	14.48	5.0	NA	1.0
3	10	2035	20.6	2	B	7.43	18.0	3.0	1.770	0.040	0.948	NA	NA	15.52	5.0	10.00	2.9
3	10	2210	22.2	2	B	7.40	17.0	2.6	1.580	0.046	0.757	2.74	0.641	9.31	5.0	8.80	8.5
3	10	2350	23.8	2	B	7.54	12.0	2.8	1.030	0.030	0.310	NA	NA	10.39	5.5	7.50	15.0
3	11	150	25.8	2	B	7.34	5.5	3.4	1.820	0.044	0.897	1.65	0.266	5.05	5.0	8.40	8.0
3	11	450	28.8	2	B	7.38	20.0	3.0	1.670	0.051	1.350	NA	NA	7.59	5.3	9.00	2.9
3	11	725	31.4	2	B	7.42	15.0	3.0	1.750	0.056	1.670	3.00	0.458	7.08	5.3	9.40	1.8
3	11	940	33.7	2	B	7.40	12.0	2.1	1.630	0.044	1.020	1.98	0.455	7.76	5.0	8.40	5.0
3	11	1135	35.6	2	B	7.40	12.0	3.0	1.170	0.023	0.388	NA	NA	6.74	5.3	7.75	12.8
3	11	1405	38.1	2	B	7.40	6.0	2.8	1.170	0.036	0.751	2.64	0.367	9.44	5.3	10.00	8.3
3	11	1620	40.3	2	B	7.50	15.0	2.7	1.730	0.046	1.220	NA	NA	9.40	5.5	7.40	3.9
3	11	1810	42.2	2	B	7.50	15.0	3.3	1.780	0.046	1.410	2.98	0.493	10.34	5.5	8.80	1.9
3	11	2015	44.3	2	B	7.50	8.5	2.7	1.720	0.046	1.170	NA	NA	9.87	5.5	10.50	6.5
3	11	2210	46.2	2	B	7.40	22.0	4.1	1.660	0.044	0.823	2.98	0.761	12.23	5.0	5.00	12.2
3	11	2340	47.7	2	B	7.40	20.0	3.9	1.520	0.041	0.719	NA	NA	11.29	5.1	8.50	12.0
3	12	125	49.4	2	B	7.40	5.5	2.8	1.110	0.041	0.665	2.46	0.339	12.14	5.0	7.90	14.8
3	12	345	51.8	2	B	7.50	7.0	2.8	1.400	0.046	1.010	NA	NA	11.13	4.8	9.00	7.0
3	12	520	53.3	2	B	7.40	17.0	3.4	1.740	0.046	1.110	3.19	0.579	11.29	4.9	8.90	3.9
3	12	715	55.3	2	B	7.40	15.0	3.3	1.970	0.051	1.510	NA	NA	11.29	5.0	9.20	2.0
3	12	850	56.8	2	B	7.20	15.0	3.4	1.370	0.028	0.759	3.27	0.426	11.28	5.0	8.50	5.5
3	12	1040	58.7	2	B	7.20	35.0	6.4	1.830	0.046	1.190	NA	NA	16.93	5.0	8.25	5.0
3	12	1208	60.1	2	B	7.30	25.0	4.6	1.420	0.041	0.826	3.01	0.536	15.99	5.0	7.50	11.8

946510304

BASELINE H - RIVER SAMPLING
JACKSON STREET - LEVEL B - 2/3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	12	1400	62.0	2	B	7.30	7.5	3.3	1.190	0.031	0.545	NA	NA	12.48	5.3	7.10	14.0
3	12	1533	63.5	2	B	7.30	6.0	2.4	1.600	0.046	0.921	2.81	0.369	7.42	6.0	NA	6.8
3	12	1735	65.6	2	B	7.30	6.5	2.8	1.720	0.044	0.986	NA	NA	9.44	6.0	9.20	4.1
3	12	2030	68.5	2	B	7.40	8.0	2.6	1.640	0.044	0.986	NA	NA	7.76	5.5	8.80	7.9
3	12	2320	71.3	2	B	7.30	6.8	2.1	1.800	0.041	0.880	NA	NA	14.16	5.0	8.40	7.5
3	13	208	74.1	2	B	7.30	5.0	3.3	0.961	0.026	0.358	1.55	0.242	8.43	5.0	7.60	15.0
3	13	409	76.1	2	B	7.30	5.0	3.3	1.570	0.039	0.667	NA	NA	11.46	5.0	8.20	7.0
3	13	631	78.5	2	B	7.30	6.0	3.9	1.360	0.034	0.592	2.02	0.354	14.16	5.0	8.70	5.0
3	13	1000	82.0	2	B	7.10	20.0	2.0	1.800	0.041	1.020	NA	NA	6.74	5.8	9.40	4.0
3	13	1225	84.4	2	B	7.20	8.5	1.0	1.900	0.044	0.904	2.67	0.490	11.80	5.5	8.30	7.8
3	13	1530	87.5	2	B	7.20	4.0	2.0	1.580	0.041	0.692	NA	NA	14.10	5.2	7.70	13.8
3	13	1731	89.5	2	B	7.20	15.0	3.2	1.620	0.046	1.030	3.70	0.535	14.10	6.0	7.90	7.5
3	13	1945	91.8	2	B	7.30	8.0	2.0	1.930	0.049	1.030	NA	NA	7.42	6.2	8.40	4.0
3	13	2222	94.4	2	B	7.30	7.5	1.6	1.480	0.026	0.626	3.51	0.490	9.77	5.8	8.00	9.0
3	14	29	96.5	2	B	7.20	9.5	2.4	1.100	0.026	0.438	NA	NA	18.80	6.0	8.40	9.0
3	14	326	99.4	2	B	7.30	4.5	3.2	1.520	0.041	0.665	NA	NA	13.82	6.0	7.20	16.0
3	14	627	102.4	2	B	7.30	5.5	2.8	1.330	0.031	0.621	NA	NA	12.14	6.0	8.70	7.0
3	14	905	105.1	2	B	7.30	5.0	2.8	2.140	0.056	1.290	3.37	0.422	8.46	6.5	10.40	3.2
3	14	1230	108.5	2	B	7.30	7.5	4.0	2.000	0.051	1.140	NA	NA	15.04	6.2	9.20	3.5
3	14	1545	111.8	2	B	7.20	4.2	1.4	1.600	0.041	0.719	3.17	0.470	16.92	6.0	9.00	15.0
3	14	1835	114.6	2	B	7.30	7.6	3.0	1.900	0.046	1.010	NA	NA	14.16	6.2	8.40	5.5
3	14	2142	117.7	2	B	7.40	7.5	2.8	2.000	0.046	1.090	3.44	0.382	8.46	6.2	8.80	3.0
3	14	2349	119.8	2	B	7.30	5.3	3.0	1.590	0.041	0.773	NA	NA	9.40	6.5	8.10	7.0
3	15	245	122.4	2	B	7.30	15.0	4.4	1.390	0.039	0.640	3.32	1.380	17.86	5.5	8.70	10.0
3	15	548	125.8	2	B	7.40	4.5	3.0	1.380	0.036	0.616	NA	NA	14.16	6.0	9.00	10.0
3	15	845	128.8	2	B	7.30	7.8	3.0	1.760	0.044	1.040	3.98	0.475	14.47	5.9	10.40	6.9

946510305

BASELINE H - RIVER SAMPLING
JACKSON STREET - LEVEL B - 2/3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	15	1155	131.9	2	B	7.30	8.0	3.4	2.000	0.051	1.190	NA	NA	12.61	5.9	9.20	2.8
3	15	1500	135.0	2	B	7.30	32.0	5.8	1.540	0.051	1.090	NA	NA	19.28	6.0	9.00	10.0
3	15	1709	137.1	2	B	7.40	5.7	4.6	1.400	0.041	0.773	3.98	0.471	15.57	6.0	8.00	13.2
3	15	2017	140.3	2	B	7.40	7.5	2.8	1.660	0.051	1.090	NA	NA	13.72	6.2	8.80	8.0
3	15	2309	143.1	2	B	7.40	8.2	4.4	2.180	0.056	1.400	3.99	0.456	12.24	6.2	8.90	4.2
3	16	37	144.6	2	B	7.40	15.0	6.5	0.733	0.018	0.312	NA	NA	16.55	6.0	9.20	8.0
3	16	334	147.6	2	B	7.40	14.0	4.1	0.733	0.016	0.260	3.73	0.722	13.72	6.0	8.90	10.0
3	16	633	150.5	2	B	7.40	5.6	3.3	0.906	0.023	0.603	NA	NA	14.47	6.0	8.30	12.0
3	16	1005	154.1	2	B	7.40	15.0	2.6	1.970	0.049	1.060	NA	NA	26.33	6.1	9.40	9.2
3	16	1305	157.1	2	B	7.40	7.6	2.8	2.040	0.051	1.090	3.61	0.438	12.23	6.2	8.80	5.5
3	16	1555	159.9	2	B	7.40	8.2	3.6	1.770	0.046	0.794	NA	NA	15.05	6.5	9.80	11.2
3	16	1747	161.8	2	B	7.50	5.0	2.6	NA	NA	NA	2.74	0.357	17.87	5.5	9.70	15.0
3	16	2025	164.4	2	B	7.50	4.6	3.0	NA	NA	NA	NA	NA	15.05	6.0	9.00	8.0
3	16	2340	167.7	2	B	7.40	5.8	2.7	NA	NA	NA	2.98	0.380	15.99	5.9	10.00	4.0
3	17	232	170.5	2	B	7.40	20.0	5.1	2.000	0.054	1.170	NA	NA	35.74	5.0	10.00	4.0
3	17	524	173.4	2	B	7.50	6.5	2.9	0.996	0.026	0.519	2.29	0.341	20.69	5.0	9.80	15.0
3	17	900	177.0	2	B	7.40	6.2	2.6	NA	NA	NA	2.51	0.333	11.29	3.8	11.20	15.5
3	17	1230	180.5	2	B	7.40	35.0	5.0	NA	NA	NA	NA	NA	32.92	5.2	9.20	6.7
3	17	1550	183.8	2	B	7.40	30.0	5.2	NA	NA	NA	3.83	0.980	15.99	5.2	8.60	11.5
3	17	1800	186.0	2	B	7.40	8.5	3.3	0.924	0.009	0.312	NA	NA	26.33	5.0	11.00	10.8
3	17	2050	188.8	2	B	7.50	6.0	2.8	1.110	0.006	0.232	2.36	0.349	14.11	5.0	10.25	10.0
3	17	2340	191.7	2	B	7.40	34.0	6.2	1.370	0.019	0.357	NA	NA	13.17	5.0	11.00	5.0
3	18	228	194.5	2	B	7.40	18.0	3.8	1.560	0.047	0.910	2.84	0.486	20.22	5.0	10.80	2.0
3	18	525	197.4	2	B	7.30	63.0	12.8	1.800	0.063	0.867	NA	NA	11.46	4.0	10.80	9.0
3	18	835	200.6	2	B	7.30	9.7	10.8	1.720	0.042	0.888	3.04	0.568	15.99	4.0	9.60	12.2
3	18	1135	203.6	2	B	7.30	18.0	4.4	2.010	0.047	1.160	NA	NA	15.99	4.1	11.40	7.1

946510306

BASELINE-RIVER SAMPLING
BELLEVILLE TWP. - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	520	77.3	3	A	7.50	20.0	3.9	2.500	0.062	1.610	3.04	0.546	5.05	6.0	10.00	0.0
3	13	714	79.2	3	A	7.50	15.0	3.6	2.430	0.059	1.580	NA	NA	4.72	6.0	10.80	0.0
3	13	825	80.4	3	A	7.50	6.5	2.8	2.470	0.059	1.610	3.70	0.535	3.71	6.0	11.00	0.1
3	13	1045	82.8	3	A	7.50	5.0	2.4	2.400	0.059	1.610	NA	NA	4.04	6.2	10.60	0.2
3	13	1340	85.7	3	A	7.40	5.5	2.0	2.430	0.062	1.610	3.98	0.400	11.46	6.5	9.20	0.5
3	13	1632	88.5	3	A	7.40	5.0	1.0	2.080	0.049	1.210	NA	NA	6.09	7.0	9.50	0.5
3	13	1840	90.7	3	A	7.50	20.0	3.2	2.160	0.049	1.300	4.53	0.783	7.08	6.5	10.20	0.2
3	13	2056	92.9	3	A	7.50	7.0	1.0	2.550	0.059	1.610	NA	NA	24.40	6.2	10.00	0.2
3	13	2317	95.3	3	A	7.50	8.0	2.4	2.550	0.059	1.640	3.67	0.490	26.32	6.2	10.00	0.2
3	14	148	97.8	3	A	7.40	5.5	1.6	1.820	0.038	0.995	NA	NA	3.76	7.0	9.70	0.5
3	14	424	100.4	3	A	7.50	6.0	2.0	2.870	0.057	1.490	3.42	0.618	28.20	7.0	9.50	0.3
3	14	729	103.5	3	A	7.50	7.0	2.4	2.280	0.049	1.270	NA	NA	2.82	7.0	11.00	0.0
3	14	1000	106.0	3	A	7.40	17.0	4.0	2.470	0.059	1.610	3.82	0.628	4.72	7.0	11.40	0.0
3	14	1315	109.3	3	A	7.40	20.0	4.4	2.620	0.059	1.580	NA	NA	6.07	7.0	11.00	0.5
3	14	1703	113.0	3	A	7.50	15.0	3.6	2.600	0.059	1.580	NA	NA	8.59	7.0	9.90	0.2
3	14	1940	115.7	3	A	7.50	18.0	4.4	2.420	0.059	1.580	4.12	0.684	4.70	6.5	9.40	0.2
3	14	2240	118.7	3	A	7.50	15.0	3.6	2.110	0.049	1.210	NA	NA	2.54	7.0	10.00	0.1
3	15	44	120.7	3	A	7.50	8.5	5.2	2.040	0.049	1.330	3.06	0.773	6.41	6.0	9.70	0.0
3	15	340	123.7	3	A	7.40	8.7	4.4	2.300	0.049	1.330	NA	NA	1.35	6.0	9.50	0.0
3	15	643	126.7	3	A	7.50	8.0	4.0	1.940	0.038	0.992	3.09	0.369	6.07	6.0	9.70	0.0
3	15	925	129.4	3	A	7.50	22.0	9.4	2.180	0.062	1.580	3.87	0.689	6.68	6.8	10.50	0.1
3	15	1230	132.5	3	A	7.50	15.0	4.0	2.180	0.059	1.550	NA	NA	4.08	6.5	9.30	0.1
3	15	1535	135.6	3	A	7.40	30.0	9.8	2.290	0.059	1.580	5.05	0.922	NA	6.9	9.20	0.9
3	15	1802	138.0	3	A	7.40	12.0	3.8	2.290	0.059	1.580	NA	NA	8.53	6.9	8.90	1.0
3	15	2110	141.2	3	A	7.50	20.0	6.6	2.210	0.065	1.600	3.98	0.772	5.93	6.9	10.00	0.1
[redacted]	[redacted]	1[redacted]	145[redacted]	3	[redacted]	7.[redacted]	20[redacted]	[redacted]	2.180	[redacted]	[redacted]	[redacted]	[redacted]	10.39	[redacted]	[redacted]	[redacted]

9465103O7

BASELINE-RIVER SAMPLING
BELLEVILLE TWP. - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	434	148.6	3	A	7.40	15.0	4.5	2.120	0.054	1.330	4.40	0.533	14.47	6.5	8.90	2.0
3	16	731	151.5	3	A	7.40	12.0	3.3	2.180	0.062	1.580	NA	NA	8.75	6.5	9.70	0.8
3	16	1040	154.7	3	A	7.50	25.0	4.5	2.010	0.049	1.440	NA	NA	10.34	6.5	10.80	0.0
3	16	1340	157.7	3	A	7.50	15.0	3.3	2.320	0.059	1.550	3.09	0.541	7.52	6.5	10.30	0.1
3	16	1652	160.9	3	A	7.40	23.0	4.4	NA	NA	NA	NA	NA	19.75	6.5	9.90	2.0
3	16	1934	163.6	3	A	7.40	15.0	2.8	NA	NA	NA	3.88	0.434	10.34	6.2	10.60	0.9
3	16	2234	166.6	3	A	7.50	18.0	4.2	NA	NA	NA	NA	NA	13.17	5.5	11.60	0.0
3	17	138	169.6	3	A	7.60	9.0	3.4	2.090	0.044	1.020	3.29	0.468	5.06	5.0	10.80	0.0
3	17	427	172.4	3	A	7.40	30.0	5.6	1.800	0.054	1.270	NA	NA	19.75	5.3	9.90	1.0
3	17	728	175.5	3	A	7.40	15.0	3.4	1.780	0.051	1.340	3.75	0.469	11.29	5.0	9.70	3.0
3	17	1000	178.0	3	A	7.30	27.0	4.4	NA	NA	NA	3.98	0.774	9.77	5.0	9.80	0.9
3	17	1315	181.3	3	A	7.60	25.0	5.6	NA	NA	NA	NA	NA	8.77	5.0	9.60	0.2
3	17	1650	184.8	3	A	7.40	30.0	4.4	1.640	0.033	0.907	2.62	0.329	7.42	5.3	11.00	0.7
3	17	1930	187.5	3	A	7.50	15.0	3.8	1.640	0.038	1.020	NA	NA	7.08	5.0	11.00	0.3
3	17	2220	190.3	3	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.5	11.75	0.0
3	18	129	193.5	3	A	7.60	25.0	4.6	2.290	0.049	1.210	3.78	0.907	5.05	5.0	11.40	0.0
3	18	431	196.5	3	A	7.50	30.0	6.0	2.650	0.059	1.550	NA	NA	5.40	4.0	11.60	0.0
3	18	729	199.5	3	A	7.40	18.0	3.4	2.480	0.059	1.490	3.90	0.525	7.52	4.0	10.40	1.0
3	18	940	201.7	3	A	7.50	18.0	4.0	2.580	0.059	1.580	4.04	0.733	10.45	4.0	11.80	0.0
3	18	1240	204.7	3	A	7.60	25.0	5.0	2.680	0.059	1.550	NA	NA	8.77	4.2	11.10	0.0
3	18	1630	208.5	3	A	7.50	33.0	5.8	2.690	0.059	1.550	3.96	0.892	8.09	5.5	10.60	0.0
3	18	1920	211.3	3	A	7.50	18.0	4.2	2.400	0.055	1.420	NA	NA	24.45	4.5	8.50	1.0
3	18	2215	214.3	3	A	7.50	17.0	3.6	2.540	0.044	1.200	3.85	0.815	8.09	4.5	9.50	0.2
3	19	113	217.2	3	A	7.60	25.0	4.6	2.190	0.044	1.260	NA	NA	13.49	4.2	8.90	0.0
3	19	411	220.2	3	A	7.50	25.0	4.6	2.170	0.039	1.140	3.68	0.682	8.77	4.0	10.40	0.0
3	19	709	223.1	3	A	7.40	22.0	4.8	2.210	0.049	1.270	NA	NA	18.81	4.0	9.20	2.0

946510308

BASELINE-RIVER SAMPLING
BELLEVILLE TWP. - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	925	225.4	3	A	7.40	15.0	12.0	2.060	0.039	1.070	3.74	0.403	28.22	4.2	9.70	1.5
3	19	1225	228.4	3	A	7.50	35.0	6.9	2.470	0.055	1.560	NA	NA	9.40	4.5	11.20	0.0
3	19	1525	231.4	3	A	7.50	14.0	2.8	2.240	0.049	1.600	3.45	0.429	7.42	4.2	10.50	0.0
3	19	1730	233.5	3	A	7.40	40.0	6.9	1.720	0.033	0.904	NA	NA	11.29	4.5	9.75	1.0
3	19	2020	236.3	3	A	7.40	19.0	3.4	2.060	0.049	1.210	2.91	0.291	21.63	4.5	8.75	2.8
3	19	2315	239.3	3	A	7.50	22.0	5.7	2.000	0.049	1.250	3.53	0.533	12.70	4.0	9.75	0.3
3	20	113	241.2	3	A	7.50	27.0	5.0	2.570	0.049	1.310	4.19	0.860	10.34	4.0	10.20	0.0
3	20	410	244.2	3	A	7.50	8.3	2.7	1.220	0.023	0.675	NA	NA	6.58	4.0	10.60	0.0
3	20	712	247.2	3	A	7.40	40.0	7.4	2.350	0.044	1.150	3.44	0.850	52.67	4.0	9.00	3.0

946510309

BASELINE

BELLEVILLE

TURNPIKE

3-10/3-20-81

1/3 DEPTH

946510310

BASELINE-RIVER SAMPLING
BELLEVILLE TWP. - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	900	9.0	3	A	7.42	30.0	7.8	2.000	0.051	1.400	4.16	1.360	8.16	5.0	9.30	0.2
3	10	1200	12.0	3	A	7.37	10.0	2.7	1.740	0.051	1.630	NA	NA	8.53	5.0	9.70	0.5
3	10	1515	15.3	3	A	7.38	18.0	5.8	2.050	0.056	1.620	3.07	0.825	6.31	6.5	10.30	0.2
3	10	1815	18.3	3	A	7.50	10.0	4.4	2.280	0.056	1.710	NA	NA	5.56	6.2	10.60	0.0
3	10	2108	21.1	3	A	7.41	15.0	7.2	1.920	0.056	1.710	3.46	1.200	15.58	6.0	11.70	0.0
3	10	2346	23.8	3	A	7.40	13.0	3.2	1.860	0.056	1.710	NA	NA	8.90	6.0	8.60	0.0
3	11	245	26.8	3	A	7.42	22.0	4.1	1.800	0.051	1.540	2.90	0.513	3.71	5.8	10.40	0.5
3	11	508	29.1	3	A	7.50	30.0	5.7	2.330	0.059	1.760	NA	NA	5.73	6.0	10.80	0.5
3	11	715	31.3	3	A	7.55	18.0	3.9	2.430	0.064	1.810	3.28	0.473	3.37	5.5	10.20	0.5
3	11	955	33.9	3	A	7.45	20.0	7.5	2.160	0.049	1.770	2.98	0.485	12.14	5.9	10.80	0.5
3	11	1225	36.4	3	A	7.43	5.7	3.3	1.990	0.049	1.740	NA	NA	8.43	5.9	10.80	0.6
3	11	1616	40.3	3	A	7.48	5.6	6.4	2.050	0.049	1.680	3.46	0.829	8.46	6.5	9.70	0.5
3	11	1853	42.9	3	A	7.53	9.5	4.1	2.210	0.059	1.780	NA	NA	6.74	6.5	9.80	0.3
3	11	2135	45.6	3	A	7.50	16.0	5.6	2.170	0.054	1.740	3.61	0.746	7.76	6.0	10.00	0.2
3	12	35	48.6	3	A	7.43	8.5	3.3	2.020	0.049	1.710	NA	NA	6.07	6.0	8.20	0.2
3	12	255	50.9	3	A	7.42	5.8	2.4	2.020	0.049	1.590	3.00	0.418	3.37	6.0	9.80	0.5
3	12	542	53.7	3	A	7.49	20.0	5.6	2.400	0.054	1.680	NA	NA	6.41	6.1	10.50	0.1
3	12	815	56.3	3	A	7.50	9.5	3.4	2.520	0.062	1.730	3.00	0.467	4.38	6.0	9.90	0.0
3	12	1040	58.7	3	A	7.40	20.0	4.8	2.460	0.059	1.700	NA	NA	6.07	6.5	9.80	0.1
3	12	1320	61.3	3	A	7.40	15.0	3.3	2.400	0.054	1.710	3.13	0.358	7.08	6.0	9.40	0.2
3	12	1535	63.6	3	A	7.40	9.0	3.9	2.460	0.059	1.730	NA	NA	4.38	6.5	10.20	0.1
3	12	1821	66.3	3	A	7.50	17.0	4.2	2.510	0.059	1.640	3.62	0.597	8.43	6.5	9.80	0.2
3	12	2033	68.5	3	A	7.60	7.5	3.3	1.940	0.044	1.220	NA	NA	3.71	6.5	10.50	0.2
3	12	2300	71.0	3	A	7.50	27.0	5.4	2.440	0.065	1.660	3.51	0.701	7.75	6.2	9.00	0.2
3	13	48	72.8	3	A	7.40	20.0	4.2	1.760	0.028	0.824	2.58	0.558	1.69	6.0	9.80	0.5
3	13	251	74.8	3	A	7.40	7.0	2.7	1.980	0.041	1.100	NA	NA	5.73	6.0	9.60	0.5

94510311

BASELINE-RIVER SAMPLING
BELLEVILLE TWP. - LEVEL A - 1\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	520	77.3	3	A	7.50	20.0	3.9	2.500	0.062	1.610	3.04	0.546	5.05	6.0	10.00	0.0
3	13	714	79.2	3	A	7.50	15.0	3.6	2.430	0.059	1.580	NA	NA	4.72	6.0	10.80	0.0
3	13	825	80.4	3	A	7.50	6.5	2.8	2.470	0.059	1.610	3.70	0.535	3.71	6.0	11.00	0.1
3	13	1045	82.8	3	A	7.50	5.0	2.4	2.400	0.059	1.610	NA	NA	4.04	6.2	10.60	0.2
3	13	1340	85.7	3	A	7.40	5.5	2.0	2.430	0.062	1.610	3.98	0.400	11.46	6.5	9.20	0.5
3	13	1632	88.5	3	A	7.40	5.0	1.0	2.080	0.049	1.210	NA	NA	6.09	7.0	9.50	0.5
3	13	1840	90.7	3	A	7.50	20.0	3.2	2.160	0.049	1.300	4.53	0.783	7.08	6.5	10.20	0.2
3	13	2056	92.9	3	A	7.50	7.0	1.0	2.550	0.059	1.610	NA	NA	24.40	6.2	10.00	0.2
3	13	2317	95.3	3	A	7.50	8.0	2.4	2.550	0.059	1.640	3.67	0.490	26.32	6.2	10.00	0.2
3	14	148	97.8	3	A	7.40	5.5	1.6	1.820	0.038	0.995	NA	NA	3.76	7.0	9.70	0.5
3	14	424	100.4	3	A	7.50	6.0	2.0	2.870	0.057	1.490	3.42	0.618	28.20	7.0	9.50	0.3
3	14	729	103.5	3	A	7.50	7.0	2.4	2.280	0.049	1.270	NA	NA	2.82	7.0	11.00	0.0
3	14	1000	106.0	3	A	7.40	17.0	4.0	2.470	0.059	1.610	3.82	0.628	4.72	7.0	11.40	0.0
3	14	1315	109.3	3	A	7.40	20.0	4.4	2.620	0.059	1.580	NA	NA	6.07	7.0	11.00	0.5
3	14	1703	113.0	3	A	7.50	15.0	3.6	2.600	0.059	1.580	NA	NA	8.59	7.0	9.90	0.2
3	14	1940	115.7	3	A	7.50	18.0	4.4	2.420	0.059	1.580	4.12	0.684	4.70	6.5	9.40	0.2
3	14	2240	118.7	3	A	7.50	15.0	3.6	2.110	0.049	1.210	NA	NA	2.54	7.0	10.00	0.1
3	15	44	120.7	3	A	7.50	8.5	5.2	2.040	0.049	1.330	3.06	0.773	6.41	6.0	9.70	0.0
3	15	340	123.7	3	A	7.40	8.7	4.4	2.300	0.049	1.330	NA	NA	1.35	6.0	9.50	0.0
3	15	643	126.7	3	A	7.50	8.0	4.0	1.940	0.038	0.992	3.09	0.369	6.07	6.0	9.70	0.0
3	15	925	129.4	3	A	7.50	22.0	9.4	2.180	0.062	1.580	3.87	0.689	6.68	6.8	10.50	0.1
3	15	1230	132.5	3	A	7.50	15.0	4.0	2.180	0.059	1.550	NA	NA	4.08	6.5	9.30	0.1
3	15	1535	135.6	3	A	7.40	30.0	9.8	2.290	0.059	1.580	5.05	0.922	NA	6.9	9.20	0.9
3	15	1802	138.0	3	A	7.40	12.0	3.8	2.290	0.059	1.580	NA	NA	8.53	6.9	8.90	1.0
3	15	2110	141.2	3	A	7.50	20.0	6.6	2.210	0.065	1.600	3.98	0.772	5.93	6.9	10.00	0.1
3	16	138	145.6	3	A	7.50	20.0	4.6	2.180	0.059	1.580	NA	NA	10.39	6.5	9.80	0.0

94651O312

BASELINE-RIVER SAMPLING
BELLEVILLE TWP - LEVEL 3 - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O. [PPM]	SAL [PPT]
3	16	425	148.4	3	B	7.40	20.0	3.4	2.000	0.055	1.420	NA	NA	13.45	6.5	9.10	2.0
3	16	723	151.4	3	B	7.40	15.0	3.2	2.240	0.057	1.500	NA	NA	9.27	7.0	9.30	1.0
3	16	1055	154.9	3	B	7.50	25.0	4.0	2.270	0.056	1.610	NA	NA	7.52	6.3	10.10	0.0
3	16	1355	157.9	3	B	7.50	17.0	3.0	2.270	0.051	1.470	3.36	0.581	10.34	6.5	10.20	0.1
3	16	1650	160.8	3	B	7.40	30.0	5.0	NA	NA	NA	NA	NA	22.57	6.5	9.60	2.2
3	16	1930	163.5	3	B	7.40	14.0	2.2	NA	NA	NA	2.61	0.358	6.41	6.2	10.20	0.9
3	16	2229	166.5	3	B	7.50	22.0	4.6	NA	NA	NA	NA	NA	10.34	5.5	11.20	0.0
3	17	127	169.4	3	B	7.60	9.2	3.8	1.520	0.023	0.674	3.50	0.522	3.71	5.0	11.00	0.0
3	17	420	172.3	3	B	7.40	32.0	6.0	2.250	0.048	1.280	NA	NA	22.57	5.3	10.20	1.0
3	17	720	175.3	3	B	7.40	27.0	5.2	1.980	0.038	0.992	4.48	0.760	18.81	5.0	10.00	3.0
3	17	1015	178.3	3	B	7.50	30.0	5.4	NA	NA	NA	3.98	0.785	7.42	5.0	9.60	0.9
3	17	1330	181.5	3	B	7.60	25.0	4.8	NA	NA	NA	NA	NA	4.05	5.0	9.40	0.2
3	17	1645	184.8	3	B	7.50	27.0	5.4	2.350	0.051	1.470	3.65	0.790	12.23	5.0	11.00	0.8
3	17	1940	187.7	3	B	7.50	15.0	3.0	2.260	0.046	1.400	NA	NA	9.10	5.0	11.25	0.5
3	17	2220	190.3	3	B	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.5	12.00	0.0
3	18	122	193.4	3	B	7.60	25.0	5.8	2.400	0.048	1.370	3.89	0.804	8.43	5.0	11.40	0.0
3	18	424	196.4	3	B	7.60	32.0	6.8	2.650	0.056	1.580	NA	NA	8.77	4.0	12.00	0.0
3	18	720	199.3	3	B	7.50	20.0	4.7	1.920	0.033	0.957	3.99	0.508	16.93	4.0	10.80	1.0
3	18	955	201.9	3	B	7.50	26.0	4.6	2.640	0.059	1.580	4.08	0.778	8.09	4.2	12.20	0.0
3	18	1255	204.9	3	B	7.60	27.0	4.6	2.740	0.056	1.580	NA	NA	12.14	4.0	11.40	0.0
3	18	1625	208.4	3	B	7.50	32.0	5.6	2.650	0.056	1.520	4.27	0.940	5.70	4.5	10.50	0.1
3	18	1915	211.3	3	B	7.50	26.0	4.6	2.570	0.059	1.520	NA	NA	13.17	4.5	8.75	1.0
3	18	2210	214.2	3	B	7.50	18.0	4.0	2.610	0.061	1.580	4.02	0.610	6.07	4.5	9.75	0.0
3	19	105	217.1	3	B	7.60	32.0	4.8	2.600	0.056	1.550	NA	NA	6.74	4.2	9.00	0.1
3	19	406	220.1	3	B	7.50	27.0	5.0	2.640	0.056	1.580	3.96	0.702	8.09	4.0	10.40	0.0
3	19	704	223.1	3	B	7.40	38.0	7.8	2.580	0.056	1.420	NA	NA	20.23	4.0	9.20	2.0

94651031 3

BASELINE-RIVER SAMPLING
BELLEVILLE TWP - LEVEL 3 - 2\3 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	940	225.7	3	B	7.10	15.0	3.4	2.060	0.041	1.170	3.95	0.466	25.39	4.2	9.20	2.0
3	19	1240	228.7	3	B	7.50	32.0	6.2	2.290	0.038	1.290	NA	NA	22.57	4.5	11.40	0.0
3	19	1540	231.7	3	B	7.50	14.0	3.7	2.180	0.046	1.530	3.76	0.498	7.06	4.2	10.70	0.0
3	19	1725	233.4	3	B	7.40	37.0	8.0	1.430	0.025	0.672	NA	NA	1.88	4.5	10.00	0.9
3	19	2015	236.3	3	B	7.40	16.0	3.7	1.720	0.038	0.992	3.94	0.395	6.74	4.5	9.00	3.0
3	19	2310	239.2	3	B	7.50	30.0	5.9	2.060	0.048	0.588	NA	NA	24.54	4.0	10.00	0.5
3	20	106	241.1	3	B	7.50	27.0	5.9	2.690	0.059	0.699	4.11	0.915	10.12	4.0	10.20	0.0
3	20	404	244.1	3	B	7.50	15.0	3.3	2.540	0.056	0.671	NA	NA	8.59	4.0	10.60	0.0
3	20	706	247.1	3	B	7.40	48.0	8.6	2.680	0.059	0.668	2.98	0.480	62.07	4.0	9.00	3.0

946510314

BASELINE

UNION AVENUE

3-10/3-20-81

1/2 DEPTH

046510315

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	945	9.4	5	C	7.55	15.0	3.0	2.090	0.048	1.490	3.17	0.495	7.24	6.8	8.60	0.2
3	10	1235	12.6	5	C	7.55	12.0	2.3	2.420	0.056	1.760	NA	NA	4.82	6.5	10.50	0.2
3	10	1555	15.9	5	C	7.55	10.0	2.2	2.530	0.056	1.710	3.45	0.475	6.31	7.0	10.50	0.2
3	10	1855	18.9	5	C	7.60	14.0	4.1	2.710	0.067	1.800	NA	NA	7.79	7.0	10.40	0.0
3	10	2145	21.8	5	C	7.54	10.0	3.3	2.550	0.056	1.690	3.12	0.434	8.16	6.5	9.80	0.0
3	11	37	24.6	5	C	7.53	6.5	1.7	2.510	0.056	1.670	NA	NA	1.69	5.0	9.20	0.0
3	11	317	27.3	5	C	7.61	7.2	3.9	2.510	0.067	1.610	3.64	0.527	1.41	7.0	12.00	0.5
3	11	529	29.5	5	C	7.61	8.0	4.1	2.430	0.067	1.570	NA	NA	1.69	7.0	11.60	0.3
3	11	744	31.7	5	C	7.60	8.8	4.4	2.670	0.070	1.730	3.07	0.420	2.72	6.5	10.20	0.5
3	11	1030	34.5	5	C	7.58	8.0	2.7	2.310	0.058	1.650	3.45	0.435	2.92	7.0	11.90	0.5
3	11	1359	37.8	5	C	7.59	8.4	3.3	2.370	0.056	1.560	NA	NA	2.73	7.0	11.30	0.5
3	11	1655	40.9	5	C	7.55	7.0	3.0	2.710	0.058	1.600	2.63	0.328	2.82	6.5	9.80	0.5
3	11	1923	43.4	5	C	7.64	5.4	3.2	2.570	0.061	1.680	NA	NA	1.99	7.0	10.00	0.2
3	11	2205	46.1	5	C	7.57	5.0	2.7	2.130	0.038	0.982	2.16	0.361	2.76	6.2	10.30	0.2
3	12	57	48.9	5	C	7.56	5.2	2.8	2.630	0.056	1.610	NA	NA	2.07	6.0	10.20	0.5
3	12	330	51.5	5	C	7.58	5.0	3.0	2.540	0.061	1.620	3.46	0.422	1.44	6.0	10.90	0.2
3	12	605	54.1	5	C	7.64	6.0	3.4	2.460	0.058	1.630	NA	NA	3.99	6.0	11.30	0.0
3	12	845	56.8	5	C	7.50	7.5	3.3	2.490	0.058	1.560	3.43	0.271	2.73	5.8	10.10	0.0
3	12	1115	59.3	5	C	7.50	7.0	3.6	2.630	0.058	1.620	NA	NA	2.73	6.0	10.30	0.1
3	12	1355	61.9	5	C	7.60	7.0	2.7	2.600	0.058	1.570	2.51	0.423	2.54	6.2	10.60	0.5
3	12	1626	64.4	5	C	7.50	6.5	3.3	2.820	0.061	1.580	NA	NA	2.45	6.0	10.50	0.1
3	12	1844	66.7	5	C	7.60	7.2	3.0	2.610	0.058	1.560	3.43	0.391	2.73	5.9	10.50	0.2
3	12	2057	68.9	5	C	7.60	7.0	3.6	2.510	0.046	1.240	NA	NA	2.16	6.2	10.40	0.2
3	12	2328	71.5	5	C	7.50	7.5	4.2	2.530	0.051	1.360	3.44	0.383	2.92	5.9	10.00	0.2
3	13	120	73.3	5	C	7.50	7.2	3.6	2.710	0.051	1.290	3.23	0.387	2.54	5.8	11.00	0.0
3	13	317	75.3	5	C	7.50	7.0	3.6	2.720	0.056	1.540	NA	NA	1.69	6.0	10.40	0.0

946510316

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	537	77.6	5	C	7.60	8.0	3.9	2.540	0.061	1.620	3.11	0.427	2.78	6.0	12.00	0.0
3	13	724	79.4	5	C	7.60	8.5	3.9	2.390	0.056	1.510	NA	NA	1.88	6.0	11.50	0.0
3	13	900	81.0	5	C	7.50	6.2	3.2	2.600	0.058	1.470	3.29	0.407	2.45	6.0	11.20	0.1
3	13	1120	83.3	5	C	7.60	5.5	1.8	2.400	0.061	1.550	NA	NA	1.98	6.4	10.50	0.1
3	13	1430	86.5	5	C	7.60	5.4	2.6	2.440	0.056	1.560	3.57	0.460	2.06	6.9	10.40	0.1
3	13	1655	88.9	5	C	7.50	5.7	2.4	2.460	0.061	1.540	NA	NA	2.16	7.0	10.80	0.2
3	13	1906	91.1	5	C	7.50	6.4	3.0	2.410	0.056	1.490	3.45	0.396	2.54	6.2	10.90	0.2
3	13	2125	93.4	5	C	7.60	6.0	3.2	2.330	0.061	1.620	NA	NA	2.63	7.0	11.10	0.1
3	13	2340	95.7	5	C	7.50	6.7	3.0	2.350	0.058	1.560	3.34	0.390	2.35	6.5	10.80	0.1
3	14	221	98.3	5	C	7.50	5.8	2.7	1.870	0.040	1.080	NA	NA	2.63	7.0	10.60	0.0
3	14	452	100.9	5	C	7.50	6.6	2.7	2.340	0.061	1.550	3.31	0.381	2.63	7.0	11.00	0.0
3	14	756	103.9	5	C	7.60	6.5	3.6	2.220	0.066	1.590	NA	NA	3.70	8.0	11.00	0.0
3	14	1045	106.8	5	C	7.60	15.0	2.8	2.340	0.066	1.630	6.68	0.493	2.53	7.0	11.20	0.0
3	14	1425	110.4	5	C	7.60	17.0	4.0	2.370	0.066	1.600	NA	NA	0.12	7.2	10.40	0.0
3	14	1746	113.8	5	C	7.60	9.0	2.8	2.340	0.066	1.560	3.29	0.379	0.11	7.0	10.00	0.2
3	14	2020	116.3	5	C	7.70	8.0	2.8	2.250	0.061	1.540	NA	NA	3.29	6.2	10.00	0.1
3	14	2315	119.3	5	C	7.80	8.6	3.0	2.240	0.064	1.580	3.72	0.388	0.13	7.0	11.00	0.1
3	15	125	121.4	5	C	7.70	8.0	3.4	1.460	0.035	0.870	NA	NA	2.96	7.0	11.20	0.0
3	15	420	124.3	5	C	7.60	7.8	3.0	2.170	0.061	1.530	3.23	0.405	2.73	6.0	11.00	0.0
3	15	721	127.3	5	C	7.70	8.5	3.4	2.010	0.061	1.540	NA	NA	3.01	6.0	11.40	0.0
3	15	1025	130.4	5	C	7.60	6.0	8.8	2.550	0.071	1.610	3.76	0.550	NA	5.0	10.60	0.0
3	15	1330	133.5	5	C	7.60	8.0	4.2	2.640	0.074	1.710	NA	NA	NA	5.1	10.40	0.1
3	15	1625	136.4	5	C	7.50	18.0	6.9	2.320	0.064	1.570	4.05	0.726	2.35	6.2	9.90	0.1
3	15	1920	139.3	5	C	7.60	7.8	4.4	2.580	0.071	1.640	NA	NA	8.90	5.2	10.40	0.1
3	15	2223	142.4	5	C	7.60	7.0	5.0	2.520	0.064	1.550	3.34	0.439	3.34	6.0	11.00	0.1
3	16	218	146.3	5	C	7.70	7.5	3.9	2.640	0.064	1.570	NA	NA	3.87	6.0	12.00	0.0

946510317

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	520	149.3	5	C	7.60	7.5	8.6	2.610	0.066	1.560	3.24	0.509	2.73	5.0	10.80	0.0
3	16	830	152.5	5	C	7.60	7.8	5.1	2.410	0.061	1.530	NA	NA	2.70	6.5	11.60	0.0
3	16	1125	155.4	5	C	7.60	7.0	3.8	2.630	0.061	1.550	3.96	0.538	2.63	5.8	11.40	0.0
3	16	1425	158.4	5	C	7.60	6.6	3.6	2.580	0.061	1.520	NA	NA	2.26	6.0	11.50	0.0
3	16	1716	161.3	5	C	7.70	7.8	3.6	NA	NA	NA	3.74	0.521	3.37	6.2	12.00	0.1
3	16	1954	163.9	5	C	7.60	18.0	5.7	NA	NA	NA	NA	NA	6.74	5.9	12.20	0.1
3	16	2300	167.0	5	C	7.60	7.0	5.7	NA	NA	NA	3.91	0.523	2.82	5.9	12.30	0.0
3	17	157	169.9	5	C	7.70	7.3	3.8	1.730	0.035	0.783	NA	NA	2.63	6.0	12.20	0.0
3	17	447	172.8	5	C	7.60	8.4	3.8	NA	0.066	1.590	4.13	0.504	3.03	5.0	10.60	0.0
3	17	748	175.8	5	C	7.60	7.4	3.2	1.420	0.025	0.552	NA	NA	2.26	5.0	10.80	0.0
3	17	1050	178.8	5	C	7.60	7.8	3.0	NA	NA	NA	3.13	0.346	3.34	5.2	11.10	0.2
3	17	1410	182.2	5	C	7.60	6.4	3.4	NA	NA	NA	NA	NA	2.16	4.2	9.60	0.2
3	17	1725	185.4	5	C	7.60	18.0	4.8	2.260	0.051	1.410	3.69	0.524	0.16	5.5	12.25	0.0
3	17	2010	188.2	5	C	7.60	7.4	3.6	2.280	0.056	1.510	NA	NA	2.73	5.0	12.25	0.0
3	17	2300	191.0	5	C	7.60	6.3	2.2	2.320	0.043	1.130	3.81	0.546	1.79	3.0	13.00	0.0
3	18	157	193.9	5	C	7.80	6.2	4.5	2.100	0.049	1.230	NA	NA	2.45	4.5	12.80	0.0
3	18	455	196.9	5	C	7.60	7.8	3.2	2.440	0.056	1.420	3.17	0.360	2.54	3.0	12.40	0.0
3	18	745	199.8	5	C	7.60	8.5	3.6	2.460	0.067	1.590	NA	NA	2.45	3.0	11.80	0.0
3	18	1020	202.3	5	C	7.60	6.8	3.9	2.540	0.062	1.540	3.42	0.350	5.40	3.5	12.60	0.0
3	18	1320	205.3	5	C	7.70	6.5	3.4	2.470	0.067	1.640	NA	NA	5.73	3.5	11.80	0.0
3	18	1710	209.2	5	C	7.70	8.4	3.9	2.560	0.062	1.510	3.45	0.349	7.08	4.5	10.70	0.0
3	18	2005	212.1	5	C	7.70	7.3	3.6	2.340	0.067	1.580	NA	NA	6.41	4.0	10.50	0.0
3	18	2300	215.0	5	C	7.60	6.6	3.8	2.440	0.062	1.490	NA	NA	3.11	4.0	10.75	0.0
3	19	140	217.9	5	C	7.70	5.3	3.6	2.430	0.062	1.560	3.38	0.260	2.73	3.8	12.90	0.2
3	19	433	220.5	5	C	7.60	5.7	3.6	2.630	0.069	1.660	NA	NA	2.54	2.3	11.20	0.0
3	19	735	223.6	5	C	7.70	7.8	2.8	2.340	0.067	1.590	3.24	0.269	8.77	4.0	10.20	0.0

946510318

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL SC - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1300	229.3	5	C	7.70	5.2	3.0	2.750	0.062	1.600	4.21	0.514	2.54	4.0	13.00	0.0
3	19	1600	232.0	5	C	7.70	5.0	3.4	2.350	0.051	1.250	NA	NA	3.07	4.0	12.50	0.0
3	19	1945	235.8	5	C	7.60	7.2	3.3	2.320	0.062	1.490	3.65	0.453	4.29	3.5	11.00	0.0
3	19	2140	237.7	5	C	7.60	5.8	2.8	2.640	0.067	1.640	NA	NA	3.99	3.5	11.50	0.0
3	20	134	241.6	5	C	7.60	5.0	2.6	2.770	0.077	1.750	2.47	0.374	2.16	3.8	11.00	0.0
3	20	430	244.5	5	C	7.60	4.7	2.6	2.410	0.067	1.530	NA	NA	2.16	3.5	11.00	0.0
3	20	735	247.6	5	C	7.60	7.1	3.1	2.400	0.056	1.360	2.74	0.483	4.29	3.0	11.40	0.0

946510319

BASELINE

SECØND

RIVER

3-10/3-20-81

1/2 DEPTH

946510320

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	945	9.4	5	C	7.55	15.0	3.0	2.090	0.048	1.490	3.17	0.495	7.24	6.8	8.60	0.2
3	10	1235	12.6	5	C	7.55	12.0	2.3	2.420	0.056	1.760	NA	NA	4.82	6.5	10.50	0.2
3	10	1555	15.9	5	C	7.55	10.0	2.2	2.530	0.056	1.710	3.45	0.475	6.31	7.0	10.50	0.2
3	10	1855	18.9	5	C	7.60	14.0	4.1	2.710	0.067	1.800	NA	NA	7.79	7.0	10.40	0.0
3	10	2145	21.8	5	C	7.54	10.0	3.3	2.550	0.056	1.690	3.12	0.434	8.16	6.5	9.80	0.0
3	11	37	24.6	5	C	7.53	6.5	1.7	2.510	0.056	1.670	NA	NA	1.69	5.0	9.20	0.0
3	11	317	27.3	5	C	7.61	7.2	3.9	2.510	0.067	1.610	3.64	0.527	1.41	7.0	12.00	0.5
3	11	529	29.5	5	C	7.61	8.0	4.1	2.430	0.067	1.570	NA	NA	1.69	7.0	11.60	0.3
3	11	744	31.7	5	C	7.60	8.8	4.4	2.670	0.070	1.730	3.07	0.420	2.72	6.5	10.20	0.5
3	11	1030	34.5	5	C	7.58	8.0	2.7	2.310	0.058	1.650	3.45	0.435	2.92	7.0	11.90	0.5
3	11	1350	37.8	5	C	7.59	8.4	3.3	2.370	0.056	1.560	NA	NA	2.73	7.0	11.30	0.5
3	11	1655	40.9	5	C	7.55	7.0	3.0	2.710	0.058	1.600	2.63	0.328	2.82	6.5	9.80	0.5
3	11	1923	43.4	5	C	7.64	5.4	3.2	2.570	0.061	1.680	NA	NA	1.99	7.0	10.00	0.2
3	11	2205	46.1	5	C	7.57	5.0	2.7	2.130	0.038	0.982	2.16	0.361	2.76	6.2	10.30	0.2
3	12	57	48.9	5	C	7.56	5.2	2.8	2.630	0.056	1.610	NA	NA	2.07	6.0	10.20	0.5
3	12	336	51.5	5	C	7.58	5.0	3.0	2.540	0.061	1.620	3.46	0.422	1.44	6.0	10.90	0.2
3	12	605	54.1	5	C	7.64	6.0	3.4	2.460	0.058	1.630	NA	NA	3.99	6.0	11.30	0.0
3	12	845	56.8	5	C	7.50	7.5	3.3	2.490	0.058	1.560	3.43	0.271	2.73	5.8	10.10	0.0
3	12	1115	59.3	5	C	7.50	7.0	3.6	2.630	0.058	1.620	NA	NA	2.73	6.0	10.30	0.1
3	12	1355	61.9	5	C	7.60	7.0	2.7	2.600	0.058	1.570	2.51	0.423	2.54	6.2	10.60	0.5
3	12	1626	64.4	5	C	7.50	6.5	3.3	2.820	0.061	1.580	NA	NA	2.45	6.0	10.50	0.1
3	12	1844	66.7	5	C	7.60	7.2	3.0	2.610	0.058	1.560	3.43	0.391	2.73	5.9	10.50	0.2
3	12	2057	68.9	5	C	7.60	7.0	3.6	2.510	0.046	1.240	NA	NA	2.16	6.2	10.40	0.2
3	12	2328	71.5	5	C	7.50	7.5	4.2	2.530	0.051	1.360	3.44	0.383	2.92	5.9	10.00	0.2
3	13	120	73.3	5	C	7.50	7.2	3.6	2.710	0.051	1.290	3.23	0.387	2.54	5.8	11.00	0.0
3	13	317	75.3	5	C	7.50	7.0	3.6	2.720	0.056	1.540	NA	NA	1.69	6.0	10.40	0.0

946510321

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	537	77.6	5	C	7.60	8.0	3.9	2.540	0.061	1.620	3.11	0.427	2.78	6.0	12.00	0.0
3	13	724	79.4	5	C	7.60	8.5	3.9	2.390	0.056	1.510	NA	NA	1.88	6.0	11.50	0.0
3	13	900	81.0	5	C	7.50	6.2	3.2	2.600	0.058	1.470	3.29	0.407	2.45	6.0	11.20	0.1
3	13	1120	83.3	5	C	7.60	5.5	1.8	2.400	0.061	1.550	NA	NA	1.98	6.4	10.50	0.1
3	13	1430	86.5	5	C	7.60	5.4	2.6	2.440	0.056	1.560	3.57	0.460	2.06	6.9	10.40	0.1
3	13	1655	88.9	5	C	7.50	5.7	2.4	2.460	0.061	1.540	NA	NA	2.16	7.0	10.80	0.2
3	13	1906	91.1	5	C	7.50	6.4	3.0	2.410	0.056	1.490	3.45	0.396	2.54	6.2	10.90	0.2
3	13	2125	93.4	5	C	7.60	6.0	3.2	2.330	0.061	1.620	NA	NA	2.63	7.0	11.10	0.1
3	13	2340	95.7	5	C	7.50	6.7	3.0	2.350	0.058	1.560	3.34	0.390	2.35	6.5	10.80	0.1
3	14	221	98.3	5	C	7.50	5.8	2.7	1.870	0.040	1.080	NA	NA	2.63	7.0	10.60	0.0
3	14	452	100.9	5	C	7.50	6.6	2.7	2.340	0.061	1.550	3.31	0.381	2.63	7.0	11.00	0.0
3	14	756	103.9	5	C	7.60	6.5	3.6	2.220	0.066	1.590	NA	NA	3.70	8.0	11.00	0.0
3	14	1045	106.8	5	C	7.60	15.0	2.8	2.340	0.066	1.630	6.68	0.493	2.53	7.0	11.20	0.0
3	14	1425	110.4	5	C	7.60	17.0	4.0	2.370	0.066	1.600	NA	NA	0.12	7.2	10.40	0.0
3	14	1746	113.8	5	C	7.60	9.0	2.8	2.340	0.066	1.560	3.29	0.379	0.11	7.0	10.00	0.2
3	14	2020	116.3	5	C	7.70	8.0	2.8	2.250	0.061	1.540	NA	NA	3.29	6.2	10.00	0.1
3	14	2315	119.3	5	C	7.80	8.6	3.0	2.240	0.064	1.580	3.72	0.388	0.13	7.0	11.00	0.1
3	15	125	121.4	5	C	7.70	8.0	3.4	1.460	0.035	0.870	NA	NA	2.96	7.0	11.20	0.0
3	15	420	124.3	5	C	7.60	7.8	3.0	2.170	0.061	1.530	3.23	0.405	2.73	6.0	11.00	0.0
3	15	721	127.3	5	C	7.70	8.5	3.4	2.010	0.061	1.540	NA	NA	3.01	6.0	11.40	0.0
3	15	1025	130.4	5	C	7.60	6.0	8.8	2.550	0.071	1.610	3.76	0.550	NA	5.0	10.60	0.0
3	15	1330	133.5	5	C	7.60	8.0	4.2	2.640	0.074	1.710	NA	NA	NA	5.1	10.40	0.1
3	15	1625	136.4	5	C	7.50	18.0	6.9	2.320	0.064	1.570	4.05	0.726	2.35	6.2	9.90	0.1
3	15	1920	139.3	5	C	7.60	7.8	4.4	2.580	0.071	1.640	NA	NA	8.90	5.2	10.40	0.1
3	15	2223	142.4	5	C	7.60	7.0	5.0	2.520	0.064	1.550	3.34	0.439	3.34	6.0	11.00	0.1
3	16	218	146.3	5	C	7.70	7.5	3.9	2.640	0.064	1.570	NA	NA	3.87	6.0	12.00	0.0

94510322

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	520	149.3	5	C	7.60	7.5	8.6	2.610	0.066	1.560	3.24	0.509	2.73	5.0	10.80	0.0
3	16	830	152.5	5	C	7.60	7.8	5.1	2.410	0.061	1.530	NA	NA	2.70	6.5	11.60	0.0
3	16	1125	155.4	5	C	7.60	7.0	3.8	2.630	0.061	1.550	3.96	0.538	2.63	5.8	11.40	0.0
3	16	1425	158.4	5	C	7.60	6.6	3.6	2.580	0.061	1.520	NA	NA	2.26	6.0	11.50	0.0
3	16	1716	161.3	5	C	7.70	7.8	3.6	NA	NA	NA	3.74	0.521	3.37	6.2	12.00	0.1
3	16	1954	163.9	5	C	7.60	18.0	5.7	NA	NA	NA	NA	NA	6.74	5.9	12.20	0.1
3	16	2300	167.0	5	C	7.60	7.0	5.7	NA	NA	NA	3.91	0.523	2.82	5.9	12.30	0.0
3	17	157	169.9	5	C	7.70	7.3	3.8	1.730	0.035	0.783	NA	NA	2.63	6.0	12.20	0.0
3	17	447	172.8	5	C	7.60	8.4	3.8	NA	0.066	1.590	4.13	0.504	3.03	5.0	10.60	0.0
3	17	748	175.8	5	C	7.60	7.4	3.2	1.420	0.025	0.552	NA	NA	2.26	5.0	10.80	0.0
3	17	1050	178.8	5	C	7.60	7.8	3.0	NA	NA	NA	3.13	0.346	3.34	5.2	11.10	0.2
3	17	1410	182.2	5	C	7.60	6.4	3.4	NA	NA	NA	NA	NA	2.16	4.2	9.60	0.2
3	17	1725	185.4	5	C	7.60	18.0	4.8	2.260	0.051	1.410	3.69	0.524	0.16	5.5	12.25	0.0
3	17	2010	188.2	5	C	7.60	7.4	3.6	2.280	0.056	1.510	NA	NA	2.73	5.0	12.25	0.0
3	17	2300	191.0	5	C	7.60	6.3	2.2	2.320	0.043	1.130	3.81	0.546	1.79	3.0	13.00	0.0
3	18	157	193.9	5	C	7.80	6.2	4.5	2.100	0.049	1.230	NA	NA	2.45	4.5	12.80	0.0
3	18	455	196.9	5	C	7.60	7.8	3.2	2.440	0.056	1.420	3.17	0.360	2.54	3.0	12.40	0.0
3	18	745	199.8	5	C	7.60	8.5	3.6	2.460	0.067	1.590	NA	NA	2.45	3.0	11.80	0.0
3	18	1020	202.3	5	C	7.60	6.8	3.9	2.540	0.062	1.540	3.42	0.350	5.40	3.5	12.60	0.0
3	18	1320	205.3	5	C	7.70	6.5	3.4	2.470	0.067	1.640	NA	NA	5.73	3.5	11.80	0.0
3	18	1710	209.2	5	C	7.70	8.4	3.9	2.560	0.062	1.510	3.45	0.349	7.08	4.5	10.70	0.0
3	18	2005	212.1	5	C	7.70	7.3	3.6	2.340	0.067	1.580	NA	NA	6.41	4.0	10.50	0.0
3	18	2300	215.0	5	C	7.60	6.6	3.8	2.440	0.062	1.490	NA	NA	3.11	4.0	10.75	0.0
3	19	140	217.9	5	C	7.70	5.3	3.6	2.430	0.062	1.560	3.38	0.260	2.73	3.8	12.90	0.2
3	19	433	220.5	5	C	7.60	5.7	3.6	2.630	0.069	1.660	NA	NA	2.54	2.3	11.20	0.0
3	19	735	223.6	5	C	7.70	7.8	2.8	2.340	0.067	1.590	3.24	0.269	8.77	4.0	10.20	0.0

94510323

BASELINE-RIVER SAMPLING
UNION-AVENUE - LEVEL 5C - 1/2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1300	229.3	5	C	7.70	5.2	3.0	2.750	0.062	1.600	4.21	0.514	2.54	4.0	13.00	0.0
3	19	1600	232.0	5	C	7.70	5.0	3.4	2.350	0.051	1.250	NA	NA	3.07	4.0	12.50	0.0
3	19	1945	235.7	5	C	7.60	7.2	3.3	2.320	0.062	1.490	3.65	0.453	4.29	3.5	11.00	0.0
3	19	2140	237.7	5	C	7.60	5.8	2.8	2.640	0.067	1.640	NA	NA	3.99	3.5	11.50	0.0
3	20	134	241.6	5	C	7.60	5.0	2.6	2.770	0.077	1.750	2.47	0.374	2.16	3.8	11.00	0.0
3	20	430	244.5	5	C	7.60	4.7	2.6	2.410	0.067	1.530	NA	NA	2.16	3.5	11.00	0.0
3	20	735	247.6	5	C	7.60	7.1	3.1	2.400	0.056	1.360	2.74	0.483	4.29	3.0	11.40	0.0

946510324

BASELINE

SECOND RIVER

3-10/3-20-81

1/2 DEPTH

946510325

BASELINE-RIVER SAMPLING
SECOND-RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	830	8.5	4	C	8.27	1.4	3.9	0.150	0.035	2.520	1.37	0.131	0.98	8.2	13.20	NA
3	10	1140	11.7	4	C	8.68	1.8	4.1	0.557	0.030	2.460	NA	NA	1.88	10.5	13.40	NA
3	10	1500	15.0	4	C	8.64	1.7	1.6	0.164	0.030	2.440	1.15	0.107	1.04	11.2	12.00	NA
3	10	1746	17.8	4	C	8.89	2.0	1.5	0.197	0.030	2.480	NA	NA	0.74	9.8	10.80	NA
3	10	2038	20.6	4	C	8.04	1.5	2.1	0.136	0.030	2.600	1.06	0.353	0.61	8.5	10.80	NA
3	10	2315	23.3	4	C	8.00	1.6	1.1	0.133	0.032	2.670	NA	NA	0.67	8.0	10.40	NA
3	11	217	26.3	4	C	7.91	5.5	4.1	0.119	0.024	2.490	1.62	0.249	0.50	7.5	11.20	NA
3	11	445	28.8	4	C	7.92	3.4	2.6	0.101	0.024	2.560	NA	NA	0.44	7.0	11.50	NA
3	11	652	30.9	4	C	7.95	2.1	1.7	0.075	0.023	2.500	0.68	0.245	0.21	7.0	11.60	NA
3	11	940	33.7	4	C	8.45	3.5	2.2	0.003	0.025	2.300	0.75	0.198	1.13	8.0	13.30	NA
3	11	1210	36.2	4	C	8.80	7.1	2.2	0.091	0.028	2.100	NA	NA	1.88	9.0	13.30	NA
3	11	1545	39.8	4	C	7.89	42.0	23.0	0.470	0.085	2.300	2.71	NA	7.52	9.0	11.40	NA
3	11	1823	42.4	4	C	7.85	7.0	7.6	0.125	0.062	2.360	NA	NA	1.69	7.5	10.20	NA
3	11	2105	45.1	4	C	7.72	6.3	9.6	0.093	0.072	2.150	0.81	0.363	0.91	7.0	10.40	NA
3	12	15	48.3	4	C	7.74	8.5	7.6	0.073	0.095	2.360	NA	NA	NA	6.5	9.80	NA
3	12	223	50.4	4	C	7.75	5.4	5.0	0.003	0.082	2.280	0.21	0.130	1.69	6.8	9.10	NA
3	12	513	53.2	4	C	7.79	4.5	5.0	0.003	0.072	2.470	NA	NA	1.03	6.0	11.50	NA
3	12	735	55.6	4	C	7.95	4.5	2.4	0.002	0.062	2.390	0.42	0.124	0.85	6.0	12.30	NA
3	12	1015	58.3	4	C	8.40	4.5	3.9	0.002	0.062	2.390	NA	NA	1.32	8.2	13.20	NA
3	12	1300	61.0	4	C	8.70	7.0	4.5	0.032	0.062	2.310	0.26	0.182	1.03	10.2	12.60	NA
3	12	1520	63.3	4	C	8.60	5.0	2.7	0.003	0.056	2.340	NA	NA	1.69	9.8	11.60	NA
3	12	1756	65.9	4	C	8.20	3.0	2.1	0.100	0.046	1.920	0.35	0.321	0.81	8.9	10.60	NA
3	12	2008	68.1	4	C	8.00	2.5	2.1	0.067	0.051	2.350	NA	NA	0.57	8.0	10.00	NA
3	12	2236	70.6	4	C	7.90	2.5	2.7	0.082	0.046	1.890	0.21	0.446	0.37	7.2	9.80	NA
3	13	144	73.7	4	C	7.90	4.0	4.5	0.056	0.056	2.450	0.45	0.130	1.22	7.0	10.60	NA
3	13	339	75.8	4	C	7.90	3.2	4.8	0.060	0.049	2.250	NA	NA	0.88	7.0	10.60	NA

946510326

BASELINE-RIVER SAMPLING
SECOND-RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	607	78.1	4	C	7.90	2.5	2.1	0.050	0.044	2.250	0.55	0.077	0.78	7.0	10.50	NA
3	13	802	80.0	4	C	8.10	3.0	2.4	0.049	0.046	2.330	NA	NA	1.41	7.0	12.60	NA
3	13	1030	82.5	4	C	8.60	2.1	2.1	0.093	0.046	1.880	0.94	0.145	3.76	10.5	11.30	NA
3	13	1325	85.4	4	C	8.90	2.5	3.3	0.122	0.046	1.860	NA	NA	2.91	11.9	13.20	NA
3	13	1553	87.9	4	C	8.80	2.2	2.7	0.085	0.049	2.300	0.96	0.091	1.41	11.2	12.50	NA
3	13	1819	90.3	4	C	8.40	2.7	2.0	0.056	0.054	2.250	NA	NA	1.13	10.5	10.10	NA
3	13	2034	92.6	4	C	8.00	2.0	1.5	0.090	0.056	2.070	0.47	0.093	0.94	10.0	11.80	NA
3	13	2256	94.9	4	C	7.90	1.5	1.2	0.083	0.049	2.290	NA	NA	0.75	9.2	10.20	NA
3	14	248	98.8	4	C	7.90	2.4	1.4	0.058	0.051	2.390	0.84	0.198	0.94	9.0	10.20	NA
3	14	536	101.6	4	C	7.90	3.2	1.2	0.086	0.049	2.440	NA	NA	0.84	7.0	10.60	NA
3	14	820	104.3	4	C	8.30	2.6	2.8	0.084	0.049	2.400	1.45	0.119	1.13	6.7	13.40	NA
3	14	1130	107.5	4	C	8.70	2.4	2.4	0.096	0.051	2.210	NA	NA	2.45	8.0	13.80	NA
3	14	1455	110.9	4	C	8.80	3.4	3.2	0.077	0.051	2.210	1.14	0.202	2.26	7.8	12.80	NA
3	14	1639	112.6	4	C	8.60	2.7	3.2	0.112	0.056	2.290	NA	NA	1.13	6.2	12.60	NA
3	14	1919	115.3	4	C	8.20	2.0	2.1	0.102	0.056	2.290	0.50	0.342	1.13	5.0	11.00	NA
3	14	2216	118.3	4	C	7.90	2.0	2.7	0.088	0.051	2.360	NA	NA	0.20	4.9	11.60	NA
3	15	158	122.0	4	C	7.90	3.0	2.8	0.082	0.046	1.850	0.51	0.170	0.85	5.0	11.60	NA
3	15	502	125.0	4	C	7.90	2.6	2.1	0.064	0.046	2.420	NA	NA	1.42	5.0	11.80	NA
3	15	800	128.0	4	C	8.10	1.8	1.6	0.020	0.041	2.420	1.27	0.065	0.28	5.0	13.00	NA
3	15	1110	131.2	4	C	8.70	2.0	6.9	0.020	0.044	2.170	0.58	0.194	NA	9.0	13.20	NA
3	15	1415	134.3	4	C	8.90	1.9	2.7	0.020	0.049	2.140	NA	NA	0.07	10.0	13.40	NA
3	15	1742	137.7	4	C	8.50	2.0	2.7	0.020	0.051	2.100	1.08	0.138	1.28	9.0	10.80	NA
3	15	2052	140.9	4	C	8.00	2.2	3.9	0.020	0.059	2.150	NA	NA	0.74	7.9	10.90	NA
3	15	2347	143.8	4	C	7.90	1.7	3.8	NA	0.051	2.160	0.50	0.170	0.61	7.0	11.20	NA
3	16	258	147.0	4	C	7.90	1.6	3.9	NA	0.022	1.640	NA	NA	0.78	7.0	10.50	NA
3	16	559	150.0	4	C	7.90	1.8	1.6	NA	0.030	2.180	0.21	0.077	5.55	7.0	10.60	NA

9465103 27

BASELINE-RIVER SAMPLING
SECOND-RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	915	153.3	4	C	8.40	2.4	7.4	0.102	0.035	2.100	NA	NA	1.69	8.2	13.30	NA
3	16	1215	156.3	4	C	8.60	2.2	8.7	0.172	0.040	2.320	1.17	0.148	2.26	9.0	13.30	NA
3	16	1510	159.2	4	C	8.70	4.0	5.1	0.361	0.062	2.300	NA	NA	4.72	9.3	13.20	NA
3	16	1634	160.6	4	C	8.60	3.4	2.8	NA	NA	NA	1.71	0.197	2.44	8.2	12.00	NA
3	16	1915	163.3	4	C	8.10	3.8	2.0	NA	NA	NA	NA	NA	1.88	6.8	12.00	NA
3	16	2213	166.2	4	C	7.90	3.3	2.6	NA	NA	NA	1.56	0.100	0.84	5.2	12.80	NA
3	17	107	169.1	4	C	7.90	3.0	2.4	0.629	0.046	2.580	NA	NA	4.38	4.0	12.20	NA
3	17	405	172.1	4	C	7.90	2.3	2.1	0.540	0.040	2.120	1.71	0.156	0.78	3.0	12.20	NA
3	17	706	175.1	4	C	8.00	2.5	2.2	0.636	0.035	1.780	1.65	0.226	1.21	3.0	13.00	NA
3	17	1135	179.6	4	C	8.70	1.8	3.0	NA	NA	NA	NA	NA	2.07	7.5	13.90	NA
3	17	1455	182.9	4	C	8.90	2.5	2.6	NA	NA	NA	1.83	0.224	1.60	8.2	13.60	NA
3	17	1620	184.3	4	C	8.70	2.2	2.0	1.570	0.038	2.340	NA	NA	1.38	7.3	13.25	NA
3	17	1910	187.2	4	C	8.30	1.9	2.7	1.630	0.040	2.250	2.10	0.153	0.84	6.0	11.50	NA
3	17	2150	189.8	4	C	8.10	2.3	2.6	1.500	0.035	2.120	NA	NA	0.51	4.0	12.75	NA
3	18	106	193.1	4	C	7.90	3.8	7.1	1.010	0.025	2.010	1.93	0.279	0.57	3.0	12.20	NA
3	18	405	196.1	4	C	8.00	4.7	2.1	0.641	0.030	2.510	NA	NA	1.03	1.5	13.00	NA
3	18	704	199.1	4	C	8.00	4.7	1.6	0.473	0.030	2.360	NA	NA	1.11	1.5	13.70	NA
3	18	915	201.3	4	C	8.40	2.8	2.0	0.271	0.030	2.520	0.65	0.472	2.26	4.2	15.50	NA
3	18	1215	204.3	4	C	8.80	7.2	2.1	0.555	0.032	2.540	NA	NA	3.20	6.5	14.90	NA
3	18	1520	207.3	4	C	8.70	2.7	2.6	0.576	0.035	2.460	1.24	0.401	2.02	8.2	13.40	NA
3	18	1735	209.6	4	C	8.50	3.3	3.0	1.310	0.035	2.580	NA	NA	2.82	6.8	12.00	NA
3	18	2030	212.5	4	C	8.20	2.6	2.7	1.200	0.048	2.540	2.30	0.377	0.71	6.0	10.50	NA
3	18	2325	215.4	4	C	8.00	2.2	2.8	1.340	0.046	2.550	NA	NA	1.11	5.0	10.50	NA
3	19	208	218.1	4	C	8.00	2.4	2.6	0.740	0.032	2.150	1.63	0.157	13.17	5.0	11.40	NA
3	19	457	220.9	4	C	7.90	5.6	6.4	1.200	0.032	1.970	NA	NA	37.62	4.0	11.50	NA
3	19	758	224.0	4	C	8.10	2.5	2.6	0.616	0.032	2.010	1.87	0.256	17.87	4.0	11.40	NA

94510328

BASELINE-RIVER SAMPLING
SECOND-RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1045	226.9	4	C	8.70	2.0	3.2	0.883	0.043	2.520	2.33	0.171	5.21	8.0	15.20	NA
3	19	1345	229.8	4	C	8.80	2.3	6.9	1.170	0.062	2.430	1.93	0.188	5.38	8.2	15.20	NA
3	19	1625	232.4	4	C	8.70	2.4	3.4	2.090	0.062	2.010	NA	NA	2.92	8.0	13.00	NA
3	19	1920	235.3	4	C	8.30	2.5	3.2	2.240	0.062	2.560	2.67	0.151	1.98	7.0	10.00	NA
3	19	2215	238.3	4	C	8.00	3.8	5.0	2.090	0.062	2.500	NA	NA	1.03	6.0	10.00	NA
3	20	147	241.8	4	C	7.90	4.6	3.4	1.230	0.093	2.850	NA	NA	1.98	5.8	10.60	NA
3	20	446	244.8	4	C	7.90	4.0	3.1	1.110	0.067	2.500	1.43	0.197	2.44	5.0	10.60	NA
3	20	753	247.9	4	C	8.20	3.3	1.5	1.010	0.062	2.560	NA	NA	1.41	5.0	10.60	NA

946510329

BASELINE

SADDLE

RIVER

3-10/3-20-81

1/2 DEPTH

946510330

BASELINE-RIVER SAMPLING
SADDLE RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	1050	10.8	7	C	7.54	3.2	4.2	2.970	0.123	2.530	5.02	0.585	2.73	6.5	10.00	NA
3	10	1340	13.7	7	C	7.54	9.5	4.6	2.790	0.130	2.690	NA	NA	4.08	8.5	9.70	NA
3	10	1655	16.9	7	C	7.55	25.0	4.8	2.630	0.123	2.420	4.07	0.678	4.45	8.7	9.70	NA
3	10	1945	19.8	7	C	7.59	12.0	5.2	3.270	0.118	2.260	NA	NA	4.82	8.5	10.40	NA
3	10	2225	22.4	7	C	7.64	12.0	4.8	2.590	0.126	2.550	3.73	0.591	3.71	7.5	10.20	NA
3	11	124	25.4	7	C	7.65	6.5	7.6	2.860	0.126	2.250	NA	NA	2.16	6.0	11.60	NA
3	11	402	28.0	7	C	7.66	5.6	6.6	3.190	0.123	2.140	4.95	0.719	1.13	6.0	10.60	NA
3	11	613	30.2	7	C	7.64	5.2	11.6	3.290	0.126	2.200	NA	NA	2.26	6.0	10.60	NA
3	11	845	32.8	7	C	7.60	3.0	4.6	2.810	0.099	1.810	2.97	0.519	1.60	5.8	10.80	NA
3	11	1115	35.3	7	C	7.63	3.5	5.0	3.190	0.120	2.260	NA	NA	2.07	6.5	10.80	NA
3	11	1445	38.8	7	C	7.57	7.5	4.2	2.690	0.120	2.260	2.93	0.500	1.88	7.3	10.60	NA
3	11	1735	41.6	7	C	7.60	4.5	3.6	3.190	0.109	2.110	NA	NA	1.22	7.2	9.90	NA
3	11	2017	44.3	7	C	7.62	4.0	5.1	3.700	0.114	2.190	4.49	0.587	1.88	7.0	10.00	NA
3	11	2252	46.9	7	C	7.63	4.3	4.6	3.020	0.106	2.190	NA	NA	1.44	6.0	10.00	NA
3	12	130	49.5	7	C	7.62	5.0	5.8	2.870	0.114	2.190	3.79	0.417	2.10	5.5	10.10	NA
3	12	420	52.3	7	C	7.61	3.7	7.6	3.620	0.125	2.200	NA	NA	1.60	5.0	11.80	NA
3	12	645	54.8	7	C	7.62	6.0	7.1	3.740	0.130	2.220	4.90	0.665	2.82	4.9	10.80	NA
3	12	935	57.6	7	C	7.60	6.0	4.8	3.330	0.125	2.180	NA	NA	2.16	4.9	10.60	NA
3	12	1150	59.8	7	C	7.60	5.5	5.1	3.260	0.125	2.220	4.40	0.610	1.88	6.5	10.50	NA
3	12	1445	62.8	7	C	7.50	20.0	5.4	2.900	0.133	2.300	NA	NA	2.35	8.5	10.00	NA
3	12	1715	65.3	7	C	7.60	10.0	5.4	2.610	0.120	1.980	2.30	0.426	1.41	9.5	10.30	NA
3	12	1917	67.3	7	C	7.60	15.0	4.8	2.840	0.140	2.260	NA	NA	0.74	9.2	9.80	NA
3	12	2150	69.8	7	C	7.60	8.0	5.7	3.060	0.135	2.140	3.86	0.526	1.03	8.0	9.40	NA
3	13	330	75.5	7	C	7.50	6.5	6.3	4.190	0.156	2.300	5.73	0.694	0.94	6.0	9.10	NA
3	13	545	77.8	7	C	7.50	7.0	4.2	2.320	0.052	1.350	3.58	0.240	0.71	5.8	9.50	NA
3	13	915	81.3	7	C	7.70	5.2	8.9	5.080	0.166	2.450	NA	NA	1.69	6.0	8.50	NA

946510331

BASELINE-RIVER SAMPLING
SADDLE RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	13	1210	84.2	7	C	7.70	5.0	5.6	4.830	0.166	2.410	6.78	0.927	1.50	8.5	8.80	NA
3	13	1520	87.5	7	C	7.60	20.0	6.0	4.420	0.174	2.510	NA	NA	2.44	11.0	8.70	NA
3	13	1755	89.9	7	C	7.70	22.0	8.0	4.240	0.182	2.680	5.73	0.782	1.69	10.8	9.20	NA
3	13	2115	93.3	7	C	7.70	9.7	8.2	4.180	0.182	2.670	NA	NA	1.88	10.4	8.80	NA
3	14	100	97.0	7	C	7.70	8.5	11.4	4.910	0.178	2.660	6.20	0.904	1.88	8.8	7.50	NA
3	14	430	100.5	7	C	7.70	8.5	7.6	4.380	0.161	2.530	NA	NA	1.32	7.0	8.25	NA
3	14	735	103.6	7	C	7.70	6.2	6.2	4.780	0.177	2.690	NA	NA	1.31	5.0	9.25	NA
3	14	1100	107.9	7	C	7.70	5.8	4.1	5.150	0.198	2.810	8.28	1.010	1.79	5.3	9.60	NA
3	14	1430	110.5	7	C	7.70	6.4	6.0	4.830	0.208	2.830	NA	NA	1.79	7.1	10.50	NA
3	14	1750	113.8	7	C	7.80	6.5	4.1	2.670	0.120	1.530	5.62	1.020	1.88	6.2	10.80	NA
3	14	2115	117.3	7	C	7.70	5.5	4.1	3.250	0.120	1.370	NA	NA	1.41	5.9	10.20	NA
3	15	45	120.8	7	C	7.70	5.0	2.8	6.420	0.166	2.680	$10.	1.060	1.41	3.3	9.50	NA
3	15	435	124.6	7	C	7.70	4.5	4.5	5.290	0.166	2.290	NA	NA	1.32	2.0	10.00	NA
3	15	837	128.6	7	C	7.60	4.4	8.6	5.310	0.177	2.430	9.63	2.500	1.69	2.5	10.20	NA
3	15	1159	131.8	7	C	7.60	4.2	10.2	5.230	0.177	2.580	NA	NA	0.94	6.0	10.70	NA
3	15	1519	135.2	7	C	7.60	4.7	4.6	4.820	0.166	2.590	6.46	1.210	0.66	7.8	11.00	NA
3	15	1825	138.4	7	C	7.60	5.0	11.4	4.190	0.161	2.600	NA	NA	1.13	8.5	9.00	NA
3	15	2150	141.8	7	C	7.60	5.6	6.6	4.020	0.164	2.630	5.24	1.060	1.98	8.0	9.00	NA
3	16	150	145.8	7	C	7.60	6.3	12.2	4.900	0.156	2.400	NA	NA	1.69	6.8	9.30	NA
3	16	510	149.1	7	C	7.60	5.8	8.1	5.300	0.140	2.260	7.23	1.410	2.07	6.0	9.00	NA
3	16	738	151.5	7	C	7.60	5.4	12.9	5.100	0.159	2.630	NA	NA	1.60	6.2	8.80	NA
3	16	1055	154.9	7	C	7.60	4.5	6.2	5.030	0.177	2.800	NA	NA	1.69	8.0	8.60	NA
3	16	1410	158.2	7	C	7.60	18.0	7.2	4.940	0.203	3.170	8.43	1.310	1.41	8.1	8.60	NA
3	16	1815	162.2	7	C	7.60	16.0	5.9	3.730	0.172	2.650	NA	NA	1.69	7.0	8.90	NA
3	16	2210	166.2	7	C	7.60	7.8	5.6	4.200	0.159	2.560	6.16	1.090	1.60	5.0	9.40	NA
3	17	140	169.7	7	C	7.70	5.5	4.6	5.130	0.164	2.630	NA	NA	1.88	3.0	9.50	NA

946510332

BASELINE-RIVER SAMPLING
SADDLE RIVER - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	17	525	173.4	7	C	7.70	4.5	4.1	4.880	0.161	2.740	6.73	1.100	1.32	1.0	10.10	NA
3	17	835	176.9	7	C	7.60	4.5	1.5	NA	NA	NA	NA	NA	1.32	1.0	10.20	NA
3	17	1140	179.7	7	C	7.60	4.3	8.1	NA	NA	NA	NA	NA	1.15	3.0	10.50	NA
3	17	1510	183.2	7	C	7.60	5.2	3.9	NA	NA	NA	6.84	1.140	0.91	5.0	10.30	NA
3	17	1805	186.1	7	C	7.70	5.0	9.4	4.120	0.146	2.510	NA	NA	1.04	5.7	10.60	NA
3	17	2100	189.-	7	C	7.60	5.2	4.4	3.310	0.083	1.600	5.83	0.968	0.98	5.0	10.20	NA
3	18	35	192.6	7	C	7.70	4.5	6.8	3.310	0.161	2.580	NA	NA	0.74	2.0	10.20	NA
3	18	335	195.6	7	C	7.60	4.3	3.2	5.080	0.156	2.500	7.08	1.050	0.75	1.0	10.00	NA
3	18	635	198.6	7	C	7.70	4.4	6.6	5.250	0.156	2.470	NA	NA	0.94	1.0	9.50	NA
3	18	1005	202.1	7	C	7.80	4.3	3.3	5.100	0.182	2.720	$10.	1.630	1.13	0.8	10.60	NA
3	18	1305	205.1	7	C	7.80	4.5	3.3	5.130	0.187	2.680	NA	NA	1.41	3.0	10.40	NA
3	18	1630	208.5	7	C	7.80	4.8	3.4	4.120	0.140	2.240	6.03	1.110	1.31	5.5	10.50	NA
3	18	1920	211.3	7	C	7.80	5.0	3.0	4.020	0.116	2.100	NA	NA	1.31	6.0	10.50	NA
3	18	2210	214.2	7	C	7.80	5.5	5.8	3.830	0.159	2.600	5.82	1.040	1.60	5.0	9.20	NA
3	19	150	217.4	7	C	7.80	5.0	4.5	5.240	0.151	2.450	NA	NA	1.13	4.0	9.50	NA
3	19	515	221.3	7	C	7.80	4.5	3.3	5.170	0.156	2.400	9.45	1.670	0.94	2.9	10.10	NA
3	19	835	224.6	7	C	7.60	4.2	3.4	4.850	0.177	2.640	9.42	1.090	0.94	3.0	10.00	NA
3	19	1135	227.6	7	C	7.60	4.4	3.4	4.620	0.182	2.720	NA	NA	1.88	4.8	10.50	NA
3	19	1435	230.6	7	C	7.60	14.0	3.8	5.050	0.169	2.880	7.86	1.160	1.69	6.0	10.20	NA
3	19	1750	233.9	7	C	7.60	20.0	4.6	4.480	0.153	2.760	NA	NA	1.69	6.5	9.30	NA
3	19	2040	236.7	7	C	7.60	18.0	4.1	NA	NA	NA	4.86	1.110	1.50	6.0	9.20	NA
3	19	2345	239.9	7	C	7.60	7.3	5.0	4.620	0.156	2.740	NA	NA	0.90	4.1	9.10	NA
3	20	245	242.-	7	C	7.60	5.8	3.1	5.150	0.159	2.700	6.36	1.270	0.98	3.0	10.10	NA
3	20	545	245.3	7	C	7.60	4.7	2.7	5.050	0.153	2.620	NA	NA	1.20	2.0	9.90	NA

946510333

BASELINE

MARKET

STREET

3-10/3-20-81

1/2 DEPTH

946510334

BASELINE-RIVER SAMPLING
MARKET-STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	1045	10.8	9	C	7.49	5.3	3.2	2.930	0.051	1.450	4.92	0.519	2.35	6.5	9.20	NA
3	10	1325	13.4	9	C	7.51	5.8	3.9	3.050	0.051	1.450	NA	NA	1.50	7.5	10.20	NA
3	10	1515	15.3	9	C	7.50	6.8	5.2	3.070	0.051	1.400	4.65	0.501	1.41	7.5	10.30	NA
3	10	1725	17.4	9	C	7.56	6.0	3.3	2.870	0.048	1.350	NA	NA	1.69	7.0	9.60	NA
3	10	1905	19.1	9	C	7.55	5.6	3.3	2.820	0.051	1.350	3.79	0.533	1.79	7.1	10.60	NA
3	10	2115	21.3	9	C	7.57	5.5	3.3	2.740	0.051	1.400	NA	NA	1.69	7.0	11.00	NA
3	11	2315	47.3	9	C	7.60	5.6	3.0	2.510	0.051	1.420	3.85	0.484	1.13	7.0	11.40	NA
3	11	400	28.0	9	C	7.58	7.0	5.0	NA	NA	NA	NA	NA	1.03	6.0	11.20	NA
3	11	600	30.0	9	C	7.31	7.6	3.5	2.830	0.046	1.230	3.42	0.324	0.85	5.5	12.50	NA
3	11	750	31.8	9	C	7.36	8.1	4.8	2.850	0.049	1.280	NA	NA	0.85	5.5	10.00	NA
3	11	1040	34.7	9	C	7.53	6.8	3.3	3.040	0.048	1.430	4.53	0.409	0.75	6.5	10.40	NA
3	11	1238	36.6	9	C	7.58	7.0	3.6	3.100	0.048	1.430	4.48	0.427	0.94	6.0	10.10	NA
3	11	1500	39.0	9	C	7.58	7.2	2.8	2.920	0.046	1.440	NA	NA	1.60	6.5	10.20	NA
3	11	1700	41.0	9	C	7.56	5.6	2.7	2.570	0.046	1.230	4.34	0.449	1.60	6.0	11.30	NA
3	11	1855	42.9	9	C	7.55	5.7	2.4	2.660	0.046	1.420	NA	NA	1.60	6.0	11.50	NA
3	11	2048	44.8	9	C	7.56	6.0	4.6	2.250	0.029	0.942	3.75	0.425	1.60	5.9	11.40	NA
3	11	2310	47.2	9	C	7.53	7.2	5.6	2.580	0.046	1.480	NA	NA	0.64	5.9	11.60	NA
3	12	130	49.5	9	C	7.56	7.0	4.4	2.570	0.046	1.480	3.50	0.344	1.22	5.1	12.10	NA
3	12	245	50.8	9	C	7.56	7.2	4.6	2.540	0.046	1.470	NA	NA	1.17	5.0	12.00	NA
3	12	430	52.5	9	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.1	11.50	NA
3	12	545	53.8	9	C	7.55	6.5	4.4	2.690	0.046	1.470	NA	NA	1.50	4.9	11.50	NA
3	12	837	56.6	9	C	7.40	6.5	6.0	2.720	0.046	1.440	4.86	0.241	0.75	5.0	10.80	NA
3	12	1028	58.5	9	C	7.50	6.0	6.0	2.630	0.046	1.450	NA	NA	0.75	5.0	11.00	NA
3	12	1217	60.3	9	C	7.50	7.0	6.6	2.840	0.048	1.440	3.98	0.351	0.94	6.0	10.80	NA
3	12	1425	62.4	9	C	7.50	6.0	6.0	2.630	0.046	1.440	NA	NA	0.85	7.0	10.50	NA
3	12	1557	63.9	9	C	7.50	6.5	5.4	2.720	0.046	1.440	3.61	0.422	1.41	6.5	11.80	NA

946510335

BASELINE-RIVER SAMPLING
MARKET-STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB (NTU)	BOD (PPM)	NH3 (PPM)	NO2 (PPM)	NO3 (PPM)	TKN (PPM)	TP (PPM)	CHLOR (PPB)	TEMP (*C)	D.O. (PPM)	SAL (PPT)
3	12	1800	66.0	9	C	7.50	6.6	4.2	2.47[illegible]	[illegible].046	1.32[illegible]	NA	NA	1.03	6.5	11.50	NA
3	12	1955	67.9	9	C	7.60	7.0	4.0	1.860	0.032	0.989	4.02	0.399	1.36	6.5	11.30	NA
3	12	22[illegible]	70.[illegible]	9	C	7.50	7.5	4.6	2.22[illegible]	0.046	1.430	NA	NA	1.22	7.0	11.60	NA
3	13	100	73.0	9	C	7.60	7.0	4.8	2.110	0.400	1.280	2.90	0.344	1.03	6.2	11.20	NA
3	13	35[illegible]	75.[illegible]	9	C	7.50	7.0	4.4	2.209	0.051	1.620	NA	NA	1.13	5.5	11.60	NA
3	13	632	78.5	9	C	7.50	6.5	6.0	2.250	0.046	1.410	2.97	0.452	1.03	6.0	12.10	NA
3	13	953	81.9	9	C	7.60	7.8	3.9	2.310	0.048	1.440	3.45	0.338	0.94	6.5	10.60	NA
3	13	1249	84.7	9	C	7.60	7.5	3.9	2.360	0.051	1.430	NA	NA	1.03	7.0	10.40	NA
3	13	1547	87.8	9	C	7.60	7.4	3.4	2.360	0.048	1.420	3.14	0.385	1.03	7.5	10.70	NA
3	13	1830	90.5	9	C	7.70	6.8	3.8	2.220	0.048	1.420	NA	NA	1.03	7.5	11.00	NA
3	13	2205	94.1	9	C	7.60	7.0	3.9	2.170	0.065	1.860	2.72	0.354	1.88	7.5	12.00	NA
3	14	140	97.7	9	C	7.70	6.7	3.6	2.053	0.048	1.390	NA	NA	1.12	6.5	NA	NA
3	14	515	101.3	9	C	7.70	6.8	3.9	NA	NA	NA	NA	NA	1.22	5.5	12.00	NA
3	14	825	104.4	9	C	7.60	7.0	2.7	2.390	0.046	1.200	3.71	0.498	1.03	5.4	11.00	NA
3	14	1137	107.[illegible]	9	C	7.60	7.5	3.2	2.610	0.054	1.360	NA	NA	1.88	5.5	10.90	NA
3	14	1510	111.0	9	C	7.60	8.0	3.8	2.560	0.051	1.360	4.03	0.516	1.13	5.8	11.50	NA
3	14	1840	114.7	9	C	7.70	8.4	3.8	2.453	0.051	1.290	NA	NA	1.32	6.0	11.80	NA
3	14	2205	118.1	9	C	7.70	7.5	3.3	2.500	0.051	1.360	3.47	0.472	1.69	5.7	11.60	NA
3	15	146	121.7	9	C	7.70	6.8	3.2	2.570	0.051	1.430	NA	NA	1.22	4.5	12.00	NA
3	15	52[illegible]	125.3	9	C	7.70	6.5	2.6	2.580	0.059	1.410	4.67	0.614	2.26	3.0	12.25	NA
3	15	907	129.4	9	C	7.5[illegible]	6.3	4.2	2.783	0.054	1.460	4.45	0.525	2.35	4.0	11.70	NA
3	15	1240	132.7	9	C	7.60	7.0	7.8	2.890	0.054	1.430	NA	NA	2.07	5.5	11.70	NA
3	15	1545	135.8	9	C	7.50	7.2	4.2	2.890	0.057	1.450	3.77	0.474	1.79	6.0	11.90	NA
3	15	1915	139.4	9	C	7.60	7.8	4.8	2.750	.057	1.470	NA	NA	2.07	5.8	11.70	NA
3	15	2240	142.7	9	C	7.60	7.0	4.4	2.561	0.057	1.32[illegible]	4.17	0.455	1.88	5.5	12.30	NA
3	16	225	146.4	9	C	7.6[illegible]	7.2	6.4	2.393	[illegible].048	1.340	NA	NA	1.45	5.8	11.70	NA

946510336

BASELINE-RIVER SAMPLING
MARKET-STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	16	530	149.5	9	C	7.60	6.6	4.5	2.420	0.046	1.290	3.47	0.496	1.69	5.0	11.40	NA
3	16	835	152.6	9	C	7.50	6.0	3.8	2.500	0.051	1.330	NA	NA	NA	5.5	10.70	NA
3	16	1130	155.5	9	C	7.60	5.7	3.3	2.560	0.051	1.350	4.31	0.466	1.79	6.5	10.60	NA
3	16	1500	159.0	9	C	7.60	6.3	3.9	2.580	0.046	1.290	NA	NA	1.88	6.0	11.20	NA
3	16	1900	163.0	9	C	7.60	6.0	3.8	2.640	0.051	1.360	3.85	0.433	1.98	5.8	12.00	NA
3	16	2300	167.0	9	C	7.60	6.4	3.9	1.920	0.051	1.390	NA	NA	2.63	5.0	11.20	NA
3	17	225	170.3	9	C	7.60	6.7	4.1	1.890	0.051	1.360	3.67	0.443	1.79	4.5	12.00	NA
3	17	610	174.2	9	C	7.60	6.5	3.3	1.830	0.024	0.834	NA	NA	1.60	3.5	11.60	NA
3	17	915	177.3	9	C	7.60	5.5	2.8	NA	NA	NA	4.15	0.472	1.69	4.0	11.30	NA
3	17	1245	180.8	9	C	7.60	5.2	8.4	NA	NA	NA	NA	NA	1.60	3.1	11.20	NA
3	17	1545	183.8	9	C	7.60	5.6	2.7	NA	NA	NA	4.58	0.460	1.60	3.8	10.90	NA
3	17	1845	186.8	9	C	7.60	5.7	4.4	1.390	0.029	0.944	NA	NA	1.22	4.0	11.50	NA
3	17	2140	189.7	9	C	7.70	5.7	2.2	2.000	0.048	1.360	3.26	0.448	1.55	4.0	12.00	NA
3	18	115	193.3	9	C	7.70	5.6	3.3	2.720	0.043	1.160	NA	NA	1.13	3.0	NA	NA
3	18	415	196.3	9	C	7.70	5.8	2.8	2.720	0.051	1.380	3.79	0.450	0.75	2.5	12.20	NA
3	18	715	199.3	9	C	7.70	6.1	6.8	2.720	0.050	1.370	NA	NA	1.13	2.5	12.50	NA
3	18	1050	202.8	9	C	7.80	5.7	1.6	2.640	0.036	1.080	4.29	0.523	8.46	2.0	9.80	NA
3	18	1350	205.8	9	C	7.80	5.0	3.4	2.810	0.044	1.400	NA	NA	0.98	2.5	10.60	NA
3	19	1710	209.2	9	C	7.90	5.3	3.2	2.920	0.036	1.080	4.25	0.492	0.88	2.5	11.40	NA
3	19	2000	212.0	9	C	7.90	5.2	2.7	3.000	0.049	1.410	NA	NA	0.94	2.6	11.60	NA
3	19	2250	214.4	9	C	7.90	5.1	5.0	1.720	0.028	0.767	4.86	0.561	0.84	3.0	11.50	NA
3	19	230	218.5	9	C	7.80	5.6	3.3	3.220	0.049	1.380	NA	NA	0.91	3.9	12.90	NA
3	19	535	221.6	9	C	8.00	5.7	3.3	3.370	0.036	0.953	4.89	0.544	0.97	4.0	11.40	NA
3	19	835	225.4	9	C	7.80	5.4	4.2	3.670	0.052	1.420	5.21	0.494	0.65	4.0	10.10	NA
3	19	1225	228.4	9	C	7.80	5.5	4.2	3.240	0.044	1.450	NA	NA	0.98	4.0	11.80	NA
3	19	1525	231.4	9	C	7.80	5.1	3.9	3.620	0.052	1.440	5.42	0.443	0.84	4.0	10.40	NA

946510337

BASELINE-RIVER SAMPLING
MARKET-STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1830	234.5	9	C	7.80	5.2	4.5	3.330	0.049	1.350	NA	NA	0.68	3.7	12.00	NA
3	19	2120	237.3	9	C	7.70	5.5	5.6	3.240	0.049	1.340	5.14	0.397	0.70	3.5	11.50	NA
3	20	50	240.3	9	C	7.80	5.3	3.9	2.500	0.028	0.982	NA	NA	0.75	3.1	11.40	NA
3	20	425	244.4	9	C	7.90	5.1	3.4	3.280	0.044	1.220	4.62	0.378	0.73	3.1	11.50	NA
3	20	725	247.4	9	C	8.10	6.0	4.1	3.560	0.054	1.460	NA	NA	0.92	4.0	11.50	NA

946510338

BASELINE

LINCØLN AVENUE

3-10/3-20-81

1/2 DEPTH

946510339

BASELINE-RIVER SAMPLING
LINCOLN AVENUE - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	1015	10.3	10	C	7.56	5.5	3.8	2.860	0.046	1.370	4.99	0.648	0.75	7.0	10.70	NA
3	10	1245	12.8	10	C	7.62	5.6	8.6	2.650	0.046	1.370	NA	NA	0.85	7.5	11.00	NA
3	10	1450	14.8	10	C	7.66	6.3	3.1	2.630	0.046	1.370	4.27	0.609	0.64	8.0	11.20	NA
3	10	1700	17.0	10	C	7.66	6.1	3.1	1.940	0.033	1.020	NA	NA	1.13	7.0	13.00	NA
3	10	1830	18.5	10	C	7.59	5.9	3.4	2.400	0.041	1.240	NA	NA	2.16	7.0	9.00	NA
3	10	2030	20.5	10	C	7.66	6.5	3.3	2.750	0.046	1.330	3.42	0.462	1.79	6.8	10.20	NA
3	10	2235	22.6	10	C	7.61	6.6	3.6	2.860	0.046	1.370	NA	NA	1.32	6.5	12.00	NA
3	11	300	27.0	10	C	7.65	8.0	4.4	NA	NA	NA	3.72	0.536	0.67	7.1	11.90	NA
3	11	515	29.3	10	C	7.63	7.7	4.8	2.920	0.052	1.280	NA	NA	1.13	5.5	11.60	NA
3	11	721	31.3	10	C	7.36	8.3	4.6	2.850	0.049	1.280	4.60	0.583	1.69	6.5	10.00	NA
3	11	1010	34.2	10	C	7.58	5.8	3.6	2.660	0.047	1.300	3.94	0.522	1.32	6.0	11.30	NA
3	11	1208	36.1	10	C	7.59	5.5	3.9	2.400	0.049	1.420	NA	NA	1.41	6.5	11.40	NA
3	11	1435	38.6	10	C	7.61	5.3	3.6	2.570	0.049	1.410	4.18	0.479	1.41	7.0	11.20	NA
3	11	1635	40.6	10	C	7.60	6.5	3.8	2.480	0.047	1.340	NA	NA	1.13	5.5	11.50	NA
3	11	1815	42.3	10	C	7.59	6.1	4.4	2.530	0.055	1.480	4.73	0.587	1.41	5.5	12.50	NA
3	11	2020	44.3	10	C	7.58	6.0	3.9	2.250	0.039	1.030	3.72	0.410	1.50	5.6	11.60	NA
3	11	2235	46.6	10	C	7.57	6.9	4.1	2.810	0.049	1.400	NA	NA	1.32	5.7	12.00	NA
3	12	100	49.0	10	C	7.60	6.5	4.1	2.810	0.049	1.390	4.58	0.519	1.32	6.0	12.90	NA
3	12	230	50.5	10	C	7.63	6.9	4.4	2.810	0.052	1.380	NA	NA	1.22	5.0	12.50	NA
3	12	400	52.0	10	C	7.62	7.3	4.5	2.810	0.052	1.380	NA	NA	1.22	5.5	12.50	NA
3	12	536	53.5	10	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.9	12.20	NA
3	12	645	54.8	10	C	7.61	7.2	4.6	2.690	0.052	1.370	3.98	0.531	1.41	5.0	12.00	NA
3	12	1005	58.1	10	C	7.50	7.0	4.4	2.520	0.052	1.370	3.39	0.400	1.41	5.0	12.20	NA
3	12	1157	59.9	10	C	7.59	7.8	4.4	2.470	0.049	1.370	NA	NA	1.41	5.8	12.10	NA
3	12	1400	62.0	10	C	7.60	7.5	4.0	2.320	0.049	1.390	3.73	0.473	1.22	6.5	12.20	NA
3	12	1535	63.6	10	C	7.60	7.0	4.2	2.180	0.049	1.390	NA	NA	1.32	7.0	11.90	NA

946510340

BASELINE-RIVER SAMPLING
LINCOLN AVENUE - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	12	1735	65.6	10	C	7.60	7.5	4.6	2.280	0.052	1.450	3.56	0.436	1.22	6.5	11.60	NA
3	12	1930	67.5	10	C	7.60	7.0	3.6	2.330	0.052	1.440	NA	NA	1.13	5.8	12.20	NA
3	12	2135	69.6	10	C	7.50	7.2	4.0	2.310	0.049	1.320	3.57	0.460	1.03	5.9	11.70	NA
3	12	2340	71.7	10	C	7.60	7.0	4.0	2.390	0.049	1.390	NA	NA	1.22	6.0	11.60	NA
3	13	220	74.3	10	C	7.50	8.2	4.6	2.050	0.041	1.080	3.00	0.472	0.94	5.8	11.60	NA
3	13	500	77.0	10	C	7.60	7.5	4.6	2.560	0.052	1.340	NA	NA	1.32	6.0	12.80	NA
3	13	800	80.0	10	C	7.50	6.8	4.4	2.390	0.041	1.310	NA	NA	1.13	5.9	11.50	NA
3	13	1125	83.4	10	C	7.50	7.3	3.9	2.280	0.049	1.340	3.45	0.485	1.03	7.0	11.70	NA
3	13	1417	86.3	10	C	7.70	6.8	3.3	2.250	0.052	1.340	NA	NA	1.03	7.5	12.20	NA
3	13	1715	89.3	10	C	7.70	6.8	3.3	2.280	0.052	1.380	3.30	0.531	0.94	7.0	12.00	NA
3	13	2015	92.3	10	C	7.70	7.3	3.9	2.460	0.055	1.360	NA	NA	1.12	7.0	11.60	NA
3	13	2345	95.8	10	C	7.70	7.5	4.5	2.670	0.058	1.370	3.63	0.557	1.12	7.0	11.40	NA
3	14	650	102.8	10	C	7.80	7.6	3.6	2.610	0.051	1.340	3.51	0.427	0.94	5.0	12.00	NA
3	14	310	99.2	10	C	7.70	7.8	4.5	2.780	0.060	1.370	NA	NA	1.22	6.3	11.50	NA
3	14	945	105.8	10	C	7.60	7.5	3.3	2.580	0.055	1.340	3.85	0.531	0.66	5.4	12.40	NA
3	14	1328	109.5	10	C	7.70	7.0	3.2	2.580	0.060	1.510	NA	NA	1.50	6.0	12.80	NA
3	14	1655	112.9	10	C	7.70	7.5	3.0	2.500	0.049	1.240	4.12	0.560	1.41	6.0	12.20	NA
3	14	2020	116.3	10	C	7.70	8.0	4.6	2.840	0.049	1.340	NA	NA	1.79	4.9	12.60	NA
3	14	2345	119.8	10	C	7.70	8.2	3.3	2.890	0.060	1.360	3.75	0.562	1.60	5.0	11.60	NA
3	15	320	123.3	10	C	7.70	8.5	3.8	NA	NA	NA	NA	NA	1.60	4.5	12.50	NA
3	15	655	126.9	10	C	7.70	8.0	3.9	NA	NA	NA	NA	NA	1.50	3.5	12.75	NA
3	15	1110	131.2	10	C	7.60	7.2	6.6	2.610	0.055	1.310	4.06	0.488	1.88	5.5	13.60	NA
3	15	1425	134.4	10	C	7.70	6.8	4.2	2.530	0.052	1.300	NA	NA	1.79	6.3	13.40	NA
3	15	1730	137.5	10	C	7.70	7.3	5.7	2.530	0.055	1.320	3.77	0.507	2.63	5.8	12.10	NA
3	15	2100	141.0	10	C	7.60	7.0	3.0	2.560	0.058	1.350	NA	NA	1.41	5.3	11.00	NA
3	16	45	144.8	10	C	7.60	7.4	5.0	2.720	0.055	1.350	3.63	0.437	1.88	6.0	12.00	NA

94510341

BASELINE-RIVER SAMPLING
LINCOLN AVENUE - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	355	147.9	10	C	7.60	7.0	3.3	2.780	0.055	1.340	NA	NA	1.69	5.8	11.90	NA
3	16	635	150.6	10	C	7.60	7.5	9.0	2.810	0.055	1.310	3.95	0.493	2.54	5.9	11.60	NA
3	16	1000	154.0	10	C	7.60	6.4	3.8	2.700	0.055	1.290	NA	NA	1.98	7.0	11.50	NA
3	16	1315	157.3	10	C	7.60	6.2	3.4	2.500	0.055	1.340	3.89	0.453	1.88	6.0	12.10	NA
3	16	1715	161.3	10	C	7.70	6.3	3.6	2.470	0.055	1.360	NA	NA	2.63	5.9	12.40	NA
3	16	2040	164.7	10	C	7.60	6.2	3.8	2.640	0.056	1.390	3.85	0.432	1.60	4.8	11.40	NA
3	17	50	168.8	10	C	7.60	7.0	5.1	2.810	0.053	1.370	NA	NA	1.32	3.5	10.10	NA
3	17	420	172.3	10	C	7.70	6.8	3.3	2.920	0.059	1.400	4.00	0.445	1.50	3.0	12.50	NA
3	17	740	175.7	10	C	7.70	6.2	3.8	2.920	0.056	1.370	NA	NA	2.16	3.0	12.00	NA
3	17	1055	178.9	10	C	7.60	6.2	3.0	NA	NA	NA	4.27	0.470	1.32	3.8	13.00	NA
3	17	1425	182.4	10	C	7.70	5.4	7.5	NA	NA	NA	NA	NA	0.85	4.1	13.20	NA
3	17	1720	185.3	10	C	7.80	5.5	3.3	2.140	0.037	1.160	NA	NA	1.03	4.0	13.20	NA
3	17	2015	188.3	10	C	7.90	5.4	4.4	1.750	0.026	0.875	3.57	0.403	0.66	3.4	12.70	NA
3	17	2330	191.5	10	C	7.90	5.6	3.2	2.250	0.031	1.040	4.41	0.438	0.75	3.5	12.40	NA
3	18	240	194.7	10	C	7.80	5.4	6.9	3.000	0.053	1.380	NA	NA	0.85	1.5	12.00	NA
3	18	540	197.7	10	C	7.70	5.8	3.0	3.170	0.053	1.390	4.29	0.445	0.94	1.8	12.80	NA
3	18	915	201.3	10	C	7.90	5.8	4.2	3.420	0.053	1.410	5.13	0.493	1.15	2.0	12.20	NA
3	18	1215	204.3	10	C	7.90	6.0	3.6	3.720	0.056	1.430	NA	NA	1.08	3.5	12.80	NA
3	18	1515	207.3	10	C	8.10	6.2	2.7	3.800	0.053	1.420	5.71	0.549	1.01	3.8	13.10	NA
3	18	1835	210.6	10	C	8.10	6.0	2.8	3.670	0.053	1.420	NA	NA	1.04	3.0	13.60	NA
3	18	2125	213.4	10	C	8.00	6.4	3.2	3.470	0.053	1.370	5.47	0.506	1.50	3.0	12.60	NA
3	19	100	217.0	10	C	7.80	5.8	3.6	2.970	0.053	1.330	NA	NA	0.98	2.0	12.50	NA
3	19	430	220.5	10	C	8.00	5.7	3.2	3.530	0.053	1.390	5.00	0.469	0.94	3.0	12.00	NA
3	19	730	223.5	10	C	8.00	7.0	3.7	3.310	0.053	1.400	NA	NA	0.91	3.0	12.00	NA
3	19	1050	226.8	10	C	8.20	5.5	3.4	4.250	0.053	1.440	5.88	0.461	0.97	4.0	12.30	NA
3	19	1350	229.8	10	C	8.60	5.7	3.0	5.170	0.053	1.490	NA	NA	1.58	5.0	12.80	NA

94651034 2

BASELINE-RIVER SAMPLING
LINCOLN AVENUE - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1700	233.0	10	C	7.80	5.5	4.6	2.240	0.034	1.120	4.30	0.441	1.13	5.0	12.70	NA
3	19	1950	235.[illegible]	10	C	7.80	5.7	4.6	3.040	0.059	1.450	NA	NA	1.05	4.0	12.00	NA
3	19	2255	238.[illegible]	10	C	7.80	6.0	4.3	2.870	0.056	1.350	4.68	0.419	0.97	3.0	12.10	NA
3	20	210	242.2	10	C	7.70	6.2	4.2	1.920	0.031	0.893	NA	NA	1.13	2.5	12.00	NA
3	20	515	245.3	10	C	7.70	6.0	3.4	3.140	0.062	1.420	4.54	0.458	0.84	1.9	12.50	NA

946510343

BASELINE

MARKET

ISLAND

3-10/3-20-81

1/2 DEPTH

946510344

BASELINE-RIVER-SAMPLING
MARKET ISLAND - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	1000	10.0	11	C	7.64	6.5	3.6	2.760	0.046	1.280	4.54	0.504	1.98	6.5	11.50	NA
3	10	1220	12.3	11	C	7.67	6.2	3.3	6.330	0.046	1.300	NA	NA	1.41	7.0	12.40	NA
3	10	1430	14.5	11	C	7.66	6.8	3.8	2.630	0.044	1.290	3.62	0.363	1.50	7.0	12.20	NA
3	10	1640	16.7	11	C	7.66	6.9	3.4	2.630	0.046	1.330	NA	NA	1.69	7.0	9.00	NA
3	10	1817	18.3	11	C	7.62	6.8	4.7	2.870	0.046	1.300	3.87	0.452	1.60	7.0	12.00	NA
3	10	2010	20.2	11	C	7.67	6.4	4.1	2.490	0.038	1.100	4.59	0.524	1.22	7.0	11.20	NA
3	10	2220	22.3	11	C	7.68	7.4	3.9	3.130	0.046	1.230	NA	NA	1.32	7.0	12.00	NA
3	11	155	25.9	11	C	7.68	7.5	3.8	2.630	0.044	1.290	4.53	0.534	0.75	6.0	14.00	NA
3	11	450	28.8	11	C	7.69	7.7	3.9	2.870	0.046	1.190	NA	NA	1.13	5.5	13.40	NA
3	11	730	31.0	11	C	7.34	8.2	3.8	2.890	0.052	1.230	4.29	0.499	1.41	6.0	10.50	NA
3	11	950	33.9	11	C	7.63	6.7	3.6	2.470	0.043	1.360	5.23	0.365	1.41	6.0	12.20	NA
3	11	1149	35.8	11	C	7.66	7.3	3.0	2.700	0.043	1.260	NA	NA	1.50	6.0	12.20	NA
3	11	1410	38.2	11	C	7.65	7.2	2.8	2.470	0.040	1.280	3.83	0.446	1.50	6.5	12.20	NA
3	11	1610	40.2	11	C	7.66	7.0	3.3	2.810	0.040	1.300	NA	NA	1.41	6.0	12.00	NA
3	11	1800	42.1	11	C	7.64	6.8	4.2	2.800	0.045	1.280	NA	NA	1.60	5.8	12.80	NA
3	11	2000	44.4	11	C	7.64	7.1	4.2	2.830	0.045	1.300	3.26	0.559	1.78	5.8	12.60	NA
3	11	2210	46.2	11	C	7.69	6.5	4.5	2.800	0.056	1.510	NA	NA	1.60	5.8	13.20	NA
3	12	45	48.8	11	C	7.67	7.5	5.0	2.930	0.048	1.350	2.76	0.550	1.64	7.5	10.50	NA
3	12	215	50.3	11	C	7.65	6.8	4.5	2.870	0.045	1.280	NA	NA	1.50	6.0	10.00	NA
3	12	345	51.8	11	C	7.65	7.0	4.2	2.780	0.045	1.260	4.03	0.634	1.69	5.5	12.20	NA
3	12	510	53.2	11	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.0	13.10	NA
3	12	630	54.5	11	C	7.67	7.7	4.5	2.550	0.045	1.340	3.33	0.563	1.41	6.0	13.00	NA
3	12	942	57.7	11	C	7.60	7.5	4.8	2.470	0.040	1.240	NA	NA	0.94	5.0	13.20	NA
3	12	1135	59.6	11	C	7.60	7.0	NA	2.320	0.045	1.360	3.08	0.536	1.32	5.4	12.90	NA
3	12	1342	61.7	11	C	7.60	8.4	3.8	2.240	0.045	1.340	NA	NA	1.13	5.8	12.80	NA
3	12	1515	63.3	11	C	7.60	7.8	3.4	2.350	0.045	1.300	3.33	0.546	1.22	6.0	12.60	NA

946510345

BASELINE-RIVER-SAMPLING
MARKET ISLAND - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	12	1715	65.3	11	C	7.60	7.4	4.0	1.940	0.033	0.997	3.05	0.513	1.03	6.2	12.00	NA
3	12	1905	67.1	11	C	7.60	7.8	3.6	2.290	0.040	1.170	NA	NA	1.13	6.4	12.20	NA
3	12	2110	69.2	11	C	7.60	7.5	3.6	2.170	0.045	1.120	3.43	0.667	1.41	6.2	13.20	NA
3	12	2315	71.3	11	C	7.60	8.0	3.8	NA	NA	NA	NA	NA	1.03	6.5	12.00	NA
3	13	200	74.0	11	C	7.60	7.5	4.0	2.530	0.045	1.300	3.36	0.635	1.13	5.8	12.80	NA
3	13	445	76.8	11	C	7.60	7.8	4.4	2.550	0.045	1.260	NA	NA	1.50	5.5	12.50	NA
3	13	745	79.8	11	C	7.60	7.0	4.4	2.350	0.045	1.280	3.63	0.602	1.50	6.0	12.90	NA
3	13	1108	83.1	11	C	7.70	7.2	3.3	2.230	0.048	1.340	NA	NA	0.94	6.5	12.20	NA
3	13	1355	85.9	11	C	7.70	7.0	3.4	2.350	0.045	1.260	3.43	0.565	1.03	6.8	12.30	NA
3	13	1655	88.9	11	C	7.70	7.5	3.4	2.380	0.048	1.280	NA	NA	1.12	7.0	12.70	NA
3	13	1950	91.8	11	C	7.70	7.8	5.4	2.320	0.043	1.110	4.01	0.667	1.03	7.5	12.60	NA
3	13	2320	95.3	11	C	7.70	8.0	5.2	2.800	0.053	1.320	NA	NA	1.03	7.0	12.70	NA
3	14	240	98.7	11	C	7.70	8.0	4.6	2.730	0.048	1.250	3.82	0.652	0.94	6.0	13.00	NA
3	14	625	102.4	11	C	7.80	7.5	3.8	2.760	0.048	1.290	NA	NA	1.32	5.0	13.75	NA
3	14	928	105.5	11	C	7.70	8.5	3.2	2.700	0.048	1.290	3.88	0.614	1.32	5.1	13.40	NA
3	14	1305	109.1	11	C	7.70	8.0	3.6	2.760	0.045	1.320	NA	NA	1.50	5.5	13.60	NA
3	14	1630	112.5	11	C	7.80	9.5	3.9	2.290	0.055	1.360	3.49	0.646	1.64	5.9	13.00	NA
3	14	1955	115.9	11	C	7.80	9.0	4.1	2.940	0.055	1.320	NA	NA	1.79	5.4	13.70	NA
3	14	2320	119.3	11	C	7.80	8.8	3.8	2.640	0.040	0.878	4.70	0.678	1.60	5.3	13.00	NA
3	15	300	123.0	11	C	7.70	9.0	4.8	3.090	0.060	1.350	NA	NA	1.50	4.0	13.75	NA
3	15	625	126.4	11	C	7.80	8.5	4.1	2.640	0.052	1.220	3.84	0.579	1.60	3.5	14.00	NA
3	15	1040	130.7	11	C	7.60	7.3	4.4	2.700	0.047	1.190	4.28	0.569	1.98	5.0	14.20	NA
3	15	1400	134.1	11	C	7.70	7.5	6.6	2.760	0.047	1.210	NA	NA	1.69	5.5	14.00	NA
3	15	1705	137.1	11	C	7.70	7.6	3.8	1.560	0.052	1.310	4.13	0.537	1.98	5.8	12.80	NA
3	15	2035	140.6	11	C	7.70	8.0	6.6	1.940	0.050	1.260	NA	NA	1.79	6.0	12.80	NA
3	15	2355	143.9	11	C	7.70	7.5	3.9	2.640	0.047	1.190	3.29	0.467	1.79	6.0	13.00	NA

946510346

BASELINE-RIVER-SAMPLING
MARKET ISLAND - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	16	335	147.6	11	C	7.70	7.5	7.1	2.880	0.050	1.210	NA	NA	1.88	5.8	12.80	NA
3	16	620	150.3	11	C	7.70	7.3	4.4	2.410	0.050	1.230	5.94	0.564	2.16	5.3	12.90	NA
3	16	940	153.7	11	C	7.70	7.5	4.5	2.640	0.050	1.250	NA	NA	1.64	6.0	12.30	NA
3	16	1245	156.8	11	C	7.70	6.7	10.8	2.500	0.050	1.280	3.98	0.460	1.98	6.0	12.60	NA
3	16	1650	160.8	11	C	7.70	7.0	5.0	2.410	0.050	1.270	NA	NA	1.41	5.5	13.10	NA
3	16	2015	164.3	11	C	7.70	7.0	8.1	2.820	0.047	1.210	4.32	0.613	1.50	5.0	13.20	NA
3	17	30	168.5	11	C	7.70	6.5	5.3	2.940	0.050	1.260	NA	NA	1.22	4.0	13.00	NA
3	17	400	172.2	11	C	7.70	6.3	11.7	2.970	0.050	1.260	4.68	0.549	1.69	3.0	14.00	NA
3	17	720	175.3	11	C	7.70	6.5	3.4	2.940	0.050	1.210	NA	NA	1.50	3.1	13.60	NA
3	17	1030	178.5	11	C	7.60	5.8	5.0	NA	NA	NA	4.26	0.492	1.32	3.1	13.80	NA
3	17	1400	182.0	11	C	7.70	5.4	3.8	NA	NA	NA	NA	NA	0.85	3.4	13.60	NA
3	17	1700	185.0	11	C	7.70	5.8	3.9	1.530	0.012	0.413	3.84	0.461	0.75	3.5	13.40	NA
3	17	1955	187.9	11	C	7.70	6.0	3.3	2.410	0.034	1.010	NA	NA	0.85	3.2	13.20	NA
3	17	2310	191.2	11	C	7.70	5.7	3.0	2.410	0.042	1.190	3.37	0.473	0.99	3.0	13.80	NA
3	18	220	194.3	11	C	7.70	6.2	2.7	2.880	0.047	1.230	NA	NA	1.32	3.0	13.30	NA
3	18	540	197.7	11	C	7.70	6.4	3.6	3.170	0.047	1.210	4.68	0.566	1.41	2.0	14.10	NA
3	18	850	200.9	11	C	7.80	6.5	4.1	3.230	0.050	1.280	5.37	0.631	1.22	2.5	13.50	NA
3	18	1150	203.8	11	C	7.80	6.7	4.6	3.140	0.050	1.220	NA	NA	1.03	2.5	13.70	NA
3	18	1450	206.8	11	C	7.90	6.0	3.9	3.050	0.050	1.250	4.50	0.526	0.88	3.0	13.50	NA
3	18	1815	210.3	11	C	7.80	6.5	4.8	2.940	0.045	1.200	NA	NA	0.91	3.0	13.40	NA
3	18	2135	213.1	11	C	7.90	7.5	5.6	2.850	0.045	1.180	4.29	0.550	1.69	3.0	13.40	NA
3	19	40	216.7	11	C	7.90	6.3	5.4	2.820	0.047	1.260	NA	NA	1.11	3.0	13.20	NA
3	19	345	219.8	11	C	7.90	6.0	4.5	2.760	0.050	1.330	4.34	0.537	0.98	3.9	12.90	NA
3	19	645	222.9	11	C	7.90	6.6	3.3	2.980	0.047	1.290	NA	NA	1.04	4.1	12.40	NA
3	19	1030	226.5	11	C	7.80	6.0	3.8	3.000	0.050	1.340	4.87	0.497	0.81	4.0	13.40	NA
3	19	1330	229.5	11	C	7.80	6.2	5.2	3.000	0.050	1.300	NA	NA	1.02	3.5	13.40	NA

94510347

BASELINE-RIVER-SAMPLING
MARKET ISLAND - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	19	1640	232.7	11	C	7.80	6.2	4.6	3.160	0.045	1.100	4.62	0.478	1.13	3.5	13.30	NA
3	19	1930	235.5	11	C	7.80	6.3	4.1	3.240	0.055	1.280	NA	NA	0.65	3.5	13.40	NA
3	19	2230	238.5	11	C	7.90	6.2	3.8	1.950	0.029	0.712	3.91	0.492	0.59	3.0	13.50	NA
3	20	155	241.9	11	C	7.80	6.0	3.8	3.450	0.055	1.320	NA	NA	0.81	3.1	12.90	NA
3	20	500	245.0	11	C	7.90	6.3	3.3	3.380	0.055	1.340	4.28	0.548	0.94	3.1	13.00	NA
3	20	835	248.1	11	C	7.90	6.0	5.6	3.440	0.055	1.340	NA	NA	0.75	3.0	13.10	NA

946510348

BASELINE

MCBRIDE

AVENUE

3-10/3-20-81

1/2 DEPTH

946510349

BASELINE-RIVER SAMPLING
MC-BRIDE AVERAGE - LEVEL C - 1X2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	1[illegible]	915	9.3	12	C	7.32	5.9	4.4	2.780	0.044	1.270	NA	NA	2.07	6.5	8.20	NA
3	10	1155	11.[illegible]	12	C	7.33	6.2	3.8	2.480	0.044	1.310	4.24	0.531	1.98	8.0	7.80	NA
3	10	1415	14.3	12	C	7.33	5.6	3.3	2.700	0.044	1.270	NA	NA	1.88	8.0	9.50	NA
3	10	1635	16.1	12	C	7.32	7.0	3.9	2.800	0.044	1.270	4.26	0.434	1.88	7.5	9.70	NA
3	10	1805	18.1	12	C	7.34	7.2	4.2	3.000	0.046	1.280	NA	NA	1.22	7.0	9.40	NA
3	10	1948	19.8	12	C	7.34	6.7	3.6	3.140	0.046	1.280	4.81	0.550	1.41	7.1	8.90	NA
3	10	2200	22.0	12	C	7.35	8.2	4.1	3.190	0.049	1.280	NA	NA	1.41	7.2	8.20	NA
3	11	12	24.2	12	C	7.34	7.3	4.2	3.140	0.046	1.270	NA	0.600	2.07	6.2	9.40	NA
3	11	430	28.5	12	C	7.32	8.8	4.8	2.870	0.003	0.990	4.66	0.614	1.13	5.5	10.20	NA
3	11	640	30.7	12	C	7.34	7.8	4.2	2.860	0.049	1.310	NA	NA	3.01	6.0	10.50	NA
3	11	930	33.5	12	C	7.26	6.5	3.3	2.810	0.043	1.340	4.24	0.408	1.50	6.5	9.60	NA
3	11	1128	35.5	12	C	7.28	6.9	2.7	2.810	0.043	1.330	NA	NA	1.60	6.5	9.60	NA
3	11	1349	37.8	12	C	7.30	8.0	2.6	2.640	0.043	1.310	3.98	0.427	1.32	7.0	9.90	NA
3	11	1551	39.8	12	C	7.31	7.3	3.0	2.870	0.043	1.310	NA	NA	1.88	7.0	8.60	NA
3	11	1743	41.7	12	C	7.31	7.0	3.8	2.900	0.028	0.849	3.64	0.484	1.60	5.8	10.40	NA
3	11	1940	43.7	12	C	7.33	7.2	3.3	2.870	0.043	1.310	NA	NA	1.41	6.0	10.00	NA
3	11	2135	45.6	12	C	7.35	8.0	5.0	2.850	0.048	1.400	4.26	0.484	1.13	7.7	10.70	NA
3	12	3[illegible]	48.5	12	C	7.36	7.7	4.6	2.930	0.048	1.360	NA	NA	1.78	7.0	10.10	NA
3	12	200	50.0	12	C	7.15	8.0	4.5	2.930	0.048	1.360	3.39	0.521	1.50	5.0	10.50	NA
3	12	33[illegible]	51.5	12	C	7.31	7.3	3.9	2.780	0.045	1.280	NA	NA	1.03	6.0	10.10	NA
3	12	5[illegible]	53.	12	C	7.36	7.0	3.6	2.670	0.038	1.150	3.66	0.457	1.22	5.0	10.10	NA
3	12	615	54.3	12	C	7.62	4.5	NA	2.640	0.043	1.300	NA	NA	NA	4.9	10.10	NA
3	12	925	57.4	12	C	7.20	8.0	4.2	2.520	0.043	1.340	NA	NA	1.22	5.0	9.80	NA
3	12	1119	59.3	12	C	7.36	7.5	4.0	2.470	0.048	1.490	NA	NA	1.03	5.5	9.90	NA
3	12	1328	61.5	12	C	7.38	7.5	3.8	2.490	0.043	1.320	3.37	0.425	1.36	6.0	9.70	NA
3	12	1502	63.	12	C	7.38	8.0	3.8	2.500	0.043	1.320	NA	NA	1.50	6.0	10.00	NA

946510350

BASELINE-RIVER SAMPLING
MC-BRIDE AVENUE - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	12	1700	95.3	12	C	7.30	8.2	3.8	2.450	0.038	1.120	4.01	0.454	0.94	5.4	9.80	NA
3	12	1840	96.7	12	C	7.30	8.0	3.4	2.370	0.043	1.240	NA	NA	0.94	8.8	10.00	NA
3	12	2045	98.9	12	C	7.35	7.5	3.4	2.940	0.043	1.200	3.12	0.457	0.94	7.5	10.00	NA
3	12	2250	70.8	12	C	7.30	7.7	4.2	2.610	0.043	1.230	NA	NA	1.22	6.8	9.80	NA
3	13	145	73.8	12	C	7.30	7.5	5.2	2.150	0.033	0.922	3.23	0.539	1.41	5.7	9.60	NA
3	13	430	76.5	12	C	7.30	7.0	4.2	2.540	0.043	1.260	NA	NA	1.13	6.0	10.10	NA
3	13	710	79.2	12	C	7.30	7.0	4.6	2.450	0.043	1.260	NA	NA	1.22	6.0	9.50	NA
3	13	1035	82.6	12	C	7.30	7.5	3.8	2.440	0.043	1.270	3.82	0.482	0.66	6.0	9.50	NA
3	13	1337	85.6	12	C	7.40	7.2	3.6	2.430	0.048	1.400	NA	NA	1.12	7.0	9.50	NA
3	13	1635	88.6	12	C	7.50	7.6	4.1	2.650	0.045	1.180	4.30	0.687	1.12	7.0	9.80	NA
3	13	1925	91.4	12	C	7.50	7.5	4.2	2.680	0.059	1.480	NA	NA	0.94	NA	9.80	NA
3	13	2255	94.9	12	C	7.50	8.5	4.8	2.570	0.054	1.320	4.38	0.564	1.22	7.0	7.40	NA
3	14	225	98.4	12	C	7.40	7.8	4.1	2.610	0.048	1.250	NA	NA	0.94	6.3	10.25	NA
3	14	600	102.0	12	C	7.50	7.3	4.2	2.560	0.051	1.350	3.59	0.422	1.31	5.3	10.75	NA
3	14	915	105.3	12	C	7.40	7.2	2.2	2.530	0.043	1.250	4.17	0.571	1.32	5.5	10.30	NA
3	14	1249	108.8	12	C	7.40	8.0	3.2	2.730	0.048	1.310	NA	NA	1.32	5.5	9.60	NA
3	14	1547	111.8	12	C	7.50	8.7	4.1	2.840	0.048	1.220	5.58	0.591	1.79	5.5	10.60	NA
3	14	1930	115.5	12	C	7.50	9.0	4.1	2.280	0.028	0.900	NA	NA	2.07	6.0	10.70	NA
3	14	2255	118.9	12	C	7.50	8.8	3.9	2.880	0.051	1.240	4.01	0.478	1.69	5.2	10.60	NA
3	15	235	122.6	12	C	7.50	8.4	3.6	3.190	0.051	1.260	NA	NA	2.73	4.0	10.75	NA
3	15	615	126.1	12	C	7.50	8.5	3.4	2.520	0.048	1.260	4.08	0.522	0.66	4.0	10.75	NA
3	15	1020	130.3	12	C	7.30	7.8	5.7	2.530	0.045	1.220	2.84	0.360	2.35	5.0	10.70	NA
3	15	1335	133.6	12	C	7.40	8.2	3.9	2.620	0.048	1.210	NA	NA	1.84	6.0	10.50	NA
3	15	1640	136.7	12	C	7.40	7.6	5.4	2.280	0.043	1.210	3.56	0.381	1.50	6.0	10.10	NA
3	15	2010	140.2	12	C	7.40	7.7	3.8	2.530	0.043	1.170	NA	NA	1.60	6.0	11.00	NA
3	15	2330	143.5	12	C	7.40	8.0	8.4	2.170	0.045	1.200	3.92	0.370	2.45	6.5	10.50	NA

94510351

BASELINE-RIVER SAMPLING
MC-BRIDE AVENUE - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	16	315	147.3	12	C	7.40	7.8	4.6	2.200	0.048	1.200	NA	NA	2.26	5.5	10.20	NA
3	16	630	150.	12	C	7.40	7.2	4.5	2.540	0.048	1.220	3.57	0.425	1.60	5.2	9.50	NA
3	16	930	153.5	12	C	7.30	7.0	8.0	2.480	0.038	1.070	NA	NA	1.41	6.0	9.80	NA
3	16	1220	156.3	12	C	7.30	6.4	5.0	2.570	0.045	1.220	4.84	0.485	1.88	6.0	9.80	NA
3	16	1625	160.4	12	C	7.40	7.0	10.6	2.790	0.045	1.140	NA	NA	1.88	8.0	10.40	NA
3	16	1950	163.8	12	C	7.40	7.2	3.9	2.760	0.047	1.190	4.40	0.544	1.98	5.7	11.00	NA
3	16	2350	167.8	12	C	7.50	7.0	7.5	2.930	0.045	1.190	NA	NA	1.13	5.0	10.50	NA
3	17	310	171.2	12	C	7.50	6.8	3.9	2.680	0.050	1.230	4.80	0.592	1.50	4.0	10.20	NA
3	17	700	175..	12	C	7.40	6.4	6.4	2.560	0.045	1.180	NA	NA	1.50	3.1	10.50	NA
3	17	1005	178.1	12	C	7.30	6.0	2.4	NA	NA	NA	4.21	0.478	1.13	3.0	10.20	NA
3	17	1335	181.6	12	C	7.40	5.6	2.7	NA	NA	NA	NA	NA	1.32	3.5	10.20	NA
3	17	1640	184.7	12	C	7.40	5.8	2.4	2.600	0.035	1.010	3.94	0.457	0.67	3.5	10.30	NA
3	17	1935	187.6	12	C	7.40	6.0	3.0	2.490	0.012	0.533	NA	NA	0.66	3.8	10.80	NA
3	17	2245	190.9	12	C	7.40	6.2	2.7	1.660	0.022	0.895	4.31	0.483	1.22	3.8	11.20	NA
3	18	210	194..	12	C	7.50	6.7	3.4	2.860	0.043	1.140	NA	NA	0.84	3.0	10.50	NA
3	18	500	197.0	12	C	7.50	6.4	3.4	2.850	0.030	0.722	4.78	0.558	1.01	2.1	10.50	NA
3	18	830	200.5	12	C	7.60	6.5	4.8	3.140	0.048	1.220	5.05	0.625	1.32	2.4	10.20	NA
3	18	1130	203.5	12	C	7.70	6.4	4.6	2.900	0.045	1.240	NA	NA	0.75	2.5	10.80	NA
3	18	1430	206.5	12	C	7.60	6.1	4.5	3.030	0.045	1.180	4.22	0.468	0.91	3.0	10.80	NA
3	18	1755	209.9	12	C	7.70	6.6	3.4	2.690	0.040	1.090	NA	NA	1.03	3.0	12.00	NA
3	18	2045	212.	12	C	7.70	6.4	3.9	2.590	0.043	1.160	3.87	0.492	0.67	3.5	12.20	NA
3	18	2345	215.8	12	C	7.70	6.2	3.8	2.370	0.043	1.160	NA	NA	1.11	4.0	12.50	NA
3	19	320	218.3	12	C	7.80	7.2	3.9	2.860	0.045	1.240	4.18	0.452	0.67	3.9	11.90	NA
3	19	620	221.3	12	C	7.60	6.3	4.2	2.930	0.045	1.260	NA	NA	0.98	4.0	12.20	NA
3	19	1005	225.1	12	C	7.60	6.1	11.7	3.240	0.048	1.270	4.26	0.462	0.80	3.5	11.10	NA
3	19	1305	228.1	12	C	7.60	6.0	5.2	3.010	0.028	0.992	NA	NA	1.05	3.5	11.20	NA

946510352

BASELINE-RIVER SAMPLING
MC-BRIDE AVENUE - LEVEL C - INT DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	COD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	19	1630	232.5	12	C	7.60	6.6	4.5	3.040	0.053	1.270	5.39	0.618	0.73	3.5	11.20	NA
3	19	1910	235.2	12	C	7.60	6.4	3.9	3.010	0.053	1.250	NA	NA	0.89	3.8	11.20	NA
3	19	2210	238.2	12	C	7.60	6.3	4.1	3.070	0.043	1.030	5.00	0.634	0.57	4.0	11.00	NA
3	20	140	241.7	12	C	7.70	6.3	3.4	3.530	0.038	0.925	NA	NA	1.05	4.0	11.10	NA
3	20	455	244.4	12	C	7.70	6.7	3.4	3.300	0.050	1.290	5.33	0.565	0.70	3.9	11.50	NA
3	20	755	247.3	12	C	7.70	6.4	4.3	3.520	0.050	1.320	NA	NA	1.08	3.1	10.30	NA

946510353

BASELINE

HILLARY

STREET

3-10/3-20-81

1/2 DEPTH

946510354

BASELINE HIGH RIVER SAMPLING
HILARY STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
3	10	845	8.8	13	C	7.26	5.2	3.2	2.760	0.046	1.330	6.36	0.560	2.12	6.0	9.80	NA
3	10	1115	11.3	13	C	7.31	6.6	3.9	2.890	0.046	1.350	NA	NA	1.82	7.0	9.40	NA
3	10	1400	14.0	13	C	7.35	7.3	3.5	3.240	0.049	1.310	5.26	0.644	1.60	8.0	10.00	NA
3	10	1545	15.6	13	C	7.35	6.5	4.7	3.290	0.052	1.320	NA	NA	1.82	8.0	9.70	NA
3	10	1745	17.8	13	C	7.38	8.5	4.1	3.120	0.049	1.240	5.42	0.777	1.60	7.0	9.60	NA
3	10	1925	19.4	13	C	7.32	8.0	4.8	2.855	0.052	1.320	NA	NA	1.28	7.1	8.50	NA
3	10	2138	21.6	13	C	7.32	5.7	4.7	3.040	0.049	1.290	4.34	0.647	1.28	6.9	8.20	NA
3	10	2345	23.8	13	C	7.32	6.5	4.1	2.920	0.049	1.320	NA	NA	1.28	6.2	8.00	NA
3	11	410	28.2	13	C	7.33	7.5	3.8	2.900	0.049	1.340	4.38	0.540	1.03	5.5	10.50	NA
3	11	625	30.4	13	C	7.35	8.0	4.0	2.850	0.052	1.380	NA	NA	1.13	6.5	10.60	NA
3	11	905	33.1	13	C	7.29	7.0	3.4	2.960	0.042	1.330	4.74	0.520	0.74	6.5	9.50	NA
3	11	1110	35.2	13	C	7.33	7.5	2.8	3.010	0.047	1.320	NA	NA	1.14	6.5	9.60	NA
3	11	1320	37.3	13	C	7.35	8.4	3.2	2.810	0.032	0.998	4.19	0.558	0.97	6.0	9.30	NA
3	11	1530	39.5	13	C	7.44	7.4	3.8	2.810	0.047	1.330	NA	NA	0.64	6.5	8.30	NA
3	11	1725	41.4	13	C	7.38	7.5	4.2	3.060	0.047	1.300	4.05	0.567	0.94	8.0	9.80	NA
3	11	1920	43.3	13	C	7.32	7.8	4.2	2.850	0.050	1.320	NA	NA	0.75	6.0	10.00	NA
3	11	2120	45.3	13	C	7.30	8.1	3.6	2.740	0.047	1.320	2.04	0.635	0.94	6.0	9.50	NA
3	11	2350	47.8	13	C	7.30	7.8	3.6	2.610	0.044	1.340	NA	NA	0.94	5.0	10.20	NA
3	12	145	49.8	13	C	7.32	8.0	3.3	2.640	0.044	1.350	3.40	0.543	0.78	6.0	9.50	NA
3	12	315	51.3	13	C	7.31	7.5	3.0	2.610	0.044	1.340	NA	NA	0.54	6.5	9.90	NA
3	12	445	52.8	13	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.0	9.90	NA
3	12	610	54.8	13	C	7.33	7.7	3.2	2.610	0.047	1.300	3.55	0.472	0.94	4.5	10.50	NA
3	12	915	57.1	13	C	7.28	7.5	3.8	2.470	0.047	1.310	NA	NA	1.13	5.0	9.80	NA
3	12	1050	58.8	13	C	7.30	7.7	3.6	2.500	0.044	1.310	3.84	0.494	1.03	5.4	10.00	NA
3	12	1310	61.2	13	C	7.30	7.5	4.0	2.670	0.047	1.300	3.61	0.401	0.56	6.8	10.20	NA
3	12	1448	62.8	13	C	7.30	7.4	3.6	2.670	0.047	1.300	NA	NA	1.22	7.3	10.30	NA

9465103355

BASELINE HIGH RIVER SAMPLING
HILARY STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEPTH	PH	TURB (NTU)	POD (PPM)	NH3 (PPM)	NO2 (PPM)	NO3 (PPM)	TKN (PPM)	TP (PPM)	CHLOR (PPB)	TEMP (*C)	D.O. (PPM)	SAL (PPT)
3	12	1645	64.7	13	C	7.30	7.7	4.0	1.500	0.016	0.471	3.41	0.553	0.54	7.3	10.30	NA
3	12	1815	66.3	13	C	7.30	7.8	4.0	2.210	0.039	1.100	NA	NA	1.32	6.5	10.80	NA
3	12	2020	68.3	13	C	7.30	7.4	4.0	2.400	0.042	1.180	3.60	0.569	1.32	6.0	10.20	NA
3	12	2225	70.4	13	C	7.20	6.3	3.6	1.200	0.039	1.100	NA	NA	1.50	5.8	10.20	NA
3	13	125	73.4	13	C	7.40	7.2	3.6	2.730	0.027	0.778	3.59	0.569	1.27	7.1	9.30	NA
3	13	405	76.1	13	C	7.30	8.0	4.2	3.300	0.047	1.260	NA	NA	1.41	5.1	10.10	NA
3	13	645	78.8	13	C	7.30	6.8	3.9	2.730	0.050	1.320	3.61	0.504	1.08	5.5	9.90	NA
3	13	1015	82.3	13	C	7.30	8.0	4.6	2.670	0.047	1.280	NA	NA	1.03	6.0	9.80	NA
3	13	1320	85.3	13	C	7.40	7.6	4.2	2.730	0.052	1.310	3.86	0.570	0.94	8.0	9.00	NA
3	13	1615	88.3	13	C	7.50	7.5	5.0	2.840	0.052	1.300	NA	NA	1.03	8.0	10.40	NA
3	13	1900	91.0	13	C	7.50	9.3	5.2	2.210	0.052	1.320	3.68	0.582	1.12	7.0	10.30	NA
3	13	2230	94.5	13	C	7.40	8.2	3.8	2.670	0.047	1.240	NA	NA	1.22	6.5	11.20	NA
3	14	200	98.0	13	C	7.40	7.3	3.8	2.210	0.047	1.300	3.45	0.492	1.50	6.0	10.50	NA
3	14	540	101.7	13	C	7.40	7.5	4.1	2.920	0.050	1.290	NA	NA	1.08	5.0	10.75	NA
3	14	850	104.8	13	C	7.40	9.0	4.8	2.890	0.044	1.140	4.01	0.534	2.35	5.3	9.90	NA
3	14	1230	108.5	13	C	7.50	8.5	3.9	2.840	0.052	1.310	NA	NA	1.41	6.0	9.90	NA
3	14	1530	111.5	13	C	7.50	8.5	3.6	3.600	0.055	1.320	4.68	0.647	0.56	6.0	11.10	NA
3	14	1915	115.1	13	C	7.50	9.0	3.8	2.350	0.040	0.913	NA	NA	1.11	5.0	10.60	NA
3	14	2230	118.5	13	C	7.40	9.2	3.6	2.590	0.052	1.240	2.87	0.442	2.07	5.0	11.40	NA
3	15	210	122.2	13	C	7.50	8.5	3.3	2.730	0.047	1.240	NA	NA	1.41	4.0	10.50	NA
3	15	545	125.8	13	C	7.50	8.0	2.6	2.540	0.047	1.210	3.48	0.486	1.65	4.0	10.50	NA
3	15	950	129.8	13	C	7.40	7.7	3.9	3.080	0.044	1.170	4.19	0.476	1.32	5.0	11.00	NA
3	15	1310	133.2	13	C	7.40	7.6	11.0	3.300	0.047	1.200	NA	NA	2.35	6.5	11.30	NA
3	15	1615	136.3	13	C	7.40	8.0	4.8	3.060	0.042	1.180	3.91	0.507	1.50	6.5	10.40	NA
3	15	1945	139.9	13	C	7.40	7.5	10.4	1.830	0.024	0.580	NA	NA	1.69	6.0	10.00	NA
3	15	2315	143.1	13	C	7.30	8.0	4.4	1.580	0.052	1.270	3.75	0.552	1.69	5.2	10.00	NA

9465103S6

BASELINE HIGH RIVER SAMPLING
HILARY STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
3	16	300	147.0	13	C	7.40	7.5	4.1	2.860	0.047	1.220	NA	NA	1.69	6.5	9.60	NA
3	16	545	149.8	13	C	7.40	7.2	4.2	2.620	0.047	1.230	3.64	0.540	1.36	5.1	9.60	NA
3	16	900	153.1	13	C	7.40	6.8	3.6	2.180	0.047	1.270	NA	NA	1.13	6.0	9.80	NA
3	16	1155	155.9	13	C	7.40	7.0	10.2	2.180	0.039	1.020	5.01	0.665	1.32	6.0	9.70	NA
3	16	1545	159.8	13	C	7.50	8.3	4.4	3.600	0.042	1.010	NA	NA	1.50	6.5	10.20	NA
3	16	1925	163.4	13	C	7.40	7.5	10.8	2.780	0.050	1.260	3.79	0.673	1.69	5.0	11.00	NA
3	16	2325	167.4	13	C	7.40	6.4	4.5	2.560	0.047	1.240	NA	NA	1.22	4.0	10.20	NA
3	17	250	170.8	13	C	7.40	6.0	8.8	2.830	0.047	1.210	3.79	0.616	2.73	3.0	10.50	NA
3	17	640	174.7	13	C	7.40	6.2	3.5	3.140	0.042	1.180	NA	NA	1.41	3.0	10.50	NA
3	17	940	177.7	13	C	7.40	6.4	2.7	NA	NA	NA	4.15	0.561	0.85	4.0	10.20	NA
3	17	1310	181.2	13	C	7.40	6.5	3.2	NA	NA	NA	NA	NA	1.03	4.5	10.90	NA
3	17	1620	184.3	13	C	7.40	7.7	3.8	2.480	0.022	0.064	4.27	0.547	0.85	4.5	10.50	NA
3	17	1915	187.3	13	C	7.50	6.8	4.1	2.180	0.024	0.903	NA	NA	0.85	4.0	10.80	NA
3	17	2220	190.3	13	C	7.50	7.3	3.8	2.860	0.027	0.889	4.95	0.625	1.22	3.2	10.70	NA
3	18	140	193.7	13	C	7.50	7.0	3.6	3.330	0.047	1.190	NA	NA	0.94	2.0	10.40	NA
3	18	440	196.7	13	C	7.50	6.8	3.4	3.170	0.044	1.130	3.54	0.383	0.80	1.9	12.50	NA
3	18	800	200.3	13	C	7.50	6.5	3.6	3.110	0.044	1.140	NA	NA	1.13	2.0	12.90	NA
3	18	1115	203.3	13	C	7.60	6.4	9.3	3.060	0.042	1.170	4.44	0.570	0.84	2.5	11.20	NA
3	18	1415	206.3	13	C	7.70	7.0	5.4	3.220	0.045	1.260	NA	NA	0.81	4.5	11.20	NA
3	18	1735	209.6	13	C	7.80	6.9	4.1	3.000	0.043	1.250	4.31	0.662	1.01	5.0	12.60	NA
3	18	2025	212.4	13	C	7.70	7.4	5.6	3.060	0.048	1.240	NA	NA	1.01	3.0	12.30	NA
3	18	2320	215.3	13	C	7.60	6.8	5.6	2.620	0.038	0.953	3.14	0.628	1.01	3.0	11.80	NA
3	19	300	219.1	13	C	7.70	7.0	5.6	3.190	0.054	1.330	NA	NA	0.47	3.1	11.60	NA
3	19	600	222.3	13	C	7.70	6.8	4.2	3.560	0.056	1.310	4.35	0.593	0.74	2.9	11.90	NA
3	19	950	225.8	13	C	7.50	6.5	4.5	3.760	0.054	1.270	6.06	0.627	0.38	3.0	11.30	NA
3	19	1250	228.8	13	C	7.60	6.4	5.2	4.020	0.054	1.280	NA	NA	0.46	4.5	10.00	NA

94510357

BASELINE HIGH RIVER SAMPLING
HILARY STREET - LEVEL C - 1\2 DEPTH

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	COD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
2	14	1550	231.6	13	C	7.80	6.8	4.6	3.990	0.054	1.340	6.01	0.672	0.78	5.5	11.10	NA
3	17	1650	234.7	13	C	7.60	7.3	4.5	2.500	0.018	0.823	NA	NA	0.84	5.0	11.90	NA
5	19	2150	237.2	13	C	7.70	6.6	7.2	3.880	0.054	1.310	5.95	0.688	0.67	4.0	11.00	NA
3	20	125	241.4	13	C	7.60	6.4	6.8	3.770	0.059	1.420	NA	NA	1.00	3.1	10.90	NA
3	20	445	244.8	13	C	7.60	6.4	5.1	3.770	0.059	1.380	4.70	0.633	0.65	2.1	10.80	NA
2	20	745	247.6	13	C	7.50	6.2	11.7	3.330	0.056	1.390	NA	NA	0.54	2.0	11.30	NA

946510358

BASELINE

DUNDEE DAM

UPSTREAM

3-10/3-20-81

1/2 DEPTH

946510359

BASELINE-RIVER SAMPLING
DUNDEE DAM UPSTREAM - LEVEL 8C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
3	10	1115	8	C	6.0	11.2
3	10	1415	8	C	6.5	10.8
3	10	1713	8	C	7.2	11.3
3	10	2005	8	C	7.0	10.8
3	10	2245	8	C	7.0	11.8
3	11	0145	8	C	7.0	10.6
3	11	0419	8	C	6.5	12.0
3	11	0625	8	C	6.0	11.8
3	11	0910	8	C	6.0	11.4
3	11	1135	8	C	6.0	11.8
3	11	1500	8	C	6.2	11.7
3	11	1751	8	C	6.2	10.8
3	11	2037	8	C	6.0	11.4
3	11	2310	8	C	6.0	10.9
3	12	0145	8	C	6.0	11.9
3	12	0444	8	C	5.5	10.5
3	12	0700	8	C	5.0	12.0
3	12	0950	8	C	5.0	11.4
3	12	1203	8	C	5.9	11.2
3	12	1500	8	C	6.0	11.2
3	12	1730	8	C	6.0	11.6
3	12	1940	8	C	6.0	10.8
3	12	2207	8	C	6.0	12.2
3	13	0335	8	C	6.0	11.1
3	13	0600	8	C	6.0	11.9
3	13	0940	8	C	6.0	10.6
3	13	1228	8	C	6.5	10.5
3	13	1537	8	C	7.5	11.6
3	13	1810	8	C	7.2	11.0
3	13	2140	8	C	7.0	11.5
3	14	0120	8	C	7.0	10.8
3	14	0450	8	C	6.3	12.0
3	14	0807	8	C	5.8	11.6
3	14	1120	8	C	5.5	11.2
3	14	1455	8	C	6.0	11.4
3	14	1815	8	C	5.4	11.8
3	14	2140	8	C	5.0	11.2
3	15	0115	8	C	4.5	12.0
3	15	0455	8	C	4.0	12.5
3	15	0903	8	C	4.1	12.5
3	15	1215	8	C	5.5	11.6
3	15	1525	8	C	5.5	11.0
3	15	1850	8	C	6.0	10.6
3	15	2215	8	C	6.0	11.5
3	16	0205	8	C	5.9	11.8

946510360

BASELINE-RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL BC - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
3	16	0515	8	C	5.8	12.4
3	16	0755	8	C	5.8	11.4
3	16	1115	8	C	7.0	10.8
3	16	1435	8	C	5.5	11.4
3	16	1835	8	C	5.5	12.5
3	16	2235	8	C	5.0	11.0
3	17	0200	8	C	4.5	10.5
3	17	0550	8	C	3.0	09.5
3	17	0855	8	C	3.8	11.0
3	17	1215	8	C	3.8	11.3
3	17	1525	8	C	3.5	11.4
3	17	1825	8	C	4.0	11.0
3	17	2120	8	C	3.5	11.5
3	18	0055	8	C	2.9	11.2
3	18	0355	8	C	2.0	11.0
3	18	0655	8	C	2.1	11.0
3	18	1030	8	C	2.8	11.9
3	18	1330	8	C	3.1	12.0
3	18	1650	8	C	3.0	10.4
3	18	1940	8	C	3.0	12.0
3	18	2230	8	C	3.0	11.0
3	19	0210	8	C	2.0	12.0
3	19	0520	8	C	2.3	11.8
3	19	0900	8	C	3.5	12.0
3	19	1200	8	C	4.3	12.7
3	19	1500	8	C	4.7	12.2
3	19	1810	8	C	4.9	11.8
3	19	2100	8	C	4.0	12.0
3	20	0050	8	C	3.0	11.5
3	20	0415	8	C	3.0	10.6
3	20	0715	8	C	2.9	10.2

946510361

BASELINE

DUNDEE DAM

DOWNSTREAM

3-10/3-20-81

1/2 DEPTH

946510362

BASELINE-RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL 6C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
3	10	1015	6	C	6.0	11.8
3	10	1305	6	C	6.5	12.0
3	10	1630	6	C	7.5	11.8
3	10	1923	6	C	7.0	10.9
3	10	2208	6	C	6.5	11.4
3	11	0105	6	C	6.0	11.6
3	11	0555	6	C	6.0	12.2
3	11	0820	6	C	6.5	12.4
3	11	1100	6	C	6.5	12.5
3	11	1425	6	C	6.0	12.4
3	11	1719	6	C	6.0	11.0
3	11	2000	6	C	6.0	11.6
3	11	2236	6	C	6.0	11.0
3	12	0115	6	C	5.9	12.2
3	12	0358	6	C	5.8	11.9
3	12	0630	6	C	5.2	12.0
3	12	0910	6	C	5.5	12.3
3	12	1135	6	C	6.0	12.0
3	12	1420	6	C	6.3	12.0
3	12	1658	6	C	6.4	11.8
3	12	1907	6	C	6.0	11.7
3	12	2130	6	C	5.5	10.8
3	12	2349	6	C	5.5	12.0
3	13	0312	6	C	5.5	12.2
3	13	0530	6	C	6.0	12.5
3	13	0900	6	C	6.0	11.8
3	13	1150	6	C	7.0	11.5
3	13	1445	6	C	7.5	11.5
3	13	1740	6	C	7.1	11.6
3	13	2050	6	C	6.9	12.2
3	14	0035	6	C	7.0	11.0
3	14	0410	6	C	6.0	12.0
3	14	0715	6	C	5.5	12.8
3	14	1010	6	C	6.0	12.3
3	14	1350	6	C	6.0	12.4
3	14	1725	6	C	5.3	12.0
3	14	2050	6	C	5.0	12.6
3	15	0345	6	C	4.0	12.8
3	15	0730	6	C	4.0	13.2
3	15	1130	6	C	6.0	13.2
3	15	1450	6	C	6.0	14.6
3	15	1800	6	C	5.5	12.0
3	15	2125	6	C	5.0	12.0
3	16	0115	6	C	5.2	12.1

946510363

BASELINE-RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL 6C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
3	16	0415	6	C	5.5	12.4
3	16	0715	6	C	5.6	11.8
3	16	1040	6	C	6.5	11.2
3	16	1345	6	C	6.5	11.8
3	16	1745	6	C	5.3	12.0
3	16	2145	6	C	4.0	12.0
3	17	0120	6	C	3.5	12.5
3	17	0450	6	C	3.0	12.0
3	17	0800	6	C	3.1	12.2
3	17	1130	6	C	4.1	13.0
3	17	1455	6	C	4.7	12.8
3	17	1745	6	C	4.0	12.6
3	17	2040	6	C	3.4	12.6
3	17	2355	6	C	2.1	13.0
3	18	0300	6	C	1.5	12.2
3	18	0600	6	C	1.5	12.0
3	18	0940	6	C	2.0	13.4
3	18	1240	6	C	3.5	12.6
3	18	1540	6	C	3.8	12.7
3	18	1900	6	C	3.2	12.4
3	18	2150	6	C	3.5	12.6
3	19	0130	6	C	2.9	11.0
3	19	0500	6	C	3.0	12.9
3	19	0800	6	C	3.1	12.6
3	19	1115	6	C	4.0	13.6
3	19	1415	6	C	4.0	13.0
3	19	1730	6	C	4.0	12.6
3	19	2020	6	C	3.5	12.4
3	19	2320	6	C	3.3	12.3
3	20	0225	6	C	2.9	11.2
3	20	0530	6	C	2.5	13.0

946510364

Storm Sampling
April 1981

946510365

STØRM #1

KEARNY

PØINT

4-14/4-24-81

1/3 DEPTH

946510366

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	STA	DEP	PH	TURB [NTU]	ROU [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	815	8.3	1	A	7.50	11.0	7.2	1.220	0.071	0.939	2.55	0.397	17.59	11.9	7.20	11.1
4	14	915	9.3	1	A	7.50	13.0	5.0	1.080	0.071	0.959	NA	NA	16.55	12.0	7.20	10.8
4	14	1014	10.2	1	A	7.50	12.0	5.2	1.070	0.066	0.894	2.52	0.401	23.79	12.0	7.00	11.2
4	14	1119	11.3	1	A	7.40	10.0	7.4	1.030	0.081	1.030	NA	NA	14.84	12.0	6.30	10.2
4	14	1218	12.3	1	A	7.50	12.0	7.1	1.180	0.082	0.819	3.14	0.945	17.59	11.8	6.40	10.1
4	14	1321	13.3	1	A	7.60	12.0	4.8	0.739	0.040	0.608	NA	NA	19.66	11.6	7.60	14.0
4	14	1419	14.3	1	A	7.50	17.0	15.8	1.580	0.102	0.898	NA	NA	22.46	12.0	7.80	15.3
4	14	1515	15.3	1	A	7.70	11.0	5.8	0.890	0.061	0.699	NA	NA	29.95	11.8	8.10	15.7
4	14	1630	16.5	1	A	7.70	11.0	7.2	1.270	0.084	0.868	3.65	0.550	34.80	11.9	7.90	16.2
4	14	1730	17.5	1	A	7.60	12.0	11.0	1.110	0.012	0.601	NA	NA	31.04	11.9	7.60	15.8
4	14	1830	18.5	1	A	7.70	12.0	7.2	0.900	0.048	0.602	2.76	0.414	22.57	11.3	7.10	16.8
4	14	1937	19.6	1	A	7.40	11.0	6.8	1.240	0.015	0.335	NA	NA	24.45	12.1	7.10	14.5
4	14	2030	20.5	1	A	7.40	12.0	4.8	1.260	0.089	0.961	3.36	0.701	17.87	12.4	6.60	9.0
4	14	2130	21.5	1	A	7.40	13.0	4.2	1.250	0.012	0.360	NA	NA	22.57	12.3	6.30	9.3
4	14	2230	22.5	1	A	7.40	13.0	3.6	1.240	0.020	0.548	2.84	0.503	23.51	12.4	6.00	9.1
4	14	2330	23.5	1	A	7.30	13.0	3.4	1.190	0.099	1.140	NA	NA	20.69	12.3	5.90	8.0
4	15	20	24.3	1	A	7.30	13.0	3.6	1.130	0.069	0.828	3.13	0.592	18.81	12.5	6.40	7.2
4	15	120	25.3	1	A	7.20	14.0	4.0	1.290	0.186	1.660	NA	NA	15.05	12.3	6.40	7.3
4	15	250	26.8	1	A	7.60	12.0	4.0	1.150	0.074	0.800	3.43	0.512	32.92	12.5	6.40	14.5
4	15	420	28.3	1	A	7.70	14.0	5.6	0.590	0.058	0.702	NA	NA	22.57	11.1	6.60	15.1
4	15	550	29.8	1	A	7.70	15.0	13.6	0.865	0.058	0.668	2.80	0.423	NA	11.5	6.80	14.9
4	15	650	30.8	1	A	7.60	11.0	6.0	0.589	0.079	0.873	1.57	0.299	22.57	11.9	6.20	14.9
4	15	804	32.1	1	A	7.40	7.0	4.8	1.280	0.089	0.961	3.13	0.449	6.07	12.0	6.20	10.5
4	15	935	33.6	1	A	7.30	8.0	3.9	0.858	0.099	1.050	NA	NA	7.76	12.0	5.80	9.1
4	15	1100	35.1	1	A	7.20	8.0	6.2	0.782	0.018	0.718	2.69	0.596	5.06	12.1	5.40	8.1
4	15	1235	36.6	1	A	7.30	8.0	4.6	1.260	0.094	1.020	NA	NA	15.05	11.9	6.10	8.0

946510367

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	17	1915	91.3	1	A	7.60	7.0	3.9	0.774	0.083	0.771	NA	NA	34.80	12.5	8.00	11.8
4	17	2015	92.3	1	A	7.60	6.0	4.4	0.637	0.053	0.546	3.09	0.568	41.38	11.5	8.20	16.2
4	17	2115	93.3	1	A	7.60	7.0	3.2	0.890	0.073	0.653	NA	NA	38.56	12.0	8.00	14.0
4	17	2215	94.3	1	A	7.40	7.0	3.4	1.040	0.093	0.837	4.38	0.544	31.04	12.2	7.40	10.5
4	17	2315	95.3	1	A	7.30	8.0	5.1	1.150	0.118	1.080	NA	NA	27.27	12.0	7.00	9.0
4	18	10	96.2	1	A	7.30	8.0	4.8	1.380	0.073	0.804	3.12	0.458	20.69	11.1	6.90	8.9
4	18	110	97.2	1	A	7.30	9.0	6.6	1.190	0.058	0.683	3.20	0.322	36.68	12.0	6.20	8.0
4	18	210	98.2	1	A	7.30	11.0	6.6	0.941	0.093	0.888	3.02	0.312	28.22	12.0	5.90	8.0
4	18	310	99.2	1	A	7.30	10.0	7.2	1.310	0.103	1.030	2.26	0.297	24.45	12.0	7.00	7.0
4	18	410	100.2	1	A	7.40	8.0	5.0	1.050	0.103	0.819	2.49	0.181	34.80	12.8	7.80	13.2
4	18	510	101.2	1	A	7.50	10.0	4.5	0.822	0.073	0.665	3.26	0.295	33.86	12.5	8.00	13.0
4	18	610	102.2	1	A	7.60	7.0	4.8	0.635	0.053	0.521	3.38	0.412	41.38	11.9	8.30	14.9
4	18	710	103.2	1	A	7.50	7.0	4.1	0.572	0.063	0.586	3.08	0.231	36.68	11.5	8.00	15.3
4	18	811	104.2	1	A	7.60	6.0	3.3	NA	NA	NA	NA	NA	35.74	11.0	6.90	16.6
4	18	913	105.2	1	A	7.60	7.0	2.8	0.874	0.053	0.528	3.20	0.406	31.04	11.0	7.30	15.5
4	18	1013	106.2	1	A	7.50	7.0	3.2	0.884	0.083	0.701	NA	NA	37.62	12.0	7.10	14.8
4	18	1112	107.2	1	A	7.40	9.0	3.3	1.250	0.073	0.755	4.09	0.480	27.27	12.8	7.10	9.0
4	18	1212	108.2	1	A	7.40	10.0	3.6	1.210	0.088	0.902	NA	NA	23.51	13.0	6.60	8.9
4	18	1315	109.3	1	A	7.30	12.0	4.1	NA	NA	NA	3.63	0.550	23.13	13.0	6.40	8.2
4	18	1410	110.2	1	A	7.30	11.0	4.4	1.110	0.088	0.922	NA	NA	25.39	13.1	6.40	7.0
4	18	1515	111.3	1	A	7.30	15.0	7.1	1.250	0.073	0.791	NA	NA	21.63	12.0	6.40	6.9
4	18	1615	112.3	1	A	7.40	9.0	5.1	1.070	0.103	0.831	3.27	0.474	33.86	NA	NA	NA
4	18	1715	113.3	1	A	7.60	7.0	4.1	1.180	0.083	0.698	NA	NA	31.98	13.2	8.90	12.2
4	18	1815	114.3	1	A	7.70	8.0	4.1	0.933	0.083	0.725	3.81	0.458	37.62	12.5	9.20	13.8
4	18	1915	115.3	1	A	7.80	11.0	3.3	0.393	0.015	0.225	NA	NA	41.38	12.0	9.20	15.2
4	18	2015	116.3	1	A	7.70	11.0	3.8	0.926	0.073	0.619	2.80	0.523	59.35	11.8	8.90	16.0

946510368

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	18	2115	117.3	1	A	7.70	10.0	2.8	0.984	0.088	0.743	2.08	0.411	63.06	11.2	8.90	15.2
4	18	2215	118.3	1	A	7.70	8.0	3.2	1.000	0.083	0.705	4.02	0.502	55.64	12.0	8.20	14.0
4	18	2315	119.3	1	A	7.60	12.0	4.4	1.030	0.093	0.810	NA	NA	32.92	12.0	7.40	11.5
4	19	10	120.2	1	A	7.50	8.0	2.9	1.080	0.093	0.947	3.88	0.410	19.75	12.1	7.80	9.1
4	19	110	121.2	1	A	7.40	7.0	6.4	0.605	0.025	0.309	NA	NA	30.10	12.1	7.60	9.1
4	19	210	122.2	1	A	7.40	9.0	4.5	0.952	NA	NA	4.02	0.587	23.51	12.1	7.00	7.5
4	19	310	123.2	1	A	7.30	8.0	9.3	1.320	0.103	0.957	NA	NA	31.98	12.0	7.50	7.0
4	19	410	124.2	1	A	7.30	7.0	6.4	2.030	0.073	0.607	5.53	0.824	19.75	12.0	7.40	11.9
4	19	510	125.2	1	A	7.50	8.0	6.0	1.390	0.093	0.723	NA	NA	42.32	13.0	8.00	15.0
4	19	610	126.2	1	A	7.50	8.0	4.4	0.518	0.038	0.407	3.09	0.444	34.80	12.0	8.80	15.0
4	19	710	127.2	1	A	7.70	7.0	3.2	0.516	0.053	0.492	NA	NA	35.74	11.2	8.50	17.0
4	19	814	128.2	1	A	7.70	5.0	2.7	0.734	0.043	0.450	2.66	0.379	39.50	11.1	7.80	17.8
4	19	912	129.2	1	A	7.60	9.0	5.8	0.486	0.053	0.552	NA	NA	35.74	11.2	7.30	17.3
4	19	1008	130.1	1	A	7.70	5.0	3.2	0.666	0.053	0.538	3.59	0.382	36.68	11.2	7.30	17.5
4	19	1111	131.2	1	A	7.60	6.0	4.5	1.130	0.073	0.640	NA	NA	36.68	12.3	8.60	14.2
4	19	1210	132.2	1	A	7.50	7.0	5.2	1.660	0.093	0.840	5.96	0.757	27.27	12.7	7.80	11.5
4	19	1314	133.2	1	A	7.50	8.0	6.2	1.600	0.083	0.762	NA	NA	31.04	12.8	7.40	10.5
4	19	1412	134.2	1	A	7.40	11.0	5.4	1.450	0.078	0.794	NA	NA	27.27	13.1	7.70	8.2
4	19	1510	135.2	1	A	7.40	9.0	7.6	NA	NA	NA	NA	NA	25.39	13.0	7.40	11.5
4	19	1615	136.3	1	A	7.40	14.0	10.4	1.510	0.083	0.860	4.88	0.960	25.39	13.0	7.00	14.2
4	19	1715	137.3	1	A	7.60	7.0	5.4	0.993	0.083	0.639	NA	NA	32.92	13.0	8.70	13.8
4	19	1815	138.3	1	A	7.80	7.0	3.5	1.110	0.073	0.581	3.59	0.541	33.86	13.2	9.20	14.8
4	19	1915	139.3	1	A	7.80	8.0	3.5	0.834	0.083	0.654	NA	NA	31.04	12.2	9.40	15.8
4	19	2015	140.3	1	A	7.90	7.0	2.7	1.070	0.068	0.610	4.02	0.482	37.62	12.2	9.30	16.0
4	19	2115	141.3	1	A	7.90	7.0	3.3	0.725	0.053	0.519	NA	NA	36.68	11.8	8.80	16.8
4	19	2215	142.3	1	A	7.80	6.0	2.7	0.833	0.048	0.601	3.38	0.545	29.16	12.2	9.20	15.5

946510369

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	19	2315	143.3	1	A	7.60	6.0	3.3	0.903	0.058	0.590	NA	NA	22.57	12.5	8.70	14.0
4	20	10	144.2	1	A	7.60	5.0	3.3	1.110	0.073	0.653	3.23	0.470	8.76	12.5	8.00	13.0
4	20	110	145.2	1	A	7.50	5.0	3.4	0.926	0.063	0.645	NA	NA	8.43	12.6	6.80	10.5
4	20	210	146.2	1	A	7.50	5.0	3.4	0.982	0.073	0.774	3.59	0.558	5.06	12.5	6.60	11.5
4	20	310	147.2	1	A	7.40	6.0	3.8	1.380	0.063	0.677	NA	NA	9.41	12.8	6.60	9.0
4	20	410	148.2	1	A	7.40	6.0	3.4	1.030	0.063	1.250	3.30	0.551	9.41	12.6	5.80	8.5
4	20	510	149.2	1	A	7.60	5.0	3.9	0.683	0.038	0.369	NA	NA	13.16	13.1	8.00	14.0
4	20	610	150.2	1	A	7.60	5.0	3.3	1.140	0.073	0.583	2.80	0.401	10.34	13.0	7.60	15.0
4	20	710	151.2	1	A	7.70	6.0	3.4	0.584	0.063	0.533	NA	NA	16.93	11.7	8.80	16.6
4	20	810	152.2	1	A	7.80	3.0	3.0	0.724	0.053	0.495	2.73	0.383	17.86	11.2	8.40	18.1
4	20	912	153.2	1	A	7.80	4.0	3.0	0.504	0.053	0.502	NA	NA	15.04	11.2	7.40	18.0
4	20	1008	154.1	1	A	7.80	5.0	3.0	0.678	0.043	0.447	2.55	0.351	17.86	11.5	7.90	18.2
4	20	1109	155.1	1	A	7.70	5.0	3.4	0.912	0.073	0.612	NA	NA	18.81	12.2	8.10	16.1
4	20	1211	156.2	1	A	7.60	5.0	3.4	1.110	0.063	0.588	3.41	0.459	12.22	12.6	8.30	14.1
4	20	1335	157.6	1	A	7.50	6.0	3.9	1.140	0.068	0.695	NA	NA	11.28	12.8	7.00	11.9
4	20	1514	159.2	1	A	7.50	6.0	4.2	1.200	0.083	0.765	NA	NA	10.34	13.0	7.20	10.0
4	20	1645	160.8	1	A	7.40	7.0	5.6	1.140	0.082	1.050	NA	NA	11.28	13.0	7.40	9.8
4	20	1815	162.3	1	A	7.80	6.0	3.8	0.975	0.022	0.820	NA	NA	12.22	12.5	9.00	15.8
4	20	1945	163.8	1	A	7.90	7.0	3.6	0.623	0.057	0.656	NA	NA	20.69	11.5	9.80	16.5
4	20	2115	165.3	1	A	7.90	5.0	3.8	0.708	0.057	0.650	3.16	0.737	14.11	11.0	9.70	17.0
4	20	2245	166.8	1	A	7.80	5.0	3.3	0.795	0.077	0.823	NA	NA	17.87	11.5	9.00	16.2
4	21	10	168.2	1	A	7.70	5.0	3.4	0.626	0.034	0.446	2.66	0.398	11.28	11.9	8.80	16.1
4	21	140	169.7	1	A	7.60	6.0	3.6	NA	NA	NA	2.73	0.398	5.05	11.9	7.90	12.5
4	21	310	171.2	1	A	7.50	6.0	4.1	0.928	0.047	0.754	NA	NA	11.28	12.0	6.60	10.1
4	21	440	172.7	4	A	7.70	6.0	3.6	0.498	0.018	0.227	2.58	0.398	17.87	12.5	8.80	15.9
4	21	610	174.2	1	A	7.80	5.0	4.1	0.758	0.048	0.534	NA	NA	18.81	12.8	8.40	14.9

946510370

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	21	740	175.7	1	A	7.90	5.0	3.6	0.526	0.028	0.415	2.33	0.355	20.69	11.5	9.30	17.5
4	21	844	176.7	1	A	7.80	5.0	3.3	0.770	0.058	0.705	NA	NA	15.05	11.1	9.60	17.9
4	21	942	177.7	1	A	7.90	3.0	5.6	0.603	0.060	0.669	2.44	0.348	11.80	11.0	8.20	18.2
4	21	1045	178.8	1	A	7.90	4.0	3.3	0.951	0.078	0.865	NA	NA	22.57	11.0	8.30	18.0
4	21	1142	179.7	1	A	7.90	4.0	2.2	0.621	0.048	0.649	2.44	0.327	14.11	11.1	8.50	18.0
4	21	1245	180.8	1	A	7.80	5.0	2.6	0.803	0.078	0.942	3.16	0.416	20.69	12.2	9.50	12.3
4	21	1416	182.3	1	A	7.70	4.0	3.0	0.719	0.078	0.892	3.45	0.468	9.44	12.2	8.40	12.0
4	21	1510	183.2	1	A	7.70	3.0	2.1	0.797	0.060	0.703	2.66	0.389	11.46	12.6	7.40	15.0
4	21	1615	184.3	1	A	7.50	5.0	6.4	1.020	0.078	0.952	3.91	1.260	7.42	12.8	7.40	9.8
4	21	1715	185.3	1	A	7.50	5.0	5.4	0.908	0.078	0.828	2.51	0.591	7.75	12.8	8.70	10.2
4	21	1815	186.3	1	A	7.80	4.0	3.6	0.821	0.091	0.772	NA	NA	8.43	12.5	8.80	16.2
4	21	1915	187.3	1	A	8.00	3.0	2.2	0.688	0.070	0.725	3.02	0.476	9.78	11.5	9.90	17.0
4	21	2015	188.3	1	A	8.00	3.0	2.2	0.685	0.068	0.693	NA	NA	10.45	11.2	10.60	18.0
4	21	2115	189.3	1	A	8.10	3.0	2.0	0.563	0.060	0.664	3.63	0.549	13.17	10.8	10.20	17.8
4	21	2215	190.3	1	A	8.00	3.0	2.4	0.614	0.068	0.754	NA	NA	15.05	11.0	10.60	17.2
4	21	2315	191.3	1	A	8.00	6.0	2.2	0.843	0.067	0.724	2.75	0.358	14.11	11.2	9.80	17.2
4	22	10	192.2	1	A	7.90	6.0	2.2	0.468	0.070	0.703	NA	NA	5.73	11.5	9.80	16.3
4	22	110	193.2	1	A	7.90	5.0	2.0	0.593	0.078	0.789	3.34	0.419	6.40	11.8	8.40	15.9
4	22	210	194.2	1	A	7.70	8.0	4.1	0.856	0.081	0.888	NA	NA	12.23	11.8	8.30	13.8
4	22	310	195.2	1	A	7.70	4.0	2.2	0.768	0.078	0.904	2.94	0.474	9.44	11.8	8.30	13.9
4	22	410	196.2	1	A	7.60	6.0	2.2	0.720	0.061	0.701	NA	NA	7.42	11.4	7.80	11.9
4	22	510	197.2	1	A	7.80	7.0	2.7	0.693	0.078	0.799	3.01	0.510	6.74	11.2	7.90	12.1
4	22	610	198.2	1	A	7.70	18.0	3.4	0.520	0.040	0.479	NA	NA	5.39	11.2	7.80	14.5
4	22	710	199.2	1	A	7.90	8.0	2.7	0.949	0.078	0.731	3.27	0.419	7.42	12.0	8.80	16.5
4	22	816	200.3	1	A	7.80	11.0	6.4	0.786	0.074	0.775	2.62	0.384	6.58	11.0	8.80	17.2
4	22	900	201.1	1	A	8.00	7.0	4.1	0.690	0.063	0.690	2.75	0.448	56.01	10.5	NA	18.0

946510371

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	22	1011	202.2	1	A	8.00	8.0	3.9	0.418	0.068	0.729	2.78	0.318	28.21	10.8	NA	17.9
4	22	1114	203.2	1	A	8.00	7.0	4.1	0.628	0.060	0.628	2.88	0.350	13.17	10.8	9.60	18.0
4	22	1207	204.1	1	A	7.90	7.0	4.4	NA	NA	NA	NA	NA	48.22	11.0	9.50	17.5
4	22	1314	205.2	1	A	8.00	6.0	4.6	0.774	0.053	0.599	4.18	0.507	19.75	12.0	9.40	15.7
4	22	1411	206.2	1	A	7.80	7.0	4.1	0.702	0.081	0.853	2.13	0.490	10.34	12.2	9.90	14.0
4	22	1514	207.2	1	A	7.70	11.0	4.4	0.556	0.086	0.934	NA	NA	7.42	12.5	9.30	12.8
4	22	1615	208.3	1	A	7.70	11.0	4.6	0.965	0.084	0.986	3.40	0.697	14.11	12.5	8.90	11.5
4	22	1715	209.3	1	A	7.70	8.0	4.6	0.888	0.089	1.010	NA	NA	21.63	12.5	10.20	12.2
4	22	1815	210.3	1	A	7.90	10.0	8.0	0.974	0.063	0.763	3.79	0.733	16.93	12.5	10.10	14.5
4	22	1915	211.3	1	A	7.90	8.0	5.6	0.972	0.063	0.758	NA	NA	16.93	12.2	10.60	16.2
4	22	2015	212.3	1	A	8.00	7.0	4.8	0.804	0.063	0.642	4.80	0.576	26.33	11.8	10.80	16.2
4	22	2115	213.3	1	A	8.00	5.0	6.0	0.575	0.077	0.764	NA	NA	14.11	11.5	10.60	17.0
4	22	2215	214.3	1	A	8.10	7.0	5.8	0.571	0.057	0.655	4.05	0.771	18.81	11.2	10.40	17.5
4	22	2315	215.3	1	A	8.00	13.0	6.6	0.619	0.070	0.643	NA	NA	15.05	11.2	10.20	17.5
4	23	10	216.2	1	A	8.00	10.0	4.5	0.381	0.019	0.563	2.62	0.360	55.64	11.5	9.50	16.0
4	23	110	217.2	1	A	8.00	7.0	3.9	0.803	0.057	0.655	NA	NA	66.77	12.0	10.00	15.5
4	23	210	218.2	1	A	7.70	14.0	9.3	0.769	0.082	0.889	2.94	0.456	77.89	12.1	9.00	8.0
4	23	310	219.2	1	A	7.60	9.0	4.1	0.815	0.086	0.974	NA	NA	29.95	12.1	8.20	11.5
4	23	410	220.2	1	A	7.60	12.0	4.5	1.080	0.091	0.929	3.08	0.467	40.80	12.0	8.40	12.0
4	23	510	221.2	1	A	7.50	11.0	4.8	0.773	0.091	1.040	NA	NA	21.63	12.0	7.20	11.0
4	23	610	222.2	1	A	7.50	18.0	6.2	0.761	0.086	0.934	3.53	0.788	36.68	11.7	8.80	14.1
4	23	710	223.2	1	A	7.60	19.0	6.4	0.941	0.086	0.776	NA	NA	77.89	12.1	9.00	15.5
4	23	810	224.2	1	A	7.80	13.0	8.6	0.743	0.086	0.766	NA	NA	74.18	12.0	9.50	15.1
4	23	912	225.2	1	A	7.90	15.0	3.6	0.696	0.068	0.660	NA	NA	74.18	11.5	10.00	17.0
4	23	1013	226.2	1	A	8.00	9.0	3.0	0.304	0.020	0.434	NA	NA	70.47	11.4	10.10	15.8
4	23	1110	227.2	1	A	8.00	8.0	3.6	0.434	0.070	0.682	NA	NA	55.64	11.1	10.00	17.1

946510372

KEARNY POINT - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	23	1209	228.1	1	A	8.00	9.0	2.6	0.426	0.037	0.482	NA	NA	70.47	11.1	9.90	17.0
4	23	1314	229.2	1	A	8.00	10.0	2.7	0.819	0.086	0.770	NA	NA	59.35	12.0	9.00	15.2
4	23	1411	230.2	1	A	7.60	10.0	3.2	0.734	0.086	0.800	NA	NA	55.64	12.0	8.20	14.1
4	23	1513	231.2	1	A	7.50	12.0	2.8	1.050	0.086	0.888	NA	NA	48.22	12.0	8.20	11.2
4	23	1615	232.3	1	A	7.50	14.0	3.0	1.010	0.086	0.954	NA	NA	20.37	12.0	8.00	11.8
4	23	1715	233.3	1	A	7.60	14.0	3.3	1.120	0.089	0.981	NA	NA	31.23	12.0	7.30	11.8
4	23	1815	234.3	1	A	7.40	12.0	3.2	0.983	0.091	0.979	NA	NA	36.37	12.0	7.20	11.8
4	23	1915	235.3	1	A	7.60	9.0	2.4	1.020	0.086	0.762	NA	NA	40.65	12.0	8.80	15.0
4	23	2015	236.3	1	A	7.90	8.0	2.7	0.747	0.089	0.719	NA	NA	63.06	11.8	9.50	16.2
4	23	2115	237.3	1	A	7.90	10.0	2.6	0.559	0.082	0.731	NA	NA	36.37	11.2	8.60	16.5
4	23	2215	238.3	1	A	8.00	15.0	3.9	0.728	0.068	0.661	NA	NA	43.86	11.0	8.00	17.5
4	23	2315	239.3	1	A	8.00	8.0	2.4	0.954	0.082	0.753	NA	NA	37.44	11.0	9.50	17.8
4	24	10	240.2	1	A	8.00	12.0	3.8	0.435	0.047	0.587	NA	NA	38.51	11.0	8.40	17.1
4	24	110	241.2	1	A	8.00	7.0	2.2	0.538	0.057	0.541	NA	NA	51.92	11.0	10.20	17.0
4	24	210	242.2	1	A	7.80	7.0	2.7	0.636	0.072	0.666	NA	NA	55.64	11.8	8.20	15.1
4	24	310	243.2	1	A	7.60	9.0	2.0	0.834	0.091	0.919	NA	NA	31.02	11.9	9.00	13.0
4	24	410	244.2	1	A	7.80	13.0	3.9	0.775	0.077	0.724	NA	NA	77.88	11.7	8.00	13.1
4	24	510	245.2	1	A	7.50	10.0	2.2	0.861	0.077	0.735	NA	NA	33.16	12.0	7.10	11.2
4	24	610	246.2	1	A	7.70	10.0	2.7	0.773	0.057	0.607	NA	NA	42.79	11.5	8.40	15.0
4	24	710	247.2	1	A	7.80	10.0	2.6	0.657	0.077	0.641	NA	NA	51.93	11.8	8.60	15.5
4	24	810	248.2	1	A	7.80	9.0	3.3	0.868	0.086	0.636	NA	NA	59.35	12.0	9.10	16.1
		AVERAGE READING				7.62	8.3	4.7	0.967	0.072	0.762	3.30	0.513	26.00	11.9	7.90	13.2

946510373

STØRM #1

KEARNY

PØINT

4-14/4-24-81

2/3 DEPTH

946510374

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	810	8.2	1	B	7.30	13.0	8.0	0.887	0.012	0.354	4.47	0.452	21.40	12.0	7.70	15.9
4	14	910	9.2	1	B	7.70	11.0	4.0	0.832	0.058	0.748	NA	NA	29.95	11.2	7.40	16.1
4	14	1008	10.1	1	B	7.70	15.0	6.2	1.230	0.069	0.897	2.84	0.436	59.35	11.8	7.30	15.5
4	14	1114	11.2	1	B	7.60	12.0	4.0	0.567	0.015	0.283	NA	NA	26.74	11.5	7.20	15.2
4	14	1214	12.2	1	B	7.60	11.0	3.4	0.758	0.089	1.080	2.98	0.505	27.27	11.2	8.00	17.0
4	14	1317	13.3	1	B	7.60	16.0	4.6	0.787	0.099	1.170	NA	NA	34.23	11.3	8.10	15.0
4	14	1414	14.2	1	B	7.60	20.0	9.4	0.962	0.079	1.010	4.47	0.936	55.64	12.0	8.00	15.5
4	14	1511	15.2	1	B	7.80	12.0	4.0	0.928	0.099	1.190	NA	NA	32.92	11.5	7.90	16.8
4	14	1625	16.4	1	B	7.80	12.0	5.2	0.639	0.030	0.741	2.94	0.441	27.81	11.0	7.90	16.9
4	14	1725	17.4	1	B	7.80	12.0	6.8	0.767	0.040	0.636	NA	NA	13.91	11.0	7.40	17.1
4	14	1825	18.4	1	B	7.80	11.0	4.8	0.730	0.040	0.625	3.73	0.393	26.74	11.0	8.10	17.2
4	14	1925	19.4	1	B	7.80	10.0	4.0	1.160	0.071	0.899	NA	NA	25.67	11.2	7.50	16.9
4	14	2025	20.4	1	B	7.70	10.0	4.8	0.794	0.061	0.708	4.12	0.337	23.53	12.8	7.00	16.0
4	14	2125	21.4	1	B	7.60	14.0	7.0	1.090	0.071	0.779	NA	NA	27.81	12.2	6.60	15.0
4	14	2225	22.4	1	B	7.50	13.0	5.6	0.497	0.010	0.537	2.52	0.464	18.19	11.7	6.00	15.6
4	14	2325	23.4	1	B	7.60	14.0	10.6	1.030	0.061	0.719	NA	NA	11.77	11.7	5.80	15.1
4	15	30	24.5	1	B	7.60	13.0	7.8	1.020	0.071	0.827	2.62	0.521	27.16	11.9	7.00	15.5
4	15	300	27.0	1	B	7.60	13.0	7.6	0.806	0.030	0.609	2.26	0.443	38.51	12.1	6.70	15.2
4	15	430	28.5	1	B	7.70	12.0	3.0	1.090	0.081	0.809	NA	NA	29.95	11.0	6.90	16.5
4	15	700	31.0	1	B	7.70	17.0	9.8	0.614	0.020	0.600	NA	NA	53.79	11.0	6.90	16.4
4	15	600	30.0	1	B	NA	NA	5.0	NA	NA	NA	4.93	2.180	23.53	11.0	6.90	16.5
4	15	800	32.0	1	B	7.50	8.0	11.4	0.888	0.067	0.651	4.32	0.340	23.98	11.7	6.60	16.0
4	15	931	33.5	1	B	7.60	5.0	5.0	0.887	0.061	0.691	NA	NA	40.44	10.9	6.80	16.8
4	15	1103	35.0	1	B	7.60	8.0	14.6	0.875	0.051	0.651	3.92	0.366	23.51	10.9	7.40	17.9
4	15	1402	38.0	1	B	7.40	6.0	15.4	1.060	0.096	0.924	4.58	0.675	12.23	11.1	6.40	16.9
4	15	1532	39.5	1	B	7.60	6.0	6.6	0.884	0.051	0.669	NA	NA	15.98	11.0	7.40	17.1

946510375

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	15	1700	41.0	1	B	7.80	5.0	5.6	1.120	0.096	0.927	3.89	0.399	30.09	11.8	8.10	18.5
4	15	1800	42.0	1	B	7.70	5.0	4.0	0.829	0.051	0.621	NA	NA	31.04	11.0	8.40	18.2
4	15	1900	43.0	1	B	7.80	5.0	3.0	0.795	0.061	0.664	3.40	0.564	16.93	11.0	8.10	18.0
4	15	2000	44.0	1	B	7.70	6.0	5.2	1.100	0.081	0.819	NA	NA	30.09	12.0	8.00	11.5
4	15	2100	45.0	1	B	7.50	7.0	14.0	2.990	0.071	0.741	6.04	1.610	20.69	12.0	6.80	13.8
4	15	2200	46.0	1	B	7.50	7.0	7.6	0.706	0.030	0.649	NA	NA	39.50	12.0	6.20	11.0
4	15	2300	47.0	1	B	7.40	7.0	5.8	1.210	0.091	0.989	4.58	0.703	23.51	12.0	6.00	10.0
4	16	15	48.3	1	B	7.40	7.0	8.4	1.220	0.112	1.140	NA	NA	15.98	11.9	5.80	10.2
4	16	115	49.3	1	B	7.30	7.0	6.8	2.900	0.020	0.382	NA	2.430	24.45	11.0	5.60	13.5
4	16	215	50.3	1	B	7.40	6.0	14.2	1.790	0.020	0.356	NA	NA	23.51	11.8	7.30	16.0
4	16	315	51.3	1	B	7.60	6.0	8.4	1.220	0.071	0.686	4.71	0.826	26.33	11.5	7.90	15.9
4	16	415	52.3	1	B	7.70	7.0	11.4	0.771	0.046	0.553	NA	NA	14.10	10.9	8.00	17.1
4	16	515	53.3	1	B	7.70	6.0	4.8	0.846	0.056	0.624	3.14	0.341	15.05	10.9	8.60	17.1
4	16	615	54.3	1	B	7.70	7.0	6.6	0.352	0.020	0.330	NA	NA	12.23	10.5	7.90	17.5
4	16	715	55.3	1	B	7.60	6.0	5.2	0.467	0.010	0.301	3.01	0.348	13.17	10.6	7.80	17.5
4	16	812	56.2	1	B	7.60	7.0	8.1	0.749	0.048	0.659	5.55	1.550	16.93	10.8	6.80	17.1
4	16	910	57.2	1	B	7.60	6.0	3.9	0.394	0.020	0.428	NA	NA	13.17	10.9	6.50	17.0
4	16	1003	58.0	1	B	7.60	7.0	4.4	1.040	0.058	0.706	2.75	0.526	13.17	11.5	6.60	15.5
4	16	1111	59.2	1	B	7.50	7.0	5.7	1.160	0.120	1.340	NA	NA	10.34	11.8	6.10	10.1
4	16	1213	60.2	1	B	7.50	8.0	6.8	1.170	0.069	0.835	3.73	0.797	13.17	12.1	5.50	14.9
4	16	1306	61.1	1	B	7.50	9.0	5.8	1.230	0.069	0.810	NA	NA	14.11	11.5	5.80	14.0
4	16	1409	62.1	1	B	7.50	7.0	6.9	0.905	0.058	0.757	3.60	0.740	14.11	11.9	5.50	15.9
4	16	1506	63.1	1	B	7.50	7.0	7.8	1.040	0.079	0.821	NA	NA	16.93	12.0	6.80	15.0
4	16	1600	64.0	1	B	7.60	7.0	6.9	1.410	0.099	0.971	3.21	0.588	14.11	12.2	7.20	15.0
4	16	1700	65.0	1	B	7.70	8.0	7.6	1.130	0.074	0.788	NA	NA	18.81	11.5	8.30	14.5
4	16	1800	66.0	1	B	7.80	10.0	6.4	0.726	0.028	0.671	2.82	0.426	19.75	11.2	8.70	16.8

946510376

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	16	1900	67.0	1	B	7.70	7.0	7.1	1.150	0.089	0.856	NA	NA	18.81	11.2	8.60	16.3
4	16	2000	68.0	1	B	7.80	7.0	6.6	0.960	0.058	0.734	2.94	0.318	18.81	11.5	7.90	15.8
4	16	2100	69.0	1	B	7.70	7.0	5.7	0.906	0.089	0.861	NA	NA	11.28	12.0	7.10	14.5
4	16	2200	70.0	1	B	7.50	8.0	5.7	1.380	0.110	1.080	NA	NA	13.17	12.2	6.70	10.5
4	16	2300	71.0	1	B	7.40	8.0	7.1	1.520	0.120	1.230	NA	NA	10.34	12.0	6.00	9.0
4	17	15	72.3	1	B	7.40	11.0	7.2	1.170	0.069	0.889	3.21	0.596	10.34	12.1	5.70	8.6
4	17	115	73.3	1	B	7.30	9.0	5.7	1.000	0.043	0.653	NA	NA	8.77	12.2	4.90	10.5
4	17	215	74.3	1	B	7.30	11.0	10.6	1.440	0.150	1.490	3.47	0.494	14.11	12.1	6.60	13.5
4	17	315	75.3	1	B	7.60	10.0	12.6	1.180	0.089	0.931	NA	NA	22.57	12.1	6.70	14.5
4	17	415	76.3	1	B	7.60	8.0	5.7	1.150	0.089	0.910	3.86	0.732	17.87	12.5	7.30	14.6
4	17	515	77.3	1	B	7.50	9.0	5.4	0.773	0.023	0.665	NA	NA	12.22	11.1	7.80	16.1
4	17	615	78.3	1	B	7.60	8.0	6.4	0.741	0.058	0.700	3.21	0.337	18.81	10.9	7.80	16.5
4	17	715	79.3	1	B	7.70	8.0	5.4	0.877	0.058	0.770	NA	NA	18.81	10.9	6.30	16.7
4	17	808	80.1	1	B	7.40	6.0	4.4	0.592	0.067	0.642	3.21	0.241	NA	11.0	6.30	16.8
4	17	907	81.1	1	B	7.50	6.0	5.7	0.858	0.057	0.591	NA	NA	NA	11.0	7.30	16.6
4	17	1006	82.1	1	B	7.50	6.0	4.4	0.811	0.057	0.581	3.79	0.274	66.77	12.0	6.20	16.8
4	17	1101	83.0	1	B	7.60	7.0	3.6	0.923	0.067	0.637	NA	NA	63.06	12.0	7.30	16.0
4	17	1209	84.1	1	B	7.50	6.0	5.2	0.847	0.067	0.650	3.07	0.334	42.32	12.2	5.50	15.5
4	17	1306	85.1	1	B	7.50	8.0	5.1	1.060	0.084	0.746	NA	NA	44.20	12.2	5.50	13.0
4	17	1409	86.1	1	B	7.50	5.0	4.2	0.640	0.007	0.467	4.90	0.483	44.20	12.1	6.30	15.5
4	17	1510	87.2	1	B	7.50	7.0	5.0	1.000	0.086	0.590	3.53	0.448	63.06	12.8	7.30	14.0
4	17	1610	88.2	1	B	7.50	6.0	5.4	1.000	0.067	0.725	NA	NA	51.93	11.8	7.90	14.0
4	17	1710	89.2	1	B	7.50	6.0	5.4	1.000	0.067	0.725	NA	NA	51.93	11.8	7.90	14.0
4	17	1810	90.2	1	B	7.60	7.0	3.8	0.621	0.027	0.708	3.92	0.381	41.38	11.0	8.60	16.5
4	17	1910	91.2	1	B	7.70	6.0	3.8	0.671	0.067	0.564	NA	NA	33.86	12.5	7.90	11.0
4	17	2010	92.2	1	B	7.60	7.0	3.8	0.786	0.057	0.630	3.92	0.786	32.92	11.0	7.80	16.5
4	17	2110	93.2	1	B	7.60	5.0	3.8	1.210	0.096	0.508	NA	NA	31.98	10.8	7.80	16.0

946510377

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	17	2210	94.2	1	B	7.50	6.0	5.0	1.020	0.077	0.829	4.02	0.402	33.86	12.2	7.30	12.0
4	17	2310	95.2	1	B	7.40	6.0	10.1	1.340	0.106	1.130	NA	NA	31.98	12.0	6.70	9.0
4	18	15	96.3	1	B	7.40	6.0	9.8	1.210	0.067	0.721	4.14	0.402	70.47	12.1	6.40	9.1
4	18	115	97.3	1	B	7.40	7.0	5.7	0.962	0.082	0.714	3.06	0.391	63.06	12.1	6.00	13.1
4	18	215	98.3	1	B	7.50	6.0	4.8	0.732	0.067	0.620	2.95	0.320	40.44	12.0	6.20	14.1
4	18	315	99.3	1	B	7.40	7.0	7.2	1.150	0.116	1.160	5.40	0.406	25.39	12.0	7.60	13.0
4	18	415	100.3	1	B	7.40	7.0	5.2	0.861	0.067	0.622	3.83	0.419	66.77	12.5	7.20	14.1
4	18	515	101.3	1	B	7.50	5.0	5.2	1.040	0.096	0.810	4.02	0.629	38.56	11.8	7.60	15.0
4	18	615	102.3	1	B	7.60	8.0	8.7	0.641	0.057	0.587	2.06	0.277	38.56	10.9	8.00	16.3
4	18	715	103.3	1	B	7.60	6.0	5.2	0.908	0.077	0.728	3.10	0.399	81.60	10.5	7.40	16.8
4	18	807	104.1	1	B	7.60	6.0	2.6	0.729	0.047	0.543	2.28	0.554	31.04	11.0	7.20	17.0
4	18	909	105.1	1	B	7.60	6.0	2.8	0.569	0.057	0.588	NA	NA	22.57	11.2	6.40	16.8
4	18	1009	106.1	1	B	7.60	7.0	2.6	0.735	0.047	0.558	1.07	0.372	30.10	11.1	7.60	16.8
4	18	1107	107.1	1	B	7.50	5.0	3.9	0.993	0.077	0.731	NA	NA	25.39	12.8	7.70	13.8
4	18	1208	108.1	1	B	7.40	8.0	3.9	1.210	0.096	0.964	4.82	0.652	25.39	12.5	6.40	9.5
4	18	1310	109.2	1	B	7.50	8.0	5.6	0.830	0.067	0.688	NA	NA	31.04	12.0	6.10	15.2
4	18	1406	110.1	1	B	7.50	6.0	5.4	1.040	0.096	0.954	3.61	0.592	55.64	12.0	6.10	15.2
4	18	1506	111.1	1	B	7.40	8.0	9.3	0.831	0.067	0.692	NA	NA	63.06	11.0	6.60	16.0
4	18	1610	112.2	1	B	7.40	7.0	9.8	1.320	0.067	1.290	3.88	0.577	59.35	12.2	NA	14.5
4	18	1710	113.2	1	B	7.50	6.0	4.6	0.988	0.057	0.755	NA	NA	59.35	11.8	8.30	14.8
4	18	1810	114.2	1	B	7.70	5.0	3.9	0.664	0.057	0.583	3.31	0.556	74.18	11.0	8.60	16.2
4	18	1910	115.2	1	B	7.60	12.0	9.6	0.753	0.072	0.678	NA	NA	52.15	12.0	9.20	15.2
4	18	2010	116.2	1	B	7.70	15.0	5.4	0.563	0.067	0.646	3.75	0.768	41.38	11.5	8.00	16.0
4	18	2110	117.2	1	B	7.70	7.0	4.4	0.639	0.077	0.736	NA	NA	33.86	11.2	8.30	16.3
4	18	2210	118.2	1	B	7.70	7.0	4.6	0.767	0.052	0.733	2.31	0.845	36.68	11.0	8.00	17.5
[redacted]																	
4	18	2310	118.2	1	B	7.50	6.0	3.4	0.809	0.096	0.891	3.88	0.744	20.70	12.0	7.40	12.8

946510378

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	19	15	120.3	1	B	7.40	12.0	12.3	NA	NA	NA	NA	NA	21.63	12.1	7.40	10.4
4	19	115	121.3	1	B	7.40	8.0	12.4	3.700	0.067	0.609	NA	2.800	24.45	12.0	7.20	14.5
4	19	215	122.3	1	B	7.40	9.0	5.6	NA	0.067	0.732	NA	NA	27.27	12.1	6.50	11.9
4	19	315	123.3	1	B	7.30	11.0	5.4	1.420	0.086	0.954	4.25	1.040	23.51	11.9	6.80	13.5
4	19	415	124.3	1	B	7.40	9.0	7.5	2.350	0.042	0.664	NA	NA	18.81	12.0	7.20	14.5
4	19	515	125.3	1	B	7.50	8.0	5.8	1.020	0.096	0.739	2.88	0.584	28.22	12.0	8.00	15.8
4	19	615	126.3	1	B	7.70	7.0	8.0	0.436	0.017	0.250	NA	NA	40.44	11.0	8.50	17.8
4	19	715	127.3	1	B	7.60	6.0	5.0	0.605	0.032	0.385	3.92	0.721	28.22	11.0	8.30	17.5
4	19	809	128.1	1	B	7.70	7.0	3.7	0.680	0.057	0.584	2.81	0.525	32.92	11.0	9.40	17.9
4	19	907	129.1	1	B	7.70	8.0	3.8	0.695	0.057	0.601	NA	NA	26.33	11.0	8.00	18.0
4	19	1004	130.1	1	B	7.70	7.0	3.2	0.697	0.052	0.570	2.94	0.512	32.92	11.0	8.20	18.0
4	19	1107	131.1	1	B	7.70	7.0	2.6	0.668	0.057	0.613	NA	NA	25.39	11.2	8.30	17.5
4	19	1206	132.1	1	B	7.60	8.0	6.0	1.430	0.086	0.818	3.35	0.680	44.20	12.2	7.90	14.0
4	19	1309	133.1	1	B	7.60	7.0	4.5	0.846	0.067	0.645	NA	NA	34.80	11.9	6.80	16.1
4	19	1505	135.1	1	B	7.60	6.0	4.4	NA	NA	NA	NA	NA	24.60	12.0	7.00	15.6
4	19	1505	135.1	1	B	7.60	6.0	4.4	NA	NA	NA	NA	NA	24.63	12.0	7.00	15.6
4	19	1810	138.2	1	B	7.70	12.0	7.8	0.956	0.077	0.750	2.98	0.777	29.16	13.0	8.90	16.2
4	19	1910	139.2	1	B	7.80	9.0	5.1	0.393	0.020	0.532	NA	NA	40.44	12.0	9.30	17.2
4	19	2010	140.2	1	B	7.80	10.0	7.1	0.650	0.047	0.619	3.18	0.656	38.56	12.0	9.50	16.8
4	19	2110	141.2	1	B	7.60	7.0	4.8	0.400	0.032	0.686	NA	NA	33.86	11.2	7.60	17.2
4	19	2210	142.2	1	B	7.80	7.0	4.5	0.702	0.067	0.687	3.68	1.060	30.10	11.7	9.00	17.0
4	19	2310	143.2	1	B	7.80	7.0	4.4	0.814	0.067	0.673	NA	NA	27.27	12.5	8.40	15.2
4	20	15	144.3	1	B	7.60	5.0	4.4	0.985	0.096	0.924	1.91	0.564	15.98	12.2	7.90	13.9
4	20	115	145.3	1	B	7.40	7.0	3.4	1.130	0.067	0.773	NA	NA	13.17	12.6	6.80	11.6
4	20	215	146.3	1	B	7.50	4.0	4.6	0.837	0.062	0.607	3.01	0.649	15.98	12.0	6.50	15.0
4	20	315	147.3	1	B	7.40	7.0	4.5	1.020	0.096	1.000	NA	NA	21.63	12.5	6.00	12.5

946510379

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	20	415	148.3	1	B	7.30	7.0	6.8	1.170	0.086	0.835	3.95	0.738	12.22	12.3	5.70	12.0
4	20	515	149.3	1	B	7.60	5.0	4.2	0.852	0.086	0.704	NA	NA	11.28	12.5	7.80	15.5
4	20	615	150.3	1	B	7.60	4.0	4.6	0.732	0.086	0.717	3.61	0.620	12.22	12.8	7.30	16.1
4	20	715	151.3	1	B	7.70	4.0	6.6	0.462	0.047	0.515	NA	NA	19.75	11.5	8.30	17.9
4	20	806	152.1	1	B	7.80	4.0	4.4	0.645	0.052	0.564	3.21	0.601	22.57	11.0	8.70	18.1
4	20	908	153.1	1	B	7.80	3.0	3.3	0.633	0.052	0.587	NA	NA	24.45	11.2	7.10	18.2
4	20	1004	154.1	1	B	7.80	3.0	3.0	0.545	0.057	0.588	3.65	1.000	15.99	11.1	7.70	17.8
4	20	1105	155.1	1	B	7.80	4.0	2.7	0.486	0.057	0.569	NA	NA	17.86	11.3	7.80	18.2
4	20	1206	156.1	1	B	7.70	5.0	2.7	0.778	0.067	0.621	2.91	0.590	13.17	12.2	7.60	17.0
4	20	1331	157.5	1	B	7.60	5.0	2.7	1.110	0.086	0.934	NA	NA	15.64	12.1	7.60	16.0
4	20	1509	159.1	1	B	7.70	3.3	2.8	0.644	0.047	0.549	2.68	0.547	19.75	11.5	8.10	18.0
4	20	1640	160.7	1	B	7.70	7.0	2.4	1.150	0.086	0.914	NA	NA	15.64	12.0	7.50	16.0
4	20	1810	162.2	1	B	7.70	5.0	2.4	0.674	0.067	0.677	2.84	0.734	23.51	12.0	8.60	17.0
4	20	1940	163.7	1	B	7.90	7.0	2.2	0.629	0.027	0.542	NA	NA	23.51	11.5	9.60	18.0
4	20	2110	165.2	1	B	8.00	5.0	2.8	0.588	0.058	0.596	1.68	0.506	27.27	11.5	9.50	18.0
4	20	2240	166.7	1	B	8.00	8.0	5.0	0.555	0.058	0.561	NA	NA	26.23	11.5	8.80	18.2
4	21	15	168.3	1	B	8.00	7.0	5.3	0.658	0.048	0.503	3.11	0.540	11.28	11.5	8.60	18.0
4	21	145	169.8	1	B	7.60	5.0	3.2	NA	NA	NA	2.41	0.582	15.99	12.0	7.20	13.0
4	21	315	171.3	1	B	7.60	5.0	4.4	0.761	0.050	0.566	NA	NA	15.99	11.5	7.40	16.6
4	21	445	172.8	1	B	7.80	5.0	3.0	0.457	0.028	0.332	2.41	0.629	22.57	12.2	8.60	16.1
4	21	615	174.3	1	B	7.80	5.0	2.8	0.542	0.038	0.376	NA	NA	NA	12.3	8.80	16.0
4	21	745	175.8	1	B	7.90	7.0	2.4	0.379	0.032	0.394	1.78	0.554	23.04	11.2	9.40	17.9
4	21	840	176.7	1	B	7.80	6.0	1.8	0.406	0.057	0.616	1.98	0.526	31.04	11.0	9.70	18.0
4	21	938	177.6	1	B	7.80	9.0	2.0	0.569	0.055	0.594	2.58	0.583	30.09	11.4	7.20	18.8
4	21	1041	178.7	1	B	7.80	3.0	1.5	0.438	0.068	0.654	2.24	0.590	16.93	11.0	7.50	18.6
4	21	1137	179.6	1	B	7.90	6.0	2.0	0.437	0.038	0.588	2.38	0.606	20.69	11.2	8.00	18.5

946510380

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	21	1240	183.7	1	B	7.80	3.0	2.6	0.748	0.077	0.774	3.75	0.610	9.10	12.0	8.90	15.1
4	21	1412	182.2	1	B	7.80	6.0	2.6	0.649	0.058	0.575	2.61	0.572	15.99	11.7	7.60	16.9
4	21	1505	183.1	1	B	7.80	3.0	2.8	0.615	0.053	0.582	2.34	0.569	20.69	11.2	6.10	18.0
4	21	1610	184.2	1	B	7.70	3.3	2.8	0.624	0.068	0.643	NA	NA	18.81	11.5	7.60	15.5
4	21	1710	185.2	1	B	7.70	4.0	3.4	0.483	0.060	0.644	3.01	0.724	11.13	11.5	8.20	16.2
4	21	1810	186.2	1	B	7.80	4.0	3.4	0.900	0.089	0.687	NA	NA	29.15	12.0	8.60	17.0
4	21	1910	187.2	1	B	7.90	3.0	3.0	0.685	0.063	0.580	NA	NA	14.11	11.2	9.80	17.2
4	21	2010	188.2	1	B	8.00	4.0	2.2	0.487	0.058	0.642	NA	NA	31.04	11.2	NA	18.0
4	21	2110	189.2	1	B	8.00	4.0	5.8	0.536	0.060	0.622	2.54	0.796	9.10	11.0	9.60	18.0
4	21	2210	190.2	1	B	8.10	4.0	3.9	0.486	0.038	0.501	NA	NA	27.27	11.2	10.40	17.5
4	21	2310	191.2	1	B	7.70	5.0	4.1	0.547	0.063	0.672	3.45	0.650	19.75	11.5	10.00	16.8
4	22	15	192.3	1	B	8.00	4.0	3.4	0.451	0.053	0.608	NA	NA	31.04	11.4	9.60	17.0
4	22	115	193.3	1	B	7.90	6.0	4.2	0.473	0.040	0.642	2.74	0.685	13.17	11.9	8.80	16.1
4	22	215	194.3	1	B	7.70	5.0	3.6	0.408	0.018	0.322	NA	NA	14.11	11.9	8.40	14.2
4	22	315	195.3	1	B	7.70	5.0	3.8	0.622	0.038	0.485	2.91	0.702	17.87	11.8	8.30	13.9
4	22	415	196.3	1	B	7.60	5.0	3.8	0.745	0.091	0.909	NA	NA	20.69	11.4	7.80	11.9
4	22	515	197.3	1	B	7.70	6.0	3.4	0.470	0.013	0.487	2.41	0.690	17.87	11.2	7.90	12.1
4	22	615	198.3	1	B	7.70	5.0	3.4	0.462	0.024	0.320	NA	NA	8.43	11.2	7.80	14.5
4	22	715	199.3	1	B	7.90	6.0	3.2	0.476	0.043	0.481	3.75	0.606	31.04	12.0	8.80	16.5
4	22	812	200.2	1	B	7.80	8.0	4.1	0.685	0.065	0.622	NA	NA	48.22	10.9	10.00	18.1
4	22	905	201.1	1	B	7.90	9.0	3.3	0.526	0.048	0.538	2.61	0.611	63.06	10.2	NA	18.2
4	22	1006	202.1	1	B	8.00	10.0	6.0	0.395	0.060	0.621	NA	NA	37.09	10.3	NA	18.2
4	22	1110	203.2	1	B	8.20	8.0	4.1	0.482	0.048	0.561	2.74	0.562	16.93	10.5	9.90	18.2
4	22	1205	204.1	1	B	8.20	10.0	5.2	0.594	0.048	0.575	NA	NA	37.62	10.5	9.40	18.1
4	22	1308	205.1	1	B	7.80	12.0	4.5	0.907	0.086	0.760	3.21	0.693	34.79	11.8	9.00	16.5
4	22	1407	206.1	1	B	7.80	10.0	4.2	0.758	0.074	0.737	3.15	0.735	36.58	11.8	8.40	16.0

946510381

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	22	1510	207.2	1	B	7.80	14.0	5.4	0.944	0.091	0.842	NA	NA	30.09	12.0	8.20	15.1
4	22	1610	208.2	1	B	7.70	15.0	6.6	0.961	0.068	0.741	5.45	1.940	11.28	12.2	7.80	14.0
4	22	1710	209.2	1	B	8.00	13.0	5.6	0.789	0.091	0.959	NA	NA	20.69	12.2	8.80	14.8
4	22	1810	210.2	1	B	7.80	19.0	10.5	0.834	0.074	0.702	3.68	1.100	92.73	12.5	10.60	15.2
4	22	1910	211.2	1	B	8.00	12.0	5.4	0.897	0.091	0.713	NA	NA	28.21	12.0	10.00	16.8
4	22	2010	212.2	1	B	8.00	16.0	5.1	0.680	0.053	0.631	3.01	0.809	77.59	11.5	NA	16.8
4	22	2110	213.2	1	B	8.10	15.0	5.1	0.452	0.048	0.520	NA	NA	\$100.	11.2	10.80	17.5
4	22	2210	214.2	1	B	8.10	17.0	4.5	0.568	0.096	0.793	4.88	0.798	77.09	11.0	9.30	17.5
4	22	2310	215.2	1	B	8.10	15.0	5.4	0.525	0.048	0.564	NA	NA	89.02	11.0	9.00	17.8
4	23	15	216.3	1	B	8.00	23.0	7.6	0.238	0.008	0.294	2.21	0.688	\$129.	11.1	10.90	17.5
4	23	115	217.3	1	B	8.00	8.0	4.5	0.624	0.068	0.627	NA	NA	77.09	11.6	10.20	16.8
4	23	215	218.3	1	B	7.90	8.0	4.4	0.615	0.091	0.764	2.61	0.697	69.06	12.0	8.90	13.6
4	23	315	219.3	1	B	7.80	13.0	4.8	0.734	0.101	0.949	NA	NA	59.35	12.1	8.80	13.0
4	23	415	220.3	1	B	7.80	11.0	5.2	0.609	0.101	0.849	3.55	0.790	66.77	12.5	8.90	14.0
4	23	515	221.3	1	B	7.60	15.0	7.5	0.814	0.089	0.951	NA	NA	40.22	12.0	7.60	14.0
4	23	615	222.3	1	B	7.60	24.0	6.0	0.498	0.008	0.500	4.35	1.260	85.31	11.8	8.20	14.9
4	23	715	223.3	1	B	7.60	28.0	8.1	NA	NA	NA	NA	NA	94.58	11.8	8.90	16.0
4	23	805	224.1	1	B	7.80	19.0	4.8	0.641	0.078	0.676	3.27	0.586	\$107.	11.9	9.50	16.5
4	23	907	225.1	1	B	7.90	27.0	4.8	0.597	0.048	0.542	NA	NA	59.36	11.0	10.20	17.5
4	23	1009	226.1	1	B	8.00	12.0	3.4	0.460	0.058	0.591	3.96	0.381	92.73	11.0	10.20	17.6
4	23	1106	227.1	1	B	8.00	11.0	3.3	0.382	0.070	0.618	NA	NA	81.60	11.0	10.20	17.9
4	23	1205	228.1	1	B	8.00	7.0	2.7	0.376	0.053	0.588	2.16	0.303	74.18	11.0	10.20	17.9
4	23	1310	229.2	1	B	8.00	7.0	3.3	0.529	0.048	0.529	NA	NA	59.35	11.5	9.80	16.1
4	23	1407	230.1	1	B	7.80	10.0	3.8	0.662	0.060	0.509	3.79	0.621	63.06	12.0	8.60	15.0
4	23	1508	231.1	1	B	7.80	11.0	4.1	0.724	0.058	0.583	NA	NA	74.18	11.7	8.80	14.9
4	23	1610	232.2	1	B	7.60	14.0	4.6	0.980	0.091	0.857	4.25	0.535	59.35	11.5	8.40	16.0

946510382

KEARNY POINT - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	23	1710	233.2	1	B	7.70	15.0	4.3	0.820	0.068	0.671	NA	NA	74.18	11.8	8.20	16.0
4	23	1819	234.3	1	B	7.90	11.0	3.4	0.836	0.091	0.946	4.28	0.944	2.69	11.8	8.10	15.2
4	23	1910	235.2	1	B	7.90	11.0	3.6	0.740	0.086	0.677	NA	NA	40.80	12.0	9.20	16.0
4	23	2010	236.2	1	B	8.00	14.0	4.3	0.451	0.058	0.582	3.14	0.427	89.02	11.5	9.80	17.0
4	23	2110	237.2	1	B	8.00	17.0	4.6	0.497	0.058	0.534	NA	NA	85.31	11.0	10.00	17.5
4	23	2210	238.2	1	B	8.00	15.0	7.2	0.472	0.053	0.558	3.08	0.417	92.73	10.8	8.00	17.8
4	23	2310	239.2	1	B	8.00	20.0	7.1	0.559	0.058	0.611	NA	NA	77.89	10.8	8.40	17.8
4	24	15	240.3	1	B	8.00	18.0	4.6	0.407	0.065	0.585	2.75	0.360	89.02	10.9	9.80	17.6
4	24	115	241.3	1	B	7.80	8.0	2.8	0.430	0.060	0.558	NA	NA	74.14	10.6	9.80	18.8
4	24	215	242.3	1	B	7.90	22.0	5.6	0.408	0.058	0.581	2.94	0.375	$100.	11.5	9.60	17.5
4	24	315	243.3	1	B	7.70	9.0	3.0	0.559	0.028	0.596	NA	NA	48.22	11.9	8.80	14.9
4	24	415	244.3	1	B	7.80	15.0	5.4	0.580	0.068	0.722	2.26	0.320	74.18	11.6	8.30	15.1
4	24	515	245.3	1	B	7.80	14.0	5.4	0.685	0.078	0.786	NA	NA	48.21	11.9	7.40	13.8
4	24	615	246.3	1	B	7.60	10.0	3.8	0.572	0.065	0.576	2.33	0.324	70.47	11.0	8.20	17.2
4	24	715	247.3	1	B	7.80	10.0	4.3	0.580	0.091	0.724	NA	NA	74.18	11.3	8.90	16.5
4	24	815	248.3	1	B	7.90	15.0	4.5	0.446	0.058	0.564	3.34	0.445	74.18	11.5	9.30	16.9
		AVERAGE READING				7.68	8.7	5.3	0.824	0.063	0.690	3.33	0.652	35.74	11.6	7.87	15.7

946510383

STØRM #1

JACKSØN STREET

4-14/4-24-81

1/3 DEPTH

946510384

JACKSON STREET - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	947	9.8	2	A	7.40	11.0	3.6	1.340	0.103	1.280	6.24	0.582	15.05	13.0	6.70	4.8
4	14	1245	12.8	2	A	7.30	11.0	2.8	1.240	0.098	1.230	5.62	0.459	12.23	13.0	4.90	3.0
4	14	1550	15.8	2	A	7.40	10.0	2.4	1.370	0.093	1.100	NA	NA	15.99	12.2	6.70	8.0
4	14	1850	18.8	2	A	7.30	10.0	2.2	0.628	0.031	0.809	5.32	0.405	14.11	12.8	6.20	5.8
4	14	2150	21.8	2	A	7.30	13.0	7.5	0.851	0.052	1.040	NA	NA	11.29	13.2	5.80	2.2
4	15	55	24.9	2	A	7.20	15.0	10.2	0.777	0.062	1.180	5.63	0.473	14.11	13.0	6.50	0.0
4	15	400	28.0	2	A	7.30	14.0	7.5	1.410	0.103	1.180	4.77	0.578	15.99	12.2	6.00	5.0
4	15	700	31.0	2	A	7.40	14.0	6.6	1.410	0.109	1.260	NA	NA	26.33	12.2	5.50	4.5
4	15	945	33.8	2	A	7.30	8.0	7.5	1.350	0.134	1.520	4.65	0.517	10.34	12.6	5.30	1.0
4	15	1247	36.8	2	A	7.40	7.0	3.2	1.130	0.124	1.460	NA	NA	17.87	13.0	6.60	0.0
4	15	1544	39.7	2	A	7.30	8.0	3.2	1.200	0.119	1.370	3.23	0.495	10.34	13.0	7.20	1.0
4	15	1844	42.7	2	A	7.40	7.0	7.2	1.200	0.093	1.040	NA	NA	17.87	11.9	6.10	13.5
4	15	2144	45.7	2	A	7.30	14.0	5.8	1.430	0.134	1.420	3.88	0.557	15.99	12.2	6.10	3.0
4	16	45	48.8	2	A	7.30	8.0	11.1	1.280	0.145	1.720	NA	NA	8.93	11.0	6.00	0.1
4	16	345	51.1	2	A	7.30	12.0	3.9	1.520	0.134	1.360	2.61	0.446	17.87	11.8	6.00	4.0
4	16	645	54.8	2	A	7.30	9.0	4.8	0.591	0.010	0.550	NA	NA	15.05	11.8	5.40	10.5
4	16	945	57.8	2	A	7.20	8.0	3.6	1.260	0.145	1.530	3.17	0.465	7.76	12.0	5.60	2.8
4	16	1248	60.8	2	A	7.20	7.0	6.0	1.560	0.176	1.560	NA	NA	10.12	12.0	5.70	0.3
4	16	1546	63.6	2	A	7.30	7.0	5.4	1.630	0.176	1.560	3.28	0.458	8.77	13.0	5.50	1.0
4	16	1850	66.8	2	A	7.30	9.0	7.5	1.560	0.117	1.150	4.51	0.845	12.14	12.1	5.80	11.9
4	16	2150	69.8	2	A	7.20	8.0	5.0	1.380	0.076	0.994	NA	NA	9.78	12.1	5.10	4.2
4	17	45	72.8	2	A	7.30	11.0	7.4	1.760	0.137	1.460	4.59	0.628	7.08	12.0	6.00	0.5
4	17	345	75.8	2	A	7.30	8.0	5.0	1.760	0.157	1.550	NA	NA	6.41	12.0	5.70	1.0
4	17	645	78.8	2	A	7.30	8.0	4.5	1.480	0.132	1.160	5.61	0.574	9.10	12.0	5.20	8.0
4	17	1026	82.4	2	A	7.20	7.0	4.5	1.790	0.152	1.390	NA	NA	14.11	12.0	5.50	4.0
4	17	1319	85.3	2	A	7.30	17.0	4.6	1.690	0.127	1.490	4.69	0.625	13.17	12.0	7.00	0.5

94651038S

JACKSON STREET - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	17	1611	88.2	2	A	7.30	9.0	4.6	1.510	0.097	1.130	NA	NA	11.29	11.9	7.00	1.0
4	17	1911	91.2	2	A	7.10	8.0	5.0	1.300	0.086	0.814	4.33	0.542	25.39	11.9	6.30	9.2
4	17	2211	94.2	2	A	7.20	8.0	4.8	1.670	0.127	1.250	NA	NA	17.87	11.9	5.80	5.0
4	18	105	97.1	2	A	7.30	12.0	6.2	1.640	0.132	1.410	4.34	0.694	16.93	11.8	7.00	1.0
4	18	405	100.1	2	A	7.30	11.0	4.1	1.600	0.117	1.340	NA	NA	10.35	11.8	7.30	0.8
4	18	705	103.1	2	A	7.30	12.0	6.3	1.530	0.117	1.080	4.25	0.538	35.74	11.8	6.30	11.0
4	18	1011	106.2	2	A	7.30	10.0	4.2	0.740	0.020	0.702	NA	NA	13.17	12.0	6.60	6.0
4	18	1311	109.2	2	A	7.30	14.0	5.1	1.470	0.097	1.020	3.39	0.522	7.98	12.0	7.10	1.0
4	18	1625	112.4	2	A	7.30	10.0	4.5	1.510	0.107	1.220	NA	NA	9.41	13.0	7.90	1.0
4	18	1908	115.1	2	A	7.30	10.0	3.6	0.895	0.036	0.487	3.04	0.368	14.11	12.0	7.20	8.0
4	18	2201	118.0	2	A	7.30	10.0	3.4	0.927	0.020	0.649	NA	NA	17.87	12.2	7.10	6.8
4	19	110	121.2	2	A	7.30	18.0	4.3	1.430	0.107	1.220	3.94	0.533	15.05	13.0	6.80	2.0
4	19	410	124.2	2	A	7.30	12.0	4.5	1.370	0.097	1.120	NA	NA	8.77	12.5	6.60	1.5
4	19	705	127.1	2	A	7.30	11.0	6.0	1.410	0.061	0.656	5.47	0.862	16.93	12.0	6.70	9.0
4	19	1007	130.1	2	A	7.30	8.0	2.8	1.160	0.107	1.140	3.99	0.595	7.05	12.0	6.80	7.5
4	19	1307	133.1	2	A	7.30	10.0	5.0	1.280	0.074	1.220	NA	NA	10.01	13.0	7.30	2.0
4	19	1608	136.1	2	A	7.30	12.0	3.8	1.280	0.097	1.200	3.35	0.396	7.76	13.0	6.90	2.0
4	19	1904	139.1	2	A	7.40	9.0	4.2	1.400	0.032	0.405	NA	NA	27.27	13.0	8.00	8.0
4	19	2208	142.1	2	A	7.50	8.0	2.8	1.260	0.087	0.943	2.86	0.420	8.16	12.5	7.40	8.0
4	20	115	145.3	2	A	7.40	8.0	8.7	1.140	0.052	0.778	NA	NA	4.38	13.0	6.50	4.0
4	20	405	148.1	2	A	7.40	8.0	6.4	1.030	0.092	1.130	2.87	0.397	3.72	13.0	5.00	1.5
4	20	705	151.1	2	A	7.40	9.0	4.5	1.420	0.087	0.828	NA	NA	6.74	12.5	5.70	9.0
4	20	1006	154.1	2	A	7.40	7.0	5.0	0.829	0.097	1.030	3.16	0.601	4.72	12.5	6.70	9.0
4	20	1307	157.1	2	A	7.30	10.0	5.7	1.180	0.107	1.160	3.21	0.545	4.38	13.2	6.70	4.0
4	20	1610	160.2	2	A	7.40	9.0	7.2	1.680	0.092	1.140	NA	NA	4.38	13.2	7.20	1.8
4	20	1910	163.2	2	A	7.40	8.0	2.8	1.210	0.097	0.973	2.45	0.485	4.38	13.0	7.40	6.8

946510386

JACKSON STREET - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	20	2210	166.2	2	A	7.50	7.0	2.7	1.160	0.097	0.943	2.10	0.370	8.43	12.0	7.40	9.0
4	21	105	169.1	2	A	7.40	8.0	2.6	0.857	0.102	1.130	NA	NA	8.76	12.0	6.80	5.0
4	21	405	172.1	2	A	7.30	12.0	2.7	0.934	0.107	1.220	2.53	0.451	9.77	12.2	6.30	2.2
4	21	705	175.1	2	A	7.50	15.0	2.7	1.190	0.047	0.639	NA	NA	10.11	11.2	9.40	7.0
4	21	1014	178.2	2	A	7.50	5.0	2.7	1.240	0.057	0.633	1.90	0.285	5.39	11.7	8.10	6.0
4	21	1316	181.3	2	A	7.40	5.0	2.8	1.230	0.102	1.100	3.36	0.452	9.10	12.5	8.00	5.5
4	21	1615	184.3	2	A	7.40	5.0	3.3	1.140	0.107	1.180	NA	NA	6.41	13.1	6.20	3.2
4	21	1915	187.3	2	A	7.50	5.0	3.2	1.250	0.102	1.010	2.59	0.426	7.76	12.5	7.30	6.0
4	21	2215	190.3	2	A	7.60	4.0	3.3	0.931	0.077	0.741	NA	NA	14.11	11.5	7.60	11.2
4	22	105	193.1	2	A	7.50	6.0	2.8	0.809	0.028	0.381	2.15	0.341	8.43	12.0	6.40	8.0
4	22	410	196.2	2	A	7.40	11.0	2.6	0.988	0.037	0.729	NA	NA	5.73	12.5	6.40	4.0
4	22	710	199.2	2	A	7.40	6.0	2.2	1.120	0.097	0.953	2.91	0.483	9.44	12.0	6.90	6.0
4	22	1007	202.1	2	A	7.60	8.0	4.6	0.591	0.016	0.511	2.67	0.543	40.80	12.0	7.40	13.0
4	22	1306	205.1	2	A	7.50	9.0	4.6	1.150	0.053	0.827	NA	NA	11.46	13.0	7.70	8.8
4	22	1610	208.2	2	A	7.40	10.0	4.5	1.150	0.089	1.220	2.03	0.370	41.38	13.0	7.00	4.5
4	22	1910	211.2	2	A	7.50	9.0	4.5	1.130	0.089	1.190	NA	NA	28.97	12.8	8.10	5.5
4	22	2210	214.2	2	A	7.60	10.0	5.1	1.070	0.063	0.853	2.29	0.412	41.38	12.1	7.90	10.0
4	23	115	217.3	2	A	7.60	12.0	6.4	1.090	0.068	0.972	2.67	0.435	60.21	11.5	7.50	8.5
4	23	410	220.2	2	A	7.40	10.0	6.6	1.110	0.084	1.250	NA	NA	64.14	12.5	7.10	4.3
4	23	710	223.2	2	A	7.40	17.0	8.7	1.110	0.094	1.150	3.13	0.466	48.22	13.0	6.70	4.8
4	23	1008	226.1	2	A	7.40	17.0	5.2	1.220	0.074	0.891	NA	NA	40.80	12.0	7.40	11.8
4	23	1307	229.1	2	A	7.40	9.0	3.6	1.200	0.074	0.996	3.03	0.497	25.67	12.0	7.20	9.0
4	23	1609	232.1	2	A	7.40	12.0	3.7	1.150	0.089	1.250	NA	NA	21.63	12.5	6.30	4.8
4	23	1909	235.1	2	A	7.30	19.0	4.1	1.200	0.089	1.210	2.71	0.412	10.75	12.5	6.80	5.0
4	23	2209	238.1	2	A	7.50	11.0	4.5	1.110	0.074	0.851	NA	NA	NA	12.0	7.20	13.6
4	24	110	241.2	2	A	7.40	12.0	4.1	0.926	0.037	0.694	3.42	0.428	NA	12.5	6.50	9.0

946510387

JACKSON STREET - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	24	41[illegible]	244.2	2	A	7.36	17.0	6.3	1.220	0.084	1.220	NA	NA	29.15	12.5	6.60	5.0
4	24	71[illegible]	247.2	2	A	7.36	12.0	5.1	1.220	0.084	1.220	2.92	0.435	18.81	12.7	6.30	4.4
		AVERAGE READING				7.36	9.9	4.8	1.237	0.091	1.080	3.57	0.498	15.88	12.3	6.71	5.3

946510388

STØRM #1

JACKSØN STREET

4-14/4-24-81

2/3 DEPTH

946510389

JACKSON STREET - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	940	9.7	2	B	7.40	11.0	4.5	1.320	0.134	0.886	3.64	0.736	19.28	13.0	6.70	5.8
4	14	1238	12.6	2	B	7.30	11.0	5.7	1.540	0.134	0.876	3.22	0.566	22.57	13.0	6.30	8.0
4	14	1544	15.7	2	B	7.40	10.0	5.8	1.400	0.134	0.886	NA	NA	27.27	12.2	6.80	8.0
4	14	1844	18.7	2	B	7.40	9.0	5.4	1.320	0.124	0.829	4.07	0.555	28.22	12.0	6.50	12.0
4	14	2144	21.7	2	B	7.30	17.0	7.3	1.360	0.114	1.300	NA	NA	30.10	13.0	6.00	4.5
4	15	100	25.0	2	B	7.30	15.0	6.2	1.320	0.129	1.500	2.67	0.475	14.11	13.0	6.00	0.2
4	15	405	28.1	2	B	7.20	16.0	5.8	1.010	0.124	0.999	NA	NA	26.33	12.5	6.00	6.5
4	15	705	31.1	2	B	7.30	13.0	5.8	1.210	0.072	0.810	NA	NA	59.25	12.5	5.40	4.8
4	15	939	33.6	2	B	7.20	9.0	7.8	1.320	0.103	1.120	4.47	0.732	17.87	12.2	5.40	1.0
4	15	1240	36.7	2	B	7.20	7.0	4.4	1.480	0.072	0.853	NA	NA	10.34	13.0	6.50	0.0
4	15	1539	39.6	2	B	7.30	7.0	4.2	1.340	0.134	1.380	4.00	0.586	17.87	13.0	6.90	2.0
4	15	1839	42.6	2	B	7.40	5.0	4.5	1.190	0.067	0.695	NA	NA	34.79	11.7	6.20	15.0
4	15	2139	45.6	2	B	7.30	10.0	5.0	1.360	0.103	1.110	3.30	0.758	29.15	12.2	6.00	3.5
4	16	50	48.8	2	B	7.30	7.0	3.8	1.480	0.166	1.650	NA	NA	7.52	12.0	6.00	0.1
4	16	355	51.9	2	B	7.30	12.0	10.6	1.290	0.072	0.801	3.68	1.230	9.40	11.8	5.90	4.8
4	16	650	54.8	2	B	7.40	8.0	11.2	2.540	0.093	0.852	NA	NA	32.92	11.8	5.60	13.8
4	16	939	57.6	2	B	7.30	8.0	8.7	2.250	0.093	0.996	4.17	0.761	15.05	12.0	6.10	3.0
4	16	1241	60.7	2	B	7.30	7.0	5.0	1.600	0.171	1.520	NA	NA	18.81	12.2	6.10	0.5
4	16	1540	63.7	2	B	7.20	12.0	5.4	1.660	0.166	1.500	5.60	0.622	9.44	13.0	5.70	1.0
4	16	1838	66.6	2	B	7.40	8.0	5.7	1.220	0.086	0.726	4.04	0.743	12.69	11.8	6.60	14.0
4	16	2138	69.6	2	B	7.30	8.0	5.1	1.740	0.152	1.210	NA	NA	10.34	12.1	5.20	4.0
4	17	50	72.8	2	B	7.20	13.0	11.1	1.780	0.157	1.360	5.14	0.778	14.11	12.0	5.30	0.5
4	17	35	75.7	2	B	7.20	9.0	6.2	1.670	0.122	1.470	NA	NA	8.46	12.0	5.70	1.0
4	17	65	78.9	2	B	7.40	9.0	6.3	1.230	0.086	0.851	5.02	0.758	15.05	12.0	5.60	12.0
4	17	1020	82.3	2	B	7.30	6.0	7.8	1.770	0.147	1.230	NA	NA	32.92	12.0	5.30	4.0
4	17	1313	85.2	2	B	7.30	8.0	4.6	1.700	0.137	1.380	3.94	0.643	15.99	12.0	7.00	0.5

946510390

JACKSON STREET - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	17	1606	88.1	2	B	7.20	7.0	8.2	1.700	0.112	1.200	NA	NA	74.18	11.8	7.10	1.0
4	17	1906	91.1	2	B	7.20	6.0	3.9	1.330	0.112	0.908	4.05	0.581	33.86	11.5	6.00	11.5
4	17	2206	94.1	2	B	7.20	7.0	5.2	1.430	0.117	0.953	NA	NA	39.50	11.9	6.20	5.5
4	18	110	97.2	2	B	7.30	8.0	4.6	1.230	0.071	1.220	4.29	0.659	16.93	11.8	7.10	1.0
4	18	410	100.2	2	B	7.20	8.0	4.5	1.630	0.117	1.200	NA	NA	17.87	11.8	7.10	1.0
4	18	710	103.2	2	B	7.30	8.0	4.2	1.290	0.117	0.893	3.89	0.551	38.56	11.8	6.60	13.0
4	18	1006	106.1	2	B	7.40	12.0	4.4	1.030	0.107	0.913	NA	NA	14.11	12.0	6.40	6.0
4	18	1305	109.1	2	B	7.30	11.0	5.4	1.280	0.056	1.060	3.87	0.644	8.90	12.0	7.10	1.0
4	18	1620	112.3	2	B	7.20	17.0	5.0	1.540	0.117	1.120	NA	NA	12.23	13.0	7.90	2.0
4	18	1900	115.0	2	B	7.30	8.0	4.8	0.660	NA	NA	2.48	0.451	25.39	12.0	7.00	13.0
4	18	2155	117.9	2	B	7.40	7.0	3.8	0.748	0.026	0.598	NA	NA	21.63	12.3	7.00	7.3
4	19	115	121.3	2	B	7.40	16.0	5.8	1.390	0.107	1.080	3.65	0.648	19.80	13.0	6.80	2.0
4	19	415	124.3	2	B	7.30	2.0	7.6	0.764	0.031	0.400	NA	NA	17.87	12.5	6.60	2.0
4	19	715	127.2	2	B	7.30	24.0	10.6	2.180	0.066	0.744	4.92	1.190	33.86	12.0	6.70	10.0
4	19	1001	130.0	2	B	7.40	8.0	5.2	2.280	0.097	0.839	4.25	0.873	14.47	12.0	6.40	9.8
4	19	1302	133.0	2	B	7.40	11.0	3.6	1.290	0.096	1.340	NA	NA	14.47	13.0	7.30	2.0
4	19	1600	136.0	2	B	7.30	17.0	6.9	1.730	0.071	0.888	3.02	0.619	27.27	12.5	6.40	7.0
4	19	1855	138.9	2	B	7.40	18.0	4.5	1.230	0.066	0.771	NA	NA	30.10	13.0	7.90	10.0
4	19	2200	142.0	2	B	7.60	10.0	3.0	0.836	0.016	0.415	4.39	1.230	49.08	12.5	7.10	11.0
4	20	120	145.3	2	B	7.30	9.0	3.9	0.834	0.026	0.485	NA	NA	7.08	13.0	6.30	4.0
4	20	410	148.2	2	B	7.30	8.0	2.8	1.260	0.096	1.320	2.70	0.526	4.05	13.0	5.50	4.0
4	20	710	151.2	2	B	7.40	13.0	3.0	1.030	0.056	0.680	NA	NA	8.43	12.5	5.80	10.0
4	20	1006	154.1	2	B	7.40	7.0	1.8	0.865	0.016	0.750	2.84	0.528	4.38	12.5	6.30	13.0
4	20	1301	157.0	2	B	7.30	8.0	2.4	1.290	0.096	1.250	3.01	0.589	10.45	13.2	6.70	4.0
4	20	1605	160.1	2	B	7.30	9.0	2.4	1.200	0.096	1.330	2.74	0.460	10.34	13.2	5.80	2.2
4	20	1905	163.1	2	B	7.50	16.0	4.5	1.060	0.071	0.818	NA	NA	17.87	12.8	7.20	6.8

946510391

JACKSON STREET - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	20	2205	166.1	2	B	7.60	6.0	2.4	1.050	0.066	0.847	1.76	0.375	12.23	12.0	7.40	9.0
4	21	110	169.2	2	B	7.50	8.0	3.2	1.100	0.087	0.835	NA	NA	16.93	12.2	6.80	5.0
4	21	410	172.2	2	B	7.40	11.0	2.8	1.150	0.091	1.400	2.37	0.418	11.29	12.0	7.60	7.0
4	21	710	175.2	2	B	7.50	9.0	4.5	1.000	0.066	0.931	NA	NA	24.45	12.0	9.20	10.0
4	21	1005	178.1	2	B	7.60	6.0	3.2	1.030	0.087	0.767	1.84	0.425	11.80	11.7	8.80	16.0
4	21	1308	181.1	2	B	7.40	7.0	3.4	1.070	0.071	0.989	2.67	0.474	12.81	13.0	7.10	6.0
4	21	1608	184.1	2	B	7.40	9.0	3.9	0.712	0.026	0.447	NA	NA	18.81	13.1	6.30	4.0
4	21	1908	187.1	2	B	7.50	12.0	4.4	1.040	0.071	0.824	3.42	1.020	48.22	12.3	7.40	7.5
4	21	2208	190.1	2	B	7.70	5.0	3.4	1.000	0.071	0.939	NA	NA	63.06	11.7	8.20	13.0
4	22	110	193.2	2	B	7.60	7.0	4.8	1.010	0.071	0.926	1.82	0.403	32.09	12.0	6.30	8.5
4	22	415	196.3	2	B	7.50	8.0	5.0	0.789	0.046	0.654	NA	NA	28.88	12.5	6.20	5.0
4	22	715	199.3	2	B	7.60	15.0	4.8	1.130	0.066	0.893	3.39	1.050	77.89	12.0	6.90	6.5
4	22	1002	202.0	2	B	7.50	8.0	5.0	0.934	0.063	0.801	2.50	0.551	44.51	12.0	7.60	14.0
4	22	1300	205.0	2	B	7.50	10.0	5.4	1.050	0.074	0.966	NA	NA	43.45	13.0	7.60	9.0
4	22	1600	208.0	2	B	7.40	12.0	6.8	0.856	0.042	0.799	2.92	0.471	57.95	12.8	6.60	5.5
4	22	1900	211.0	2	B	7.40	15.0	7.1	0.582	0.074	1.010	NA	NA	76.56	12.8	8.20	7.5
4	22	2200	214.0	2	B	7.60	13.0	5.0	0.993	0.068	0.834	2.52	0.526	44.51	12.0	8.90	13.0
4	23	135	217.6	2	B	7.40	32.0	8.0	1.540	0.079	0.991	5.04	1.260	NA	11.5	7.60	9.0
4	23	415	220.3	2	B	7.40	13.0	6.6	1.210	0.094	1.230	NA	NA	NA	12.9	7.50	4.5
4	23	715	223.3	2	B	7.40	14.0	7.5	1.130	0.084	1.030	3.15	0.586	NA	12.8	6.70	5.0
4	23	1002	226.1	2	B	7.30	30.0	6.0	1.090	0.074	0.865	5.04	1.260	31.98	12.0	7.50	12.0
4	23	1301	229.0	2	B	7.40	12.0	3.6	2.740	0.068	0.841	3.17	0.616	22.57	12.0	7.20	12.5
4	23	1601	232.0	2	B	7.40	15.0	4.8	1.150	0.084	1.140	NA	NA	23.51	12.5	6.50	6.0
4	23	1901	235.1	2	B	7.40	18.0	8.6	1.110	0.074	0.986	2.64	0.513	29.15	12.5	7.20	6.5
4	23	2201	238.1	2	B	7.60	13.0	4.1	0.934	0.063	0.718	NA	NA	33.86	12.0	8.00	15.0
4	24	115	241.3	2	B	7.60	10.0	5.1	0.699	0.037	0.559	2.66	0.442	37.62	12.0	7.30	15.5

94610392

JACKSON STREET - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O• [PPM]	SAL [PPT]
4	24	415	244.3	2	B	7.40	19.0	8.1	1.090	0.079	1.040	NA	NA	33.38	12.5	6.70	5.0
4	24	715	247.3	2	B	7.56	30.0	8.9	0.973	0.068	0.837	4.05	0.888	70.47	12.6	6.20	8.0
		AVERAGE READING				7.37	11.2	5.4	1.277	0.089	0.975	3.51	0.684	26.24	12.3	6.71	6.7

946510393

STØRM #1

BELLEVILLE TURNPIKE

4-14/4-24-81

1/3 DEPTH

946510394

BELLEVILLE TPK - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	14	844	8.7	3	A	7.40	12.0	5.6	1.370	0.145	1.590	2.91	0.785	15.05	14.0	6.20	0.0
4	14	1152	11.9	3	A	7.40	11.0	4.2	1.340	0.150	1.600	NA	NA	15.99	13.8	7.40	0.0
4	14	1451	14.8	3	A	7.30	13.0	9.8	NA	0.142	1.640	2.97	0.813	27.27	13.7	6.40	0.0
4	14	1751	17.8	3	A	7.30	13.0	7.5	1.410	0.134	1.530	NA	NA	20.69	13.5	5.90	0.0
4	14	2051	20.8	3	A	7.30	14.0	6.3	1.410	0.145	1.590	2.70	0.843	29.16	13.3	6.60	0.0
4	14	2351	23.8	3	A	7.40	12.0	5.6	1.340	0.155	1.670	NA	NA	24.45	13.2	8.00	0.0
4	15	250	26.8	3	A	7.40	12.0	6.2	1.070	0.124	1.650	NA	NA	15.05	12.8	7.50	0.0
4	15	545	29.8	3	A	7.30	13.0	7.2	1.370	0.145	1.570	2.02	0.544	47.21	12.5	8.00	0.0
4	15	849	32.8	3	A	7.30	6.0	7.2	1.450	0.166	1.670	NA	NA	18.81	12.0	6.40	0.0
4	15	1147	35.8	3	A	7.30	7.0	6.4	1.500	0.160	1.620	2.20	0.568	14.11	12.1	7.10	0.0
4	15	1449	38.8	3	A	7.30	9.0	9.3	1.370	NA	NA	NA	NA	12.23	12.5	6.70	0.0
4	15	1749	41.8	3	A	7.30	8.0	7.5	1.220	0.134	1.530	2.38	0.777	20.69	12.3	6.70	0.0
4	15	2049	44.8	3	A	7.30	12.0	7.6	1.610	0.155	1.590	NA	NA	21.63	12.0	6.80	0.0
4	15	2349	47.8	3	A	7.20	13.0	11.6	1.520	0.166	1.620	2.85	0.857	13.17	11.0	7.00	0.0
4	16	250	50.8	3	A	7.30	10.0	10.3	1.520	0.166	1.620	NA	NA	8.41	11.0	6.80	0.0
4	16	545	53.8	3	A	7.20	9.0	8.1	1.260	1.150	1.560	2.26	0.550	13.17	11.2	6.00	0.0
4	16	848	56.8	3	A	7.40	6.0	5.8	1.670	0.176	1.620	NA	NA	10.38	11.0	6.40	0.0
4	16	1149	59.8	3	A	7.50	12.0	8.8	1.440	0.110	1.600	NA	NA	12.41	12.2	9.90	0.0
4	16	1450	62.8	3	A	7.40	9.0	7.4	1.460	0.121	1.600	2.14	0.561	12.41	12.0	8.00	0.0
4	16	1750	65.8	3	A	7.30	10.0	8.1	1.770	0.147	1.450	NA	NA	22.76	12.0	7.20	0.0
4	16	2050	68.8	3	A	7.40	11.0	5.2	1.770	0.127	1.400	3.12	0.633	18.62	12.1	6.00	0.0
4	16	2350	71.8	3	A	7.40	11.0	6.3	1.570	0.117	1.340	NA	NA	22.76	11.8	7.40	0.0
4	17	250	74.8	3	A	7.40	12.0	5.2	1.530	0.122	1.320	2.55	0.497	9.64	12.0	8.40	0.0
4	17	545	77.8	3	A	7.40	12.0	5.0	1.550	0.076	1.230	NA	NA	35.17	11.8	7.00	0.0
4	17	845	80.8	3	A	7.30	6.0	3.3	1.580	0.017	1.420	3.03	0.519	11.38	11.5	7.80	0.0
4	17	1136	83.6	3	A	7.40	7.0	3.8	1.530	0.117	1.290	NA	NA	16.55	12.0	9.40	0.0

946510395

BELLEVILLE TPK - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	17	1435	86.6	3	A	7.40	10.0	3.9	1.470	0.117	1.270	2.44	0.624	15.52	12.0	9.10	0.0
4	17	1650	88.8	3	A	7.40	13.0	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
4	17	1735	89.6	3	A	7.30	8.0	6.9	1.580	0.117	1.290	NA	NA	26.90	11.9	8.50	0.0
4	17	2035	92.6	3	A	7.30	12.0	3.2	1.560	0.092	1.100	2.55	0.435	10.35	11.5	7.60	0.0
4	17	2335	95.6	3	A	7.30	12.0	4.6	1.430	0.112	1.220	NA	NA	21.73	11.9	8.20	0.0
4	18	230	98.5	3	A	7.30	13.0	4.4	1.140	0.086	1.340	3.39	0.559	15.52	12.0	8.00	0.0
4	18	530	101.5	3	A	7.30	10.0	6.2	1.450	0.122	1.250	NA	NA	22.76	12.0	8.00	0.0
4	18	837	104.6	3	A	7.50	12.0	4.5	1.480	0.117	1.230	2.44	0.516	6.75	12.0	7.60	0.0
4	18	1137	107.6	3	A	7.30	13.0	9.4	1.210	0.097	1.160	NA	NA	7.36	12.0	9.60	0.0
4	18	1436	110.6	3	A	7.50	22.0	6.0	1.030	0.086	1.250	3.08	0.626	10.35	13.0	9.40	0.0
4	18	1738	113.6	3	A	7.40	23.0	4.6	1.200	0.097	1.130	NA	NA	13.50	13.1	9.30	0.0
4	18	2037	116.6	3	A	7.30	11.0	4.2	1.340	0.107	1.200	2.14	0.403	4.29	13.0	8.00	0.0
4	18	2345	119.8	3	A	7.30	12.0	5.6	1.230	0.092	1.140	NA	NA	7.06	13.0	8.10	0.0
4	19	230	122.5	3	A	7.40	17.0	6.6	1.130	0.102	1.180	1.84	0.750	9.20	12.5	8.00	0.0
4	19	530	125.5	3	A	7.30	24.0	6.9	1.160	0.092	1.130	2.38	0.874	7.06	12.5	7.80	0.0
4	19	835	128.6	3	A	7.30	10.0	3.3	1.080	0.097	1.240	2.32	0.445	8.53	12.8	7.50	0.0
4	19	1138	131.6	3	A	7.30	17.0	3.8	1.050	0.107	1.250	NA	NA	12.61	13.0	7.70	0.0
4	19	1435	134.6	3	A	7.40	10.0	2.8	0.964	0.107	1.250	1.60	0.469	8.16	13.8	9.00	0.0
4	19	1738	137.6	3	A	7.40	17.0	4.8	0.837	0.087	1.000	2.67	0.625	5.21	13.2	8.10	0.0
4	19	2045	140.8	3	A	7.30	12.0	5.0	1.150	0.052	0.665	NA	NA	17.59	13.2	7.20	1.0
4	19	2343	143.5	3	A	7.30	16.0	4.5	0.922	0.072	1.130	NA	NA	13.45	13.0	7.56	0.0
4	20	235	146.6	3	A	7.50	11.0	2.6	1.030	0.102	1.400	2.44	0.788	37.24	14.0	7.10	0.0
4	20	530	149.5	3	A	7.40	18.0	2.2	1.020	0.116	1.260	NA	NA	26.89	14.0	7.80	0.0
4	20	834	152.6	3	A	7.30	12.0	2.6	1.050	0.082	1.180	3.18	0.541	35.17	13.2	6.40	0.2
4	21	1136	155.6	3	A	7.30	11.0	2.2	1.050	0.107	1.200	2.20	0.449	26.89	13.5	7.30	0.0
4	21	1437	158.6	3	A	7.40	16.0	2.6	1.080	0.116	1.190	2.32	0.690	20.69	14.0	7.50	0.0

5465103 96

BELLEVILLE TPK - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	20	1740	161.7	3	A	7.40	13.0	2.1	1.030	0.126	1.270	NA	NA	25.83	13.8	7.60	0.2
4	20	2040	164.7	3	A	7.30	11.0	2.8	1.140	0.116	1.180	2.20	0.506	28.98	13.2	6.30	1.0
4	20	2340	167.7	3	A	7.30	12.0	2.8	1.110	0.116	1.220	NA	NA	21.72	13.2	6.80	0.2
4	21	235	170.6	3	A	7.40	17.0	2.7	1.040	0.126	1.300	2.05	0.980	60.19	13.0	8.30	0.0
4	21	535	173.6	3	A	7.40	16.0	3.8	1.030	0.126	1.310	NA	NA	48.15	12.5	8.50	0.1
4	21	938	176.6	3	A	7.40	12.0	4.8	1.180	0.126	1.220	2.44	0.515	21.72	13.0	NA	0.6
4	21	1141	179.7	3	A	7.40	7.0	6.8	1.150	0.126	1.260	NA	NA	22.99	13.0	NA	0.2
4	21	1439	182.6	3	A	7.40	17.0	7.5	0.992	0.126	1.330	1.72	0.629	28.97	13.5	9.40	0.0
4	21	1740	185.7	3	A	7.50	11.0	6.6	0.998	0.126	1.340	NA	NA	51.73	13.5	7.70	0.0
4	21	2040	188.7	3	A	7.30	19.0	5.1	1.190	0.116	1.150	2.64	0.820	33.10	12.8	6.10	3.0
4	21	2340	191.7	3	A	7.40	13.0	4.5	1.130	0.126	1.250	NA	NA	24.83	12.5	6.60	1.0
4	22	230	194.5	3	A	7.40	18.0	6.3	1.030	0.116	1.230	NA	NA	59.31	13.0	6.90	0.2
4	22	530	197.5	3	A	7.50	13.0	5.7	1.000	0.126	1.370	1.60	0.523	33.10	12.5	7.40	0.0
4	22	836	200.6	3	A	7.40	26.0	10.2	1.110	0.105	1.360	3.03	0.874	33.11	12.5	7.00	1.8
4	22	1136	203.6	3	A	7.40	10.0	9.6	1.070	0.105	1.380	NA	NA	21.73	13.0	7.50	1.0
4	22	1437	206.6	3	A	7.40	17.0	9.0	1.020	0.116	1.590	2.17	0.639	33.11	14.0	7.90	0.0
4	22	1737	209.6	3	A	7.50	14.0	8.6	1.020	0.116	1.660	NA	NA	33.11	13.2	9.00	0.0
4	22	2037	212.6	3	A	7.30	9.0	9.2	1.110	0.105	1.380	2.55	0.558	24.83	13.0	7.10	1.3
4	22	2337	215.6	3	A	7.30	9.0	9.2	1.000	0.084	1.380	NA	NA	28.97	12.9	6.80	1.2
4	23	230	218.5	3	A	7.40	35.0	9.3	1.020	0.105	1.520	3.24	0.925	41.38	13.0	8.60	0.1
4	23	530	221.5	3	A	7.60	17.0	6.8	0.926	0.110	1.640	NA	NA	55.80	12.2	9.00	0.1
4	23	837	224.6	3	A	7.40	21.0	5.4	1.090	0.105	1.460	2.85	0.634	26.89	13.0	7.20	1.0
4	23	1136	227.6	3	A	7.40	10.0	3.9	1.070	0.105	1.440	NA	NA	22.76	13.1	6.40	1.2
4	23	1436	230.6	3	A	7.40	16.0	5.2	1.070	0.110	1.570	3.33	0.562	31.04	13.0	8.60	0.0
4	23	1741	233.7	3	A	7.60	15.0	5.0	1.000	0.115	1.660	NA	NA	41.38	12.0	9.10	0.0
4	23	2041	236.7	3	A	7.40	21.0	8.0	1.110	0.094	1.410	4.05	0.691	18.62	12.6	7.70	1.5

94651039?

BELLEVILLE TPK - LEVEL A - 1/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	23	2341	239.7	3	A	7.30	10.0	4.8	0.951	0.105	1.440	NA	NA	45.52	12.8	6.10	1.0
4	24	230	242.5	3	A	7.30	15.0	8.0	1.090	0.105	1.520	2.14	0.550	26.89	12.5	7.70	0.0
4	24	530	245.5	3	A	7.50	17.0	4.6	0.907	0.115	1.720	NA	NA	41.38	12.5	9.50	0.
4	24	800	248.0	3	A	7.50	20.0	8.7	0.888	0.105	1.640	1.87	0.608	45.52	12.3	8.90	0.0
		AVERAGE READING				7.37	13.3	6.0	1.221	0.128	1.377	2.52	0.637	23.61	12.7	7.63	0.2

946510398

STØRM #1

BELLEVILLE TURNPIKE

4-14/4-24-81

2/3 DEPTH

946510399

BELLEVILLE TPK - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	14	850	8.8	3	B	7.40	12.0	6.2	1.440	0.141	1.830	2.61	0.723	37.62	14.0	6.20	0.0
4	14	1145	11.8	3	B	7.40	11.0	5.0	1.330	0.146	1.720	NA	NA	30.10	13.8	7.40	0.0
4	14	1444	14.7	3	B	7.30	13.0	11.1	1.360	0.126	1.540	3.15	0.814	33.74	13.2	6.70	0.0
4	14	1744	17.7	3	B	7.30	13.0	7.1	1.400	0.136	1.590	NA	NA	25.39	13.6	6.20	0.0
4	14	2044	20.7	3	B	7.30	12.0	5.4	1.360	0.095	1.300	2.50	0.677	24.45	13.2	6.80	0.0
4	14	2344	23.7	3	B	7.40	11.0	6.2	1.290	0.156	1.820	3.30	0.770	20.69	13.2	7.80	0.0
4	15	255	26.9	3	B	7.40	12.0	8.0	1.360	0.156	1.820	2.79	0.709	24.45	12.8	7.80	0.0
4	15	550	29.8	3	B	7.30	12.0	4.3	1.320	0.156	1.720	2.91	0.591	18.81	12.8	7.00	0.0
4	15	841	32.7	3	B	7.30	7.0	7.2	1.480	0.166	1.790	NA	NA	20.69	12.0	6.40	0.0
4	15	1140	35.7	3	B	7.30	7.0	6.3	1.340	0.156	1.690	NA	NA	15.99	12.2	7.10	0.0
4	15	1442	38.7	3	B	7.30	7.0	8.2	1.660	0.187	1.640	2.73	0.571	14.11	13.0	5.90	0.0
4	15	1742	41.7	3	B	7.30	8.0	6.2	1.480	0.146	1.610	NA	NA	19.75	12.2	6.90	0.0
4	15	2042	44.7	3	B	7.30	18.0	7.3	1.640	0.095	1.200	2.67	0.814	23.51	12.0	7.00	0.0
4	15	2342	47.7	3	B	7.20	23.0	11.1	1.600	0.166	1.700	NA	NA	24.45	11.0	7.10	0.0
4	16	255	50.9	3	B	7.20	11.0	10.2	1.600	0.177	1.740	2.85	0.796	10.34	11.0	6.80	0.1
4	16	550	53.8	3	B	7.20	10.0	6.8	1.600	0.075	0.870	3.24	0.539	13.17	11.2	5.60	0.0
4	16	843	56.7	3	B	7.20	6.0	7.1	1.760	0.080	0.970	NA	NA	6.67	11.0	6.90	0.0
4	16	1144	59.7	3	B	7.40	16.0	8.8	1.740	0.126	1.570	3.06	0.905	11.49	NA	NA	NA
4	16	1443	62.7	3	B	7.40	13.0	5.7	1.460	0.105	1.560	NA	NA	11.49	12.2	8.50	0.0
4	16	1743	65.7	3	B	7.30	12.0	9.6	1.850	0.147	1.410	3.81	1.280	12.41	12.2	8.00	0.0
4	16	2043	68.7	3	B	7.40	12.0	5.1	1.820	0.137	1.360	NA	NA	13.96	12.2	6.20	0.0
4	16	2343	71.7	3	B	7.40	17.0	6.2	1.590	0.117	1.290	3.03	1.020	5.93	11.9	7.80	0.0
4	17	245	74.8	3	B	7.40	12.0	5.4	1.590	0.117	1.270	NA	NA	31.04	11.7	7.00	0.0
4	17	550	77.8	3	B	7.40	16.0	9.2	1.690	0.117	1.340	4.41	1.620	22.76	11.8	7.00	0.1
4	17	837	80.6	3	B	7.30	19.0	3.9	1.690	0.127	1.310	NA	NA	14.48	11.5	8.10	0.0
4	17	1130	83.5	3	B	7.40	7.0	4.8	1.570	0.127	1.260	2.85	0.696	17.59	12.0	9.40	0.0

94510400

BELLEVILLE TPK - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	17	1431	86.5	3	B	7.40	8.0	5.1	1.430	0.097	1.350	NA	NA	16.55	12.0	9.10	0.0
4	17	1728	89.5	3	B	7.30	7.0	7.5	1.560	0.107	1.110	3.00	1.010	26.90	11.8	8.70	0.0
4	17	2028	92.5	3	B	7.30	6.0	3.8	1.620	0.117	1.250	NA	NA	12.41	11.5	7.80	0.0
4	17	2328	95.5	3	B	7.30	9.0	5.8	1.490	0.117	1.230	2.85	0.791	20.69	12.0	8.10	0.0
4	18	235	98.6	3	B	7.30	9.0	5.0	1.260	0.107	1.160	NA	NA	18.62	12.0	7.90	0.0
4	18	535	101.6	3	B	7.30	18.0	7.2	1.490	0.107	1.180	2.79	0.802	26.90	12.0	8.00	0.0
4	18	831	104.5	3	B	7.30	15.0	5.0	1.540	0.117	1.210	NA	NA	14.48	12.0	7.80	0.0
4	18	1130	107.5	3	B	7.30	17.0	5.6	1.280	0.102	1.130	NA	NA	9.64	12.0	9.60	0.0
4	18	1430	110.5	3	B	7.40	14.0	6.8	1.050	0.092	0.404	2.99	0.841	13.17	13.0	9.50	0.0
4	18	1731	113.5	3	B	7.30	14.0	6.6	1.270	0.097	1.120	NA	NA	15.95	13.0	9.80	0.0
4	18	2030	116.5	3	B	7.20	12.0	5.1	1.390	0.107	1.180	3.15	0.500	12.24	13.5	7.80	0.0
4	18	2337	119.6	3	B	7.30	16.0	5.7	1.240	0.056	0.754	2.50	0.735	12.24	12.8	8.00	0.0
4	19	235	122.6	3	B	7.30	28.0	6.3	1.150	0.107	1.150	NA	NA	6.68	12.5	8.00	0.0
4	19	535	125.6	3	B	7.30	23.0	6.9	1.190	0.097	1.120	NA	NA	20.03	12.5	7.80	0.0
4	19	830	128.5	3	B	7.30	21.0	4.8	1.060	0.056	1.490	2.20	0.437	7.05	12.8	7.60	0.0
4	19	1133	131.5	3	B	7.30	17.0	4.2	NA	NA	NA	NA	NA	6.31	13.0	7.70	0.0
4	19	1430	134.5	3	B	7.40	12.0	4.6	0.953	0.091	1.500	1.78	0.430	15.52	13.5	8.90	0.0
4	19	1730	137.5	3	B	7.40	13.0	5.4	0.971	0.076	1.370	1.96	0.654	14.48	13.5	8.30	0.0
4	19	2033	140.5	3	B	7.30	14.0	3.6	1.150	0.086	1.410	NA	NA	15.52	13.2	5.10	1.0
4	19	2325	143.4	3	B	7.30	13.0	4.1	1.060	0.086	1.480	NA	NA	12.41	13.2	8.00	0.0
4	20	240	146.7	3	B	7.40	16.0	2.4	1.030	0.106	1.560	2.28	0.857	21.72	14.0	7.90	0.0
4	20	535	149.6	3	B	7.40	21.0	3.8	1.020	0.096	1.520	NA	NA	32.07	14.0	7.60	0.0
4	20	830	152.5	3	B	7.30	15.0	2.7	1.110	0.091	1.460	2.73	0.610	28.98	13.0	6.50	0.2
4	20	1131	155.5	3	B	7.30	12.0	3.0	1.100	0.061	1.420	2.02	0.457	21.72	13.5	7.40	0.0
4	20	1432	158.5	3	B	7.30	13.0	2.6	1.070	0.111	1.580	2.44	0.832	21.72	14.0	7.60	0.0
4	20	1735	161.6	3	B	7.40	14.0	3.2	1.050	0.111	1.580	NA	NA	25.86	13.8	7.50	0.4

946510401

BELLEVILLE TPK - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	20	2035	164.6	3	B	7.30	14.0	2.4	1.120	0.096	1.420	3.27	0.828	15.52	13.0	6.00	1.2
4	20	2335	167.6	3	B	7.30	12.0	7.8	1.070	0.096	1.460	NA	NA	16.55	13.0	7.00	0.5
4	21	240	170.7	3	B	7.40	19.0	2.7	0.910	0.096	1.550	2.46	1.110	42.13	13.0	8.30	0.0
4	21	540	173.7	3	B	7.40	17.0	4.2	1.000	0.106	1.590	NA	NA	54.17	12.8	8.50	0.1
4	21	830	176.5	3	B	7.30	15.0	7.1	1.130	0.106	1.490	2.54	0.533	24.83	13.0	NA	0.9
4	21	1133	179.5	3	B	7.30	8.0	3.4	1.130	0.106	1.500	NA	NA	20.69	12.5	NA	0.5
4	21	1430	182.5	3	B	7.40	17.0	3.0	0.951	0.106	1.590	1.96	0.723	47.59	13.5	9.20	0.0
4	21	1730	185.5	3	B	7.20	14.0	3.2	0.949	0.106	1.630	NA	NA	31.04	13.5	7.90	0.0
4	21	2030	188.5	3	B	7.30	24.0	3.3	1.160	0.101	1.420	3.75	1.630	64.14	12.5	6.20	3.0
4	21	2330	191.5	3	B	7.30	20.0	3.8	1.110	0.101	1.460	NA	NA	33.10	12.7	6.90	2.0
4	22	235	194.6	3	B	7.30	18.0	3.8	0.999	0.106	1.630	NA	NA	28.97	13.0	6.90	0.2
4	22	535	197.6	3	B	7.50	18.0	3.8	0.968	0.106	1.690	1.90	0.597	28.97	12.5	8.00	0.0
4	22	831	200.5	3	B	7.30	35.0	9.6	1.150	0.106	1.490	3.21	0.885	55.87	12.5	7.00	1.8
4	22	1130	203.5	3	B	7.20	10.0	8.7	1.150	0.106	1.510	NA	NA	24.83	13.0	7.80	2.0
4	22	1431	206.5	3	B	7.40	18.0	8.7	1.040	0.106	1.650	2.59	0.732	33.11	14.0	7.90	0.0
4	22	1731	209.5	3	B	7.50	15.0	8.4	0.996	0.106	1.740	NA	NA	39.31	13.2	9.20	0.0
4	22	2031	212.5	3	B	7.30	17.0	8.1	1.110	0.116	1.450	2.76	0.501	28.97	12.9	7.40	1.5
4	22	2331	215.5	3	B	7.30	11.0	8.6	1.090	0.106	1.100	NA	NA	35.17	12.9	7.00	1.5
4	23	235	218.6	3	B	7.40	25.0	8.7	1.020	0.066	1.750	NA	NA	47.59	13.0	8.60	0.2
4	23	535	221.5	3	B	7.50	18.0	8.7	0.896	NA	NA	NA	NA	37.24	12.0	9.00	0.1
4	23	832	224.5	3	B	7.30	24.0	6.2	1.080	0.116	1.210	2.38	0.720	28.97	13.0	7.20	1.0
4	23	1131	227.5	3	B	7.30	10.0	4.1	1.090	0.111	1.540	NA	NA	27.76	13.2	6.40	1.2
4	23	1433	230.5	3	B	7.40	19.0	5.2	1.050	NA	NA	3.33	0.623	35.17	13.0	8.60	0.0
4	23	1733	233.5	3	B	7.60	14.0	5.0	0.992	0.106	1.850	NA	NA	35.17	12.0	8.80	0.0
4	23	2033	236.5	3	B	7.30	25.0	9.3	1.100	0.116	1.510	3.21	0.728	33.11	12.6	7.70	1.5
4	23	2333	239.5	3	B	7.30	12.0	8.6	1.090	0.101	1.580	NA	NA	23.74	12.7	5.90	1.4

94510402

BELLEVILLE TPK - LEVEL B - 2/3 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH_3 [PPM]	NO_2 [PPM]	NO_3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	24	235	242.6	3	B	7.30	16.0	8.7	1.140	0.097	1.000	3.15	0.712	26.89	12.5	7.40	0.5
4	24	535	245.6	3	B	7.50	19.0	4.8	0.922	0.116	1.850	NA	NA	39.31	12.0	9.90	0.0
4	24	805	248.1	3	B	7.50	24.0	6.3	0.899	0.111	1.800	2.32	0.848	26.89	12.1	9.20	0.0
		AVERAGE READING				7.34	14.8	6.0	1.261	0.111	1.437	2.80	0.777	23.97	12.7	7.62	0.3

946510403

STØRM #1

UNIØN AVENUE

4-14/4-24-81

1/2 DEPTH

946510404

UNION AVENUE - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	919	9.3	5	C	7.70	11.0	6.3	1.460	0.174	1.910	2.55	0.524	22.57	14.2	9.70	NA
4	14	1216	12.3	5	C	7.50	10.0	6.3	1.360	0.179	1.860	NA	NA	16.93	13.0	7.70	NA
4	14	1517	15.3	5	C	7.50	11.0	5.7	1.150	0.137	1.700	3.10	0.484	22.57	13.0	6.50	NA
4	14	1817	18.3	5	C	7.40	11.0	5.8	1.480	0.174	1.880	NA	NA	17.87	13.8	6.10	NA
4	14	2117	21.3	5	C	7.40	10.0	7.2	1.540	0.179	1.830	2.63	0.471	18.81	12.8	8.20	NA
4	15	15	24.3	5	C	7.40	13.0	9.4	0.738	0.064	1.060	NA	NA	14.11	12.0	NA	NA
4	15	330	27.5	5	C	7.40	13.0	10.6	1.360	0.158	1.580	2.75	0.532	11.76	11.2	7.80	NA
4	15	620	30.3	5	C	7.40	13.0	10.5	1.640	0.185	1.620	NA	NA	11.29	11.5	7.80	NA
4	15	915	33.3	5	C	7.30	7.0	11.4	1.760	0.200	1.700	2.94	0.575	11.38	11.0	7.80	NA
4	15	1216	36.3	5	C	7.20	9.0	10.8	1.720	0.158	1.660	NA	NA	12.41	11.0	8.10	NA
4	15	1515	39.3	5	C	7.40	9.0	9.8	1.760	0.137	1.580	2.67	0.517	17.59	12.0	9.10	NA
4	15	1815	42.3	5	C	7.30	9.0	10.1	1.210	0.148	1.610	2.97	0.494	17.59	11.2	7.80	NA
4	15	2115	45.3	5	C	7.60	8.0	8.1	1.830	0.096	1.320	NA	NA	11.38	11.0	9.80	NA
4	16	15	48.3	5	C	7.50	9.0	8.4	1.520	0.131	1.330	2.35	0.463	14.48	11.0	9.00	NA
4	16	315	51.3	5	C	7.50	11.0	7.5	1.480	0.106	1.620	NA	NA	11.38	11.0	8.80	NA
4	16	615	54.3	5	C	7.50	10.0	7.6	1.490	0.116	1.640	2.36	0.455	11.38	10.8	9.30	NA
4	16	919	57.3	5	C	7.60	8.0	7.4	1.520	0.111	1.530	2.64	0.435	10.01	11.0	10.60	NA
4	16	1217	60.3	5	C	7.50	10.0	8.6	1.560	0.111	1.500	2.16	0.486	11.86	11.0	8.40	NA
4	16	1515	63.3	5	C	7.50	10.0	7.8	1.440	0.106	1.470	2.88	0.448	11.86	12.0	NA	NA
4	16	1813	66.2	5	C	7.50	12.0	6.8	1.480	0.106	1.510	2.60	0.410	10.57	11.5	5.40	NA
4	16	2113	69.2	5	C	7.60	10.0	7.1	1.380	0.106	1.490	NA	NA	8.99	12.2	5.80	NA
4	17	15	72.3	5	C	7.60	15.0	7.6	1.410	0.106	1.470	2.44	0.487	11.38	12.0	8.90	NA
4	17	315	75.3	5	C	7.50	12.0	7.5	1.370	0.116	1.160	NA	NA	9.31	12.0	8.00	NA
4	17	615	78.3	5	C	7.50	12.0	6.4	1.300	0.081	1.650	2.38	0.440	9.27	11.5	7.50	NA
4	17	913	81.2	5	C	7.40	14.0	5.7	1.280	0.117	1.270	NA	NA	11.38	11.8	7.90	NA
4	17	1211	84.1	5	C	7.40	12.0	6.0	1.070	0.089	1.340	1.71	0.418	6.30	12.0	8.90	NA

946510405

UNION AVENUE - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM#1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	17	1459	87.0	5	C	7.40	12.0	7.1	1.020	0.077	1.290	NA	NA	1.98	12.0	9.20	NA
4	17	1755	89.9	5	C	7.40	11.0	5.1	1.050	0.082	1.240	NA	NA	1.41	11.7	8.80	NA
4	17	2055	92.9	5	C	7.40	12.0	4.5	1.290	0.077	1.230	1.88	0.371	1.22	11.5	8.60	NA
4	17	2355	95.9	5	C	7.40	13.0	5.5	0.961	0.077	1.260	NA	NA	0.94	11.9	9.10	NA
4	18	255	98.9	5	C	7.40	13.0	4.6	0.998	0.089	1.290	1.88	0.427	0.94	11.8	8.50	NA
4	18	600	102.3	5	C	7.40	12.0	4.6	1.030	0.082	1.290	1.44	0.455	0.94	12.0	8.50	0.1
4	18	858	105.0	5	C	7.60	15.0	5.2	1.030	0.089	1.340	1.30	0.381	7.79	12.0	8.50	NA
4	18	1158	108.0	5	C	7.50	14.0	6.4	0.924	0.093	1.330	1.15	0.381	9.64	12.0	8.60	NA
4	18	1500	111.6	5	C	7.50	14.0	5.0	0.906	0.098	1.340	1.36	0.429	14.09	13.0	9.30	NA
4	18	1755	113.9	5	C	7.40	15.0	5.0	0.966	0.117	0.652	NA	NA	12.98	13.0	9.20	0.1
4	18	2054	116.9	5	C	7.40	12.0	6.6	0.924	0.098	1.330	1.17	0.387	14.48	12.9	9.20	NA
4	19	15	120.3	5	C	7.50	15.0	6.8	0.961	0.089	1.300	1.30	0.426	11.38	14.0	10.10	NA
4	19	300	123.0	5	C	7.50	16.0	7.2	1.100	0.106	1.510	NA	NA	4.45	13.0	8.20	NA
4	19	600	126.0	5	C	7.50	17.0	7.8	0.998	0.098	1.340	2.05	0.495	4.45	13.5	8.20	NA
4	19	858	128.5	5	C	7.50	15.0	6.6	0.998	0.098	1.370	NA	NA	2.46	14.0	8.90	NA
4	19	1159	132.3	5	C	7.40	18.0	7.6	1.070	0.109	1.340	2.13	0.426	NA	13.0	7.90	NA
4	19	1457	134.9	5	C	7.50	13.0	6.6	0.788	0.125	1.420	1.99	0.424	NA	13.2	8.00	NA
4	19	1749	137.8	5	C	7.40	14.0	6.9	0.988	0.136	1.270	1.44	0.437	6.31	13.5	8.30	NA
4	19	2100	141.0	5	C	7.50	16.0	7.2	1.030	0.109	1.350	NA	NA	4.08	13.8	8.00	NA
4	20	15	144.3	5	C	7.40	9.0	3.3	0.961	0.109	1.410	1.69	0.458	15.52	14.0	10.10	NA
4	20	310	147.	5	C	7.60	8.0	7.2	0.943	0.119	1.470	NA	NA	23.79	15.0	9.20	NA
4	20	600	150.0	5	C	7.60	10.0	3.6	0.988	0.109	1.420	1.19	0.455	16.55	15.0	9.10	NA
4	20	859	153.0	5	C	7.50	10.0	5.1	0.961	0.109	1.390	NA	NA	18.62	14.0	7.80	NA
4	20	1157	155.9	5	C	7.50	8.0	4.8	0.961	0.119	1.470	1.49	0.419	16.55	14.5	9.50	NA
4	20	1459	159.0	5	C	7.40	7.0	6.0	0.961	0.114	1.480	NA	NA	24.45	14.0	7.60	NA
4	20	1805	162.1	5	C	7.40	7.0	4.5	0.961	0.109	1.470	1.22	0.386	31.04	13.5	7.80	0.2

946510406

UNION AVENUE - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	21	2105	165.1	5	C	7.50	8.0	4.8	0.961	0.109	1.450	NA	NA	20.69	13.5	8.20	NA
4	21	5	168.1	5	C	7.40	8.0	5.2	0.998	0.109	1.490	1.27	0.412	14.48	12.5	7.90	0.1
4	21	300	171.0	5	C	7.70	8.0	6.8	0.961	0.109	1.540	NA	NA	22.76	12.8	10.70	NA
4	21	600	174.0	5	C	7.70	10.0	6.4	0.961	0.114	1.540	1.77	0.499	27.93	12.8	10.30	NA
4	21	850	176.8	5	C	7.50	9.0	3.4	0.943	0.109	1.510	NA	NA	25.86	12.1	NA	NA
4	21	1153	179.9	5	C	7.60	7.0	3.3	0.961	0.109	1.520	2.27	0.421	24.83	13.0	9.90	NA
4	21	1452	182.9	5	C	7.50	7.0	6.8	1.030	0.119	1.600	NA	NA	20.69	11.0	9.80	NA
4	21	1805	186.1	5	C	7.50	8.0	7.8	1.070	0.119	1.660	1.38	0.413	26.89	11.1	9.80	NA
4	21	2105	189.1	5	C	7.60	9.0	7.4	0.961	0.109	1.550	NA	NA	26.89	12.5	9.20	NA
4	22	5	192.1	5	C	7.50	8.0	7.5	1.050	0.119	1.610	1.49	0.434	28.97	11.5	8.10	NA
4	22	305	195.1	5	C	7.70	8.0	7.5	0.961	0.125	1.660	NA	NA	35.17	11.0	10.00	0.1
4	22	600	198.0	5	C	8.00	8.0	6.9	0.741	0.119	1.660	1.49	0.418	35.17	12.3	11.40	NA
4	22	858	201.0	5	C	7.50	10.0	8.4	0.988	0.121	1.870	NA	NA	26.90	11.0	9.20	NA
4	22	1157	203.9	5	C	7.50	9.0	7.1	0.851	0.119	1.650	1.55	0.412	26.90	11.5	9.40	NA
4	22	1458	207.0	5	C	7.80	8.0	7.5	0.888	0.130	1.710	NA	NA	43.45	13.0	10.70	NA
4	22	1808	210.1	5	C	7.60	10.0	8.4	0.998	0.130	1.700	1.74	0.397	43.45	11.9	9.90	NA
4	22	2108	213.1	5	C	7.90	12.0	7.8	0.870	0.122	1.660	NA	NA	49.66	12.2	11.80	NA
4	23	5	216.1	5	C	7.80	10.0	8.2	0.791	0.091	1.920	1.22	0.392	68.28	11.2	10.80	NA
4	23	310	219.2	5	C	7.60	11.0	8.4	0.941	0.106	1.990	NA	NA	35.17	11.5	10.00	NA
4	23	600	222.0	5	C	7.80	11.0	9.4	0.842	0.106	1.950	1.44	0.460	39.31	13.5	12.10	NA
4	23	859	225.0	5	C	7.50	10.0	3.8	0.998	0.135	1.820	NA	NA	22.76	12.0	9.30	NA
4	23	1158	228.0	5	C	7.50	8.0	2.6	1.050	0.131	1.980	1.66	0.405	26.33	12.0	9.10	NA
4	23	1459	231.0	5	C	7.60	9.0	2.8	0.961	0.140	1.800	NA	NA	31.04	13.0	10.20	NA
4	23	1806	234.1	5	C	7.50	10.0	3.7	0.998	0.140	1.770	1.49	0.390	22.76	12.5	9.20	NA
4	23	2106	237.1	5	C	7.60	11.0	4.4	0.924	0.130	1.770	NA	NA	31.04	12.5	11.20	NA
4	24	10	240.2	5	C	7.60	12.0	3.6	1.030	0.140	1.760	1.64	0.440	20.77	13.0	9.20	NA

946510407

UNION AVENUE - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	24	300	243.0	5	C	7.40	12.0	8.2	0.888	0.140	1.680	NA	NA	26.89	12.5	7.30	NA
4	24	600	246.0	5	C	7.40	14.0	5.7	1.440	0.182	1.850	1.88	0.502	21.14	12.9	8.50	NA

946510408

STØRM #1

SECØND RIVER

4-14/4-17-81

1/2 DEPTH

946510409

SECOND RIVER - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
4	14	824	8.4	4	C	8.00	8.0	4.2	0.020	0.030	1.870	1.42	0.234	7.05	11.0	10.70	NA
4	14	1123	11.4	4	C	7.40	15.0	11.6	0.072	0.020	0.910	1.72	0.654	52.67	11.0	10.60	NA
4	14	1425	14.4	4	C	7.10	20.0	11.7	0.020	0.015	0.552	NA	NA	41.38	11.0	10.20	NA
4	14	1725	17.4	4	C	7.20	16.0	12.8	0.020	0.020	0.947	0.73	0.258	8.77	12.3	9.50	NA
4	14	2025	20.4	4	C	7.30	17.0	12.4	0.020	0.015	0.839	NA	NA	3.39	12.0	10.00	NA
4	14	2325	23.4	4	C	7.50	14.0	4.8	0.020	0.020	1.310	NA	NA	1.98	11.0	9.70	NA
4	15	225	26.4	4	C	7.70	10.0	2.2	0.020	0.020	1.650	0.43	0.121	1.13	NA	9.50	NA
4	15	525	29.4	4	C	7.80	10.0	2.2	0.020	0.020	1.730	NA	NA	NA	12.0	8.50	NA
4	15	819	32.3	4	C	8.50	5.0	2.1	0.020	0.025	1.910	0.31	0.119	20.69	9.2	13.60	NA
4	15	1121	35.3	4	C	8.90	4.0	1.6	0.020	0.030	2.030	NA	NA	18.81	14.0	12.80	NA
4	15	1420	38.3	4	C	9.20	4.0	2.1	0.020	0.025	1.920	0.33	0.098	4.45	15.0	11.60	NA
4	15	1720	41.3	4	C	8.50	4.0	2.6	0.053	0.025	1.780	NA	NA	0.24	12.8	10.80	NA
4	15	2020	44.3	4	C	8.00	3.0	3.8	0.020	0.030	2.020	0.38	0.094	0.71	11.1	9.20	NA
4	15	2320	47.3	4	C	7.90	4.0	3.2	0.020	0.030	2.150	1.31	0.125	0.40	10.1	9.30	NA
4	16	220	50.3	4	C	7.80	3.0	3.0	0.020	0.030	2.110	NA	NA	0.51	8.8	10.80	NA
4	16	520	53.3	4	C	7.80	4.0	2.0	0.020	0.030	2.110	0.88	0.079	1.03	8.5	10.50	NA
4	16	820	56.3	4	C	8.50	5.0	2.4	0.020	0.030	1.940	NA	NA	7.03	11.5	15.80	NA
4	16	1121	59.3	4	C	9.00	5.0	1.3	0.020	0.035	1.800	0.10	0.093	7.42	15.0	14.20	NA
4	16	1420	62.3	4	C	9.10	5.0	1.6	0.020	0.035	1.900	NA	NA	7.42	17.0	15.60	NA
4	16	1722	65.4	4	C	8.80	6.0	2.0	0.100	0.036	1.630	0.86	0.097	0.44	15.1	10.40	NA
4	16	2022	68.4	4	C	8.00	5.0	0.8	0.186	0.036	1.540	NA	NA	0.52	13.9	8.40	NA
4	16	2322	71.4	4	C	7.90	3.0	1.6	0.037	0.026	1.660	0.71	0.122	0.17	10.7	9.30	NA
4	17	220	74.3	4	C	7.90	4.0	1.5	0.040	0.021	1.760	0.71	0.124	0.07	13.0	8.00	NA
4	17	520	77.3	4	C	7.90	5.0	1.4	0.015	0.011	1.770	NA	NA	0.21	13.0	8.80	NA
4	17	720	79.3	4	C	8.40	3.0	1.8	0.062	0.016	1.770	NA	NA	0.37	13.0	11.10	NA

94510410

STØRM #1

SADDLE

RIVER

4-14/4-17-81

1/2 DEPTH

946510411

SADDLE RIVER - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	1100	11.0	7	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	11.5	6.20	NA
4	14	1400	14.5	7	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	10.5	8.20	NA
4	14	1740	17.7	7	C	7.50	16.0	11.7	2.110	0.232	1.450	3.82	0.846	26.33	11.5	8.40	NA
4	14	2045	20.8	7	C	7.30	17.0	12.0	1.600	0.237	1.450	NA	NA	29.16	12.0	7.80	NA
4	14	2345	23.8	7	C	7.40	15.0	12.0	1.600	0.200	1.430	2.93	0.730	34.80	11.0	8.10	NA
4	15	140	25.7	7	C	7.50	14.0	11.7	1.440	0.101	0.999	NA	NA	22.57	10.0	8.30	NA
4	15	432	28.5	7	C	7.60	15.0	11.0	1.400	0.075	0.955	2.57	0.532	20.69	8.9	8.60	NA
4	15	840	32.7	7	C	7.60	9.0	9.9	1.220	0.096	1.070	NA	NA	15.52	8.0	9.50	NA
4	15	1145	35.8	7	C	7.60	12.0	9.8	1.010	0.137	1.320	2.63	0.466	16.53	12.0	9.90	NA
4	15	1445	38.8	7	C	7.70	8.0	7.6	1.270	0.137	1.440	NA	NA	17.59	13.0	10.10	NA
4	15	1730	41.5	7	C	7.60	13.0	11.0	1.720	0.064	0.872	2.88	0.532	11.38	14.0	8.60	NA
4	15	2025	44.4	7	C	7.60	9.0	11.4	1.950	0.158	1.480	NA	NA	10.34	12.0	8.20	NA
4	15	2340	47.7	7	C	7.60	8.0	11.6	2.260	0.274	1.650	2.55	0.605	9.27	10.1	7.30	NA
4	16	130	49.5	7	C	7.60	7.0	12.4	2.490	0.345	1.880	4.12	0.769	10.38	9.5	8.20	NA
4	16	430	52.5	7	C	7.60	8.0	12.8	2.750	0.395	2.000	NA	NA	9.45	8.1	7.80	NA
4	16	850	56.8	7	C	7.60	7.0	10.2	3.060	0.405	1.960	4.54	0.929	7.79	8.0	8.20	NA
4	16	1150	59.5	7	C	7.60	7.0	7.1	2.820	0.296	1.760	NA	NA	8.16	11.0	10.00	NA
4	16	1500	63.1	7	C	7.60	14.0	8.2	2.740	0.465	2.000	4.71	0.901	12.41	14.0	9.10	NA
4	16	1825	66.4	7	C	7.60	8.0	7.2	2.610	0.507	1.670	NA	NA	5.19	15.5	8.60	NA
4	16	2125	69.4	7	C	7.60	8.0	11.0	3.120	0.425	1.980	4.76	0.942	5.19	14.1	8.00	NA
4	17	20	72.3	7	C	7.60	8.0	11.8	3.230	NA	NA	NA	NA	5.93	13.0	7.30	NA
4	17	120	73.3	7	C	NA	NA	NA	NA	0.355	1.980	NA	NA	NA	NA	NA	NA
4	17	320	75.3	7	C	7.60	7.0	11.7	3.110	0.306	1.880	5.09	0.910	6.30	12.0	7.10	NA
4	17	615	78.2	7	C	7.50	8.0	11.2	3.460	0.235	0.815	NA	NA	5.19	11.2	7.50	NA
		AVERAGE READING				7.57	10.4	10.6	2.237	0.259	1.526	3.69	0.742	13.82	11.3	8.30	NA

94651041 2

STØRM #1

MARKET STREET

4-14/4-17-81

1/2 DEPTH

946510413

MARKET STREET - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	955	9.9	9	C	7.40	11.0	9.9	1.930	0.116	1.330	3.04	0.496	9.41	12.9	7.80	NA
4	14	1310	13.2	9	C	7.40	10.0	7.8	1.400	0.122	1.280	NA	NA	10.35	13.5	8.20	NA
4	14	1805	18.1	9	C	7.40	12.0	9.4	1.990	0.169	1.550	3.71	0.537	13.17	12.5	8.10	NA
4	14	2105	21.1	9	C	7.40	17.0	12.3	2.070	0.190	2.160	NA	NA	10.79	12.2	8.20	NA
4	15	5	24.1	9	C	7.40	15.0	11.8	2.170	0.148	1.530	3.54	0.571	10.79	12.0	8.40	NA
4	15	205	26.1	9	C	7.40	17.0	11.0	2.140	0.127	1.410	NA	NA	10.45	11.6	8.40	NA
4	15	500	29.0	9	C	7.40	15.0	10.2	2.290	0.106	1.320	4.26	0.589	10.35	10.9	8.40	NA
4	15	855	32.9	9	C	7.40	10.0	9.2	1.290	0.054	0.819	NA	NA	13.44	10.0	9.00	NA
4	15	1200	36.0	9	C	7.50	10.0	10.2	1.820	0.101	1.380	3.10	0.494	13.44	11.0	10.00	NA
4	15	1500	39.0	9	C	7.50	9.0	8.6	1.630	0.096	1.370	3.04	0.434	12.41	12.0	11.50	NA
4	15	1800	42.0	9	C	7.50	9.0	8.8	1.690	0.090	1.290	NA	NA	28.43	12.0	10.20	NA
4	15	2100	45.0	9	C	7.50	9.0	9.3	1.650	0.090	1.290	2.82	0.443	23.78	11.4	9.60	NA
4	16	5	48.1	9	C	7.50	10.0	7.6	1.640	0.101	1.290	3.21	0.466	8.53	11.0	9.70	NA
4	16	305	51.1	9	C	7.50	11.0	9.2	1.580	0.101	1.300	NA	NA	8.53	10.5	9.40	NA
4	16	605	54.1	9	C	7.50	13.0	9.2	1.550	0.112	1.030	NA	NA	9.64	10.0	9.70	NA
4	16	905	57.1	9	C	7.50	13.0	8.2	1.480	0.107	1.030	2.71	0.429	8.53	10.0	9.80	NA
4	16	1218	60.3	9	C	7.50	12.0	7.5	1.520	0.081	1.220	NA	NA	10.75	11.0	NA	NA
4	16	1515	63.3	9	C	7.50	13.0	7.4	1.330	0.076	1.200	NA	NA	9.27	12.0	10.70	NA
4	16	1850	66.8	9	C	7.50	12.0	7.8	1.190	0.076	1.180	NA	NA	7.78	12.0	10.40	NA
4	16	2150	69.8	9	C	7.50	10.0	6.9	1.110	0.087	0.973	2.44	0.380	8.16	12.0	9.90	NA
4	17	40	72.7	9	C	7.50	10.0	7.2	1.040	0.046	1.270	NA	NA	10.38	11.5	9.50	NA
4	17	345	75.8	9	C	7.50	11.0	7.1	1.050	0.077	0.943	2.19	0.382	9.27	11.5	9.60	NA
4	17	635	78.6	9	C	7.40	12.0	7.4	1.030	0.062	0.815	NA	NA	9.64	11.1	9.40	NA
		AVERAGE READING				7.46	11.8	8.9	1.591	0.102	1.260	3.10	0.475	11.62	11.5	9.20	NA

94510414

STØRM #1

LINCØLN AVENUE

4-14/4-17-81

1/2 DEPTH

946510415

LINCOLN AVENUE - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	940	9.7	10	C	7.50	13.0	10.4	2.440	0.169	1.480	3.93	0.600	11.29	13.0	8.40	NA
4	14	1240	12.7	10	C	7.50	13.0	10.1	1.160	0.127	1.450	NA	NA	11.29	14.0	9.00	NA
4	14	1635	16.6	10	C	7.40	16.0	13.1	2.520	0.143	1.360	5.15	0.649	15.99	13.0	9.40	NA
4	14	1935	19.6	10	C	7.50	16.0	13.1	2.140	0.116	1.310	NA	NA	15.05	12.2	9.60	NA
4	14	2235	22.6	10	C	7.60	14.0	12.4	2.360	0.100	1.210	3.71	0.619	14.11	11.8	10.00	NA
4	15	110	25.2	10	C	7.60	15.0	10.1	1.990	0.116	1.360	NA	NA	12.23	11.5	9.90	NA
4	15	400	28.0	10	C	7.60	16.0	10.5	1.840	0.110	1.340	NA	NA	10.35	11.0	10.00	NA
4	15	730	31.5	10	C	7.50	17.0	10.3	1.840	0.095	1.340	3.16	0.508	9.41	10.2	10.20	NA
4	15	945	33.8	10	C	7.50	14.0	12.2	1.760	0.053	0.944	NA	NA	12.61	10.0	11.00	NA
4	15	1246	36.8	10	C	7.60	8.0	11.9	1.840	0.095	1.260	2.68	0.468	12.24	11.3	11.30	NA
4	15	1630	40.5	10	C	7.60	10.0	12.4	1.840	0.095	1.240	NA	NA	11.82	11.9	10.60	NA
4	15	1930	43.5	10	C	7.50	12.0	12.2	1.650	0.095	1.220	3.60	0.522	10.38	11.4	9.90	NA
4	15	2230	46.5	10	C	7.50	10.0	11.0	1.380	0.064	1.260	NA	NA	8.53	11.0	9.80	NA
4	16	100	49.0	10	C	7.60	12.0	10.6	1.550	0.102	0.978	3.04	0.518	11.13	10.4	10.70	NA
4	16	350	51.8	10	C	7.60	11.0	10.3	1.480	0.097	0.963	NA	NA	13.72	10.1	10.90	NA
4	16	725	55.4	10	C	7.60	14.0	10.1	1.460	0.087	0.963	NA	NA	14.46	9.9	11.00	NA
4	16	1010	58.2	10	C	7.50	13.0	9.3	1.330	0.087	0.943	2.66	0.504	12.98	10.2	NA	NA
4	16	1320	61.3	10	C	7.60	10.0	8.8	1.210	0.066	1.100	NA	NA	14.46	11.2	11.50	NA
4	16	1720	65.3	10	C	7.50	9.0	9.8	1.400	0.067	0.800	2.98	0.387	14.46	12.0	10.50	NA
4	16	2020	68.3	10	C	7.50	13.0	8.1	1.160	0.067	1.010	NA	NA	15.94	10.8	10.20	NA
4	16	2320	71.3	10	C	7.50	15.0	9.3	1.120	0.077	0.894	2.30	0.378	15.94	11.5	10.00	NA
4	17	125	73.4	10	C	7.50	11.0	11.0	1.100	0.077	0.905	NA	NA	14.84	11.5	10.20	NA
4	17	440	76.7	10	C	7.50	12.0	8.8	1.120	0.077	0.923	4.04	0.393	18.91	11.1	10.10	NA
4	17	720	79.3	10	C	7.50	13.0	8.8	1.110	0.077	0.943	NA	NA	18.71	NA	NA	NA
		AVERAGE READING				7.53	12.8	10.6	1.617	0.094	1.133	3.39	0.504	13.37	11.3	10.19	NA

946510416

STØRM #1

MARKET

ISLAND

4-14/4-17-81

1/2 DEPTH

946510417

MARKET ISLAND - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	925	9.4	11	C	7.70	13.0	8.3	1.800	0.095	0.985	3.59	0.535	23.51	12.8	10.60	NA
4	14	1229	12.5	11	C	7.70	14.0	9.2	2.250	0.136	1.290	NA	NA	36.68	13.2	10.20	NA
4	14	1540	15.7	11	C	7.70	15.0	7.8	2.290	0.074	0.890	3.48	0.574	10.35	12.9	12.20	NA
4	14	1905	19.1	11	C	7.70	17.0	9.9	2.590	0.136	1.310	NA	NA	16.93	12.5	10.80	NA
4	14	2205	22.1	11	C	7.70	17.0	9.3	2.250	0.105	1.180	3.71	0.585	14.11	12.0	11.30	NA
4	15	100	25.0	11	C	7.60	17.0	8.8	2.250	0.095	1.220	NA	NA	12.23	11.4	11.30	NA
4	15	349	27.8	11	C	7.70	17.0	7.6	1.720	0.084	1.160	3.37	0.542	12.70	11.0	11.30	NA
4	15	710	31.2	11	C	7.60	17.0	9.2	1.760	0.074	1.200	NA	NA	15.99	10.2	11.20	NA
4	15	930	33.5	11	C	7.60	8.0	10.5	1.950	0.079	1.140	3.09	0.464	11.98	10.0	11.50	NA
4	15	1235	36.6	11	C	7.60	10.0	8.7	1.780	0.053	0.922	NA	NA	11.98	11.0	11.90	NA
4	15	1545	39.8	11	C	7.60	9.0	7.2	1.870	0.074	1.130	3.03	0.546	8.90	NA	NA	NA
4	15	1905	43.1	11	C	7.60	10.0	8.4	1.800	0.074	1.100	NA	NA	9.64	11.5	11.00	NA
4	15	2205	46.1	11	C	7.60	13.0	7.2	1.650	0.069	1.010	2.67	0.514	11.15	10.9	10.90	NA
4	16	45	48.8	11	C	7.60	13.0	6.9	1.580	0.097	0.913	3.88	0.502	13.35	10.2	11.80	NA
4	16	340	51.7	11	C	7.60	13.0	7.2	1.480	0.087	0.894	NA	NA	14.69	10.0	11.80	NA
4	16	705	55.1	11	C	7.60	15.0	7.1	1.400	0.066	1.060	3.48	0.507	14.46	9.9	11.90	NA
4	16	951	57.8	11	C	7.50	14.0	9.9	1.370	0.077	0.855	NA	NA	12.24	NA	NA	NA
4	16	1300	61.0	11	C	7.50	14.0	9.0	1.310	0.067	0.806	3.03	0.427	11.49	11.0	11.00	NA
4	16	1655	64.9	11	C	7.50	14.0	8.8	1.230	0.067	0.817	NA	NA	17.06	12.0	11.80	NA
4	16	1955	67.9	11	C	7.60	13.0	9.2	1.190	0.051	1.010	2.42	0.347	11.12	10.9	10.80	NA
4	16	2255	70.9	11	C	7.60	14.0	7.5	1.180	0.056	1.070	NA	NA	9.27	11.5	10.80	NA
4	17	115	73.3	11	C	7.60	16.0	8.1	1.180	0.077	0.869	2.53	0.376	11.49	11.5	11.00	NA
4	17	425	76.4	11	C	7.60	16.0	7.6	1.190	0.072	0.860	NA	NA	11.12	11.1	10.90	NA
4	17	708	79.1	11	C	7.60	14.0	7.6	1.160	0.072	0.832	NA	NA	9.64	11.0	11.20	NA
		AVERAGE READING				7.61	13.9	8.4	1.676	0.081	1.022	3.19	0.493	13.84	11.3	11.24	NA

94651041B

STØRM #1

MCBRIDE AVENUE

4-14/4-17-81

1/2 DEPTH

946510419

MCBRIDE AVE - LEVEL C - 1/2 DEPTH
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	915	9.3	12	C	7.30	13.0	5.7	2.460	0.116	1.180	4.55	0.540	20.69	12.9	6.50	NA
4	14	1220	12.3	12	C	7.30	15.0	5.8	1.700	0.110	1.250	NA	NA	8.46	13.5	6.20	NA
4	14	1530	15.5	12	C	7.30	13.0	6.0	2.040	0.116	1.190	3.82	0.534	9.41	12.8	6.90	NA
4	14	1845	18.8	12	C	7.40	17.0	8.8	2.380	0.110	1.250	NA	NA	15.99	12.2	7.00	NA
4	14	2150	21.8	12	C	7.40	16.0	9.2	2.510	0.090	1.030	3.82	0.581	14.11	12.0	7.40	NA
4	15	50	24.8	12	C	7.40	15.0	8.2	2.060	0.084	1.140	NA	NA	11.29	11.5	7.90	NA
4	15	340	27.7	12	C	7.30	17.0	9.6	1.670	0.079	1.210	5.50	0.831	7.52	11.0	8.00	NA
4	15	650	30.8	12	C	7.40	17.0	8.4	1.160	0.064	1.120	NA	NA	10.35	10.5	8.10	NA
4	15	920	33.3	12	C	7.30	8.0	6.3	2.020	0.079	1.080	3.26	0.500	10.01	10.1	8.40	NA
4	15	1220	36.3	12	C	7.30	9.0	5.4	1.940	0.069	1.060	NA	NA	10.01	11.0	9.50	NA
4	15	1520	39.3	12	C	7.30	9.0	5.2	1.480	0.043	0.775	2.92	0.430	7.97	12.0	9.10	NA
4	15	1845	42.8	12	C	7.40	11.0	5.2	1.760	0.069	1.050	NA	NA	10.01	11.5	8.20	NA
4	15	2145	45.8	12	C	7.30	11.0	7.4	1.390	0.069	1.030	2.81	0.460	9.64	11.0	8.00	NA
4	16	35	48.6	12	C	7.40	13.0	6.2	1.580	0.081	1.110	3.31	0.425	14.09	10.5	8.40	NA
4	16	330	51.5	12	C	7.30	13.0	5.4	1.480	0.087	0.841	NA	NA	12.24	10.0	8.70	NA
4	16	645	54.8	12	C	7.30	13.0	6.0	1.440	0.077	0.820	2.92	0.385	14.46	10.0	8.90	NA
4	16	943	57.7	12	C	7.40	11.0	9.2	1.430	0.077	0.826	NA	NA	12.98	10.0	8.90	NA
4	16	1248	60.8	12	C	7.30	10.0	7.8	1.300	0.067	0.784	2.68	0.385	10.38	10.9	9.00	NA
4	16	1635	64.6	12	C	7.40	10.0	6.8	1.290	0.067	0.757	NA	NA	10.38	12.0	9.00	NA
4	16	1935	67.6	12	C	7.30	10.0	6.3	1.220	0.067	0.785	2.56	0.351	10.76	10.9	9.10	NA
4	16	2235	70.6	12	C	7.30	12.0	5.7	1.230	0.067	0.821	NA	NA	10.01	11.5	8.60	NA
4	17	105	73.1	12	C	7.30	14.0	6.6	1.220	0.056	1.060	3.20	0.389	10.01	11.3	9.20	NA
4	17	415	76.3	12	C	7.30	15.0	6.4	1.220	0.077	0.810	NA	NA	9.64	11.0	9.10	NA
4	17	709	79.0	12	C	7.30	12.0	7.2	1.190	0.067	0.804	2.13	0.361	NA	11.1	8.40	NA
		AVERAGE READING				7.33	12.7	6.9	1.632	0.079	0.991	3.34	0.475	11.32	11.3	8.27	NA

946510420

STØRM #1

HILLARY STREET

4-14/4-17-81

1/2 DEPTH

946510421

HILLARY ST - LEVEL 13C - 1/2 DEP
RIVER SAMPLING - STORM #1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
4	14	845	8.8	13	C	7.40	14.0	7.8	2.590	0.079	0.917	3.93	0.597	15.05	12.1	7.20	0.0
4	14	1200	12.0	13	C	7.40	15.0	8.2	2.810	0.126	1.200	0.00	0.000	12.23	13.2	6.60	0.0
4	14	1500	15.0	13	C	7.40	16.0	10.4	2.850	0.136	1.300	4.16	0.783	15.99	12.4	7.40	0.0
4	14	1830	18.5	13	C	7.40	16.0	10.8	2.440	0.095	1.060	0.00	0.000	19.75	12.0	7.60	0.0
4	14	2130	21.5	13	C	7.40	17.0	10.5	2.140	0.095	1.110	3.26	0.582	3.76	12.0	8.20	0.0
4	15	30	24.5	13	C	7.40	20.0	12.2	1.870	0.079	1.150	0.00	0.000	14.11	11.1	8.40	0.0
4	15	330	27.5	13	C	7.40	16.0	8.8	2.020	0.079	1.120	3.88	0.546	34.80	11.0	8.60	0.0
4	15	630	30.5	13	C	7.40	15.0	8.6	1.800	0.064	1.010	3.14	0.519	26.80	10.0	8.60	0.0
4	15	905	33.1	13	C	7.30	10.0	6.9	2.020	0.053	0.909	0.00	0.000	10.01	10.0	8.50	0.0
4	15	1213	36.2	13	C	7.30	9.0	7.4	1.840	0.064	0.986	3.82	0.540	10.76	11.1	8.10	0.0
4	15	1510	39.2	13	C	7.40	10.0	7.6	1.570	0.064	1.070	0.00	0.000	10.76	11.5	9.60	0.0
4	15	1825	42.4	13	C	7.30	10.0	7.6	1.760	0.079	1.010	2.67	0.449	11.13	11.0	8.40	0.0
4	15	2125	45.4	13	C	7.40	14.0	7.6	1.420	0.064	0.936	0.00	0.000	10.01	10.7	8.40	0.0
4	16	20	48.3	13	C	7.30	13.0	6.4	1.450	0.087	0.795	2.53	0.415	13.01	10.2	9.20	0.0
4	16	320	51.3	13	C	7.30	14.0	6.2	1.440	0.087	0.807	0.00	0.000	14.46	10.0	8.80	0.0
4	16	625	54.4	13	C	7.30	12.0	5.7	1.400	0.077	0.796	2.64	0.389	13.35	10.0	9.20	0.0
4	16	930	57.5	13	C	7.30	10.0	7.8	1.260	0.052	0.783	0.00	0.000	10.01	10.1	9.20	0.0
4	16	1235	60.6	13	C	7.30	12.0	7.8	1.250	0.067	0.760	2.36	0.386	10.38	11.1	9.30	0.0
4	16	1540	63.7	13	C	7.30	13.0	6.6	1.260	0.067	0.792	0.00	0.000	12.61	12.0	9.50	0.0
4	16	1915	67.3	13	C	7.30	15.0	7.6	1.250	0.067	0.832	0.00	0.000	12.98	10.5	9.00	0.0
4	16	2215	70.3	13	C	7.30	10.0	8.8	1.270	0.077	0.851	0.00	0.000	11.49	11.5	9.00	0.0
4	17	55	72.9	13	C	7.30	12.0	8.7	1.260	0.077	0.789	3.03	0.421	14.09	11.2	8.80	0.0
4	17	405	76.1	13	C	7.30	12.0	8.4	1.210	0.067	0.775	0.00	0.000	11.12	11.0	8.80	0.0
4	17	650	78.8	13	C	7.30	14.0	7.6	1.220	0.072	0.789	2.84	0.398	9.64	10.9	7.90	0.0
		AVERAGE READING				7.34	13.3	8.2	1.725	0.078	0.939	3.19	0.502	13.68	11.1	8.51	0.0

946510422

STØRM #1

DUNDEE DAM

UPSTREAM

4-14/4-24-81

1/2 DEPTH

946510423

STORM #1 - RIVER SAMPLING
DUNDEE DAM UPSTREAM - LEVEL BC - 1/2 DEPTH

MONTH	DAY	TIME	STTE	DEP	TEMP (*C)	D.O. (PPM)
4	14	1700	8	C	13.0	7.6
4	14	2005	8	C	12.5	7.3
4	14	2300	8	C	12.0	7.9
4	15	0125	8	C	12.0	8.6
4	15	0420	8	C	11.2	8.2
4	15	0750	8	C	10.8	8.4
4	15	1000	8	C	10.0	9.2
4	15	1300	8	C	11.0	9.6
4	15	1655	8	C	12.0	9.9
4	15	1955	8	C	11.9	9.6
4	15	2255	8	C	11.0	9.4
4	16	0120	8	C	10.9	9.5
4	16	0415	8	C	10.5	9.1
4	16	0745	8	C	10.0	10.0
4	16	1345	8	C	11.0	10.5
4	16	1745	8	C	12.0	10.2
4	16	2045	8	C	12.0	10.4
4	16	2345	8	C	11.8	9.7
4	17	0145	8	C	11.2	9.5
4	17	0455	8	C	11.3	9.4
4	17	0953	8	C	11.2	9.3
4	17	1241	8	C	11.5	9.0
4	17	1535	8	C	12.0	9.2
4	17	1835	8	C	11.5	9.7
4	17	2135	8	C	11.8	9.8
4	18	0030	8	C	11.5	9.5
4	18	0335	8	C	12.0	9.0
4	18	0635	8	C	11.5	9.0
4	18	0935	8	C	12.0	8.5
4	18	1236	8	C	12.0	8.6
4	18	1536	8	C	13.0	8.8
4	18	1835	8	C	14.0	9.7
4	18	2130	8	C	14.0	10.1
4	18	0045	8	C	14.0	9.0
4	18	0335	8	C	13.0	8.8
4	19	0630	8	C	12.5	8.0
4	19	0930	8	C	12.8	7.4
4	19	1232	8	C	13.0	7.3
4	19	1533	8	C	13.0	7.4
4	19	1825	8	C	14.0	9.0
4	19	2125	8	C	14.0	9.0
4	20	0045	8	C	0.0	0.0
4	20	0335	8	C	14.0	7.6
4	20	0630	8	C	13.5	7.2

946510424

STORM #1 - RIVER SAMPLING
DUNDEE DAM UPSTREAM - LEVEL BC - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
4	20	0933	8	C	13.1	8.0
4	20	1235	8	C	13.1	7.7
4	20	1532	8	C	14.0	8.1
4	20	1835	8	C	13.2	8.6
4	20	2135	8	C	12.8	8.8
4	21	0030	8	C	11.8	9.2
4	21	0330	8	C	11.5	9.5
4	21	0630	8	C	12.0	8.6
4	21	0935	8	C	11.2	10.0
4	21	1235	8	C	12.0	9.1
4	21	1525	8	C	12.0	8.5
4	21	1832	8	C	11.7	8.2
4	21	2132	8	C	11.5	7.7
4	22	0035	8	C	11.5	8.2
4	22	0335	8	C	11.5	8.4
4	22	0635	8	C	12.0	9.2
4	22	0933	8	C	12.0	8.8
4	22	1232	8	C	13.0	9.4
4	22	1531	8	C	13.5	9.3
4	22	1836	8	C	12.9	8.7
4	22	2136	8	C	12.5	8.2
4	23	0030	8	C	12.5	7.7
4	23	0335	8	C	13.0	7.5
4	23	0640	8	C	13.0	7.5
4	23	0933	8	C	13.8	9.9
4	23	1233	8	C	13.5	9.4
4	23	1531	8	C	13.0	9.0
4	23	1831	8	C	13.5	8.7
4	23	2131	8	C	12.2	8.3
4	24	0040	8	C	12.0	6.2
4	24	0335	8	C	12.5	7.0
4	24	0640	8	C	12.5	8.3

946510425

STØRM #1

DUNDEE DAM

DØWNSTREAM

4-14/4-24-81

1/2 DEPTH

946510426

STORM #1 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL AT - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
4	14	1020	6	C	13.0	8.8
4	14	1324	6	C	14.0	10.2
4	14	1725	6	C	12.2	9.8
4	14	2025	6	C	12.2	9.4
4	14	2325	6	C	12.0	9.7
4	15	0152	6	C	11.5	9.8
4	15	0445	6	C	11.0	9.8
4	15	0830	6	C	10.9	10.2
4	15	1135	6	C	11.1	11.5
4	15	1435	6	C	11.5	11.6
4	15	1710	6	C	11.5	10.2
4	15	2010	6	C	11.4	9.9
4	15	2320	6	C	11.0	9.8
4	16	0140	6	C	11.0	9.6
4	16	0440	6	C	10.2	10.3
4	16	0840	6	C	10.1	10.9
4	16	1443	6	C	11.5	10.9
4	16	1805	6	C	11.9	10.3
4	16	2105	6	C	12.0	10.2
4	17	0032	6	C	12.0	10.0
4	17	0335	6	C	11.5	9.8
4	17	0625	6	C	11.2	10.2
4	17	0930	6	C	11.5	10.2
4	17	1219	6	C	11.5	10.1
4	17	1517	6	C	11.8	9.9
4	17	1817	6	C	11.7	10.2
4	17	2117	6	C	11.5	10.1
4	18	0015	6	C	12.0	10.1
4	18	0315	6	C	11.5	10.3
4	18	0615	6	C	11.5	10.4
4	18	0917	6	C	12.0	10.4
4	18	1215	6	C	12.0	10.0
4	18	1517	6	C	13.0	9.7
4	18	1815	6	C	13.3	10.0
4	18	2115	6	C	13.2	10.2
4	19	0035	6	C	13.0	9.7
4	19	0320	6	C	13.0	9.5
4	19	0630	6	C	13.0	9.6
4	19	0914	6	C	13.0	10.4
4	19	1215	6	C	13.5	10.2
4	19	1516	6	C	13.5	10.2
4	19	1805	6	C	14.0	9.8
4	19	2112	6	C	13.5	9.6
4	20	0015	6	C	0.0	0.0

946510427

STORM #1 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL 6C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
4	20	0320	6	C	13.5	8.4
4	20	0600	6	C	13.5	8.6
4	20	0915	6	C	14.0	9.7
4	20	1217	6	C	14.0	9.9
4	20	1515	6	C	14.0	10.2
4	20	1820	6	C	13.0	9.7
4	20	2120	6	C	12.0	9.6
4	21	0020	6	C	11.5	10.3
4	21	0320	6	C	10.8	10.3
4	21	0620	6	C	10.5	11.6
4	21	0915	6	C	11.2	11.4
4	21	1215	6	C	13.0	11.2
4	21	1509	6	C	13.0	10.9
4	21	1818	6	C	12.0	9.5
4	21	2118	6	C	11.2	9.1
4	22	0020	6	C	11.0	9.2
4	22	0320	6	C	10.5	9.2
4	22	0620	6	C	10.5	9.8
4	22	0916	6	C	12.0	10.8
4	22	1215	6	C	13.8	11.0
4	22	1514	6	C	14.0	10.6
4	22	1821	6	C	12.4	10.0
4	22	2121	6	C	12.3	9.5
4	23	0020	6	C	12.5	9.5
4	23	0325	6	C	12.0	9.5
4	23	0630	6	C	12.0	9.5
4	23	0916	6	C	12.5	9.9
4	23	1215	6	C	13.0	10.1
4	23	1516	6	C	13.0	9.8
4	23	1816	6	C	13.0	9.8
4	23	2116	6	C	12.8	9.4
4	24	0025	6	C	13.0	8.9
4	24	0320	6	C	12.5	9.1
4	24	0625	6	C	12.3	9.2

946510428

Baseline Sampling
July 1981

946510429

BASELINE

KEARNY

PØINT

7-14/7-24-81

1/3 DEPTH

946510430

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	14	820	8.3	1	A	7.49	4.0	4.1	0.793	0.095	0.329	NA	NA	22.57	26.2	4.20	17.2
7	14	921	9.3	1	A	7.55	3.8	3.0	0.912	0.095	0.324	1.83	0.985	18.81	26.2	3.05	18.0
7	14	1020	10.3	1	A	7.56	3.5	3.5	0.992	0.086	0.416	NA	NA	30.10	26.1	2.90	NA
7	14	1122	11.4	1	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	26.5	3.60	16.0
7	14	1220	12.3	1	A	7.49	3.7	2.8	0.995	0.095	0.346	1.00	0.647	18.81	27.0	3.65	17.5
7	14	1322	13.4	1	A	7.44	4.0	1.8	0.997	0.095	0.316	NA	NA	14.16	27.5	3.55	18.2
7	14	1420	14.3	1	A	7.47	3.7	1.8	0.998	0.095	0.346	1.00	0.597	24.45	26.8	4.30	15.5
7	14	1519	15.3	1	A	7.52	3.7	1.7	0.943	0.095	0.319	NA	NA	16.93	27.4	5.20	17.1
7	14	1619	16.3	1	A	7.71	3.8	2.2	0.964	0.072	0.218	1.18	0.736	26.33	28.0	7.50	17.1
7	14	1715	17.3	1	A	7.60	4.6	3.2	0.871	0.062	0.196	NA	NA	31.98	27.1	6.00	18.0
7	14	1819	18.3	1	A	7.81	4.3	3.0	0.790	0.039	0.131	0.86	0.593	30.10	25.5	6.70	16.5
7	14	1914	19.2	1	A	7.86	4.6	3.2	0.755	0.086	0.257	NA	NA	31.98	26.5	6.20	19.0
7	14	2016	20.3	1	A	7.80	3.9	3.2	0.855	0.081	0.249	0.92	0.581	22.57	25.0	6.60	18.8
7	14	2115	21.3	1	A	7.75	4.4	3.0	0.606	0.058	0.189	NA	NA	26.33	25.1	6.20	18.1
7	14	2215	22.3	1	A	7.70	4.6	2.8	0.783	0.053	0.181	0.79	0.519	30.10	25.0	5.60	17.5
7	14	2314	23.2	1	A	7.50	4.5	2.7	0.671	0.048	0.170	NA	NA	16.93	25.0	5.40	17.0
7	15	2[illegible]	24.3	1	A	7.53	4.2	2.1	0.965	0.058	0.249	0.41	0.406	22.57	25.8	4.10	15.5
7	15	118	25.3	1	A	7.46	4.3	1.5	0.807	0.044	0.184	NA	NA	20.69	25.0	4.00	17.3
7	15	22[illegible]	26.3	1	A	7.40	4.7	2.2	0.861	0.044	0.220	0.97	0.494	20.69	25.1	3.50	16.2
7	15	325	27.4	1	A	7.42	4.1	1.8	0.906	0.086	0.375	1.16	0.474	26.33	25.1	3.10	14.5
7	15	422	28.4	1	A	7.49	4.2	2.0	0.975	0.039	0.192	1.37	0.702	18.81	25.5	4.00	16.8
7	15	51[illegible]	29.3	1	A	7.58	5.5	2.2	0.984	0.048	0.140	NA	NA	20.69	26.0	3.00	18.0
7	15	619	30.4	1	A	7.61	5.4	2.0	0.993	0.048	0.142	1.23	0.640	18.81	24.9	4.40	19.5
7	15	721	31.3	1	A	7.61	5.7	3.4	0.841	0.095	0.304	NA	NA	24.45	24.9	4.40	20.0
7	15	819	32.3	1	A	7.67	5.2	2.0	0.890	0.104	0.303	1.21	0.651	9.44	25.0	3.85	NA
7	15	92[illegible]	33.3	1	A	7.67	5.6	2.9	0.864	0.095	0.280	NA	NA	18.81	25.5	4.20	19.8

946510431

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	15	1020	34.3	1	A	7.63	5.0	0.9	0.897	0.095	0.319	0.95	0.574	18.88	25.0	3.70	19.5
7	15	1118	35.3	1	A	7.71	4.3	1.1	0.872	0.081	0.342	NA	NA	26.33	25.5	4.40	19.0
7	15	1221	36.3	1	A	7.66	4.3	1.1	0.929	0.076	0.290	1.00	0.592	24.45	25.8	4.20	18.8
7	15	1320	37.3	1	A	7.55	4.5	0.6	0.931	0.095	0.307	NA	NA	11.46	25.8	4.95	16.7
7	15	1419	38.3	1	A	7.58	4.3	0.9	0.940	0.100	0.315	1.04	0.631	11.46	25.7	4.10	18.6
7	15	1518	39.3	1	A	7.62	4.8	1.1	0.899	0.100	0.378	NA	NA	39.50	26.0	5.05	15.9
7	15	1615	40.3	1	A	7.71	4.8	1.1	0.567	0.048	0.181	0.73	0.528	20.69	26.5	6.10	18.8
7	15	1715	41.3	1	A	7.80	5.5	1.5	0.958	0.067	0.206	NA	NA	30.10	27.5	5.60	18.3
7	15	1814	42.2	1	A	7.88	5.7	1.6	0.712	0.090	0.260	0.85	0.488	30.10	26.8	7.50	19.8
7	15	1915	43.3	1	A	7.77	6.8	1.8	0.632	0.081	0.244	NA	NA	28.22	26.0	5.60	20.8
7	15	2011	44.2	1	A	7.82	6.7	1.5	0.661	0.053	0.180	0.90	0.599	39.50	25.3	4.60	20.5
7	15	2115	45.3	1	A	7.85	7.0	1.6	0.499	0.030	0.097	0.76	0.641	26.33	25.0	6.40	19.5
7	15	2216	46.3	1	A	7.85	5.4	1.8	0.850	0.067	0.223	1.30	0.646	6.07	25.0	5.00	19.3
7	15	2310	47.2	1	A	7.83	4.7	1.6	0.645	0.030	0.095	NA	NA	20.69	25.3	4.80	19.0
7	16	25	48.4	1	A	7.77	5.9	1.6	0.576	0.034	0.148	0.73	0.451	24.45	25.0	4.20	17.9
7	16	125	49.4	1	A	7.73	5.0	1.5	0.878	0.076	0.306	NA	NA	33.87	25.0	4.60	16.9
7	16	220	50.3	1	A	7.69	4.9	0.9	0.923	0.076	0.332	1.34	0.640	31.98	25.1	4.25	16.0
7	16	321	51.3	1	A	7.62	5.1	1.5	0.730	0.067	0.340	NA	NA	43.26	25.2	3.50	16.1
7	16	420	52.3	1	A	7.58	5.5	1.2	0.997	0.039	0.199	1.37	0.670	20.23	25.0	4.00	15.8
7	16	520	53.5	1	A	7.53	8.1	0.4	0.963	0.104	0.337	NA	NA	18.88	25.3	4.10	18.3
7	16	630	54.5	1	A	7.67	5.3	1.5	0.957	0.104	0.287	1.20	0.662	33.86	25.0	4.50	19.0
7	16	724	55.4	1	A	7.72	7.1	0.8	0.896	0.086	0.240	NA	NA	26.33	25.1	4.30	19.0
7	16	820	56.3	1	A	7.56	3.7	1.6	0.831	0.104	0.292	1.21	0.727	12.14	24.7	4.10	19.9
7	16	92	57.3	1	A	7.58	3.1	1.4	0.729	0.095	0.295	NA	NA	11.46	24.9	4.30	19.6
7	16	1019	58.3	1	A	7.58	3.5	1.0	0.907	0.104	0.321	1.30	0.603	37.62	25.6	4.15	18.3
7	16	1120	59.3	1	A	7.60	3.3	1.0	0.951	0.104	0.298	NA	NA	31.98	25.8	4.50	18.1

946510432

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	16	1221	60.3	1	A	7.48	3.4	0.8	0.952	0.104	0.318	1.32	0.588	20.69	25.6	4.20	17.5
7	16	1321	61.3	1	A	7.49	3.5	0.6	0.945	0.095	0.339	NA	NA	39.50	26.0	4.70	16.4
7	16	1418	62.3	1	A	7.45	3.9	2.4	0.929	0.095	0.369	1.14	0.659	30.10	25.9	5.00	15.5
7	16	1520	63.3	1	A	7.44	4.5	0.4	0.952	0.095	0.328	NA	NA	7.58	26.0	5.15	14.9
7	16	1614	64.2	1	A	7.43	8.7	4.6	1.090	0.095	0.369	1.79	1.190	26.33	25.9	4.70	17.3
7	16	1712	65.2	1	A	7.51	5.7	3.6	0.872	0.076	0.245	NA	NA	37.62	26.0	4.90	19.0
7	16	1816	66.3	1	A	7.69	4.1	2.0	0.869	0.095	0.268	1.52	0.807	33.86	25.7	5.40	19.9
7	16	1915	67.3	1	A	7.75	3.7	1.8	0.721	0.081	0.236	NA	NA	31.98	25.0	5.40	20.3
7	16	2016	68.3	1	A	7.72	3.9	1.8	0.720	0.039	0.131	0.89	0.555	33.86	25.0	5.20	20.3
7	16	2112	69.2	1	A	7.75	3.8	1.4	0.712	0.058	0.166	NA	NA	30.10	25.0	4.20	20.3
7	16	2215	70.3	1	A	7.65	4.7	1.6	0.757	0.053	0.270	1.37	0.695	12.14	25.0	5.80	19.8
7	16	2313	71.2	1	A	7.59	4.2	1.2	0.905	0.053	0.127	NA	NA	17.53	25.3	4.75	19.5
7	17	21	72.3	1	A	7.54	4.4	0.8	0.868	0.058	0.178	1.08	0.587	18.81	25.1	4.50	18.1
7	17	125	73.4	1	A	7.50	4.6	1.2	0.942	0.072	0.257	NA	NA	35.74	25.2	4.20	17.0
7	17	220	74.3	1	A	7.46	5.0	1.2	0.745	0.048	0.222	1.14	0.604	14.84	25.3	4.20	16.0
7	17	324	75.4	1	A	7.44	5.1	1.2	0.891	0.067	0.291	NA	NA	33.86	25.1	3.80	14.9
7	17	427	76.4	1	A	7.46	5.7	1.4	0.962	0.076	0.333	1.44	0.646	41.38	25.5	3.90	14.0
7	17	531	77.5	1	A	7.45	5.8	1.6	0.915	0.062	0.226	NA	NA	31.98	25.0	3.70	16.5
7	17	624	78.4	1	A	7.53	6.1	1.0	0.801	0.044	0.129	1.49	0.616	26.33	26.0	3.50	17.0
7	17	723	79.4	1	A	7.57	5.8	1.4	0.836	0.030	0.087	NA	NA	24.45	25.1	3.80	18.9
7	17	819	80.3	1	A	7.50	5.7	1.8	0.734	0.086	0.356	0.99	0.596	22.26	24.5	4.70	19.0
7	17	916	81.3	1	A	7.60	5.4	2.0	0.825	0.104	0.193	NA	NA	30.10	24.9	4.05	19.0
7	17	1021	82.3	1	A	7.60	5.8	2.0	0.726	0.090	0.271	0.93	0.609	26.33	25.1	4.50	18.5
7	17	1119	83.3	1	A	7.5	5.3	2.1	1.000	0.114	0.315	NA	NA	20.23	26.0	4.80	18.0
7	17	1220	84.3	1	A	7.50	6.6	1.5	1.060	0.114	0.325	1.26	0.628	30.10	26.0	4.20	17.2
7	17	1321	85.3	1	A	7.56	7.3	1.5	1.030	0.104	0.348	NA	NA	45.14	26.0	5.60	16.0

94651043 3

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1419	86.3	1	A	7.50	7.5	1.5	1.000	0.095	0.347	1.29	0.673	14.16	25.9	4.40	15.8
7	17	1520	87.3	1	A	7.40	7.0	1.4	1.080	0.100	0.368	NA	NA	39.50	25.9	3.70	15.4
7	17	1612	88.2	1	A	7.40	8.0	1.8	0.969	0.096	0.409	3.57	0.637	28.22	25.9	4.80	16.1
7	17	1712	89.2	1	A	7.50	8.2	2.4	0.914	0.101	0.402	NA	NA	50.79	26.0	4.90	16.3
7	17	1811	90.2	1	A	7.60	6.7	2.6	1.040	0.110	0.305	3.64	0.717	47.02	26.1	4.51	18.1
7	17	1915	91.3	1	A	7.70	6.0	2.0	0.419	0.020	0.262	NA	NA	41.38	26.0	4.80	18.1
7	17	2010	92.2	1	A	7.70	5.7	1.4	NA	0.063	0.184	1.15	0.695	50.79	25.5	4.40	19.0
7	17	2115	93.3	1	A	7.60	5.6	2.2	NA	0.096	0.272	NA	NA	37.62	25.0	4.00	19.8
7	17	2215	94.3	1	A	7.70	5.4	1.2	NA	0.044	0.142	0.63	0.493	43.26	25.1	3.80	19.8
7	17	2314	95.2	1	A	7.60	5.7	1.5	0.505	0.044	0.146	NA	NA	35.74	25.8	4.40	18.6
7	18	23	96.4	1	A	7.60	5.8	1.1	0.777	0.085	0.251	3.44	0.578	37.62	25.6	4.20	19.2
7	18	118	97.3	1	A	7.50	6.2	2.0	0.977	0.082	0.247	NA	NA	33.86	25.5	4.00	18.5
7	18	225	98.4	1	A	7.50	5.7	1.6	0.730	0.037	0.137	3.32	0.760	41.38	26.0	3.30	16.5
7	18	325	99.4	1	A	7.40	8.5	3.0	0.908	0.054	0.229	NA	NA	48.91	26.2	4.00	16.8
7	18	518	101.3	1	A	7.40	7.8	2.2	0.878	0.073	0.309	2.67	0.635	60.19	26.5	3.75	16.0
7	18	627	102.4	1	A	7.50	6.0	1.4	1.100	0.082	0.205	NA	NA	26.33	27.0	4.00	18.1
7	18	720	103.3	1	A	7.50	7.2	2.6	0.724	0.101	0.250	NA	NA	37.62	27.5	3.80	19.0
7	18	821	104.3	1	A	7.60	6.3	2.0	0.843	0.095	0.281	3.79	0.618	31.98	26.1	4.30	19.0
7	18	922	105.4	1	A	7.60	6.6	2.4	0.770	0.092	0.272	NA	NA	18.81	26.0	4.00	18.2
7	18	1020	106.3	1	A	7.60	5.0	1.6	0.474	0.035	0.107	NA	NA	30.10	26.0	4.50	18.5
7	18	1125	107.4	1	A	7.60	4.8	1.6	0.739	0.106	0.289	NA	NA	20.69	26.0	4.60	19.1
7	18	1224	108.4	1	A	7.60	5.6	2.6	0.977	0.114	0.337	2.94	0.616	35.74	27.0	5.50	17.1
7	18	1325	109.4	1	A	7.60	5.2	2.1	0.942	0.106	0.331	NA	NA	63.95	27.0	7.50	17.0
7	18	1423	110.4	1	A	7.50	5.5	3.0	0.930	0.101	0.331	2.35	0.579	50.79	27.0	7.70	15.8
7	18	1514	111.2	1	A	7.50	5.8	3.0	0.977	0.097	0.377	NA	NA	41.38	27.0	7.50	15.5
7	18	1613	112.3	1	A	7.50	9.5	3.4	0.873	0.101	0.409	2.50	0.693	56.43	27.7	4.70	15.0

946510434

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	18	1712	113.2	1	A	7.60	7.0	3.0	0.722	0.101	0.411	NA	NA	67.72	27.9	4.50	15.3
7	18	1812	114.2	1	A	7.80	5.6	3.0	0.698	0.092	0.369	2.49	0.576	82.76	27.9	6.70	16.1
7	18	1913	115.2	1	A	7.70	6.9	2.7	0.778	0.101	0.301	NA	NA	48.91	27.6	5.80	17.3
7	18	2014	116.2	1	A	7.70	5.7	2.6	0.557	0.032	0.102	1.09	0.531	60.19	26.9	5.40	18.1
7	18	2112	117.2	1	A	7.70	5.8	2.2	0.837	0.075	0.230	NA	NA	35.74	26.2	4.60	18.1
7	18	2234	118.1	1	A	7.70	5.2	2.6	0.590	0.056	0.168	3.05	0.439	50.79	26.1	5.10	19.5
7	18	2310	119.2	1	A	7.70	5.0	2.1	0.833	0.066	0.192	NA	NA	45.14	26.5	5.20	19.3
7	19	15	120.3	1	A	7.60	5.3	2.6	0.808	0.073	0.209	2.41	0.497	35.74	25.8	4.10	19.7
7	19	117	121.3	1	A	7.60	6.2	3.0	0.645	0.037	0.122	NA	NA	37.62	26.5	4.20	18.0
7	19	216	122.3	1	A	7.60	5.7	2.7	0.562	0.037	0.147	2.16	0.535	41.38	27.0	5.00	16.9
7	19	319	123.3	1	A	7.60	6.0	3.4	0.557	0.040	0.148	NA	NA	48.91	26.9	5.00	16.2
7	19	421	124.3	1	A	7.50	7.1	3.6	0.899	0.095	0.398	2.55	0.653	50.79	27.0	4.60	16.0
7	19	518	125.3	1	A	7.50	6.4	3.8	0.589	0.041	0.214	NA	NA	48.91	27.0	4.40	13.1
7	19	625	126.4	1	A	7.50	6.9	3.2	0.792	0.063	0.289	2.32	0.618	50.79	26.1	4.30	14.0
7	19	714	127.2	1	A	7.53	7.8	5.5	1.090	0.095	0.368	NA	NA	58.31	26.0	4.50	17.0
7	19	821	128.3	1	A	7.57	6.6	7.8	0.909	0.061	0.214	2.43	0.622	24.45	26.0	3.70	18.5
7	19	922	129.4	1	A	7.64	5.5	7.4	0.744	0.095	0.290	NA	NA	18.81	24.9	4.70	19.2
7	19	1023	130.4	1	A	7.72	4.6	7.4	0.791	0.090	0.256	2.26	0.657	33.66	26.2	6.50	18.4
7	19	1125	131.4	1	A	7.65	4.0	7.0	0.758	0.056	0.171	NA	NA	28.22	25.0	3.70	18.2
7	19	1225	132.4	1	A	7.67	4.5	7.4	0.793	0.095	0.268	1.82	0.814	43.26	26.8	4.80	17.7
7	19	1320	133.3	1	A	7.66	4.5	7.4	0.968	0.056	0.148	NA	NA	26.33	26.2	4.00	17.9
7	19	1423	134.4	1	A	7.62	4.9	7.4	0.933	0.104	0.324	2.74	0.771	37.62	26.9	4.80	17.1
7	19	1521	135.3	1	A	7.61	5.4	7.2	0.735	0.061	0.226	NA	NA	48.91	26.8	4.60	16.1
7	19	161	136.2	1	A	7.54	5.1	7.4	0.913	0.095	0.355	2.37	0.661	35.74	26.8	4.60	16.1
7	19	1712	137.2	1	A	7.64	5.3	7.6	0.846	0.070	0.316	NA	NA	54.55	27.7	5.50	14.3
7	19	1810	138.2	1	A	7.77	5.1	8.0	0.785	0.095	0.375	2.69	0.763	60.19	27.1	7.50	15.6

946510435

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	19	1911	139.2	1	A	7.74	6.1	7.2	0.845	0.066	0.238	NA	NA	47.02	27.3	6.40	16.9
7	19	2010	140.2	1	A	7.68	4.7	0.8	0.980	0.114	0.283	2.37	0.615	26.33	27.0	5.00	18.1
7	19	2114	141.2	1	A	7.73	4.7	0.4	0.764	0.095	0.279	NA	NA	37.62	26.2	5.20	18.7
7	19	2210	142.2	1	A	7.69	5.9	0.4	0.873	0.080	0.239	5.23	0.567	30.09	25.4	4.10	19.2
7	19	2308	143.1	1	A	7.70	4.6	0.8	0.721	0.095	0.275	NA	NA	30.09	26.0	4.75	19.3
7	20	16	144.3	1	A	7.70	4.1	0.4	0.810	0.061	0.181	2.29	0.588	30.09	25.5	4.00	19.0
7	20	117	145.3	1	A	7.62	5.1	0.4	0.914	0.104	0.301	NA	NA	35.74	27.0	4.50	18.0
7	20	219	146.3	1	A	7.61	4.8	0.4	0.758	0.046	0.163	3.06	0.553	37.62	27.2	4.20	17.3
7	20	320	147.3	1	A	7.56	4.8	0.8	0.816	0.027	0.160	NA	NA	43.26	27.3	3.90	16.2
7	20	415	148.3	1	A	7.51	6.1	1.8	0.732	0.066	0.252	2.20	0.868	37.62	27.1	4.10	15.0
7	20	522	149.4	1	A	7.49	4.8	2.8	0.915	0.051	0.253	NA	NA	39.50	27.0	3.80	13.3
7	20	618	150.3	1	A	7.47	5.7	0.4	0.962	0.066	0.308	3.13	0.824	47.02	27.2	3.10	13.0
7	20	713	151.2	1	A	7.46	5.0	0.4	0.577	0.066	0.339	NA	NA	55.49	27.1	3.30	15.5
7	20	822	152.4	1	A	7.51	5.1	0.4	1.100	0.120	0.291	1.76	0.943	22.57	27.8	2.80	17.2
7	20	919	153.3	1	A	7.60	4.6	0.4	0.864	0.092	0.250	NA	NA	37.62	27.1	2.50	18.0
7	20	1022	154.4	1	A	7.61	4.2	0.4	0.768	0.054	0.146	2.77	0.552	37.62	28.8	2.60	18.1
7	20	1126	155.4	1	A	7.62	4.6	0.4	0.778	0.073	0.225	NA	NA	39.50	27.7	2.90	18.9
7	20	1223	156.4	1	A	7.61	3.8	0.4	0.781	0.092	0.246	2.54	0.565	16.93	27.1	2.60	18.5
7	20	1321	157.3	1	A	7.55	4.1	0.4	0.989	0.110	0.289	NA	NA	48.91	28.0	2.10	18.5
7	20	1420	158.3	1	A	7.50	4.7	0.6	1.060	0.110	0.309	4.33	0.615	41.38	29.0	1.60	16.6
7	20	1520	159.3	1	A	7.51	4.8	0.4	0.983	0.101	0.327	NA	NA	39.50	28.2	2.10	16.2
7	20	1611	160.2	1	A	7.51	4.6	0.4	0.637	0.082	0.317	2.84	0.712	52.67	26.9	2.60	15.3
7	20	1710	161.2	1	A	7.44	4.9	0.6	0.964	0.096	0.446	NA	NA	52.67	26.9	3.20	14.3
7	20	1815	162.3	1	A	7.42	5.6	0.8	0.915	0.096	0.398	3.56	0.787	62.07	26.8	3.60	14.2
7	20	1909	163.1	1	A	7.48	5.2	0.6	0.973	0.101	0.402	NA	NA	43.26	26.5	4.40	14.9
7	20	2011	164.2	1	A	NA	NA	NA	NA	NA	NA	NA	NA	28.22	27.1	3.80	16.9

94651043 6

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2113	165.2	1	A	7.64	3.6	0.4	0.793	0.110	0.295	NA	NA	35.74	26.7	3.30	18.5
7	20	2215	166.3	1	A	7.61	4.6	0.4	0.997	0.106	0.272	2.94	0.676	20.69	28.0	3.30	18.0
7	2[illegible]	2310	167.2	1	A	7.54	4.0	0.4	0.947	0.096	0.261	NA	NA	24.45	28.5	3.20	17.5
7	21	14	168.2	1	A	7.53	3.8	0.4	0.987	0.101	0.276	3.23	0.613	28.22	27.5	2.60	18.0
7	21	122	169.4	1	A	7.46	4.2	0.4	0.848	0.054	0.157	NA	NA	30.10	26.5	3.10	19.1
7	21	219	170.3	1	A	7.43	4.6	0.4	1.040	0.092	0.366	4.10	0.294	43.26	27.0	2.90	15.2
7	21	317	171.3	1	A	7.44	4.5	0.4	0.650	0.025	0.123	NA	NA	45.14	27.2	1.60	13.5
7	21	423	172.4	1	A	7.34	5.2	0.4	0.784	0.058	0.385	3.00	0.552	28.22	27.5	0.70	11.0
7	21	525	173.4	1	A	7.33	6.0	1.2	1.060	0.214	0.308	NA	NA	35.74	28.0	0.35	8.8
7	21	614	174.2	1	A	7.33	6.7	4.0	1.160	0.479	0.240	3.57	0.595	56.43	27.1	0.15	6.5
7	21	714	175.2	1	A	7.34	7.3	4.0	0.979	0.342	0.156	NA	NA	35.74	27.0	0.10	7.1
7	21	821	176.3	1	A	7.20	5.3	0.8	1.030	0.073	0.222	4.55	0.701	33.86	26.3	0.90	12.7
7	21	920	177.3	1	A	7.40	5.0	2.6	1.250	0.068	0.176	NA	NA	22.57	27.4	1.75	16.7
7	21	1023	178.4	1	A	7.40	5.0	0.4	0.744	0.030	0.168	1.92	0.405	39.50	25.9	3.40	18.3
7	21	1125	179.4	1	A	7.50	3.8	0.4	0.636	0.044	0.135	NA	NA	16.93	25.9	3.60	18.4
7	21	1219	180.3	1	A	7.50	4.0	0.4	0.554	0.044	0.144	2.22	0.630	19.56	25.2	3.15	19.2
7	21	1323	181.4	1	A	7.50	3.7	0.4	1.020	0.252	0.274	NA	NA	26.33	25.1	2.50	19.8
7	21	1425	182.4	1	A	7.40	4.2	0.4	0.696	0.120	0.379	2.39	0.469	24.45	26.4	1.75	17.5
7	21	1518	183.3	1	A	7.40	6.3	2.1	0.837	0.129	0.366	NA	NA	82.76	26.8	1.30	14.3
7	21	1620	184.1	1	A	7.40	4.0	0.4	0.936	0.090	0.248	NA	NA	28.22	26.6	1.50	9.5
7	21	1719	185.2	1	A	7.30	6.0	0.8	1.190	0.167	0.507	1.99	0.682	13.49	26.4	1.15	7.1
7	21	1815	186.3	1	A	7.40	4.5	0.4	1.050	0.148	0.598	NA	NA	24.28	NA	0.75	4.9
7	21	1911	187.2	1	A	7.40	6.7	1.4	1.010	0.157	0.714	2.33	0.647	26.33	27.1	0.25	9.5
7	21	2020	188.3	1	A	7.30	5.4	1.2	0.675	0.062	0.565	NA	NA	26.33	26.5	2.90	13.5
7	21	2114	189.2	1	A	7.40	5.5	0.8	1.210	0.152	0.402	3.81	0.965	22.57	27.0	2.40	16.3
7	21	2213	190.2	1	A	7.50	4.5	1.8	1.130	0.138	0.351	NA	NA	28.22	26.7	2.90	17.1

946510437

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	21	2310	191.2	1	A	7.50	4.5	1.2	0.614	0.038	0.420	NA	NA	18.88	26.1	3.45	17.9
7	22	14	192.2	1	A	7.50	3.8	1.6	0.872	0.100	0.295	NA	NA	22.93	25.0	2.85	19.5
7	22	111	193.2	1	A	7.50	4.0	1.2	0.874	0.100	0.319	3.25	0.574	8.77	25.0	2.48	20.0
7	22	216	194.3	1	A	7.50	3.6	1.1	0.454	0.020	0.446	NA	NA	16.19	25.0	2.90	20.0
7	22	315	195.3	1	A	7.40	3.5	0.9	NA	NA	NA	NA	NA	16.19	25.5	2.50	17.9
7	22	414	196.2	1	A	7.40	4.6	0.8	0.888	0.081	0.340	NA	NA	17.53	26.0	1.65	16.5
7	22	524	197.4	1	A	7.40	5.3	1.2	1.060	0.129	0.771	5.75	0.708	20.91	25.8	0.30	7.8
7	22	655	198.9	1	A	7.30	4.9	0.4	0.753	0.105	0.578	NA	NA	19.79	26.0	0.25	6.5
7	22	820	200.3	1	A	7.20	7.5	3.9	0.808	0.138	0.714	2.06	0.580	15.05	25.7	0.25	6.0
7	22	918	201.3	1	A	7.40	3.7	1.2	1.070	0.110	0.343	NA	NA	20.69	26.2	1.00	13.5
7	22	1022	202.4	1	A	7.40	3.8	3.0	1.130	0.119	0.377	2.42	0.707	16.93	26.5	1.75	16.8
7	22	1120	203.3	1	A	7.40	4.7	3.8	1.120	0.129	0.426	NA	NA	22.57	26.4	2.48	16.0
7	22	1223	204.4	1	A	7.50	4.0	3.8	0.834	0.086	0.292	2.20	0.654	31.98	25.8	3.10	17.5
7	22	1321	205.3	1	A	7.50	4.3	3.0	0.817	0.086	0.279	NA	NA	11.29	25.5	3.10	18.6
7	22	1422	206.4	1	A	7.50	3.2	2.6	0.831	0.090	0.287	2.42	0.480	16.93	25.1	3.40	19.6
7	22	1518	207.3	1	A	7.50	3.5	3.2	1.050	0.119	0.383	NA	NA	35.74	27.0	3.00	15.8
7	22	1619	208.3	1	A	7.50	4.0	3.2	0.917	0.181	0.718	2.22	0.638	48.91	26.8	1.60	12.5
7	22	1720	209.3	1	A	7.40	3.6	2.6	0.756	0.038	0.296	NA	NA	16.93	26.1	1.35	13.1
7	22	1821	210.3	1	A	7.40	3.7	2.8	0.690	0.062	0.587	NA	NA	20.69	26.1	1.20	13.0
7	22	1926	211.3	1	A	7.40	4.3	3.3	1.130	0.133	0.461	NA	NA	37.62	26.2	1.70	8.2
7	22	2021	212.3	1	A	7.50	3.4	3.0	1.040	0.119	0.382	2.74	0.761	22.57	26.1	1.20	12.5
7	22	2122	213.4	1	A	7.40	4.7	3.8	1.030	0.138	0.470	NA	NA	37.62	26.3	2.45	16.0
7	22	2219	214.3	1	A	7.50	3.9	3.0	1.030	0.105	0.326	2.24	0.630	18.81	26.5	2.30	18.2
7	22	2323	215.4	1	A	7.50	3.8	2.8	1.030	0.133	0.422	NA	NA	26.33	26.0	2.70	17.5
7	23	13	216.2	1	A	7.60	3.5	3.2	0.959	0.110	0.378	1.93	0.588	22.57	24.5	2.60	19.9
7	23	116	217.3	1	A	7.60	3.6	2.8	0.947	0.105	0.341	NA	NA	22.57	24.2	2.70	20.0

946510438

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	23	215	218.3	1	A	7.50	4.4	3.3	0.704	0.062	0.230	NA	NA	9.41	24.5	2.50	19.5
7	23	313	219.2	1	A	7.50	3.7	3.3	0.731	0.052	0.201	NA	NA	22.57	24.5	2.20	20.0
7	23	419	220.3	1	A	7.40	3.3	3.2	1.040	0.129	0.432	2.42	0.766	24.45	25.0	2.00	18.5
7	23	520	221.3	1	A	7.40	4.3	3.3	0.959	0.167	0.587	NA	NA	28.22	25.3	1.00	11.4
7	23	618	222.3	1	A	7.30	4.4	3.6	0.801	0.100	0.357	1.60	0.548	22.57	25.1	1.05	12.5
7	23	720	223.3	1	A	7.30	4.1	4.7	0.726	0.138	0.524	NA	NA	26.33	25.5	1.05	16.8
7	23	819	224.3	1	A	7.33	5.4	2.7	1.050	0.148	0.604	2.67	0.770	28.22	25.0	0.70	9.0
7	23	921	225.3	1	A	7.40	3.5	0.6	1.080	0.124	0.394	NA	NA	15.51	25.0	0.54	10.2
7	23	1018	226.3	1	A	7.45	3.6	1.5	1.190	0.110	0.384	3.04	0.844	18.88	26.0	1.70	17.2
7	23	1119	227.3	1	A	7.48	4.0	1.4	1.100	0.110	0.338	NA	NA	8.09	25.5	1.80	17.9
7	23	1220	228.3	1	A	7.59	3.7	1.4	0.907	0.100	0.329	1.93	0.678	18.81	25.5	3.30	17.3
7	23	1318	229.3	1	A	7.58	3.4	1.2	0.872	0.095	0.293	NA	NA	14.16	25.0	3.50	18.4
7	23	1420	230.3	1	A	7.58	3.6	1.8	0.876	0.100	0.316	6.07	0.585	16.93	25.2	3.10	19.0
7	23	1519	231.3	1	A	7.62	3.5	2.0	0.948	0.100	0.327	NA	NA	28.22	25.0	3.40	19.1
7	23	1622	232.4	1	A	7.58	3.6	2.2	1.050	0.110	0.338	2.15	0.668	31.98	26.0	2.35	17.8
7	23	1723	233.4	1	A	7.51	3.6	1.8	1.160	0.119	0.390	NA	NA	24.45	26.2	2.25	16.5
7	23	1825	234.4	1	A	7.48	3.5	0.8	1.020	0.089	0.284	NA	NA	NA	26.2	2.00	13.9
7	23	1926	235.4	1	A	7.45	3.5	1.4	0.820	0.062	0.232	NA	NA	15.05	26.1	2.25	12.9
7	23	2020	236.3	1	A	7.46	3.7	1.6	0.992	0.100	0.442	3.03	0.691	20.69	26.0	2.55	11.1
7	23	2121	237.3	1	A	7.43	3.3	1.5	1.960	0.114	0.437	NA	NA	18.81	26.0	2.25	12.0
7	23	2220	238.3	1	A	7.51	3.8	2.1	0.871	0.072	0.267	2.46	0.678	19.56	26.2	1.80	16.0
7	23	2324	239.4	1	A	7.51	3.7	1.5	0.996	0.081	0.270	NA	NA	14.84	26.5	2.10	17.0
7	24	10	240.3	1	A	7.54	3.8	2.1	1.040	0.110	0.324	2.77	0.732	22.57	25.5	2.50	18.0
7	24	116	241.3	1	A	7.56	4.9	2.4	0.959	0.100	0.309	NA	NA	NA	25.0	2.40	18.5
7	24	214	242.3	1	A	7.58	3.4	2.0	0.965	0.100	0.325	2.15	0.625	12.81	25.0	2.55	19.0
7	24	321	243.3	1	A	7.62	3.3	1.5	0.975	0.110	0.361	NA	NA	14.16	24.9	2.40	18.8

946510439

KEARNY POINT - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	24	419	244.3	1	A	7.54	3.5	1.8	1.090	0.105	0.332	2.87	0.749	16.86	25.5	1.95	17.0
7	24	530	245.5	1	A	7.47	3.6	1.0	0.721	0.043	0.202	NA	NA	15.51	25.5	1.35	13.1
7	24	616	246.3	1	A	7.43	3.7	1.2	1.160	0.110	0.411	3.29	0.777	20.69	26.0	1.30	14.5
7	24	715	247.3	1	A	7.44	3.5	1.4	1.210	0.119	0.548	NA	NA	16.93	25.5	1.20	14.3
		AVERAGE READING				7.55	4.9	2.1	0.880	0.089	0.298	2.16	0.642	30.30	26.1	3.65	16.6

946510440

BASELINE

KEARNY

PØINT

7-14/7-24-81

2/3 DEPTH

946510441

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	815	8.3	1	B	7.40	12.0	3.9	0.730	0.095	0.324	3.49	1.420	26.33	25.0	3.50	20.0
7	14	915	9.3	1	B	7.40	16.0	4.2	1.020	0.109	0.385	NA	NA	15.05	25.0	2.80	20.0
7	14	1016	10.3	1	B	7.40	8.0	3.4	1.010	0.104	0.407	5.20	0.875	16.93	26.0	2.70	21.0
7	14	1115	11.3	1	B	7.40	5.3	3.3	NA	NA	NA	NA	NA	31.98	26.0	2.20	19.0
7	14	1215	12.3	1	B	7.40	7.6	3.0	1.000	0.104	0.408	1.68	0.896	18.81	26.9	2.40	20.8
7	14	1317	13.3	1	B	7.40	7.3	2.8	1.000	0.090	0.288	NA	NA	18.81	26.7	2.40	21.2
7	14	1416	14.3	1	B	7.40	5.5	2.7	0.701	0.067	0.222	1.51	0.640	20.69	26.0	3.50	20.3
7	14	1515	15.3	1	B	7.50	4.6	2.8	0.855	0.086	0.282	NA	NA	28.22	27.2	4.30	19.3
7	14	1624	16.4	1	B	7.67	4.4	2.6	0.702	0.067	0.246	0.53	0.432	26.33	27.0	5.40	18.0
7	14	1719	17.3	1	B	7.76	4.3	3.2	0.751	0.086	0.254	NA	NA	28.22	27.1	5.80	18.3
7	14	1823	18.4	1	B	7.70	6.7	3.3	0.560	0.067	0.205	1.31	0.414	22.57	25.8	6.00	20.0
7	14	1918	19.3	1	B	7.79	5.2	2.7	0.687	0.095	0.302	NA	NA	18.81	26.5	6.20	19.0
7	14	2022	20.4	1	B	7.72	5.5	3.0	0.653	0.086	0.269	1.06	0.548	30.10	24.8	4.80	20.0
7	14	2122	21.4	1	B	7.70	4.6	2.6	0.629	0.081	0.253	NA	NA	22.57	24.8	4.60	19.5
7	14	2220	22.3	1	B	7.60	4.6	2.2	0.601	0.057	0.170	0.84	0.527	20.69	25.5	4.90	17.8
7	14	2317	23.3	1	B	7.57	5.3	2.8	0.896	0.100	0.305	NA	NA	26.33	25.3	4.20	18.0
7	15	15	24.3	1	B	7.50	5.5	3.6	0.930	0.104	0.376	1.37	0.759	NA	25.1	3.80	16.0
7	15	113	25.2	1	B	7.51	4.4	2.1	0.813	0.090	0.282	NA	NA	NA	24.5	2.80	17.0
7	15	213	26.2	1	B	7.44	5.1	3.8	0.428	0.029	0.084	1.28	0.566	16.93	25.7	2.80	20.0
7	15	317	27.3	1	B	7.47	5.7	2.1	0.938	0.076	0.279	2.08	0.786	15.05	25.0	2.90	17.0
7	15	418	28.3	1	B	7.63	4.6	2.6	0.846	0.095	0.312	1.32	0.724	16.93	25.0	3.90	18.8
7	15	513	29.2	1	B	7.71	4.7	2.6	0.630	0.057	0.182	NA	NA	16.93	25.3	3.80	19.9
7	15	614	30.2	1	B	7.75	6.0	1.8	0.747	0.095	0.282	1.59	0.576	18.81	24.3	4.20	20.1
7	15	716	31.3	1	B	7.79	5.3	2.4	0.678	0.090	0.295	NA	NA	18.81	24.0	3.50	20.1
7	15	815	32.3	1	B	7.58	4.9	2.2	0.659	0.086	0.276	2.29	1.900	34.80	25.8	4.00	20.2
7	15	915	33.3	1	B	7.66	5.3	2.0	0.662	0.086	0.286	NA	NA	26.33	26.6	3.25	20.1

94651044

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	15	1016	34.3	1	B	7.58	6.1	1.8	0.860	0.104	0.310	1.10	0.709	33.86	25.5	4.10	18.5
7	15	1114	35.2	1	B	7.56	3.3	1.4	0.816	0.100	0.365	NA	NA	30.10	25.5	3.25	18.2
7	15	1217	36.3	1	B	7.53	3.4	0.9	0.896	0.104	0.388	2.37	0.772	24.45	25.6	3.50	20.0
7	15	1316	37.3	1	B	7.54	3.7	0.8	0.860	0.095	0.294	NA	NA	31.98	25.1	3.20	20.0
7	15	1414	38.2	1	B	7.51	4.0	0.9	0.891	0.100	0.295	1.92	0.794	30.10	25.1	3.60	18.6
7	15	1515	39.3	1	B	7.45	5.1	1.5	0.891	0.100	0.342	NA	NA	24.45	25.2	3.75	19.3
7	15	1618	40.3	1	B	7.54	5.4	1.4	0.484	0.067	0.198	0.64	0.562	30.10	25.8	4.30	20.0
7	15	1720	41.3	1	B	7.61	3.4	1.1	0.818	0.100	0.279	NA	NA	18.81	25.5	4.00	19.8
7	15	1816	42.3	1	B	7.64	4.7	1.1	0.660	0.086	0.266	1.84	0.591	35.74	26.3	NA	20.8
7	15	1918	43.3	1	B	7.68	3.8	0.9	0.540	0.067	0.206	NA	NA	30.10	24.8	4.30	21.8
7	15	2016	44.3	1	B	7.79	4.4	2.0	0.567	0.081	0.246	1.44	0.600	50.79	24.8	3.70	21.0
7	15	2120	45.3	1	B	7.75	4.4	1.6	0.523	0.057	0.190	NA	NA	41.38	24.5	5.60	19.5
7	15	2220	46.3	1	B	7.75	4.5	1.5	0.574	0.057	0.177	1.20	0.775	37.62	25.0	5.10	20.0
7	15	2315	47.3	1	B	7.68	4.1	0.8	0.761	0.081	0.268	NA	NA	39.50	25.3	4.80	19.0
7	16	17	48.3	1	B	7.63	3.7	1.2	0.260	0.053	0.256	0.88	0.612	48.91	24.5	5.00	18.3
7	16	115	49.3	1	B	7.61	4.8	0.9	0.749	0.076	0.287	NA	NA	30.10	25.0	3.60	17.1
7	16	216	50.3	1	B	7.50	5.0	1.2	0.883	0.076	0.330	1.26	0.699	41.38	25.0	4.00	16.1
7	16	317	51.3	1	B	7.35	9.9	2.8	0.968	0.086	0.300	NA	NA	31.98	24.8	3.20	18.9
7	16	416	52.3	1	B	7.31	5.5	1.8	0.769	0.076	0.248	1.56	1.100	22.57	24.5	3.50	18.0
7	16	523	53.4	1	B	7.52	4.5	1.1	0.621	0.067	0.227	NA	NA	35.74	25.3	4.15	18.4
7	16	632	54.5	1	B	7.65	6.8	1.6	0.817	0.095	0.295	1.40	0.883	28.22	25.1	4.00	19.1
7	16	718	55.3	1	B	7.65	16.8	3.0	0.868	0.104	0.320	NA	NA	35.74	25.3	4.25	18.5
7	16	816	56.3	1	B	7.68	7.5	2.0	0.786	0.100	0.291	1.11	0.630	22.57	24.2	4.00	20.4
7	16	915	57.3	1	B	7.63	9.0	3.6	0.886	0.104	0.322	NA	NA	26.33	24.2	4.30	20.0
7	16	1016	58.3	1	B	7.67	5.6	1.6	0.725	0.090	0.277	0.99	0.599	22.57	24.7	3.90	20.1
7	16	1116	59.3	1	B	7.60	6.3	2.2	0.908	0.104	0.309	NA	NA	11.46	25.5	3.60	18.9

94651043

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	16	1217	60.3	1	B	7.70	5.2	2.4	0.823	0.104	0.334	1.57	0.837	22.57	25.6	3.50	18.0
7	16	1317	61.3	1	B	7.57	5.3	2.2	0.856	0.086	0.283	NA	NA	24.28	25.6	3.60	16.8
7	16	1414	62.2	1	B	7.60	6.5	2.4	0.833	0.095	0.298	1.42	0.959	23.60	25.4	3.10	17.1
7	16	1517	63.3	1	B	7.55	5.7	3.2	0.917	0.095	0.329	NA	NA	24.28	25.2	3.60	17.9
7	16	1617	64.3	1	B	7.49	22.0	7.2	0.963	0.095	0.420	1.70	0.955	45.14	25.5	4.20	18.3
7	16	1714	65.2	1	B	7.59	17.0	4.0	0.948	0.100	0.301	NA	NA	16.93	25.8	4.20	19.8
7	16	1818	66.3	1	B	7.70	7.3	2.0	0.825	0.104	0.294	2.18	2.400	20.69	25.2	5.20	20.3
7	16	1918	67.3	1	B	7.77	5.0	2.3	0.679	0.095	0.279	NA	NA	33.86	24.9	4.85	20.8
7	16	2018	68.3	1	B	7.72	3.4	0.8	0.623	0.086	0.266	1.17	0.777	15.51	24.5	4.60	20.9
7	16	2118	69.3	1	B	7.71	3.6	1.8	0.667	0.095	0.284	NA	NA	20.69	24.5	4.10	20.8
7	16	2220	70.3	1	B	7.74	3.7	1.8	0.610	0.086	0.253	1.21	0.680	28.22	25.0	5.55	20.3
7	16	2317	71.3	1	B	7.69	3.8	1.0	0.460	0.048	0.174	NA	NA	22.93	25.1	4.80	20.0
7	17	16	72.3	1	B	7.65	4.0	1.2	0.702	0.076	0.247	0.97	0.540	27.65	25.0	4.00	18.9
7	17	120	73.3	1	B	7.54	4.6	1.4	0.897	0.104	0.352	NA	NA	20.69	25.2	4.30	17.5
7	17	216	74.3	1	B	7.53	4.6	1.0	0.500	0.039	0.154	0.87	0.575	45.14	25.2	3.90	16.9
7	17	320	75.3	1	B	7.49	5.8	4.0	0.681	0.062	0.279	NA	NA	35.74	25.3	3.50	15.5
7	17	423	76.4	1	B	7.36	5.1	1.8	0.615	0.057	0.238	1.18	0.711	22.57	25.2	3.50	15.1
7	17	527	77.4	1	B	7.46	6.7	2.2	0.549	0.048	0.228	NA	NA	24.45	25.3	3.90	17.0
7	17	626	78.3	1	B	7.50	6.9	1.8	0.856	0.067	0.177	1.18	0.601	30.10	26.0	3.60	18.2
7	17	718	79.3	1	B	7.58	11.0	5.6	0.594	0.062	0.179	NA	NA	26.33	25.2	3.30	19.0
7	17	816	80.2	1	B	7.60	15.0	1.5	0.670	0.086	0.286	1.25	0.636	20.69	24.2	4.40	19.8
7	17	915	81.3	1	B	7.60	7.0	1.1	0.652	0.086	0.279	NA	NA	20.23	24.2	3.80	19.8
7	17	1016	82.3	1	B	7.60	6.5	1.8	0.654	0.086	0.282	1.31	0.601	24.45	24.2	4.75	19.9
7	17	1115	83.3	1	B	7.6	6.4	1.4	0.882	0.104	0.317	NA	NA	22.57	25.9	4.00	18.5
7	17	1214	84.2	1	B	7.53	9.6	3.2	0.957	0.109	0.330	1.68	0.701	26.33	25.6	3.20	18.4
7	17	1315	85.3	1	B	7.50	7.6	1.1	0.997	0.104	0.334	NA	NA	28.22	25.8	3.80	17.1

94510444

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1416	86.3	1	B	7.50	8.3	1.1	0.950	0.100	0.379	1.90	0.796	45.14	25.8	3.75	16.3
7	17	1516	87.3	1	B	7.40	7.3	1.5	0.981	0.104	0.351	NA	NA	30.10	25.6	2.90	16.9
7	17	1615	88.3	1	B	7.50	6.5	1.6	0.888	0.092	0.381	2.67	0.880	17.53	26.0	3.30	16.6
7	17	1714	89.2	1	B	7.60	7.7	2.4	0.659	0.034	0.146	NA	NA	26.30	25.9	4.60	17.5
7	17	1814	90.2	1	B	7.60	5.6	1.8	0.978	0.107	0.311	2.06	0.752	20.69	25.8	4.10	18.9
7	17	1918	91.3	1	B	7.70	6.6	3.2	0.787	0.073	0.235	NA	NA	24.45	24.9	4.30	19.3
7	17	2012	92.2	1	B	7.70	7.8	1.6	0.739	0.058	0.165	4.02	1.590	31.98	24.5	4.40	19.9
7	17	2118	93.3	1	B	7.70	5.7	1.1	0.751	0.087	0.277	NA	NA	20.23	24.3	3.30	20.3
7	17	2220	94.3	1	B	7.60	5.6	0.9	0.488	0.097	0.310	2.84	0.728	30.10	24.8	3.40	20.2
7	17	2317	95.3	1	B	7.70	4.7	0.5	0.553	0.073	0.240	NA	NA	22.57	24.8	3.80	20.0
7	18	19	96.3	1	B	7.60	5.8	1.2	0.807	0.058	0.201	1.27	0.578	31.98	25.6	3.80	20.0
7	18	114	97.2	1	B	7.60	5.2	0.5	0.705	0.058	0.206	NA	NA	30.10	25.2	3.90	18.1
7	18	220	98.3	1	B	7.50	18.0	4.6	0.776	0.063	0.282	1.52	0.487	43.26	26.0	3.20	18.0
7	18	320	99.3	1	B	7.50	7.0	1.8	0.602	0.044	0.209	NA	NA	45.14	26.0	3.50	17.0
7	18	514	101.2	1	B	7.40	7.6	1.6	0.996	0.097	0.424	2.40	0.847	24.45	26.5	3.90	19.1
7	18	621	102.3	1	B	7.50	6.4	0.8	1.020	0.107	0.296	NA	NA	28.22	27.0	3.30	19.0
7	18	714	103.2	1	B	7.50	6.6	1.1	1.040	0.107	0.305	1.78	0.693	28.22	27.5	3.50	18.9
7	18	816	104.3	1	B	7.50	5.7	1.6	0.979	0.107	0.298	1.75	0.629	28.22	26.0	3.40	20.5
7	18	918	105.3	1	B	7.60	6.7	2.0	0.724	0.073	0.243	NA	NA	26.22	25.7	3.60	19.9
7	18	1016	106.3	1	B	7.60	6.0	1.8	0.715	0.082	0.263	1.69	0.463	24.45	25.5	4.10	19.2
7	18	1120	107.3	1	B	7.60	4.7	1.6	0.724	0.087	0.260	NA	NA	26.33	25.0	3.80	19.9
7	18	1218	108.3	1	B	7.50	5.4	1.8	1.020	0.107	0.296	1.97	0.690	33.86	26.7	3.40	18.2
7	18	1320	109.3	1	B	7.50	5.7	2.1	0.978	0.102	0.324	NA	NA	50.79	26.8	4.50	18.0
7	18	1418	110.3	1	B	7.50	6.0	2.2	0.988	0.097	0.347	1.73	0.606	75.24	26.5	5.50	17.0
7	18	1519	111.3	1	B	7.50	6.0	3.0	0.861	0.110	0.408	NA	NA	45.14	26.0	3.50	17.5
7	18	1615	112.3	1	B	7.40	8.5	3.2	0.545	0.068	0.260	1.15	0.353	47.02	27.6	4.30	17.6

94510445

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	18	1714	113.2	1	B	7.50	6.7	2.6	0.995	0.097	0.382	NA	NA	50.79	27.8	5.70	17.2
7	18	1814	114.2	1	B	7.80	12.0	2.6	0.881	0.097	0.350	1.79	0.654	79.00	27.7	5.80	17.0
7	18	1918	115.3	1	B	7.70	7.2	4.1	0.882	0.087	0.237	NA	NA	63.95	27.1	4.70	18.8
7	18	2016	116.3	1	B	7.70	7.4	3.2	0.841	0.102	0.302	1.63	0.663	33.86	26.2	4.60	18.8
7	18	2114	117.2	1	B	7.70	6.5	2.2	0.725	0.087	0.258	NA	NA	48.91	25.9	3.50	19.0
7	18	2207	118.1	1	B	7.60	7.0	2.2	0.540	0.092	0.273	1.48	0.550	45.14	25.5	4.35	20.1
7	18	2315	119.3	1	B	7.70	6.2	2.0	0.735	0.087	0.275	NA	NA	35.74	25.6	4.50	20.1
7	19	11	120.2	1	B	7.70	5.0	3.3	0.959	0.097	0.306	1.96	0.604	18.20	26.0	3.90	19.9
7	19	113	121.2	1	B	7.70	7.1	3.0	1.050	0.097	0.293	NA	NA	58.31	27.0	3.90	17.2
7	19	212	122.2	1	B	7.60	9.0	5.1	0.979	0.078	0.251	2.44	0.851	48.91	27.0	5.00	16.9
7	19	315	123.3	1	B	7.60	6.7	3.3	0.952	0.087	0.327	NA	NA	54.55	27.0	4.60	16.5
7	19	414	124.2	1	B	7.50	9.0	5.4	0.905	0.087	0.298	2.71	1.040	48.91	27.0	3.90	17.8
7	19	512	125.2	1	B	7.50	7.7	3.8	0.808	0.063	0.229	NA	NA	47.03	27.0	3.30	14.0
7	19	621	126.3	1	B	7.30	7.0	4.1	0.615	0.029	0.150	5.16	0.725	20.69	25.9	3.90	18.9
7	19	719	127.2	1	B	7.50	6.8	3.3	0.936	0.048	0.163	NA	NA	56.43	25.5	4.20	18.0
7	19	816	128.3	1	B	7.57	5.7	0.8	0.885	0.102	0.278	3.48	0.988	24.45	25.5	3.90	19.0
7	19	918	129.3	1	B	7.62	4.2	0.4	0.696	0.082	0.281	NA	NA	31.98	24.8	4.80	19.8
7	19	1018	130.3	1	B	7.65	3.5	0.8	0.465	0.034	0.148	1.35	0.415	24.45	24.8	5.30	19.8
7	19	1120	131.3	1	B	7.67	4.1	0.4	0.638	0.044	0.133	NA	NA	30.09	24.6	3.60	19.8
7	19	1221	132.3	1	B	7.63	4.5	1.2	0.536	0.048	0.277	2.52	0.380	39.50	26.2	4.00	17.9
7	19	1315	133.2	1	B	7.64	4.2	1.2	0.894	0.068	0.199	NA	NA	24.45	25.2	3.50	19.0
7	19	1418	134.3	1	B	7.57	4.1	5.0	0.927	0.068	0.210	2.78	0.688	35.74	26.1	3.80	18.1
7	19	1516	135.3	1	B	7.61	5.1	5.6	0.899	0.097	0.343	NA	NA	58.31	26.5	4.70	16.5
7	19	1615	136.3	1	B	7.54	4.2	1.6	0.791	0.102	0.436	2.01	0.659	28.22	25.5	2.90	19.1
7	19	1716	137.3	1	B	7.51	5.8	2.0	0.819	0.058	0.194	NA	NA	35.74	27.2	3.40	16.5
7	19	1813	138.2	1	B	7.69	5.3	2.4	0.758	0.097	0.355	1.95	0.668	62.07	27.5	7.31	18.0

946510446

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	19	1913	139.2	1	B	7.63	6.0	2.0	0.911	0.087	0.261	NA	NA	41.38	26.8	4.10	18.8
7	19	2015	140.3	1	B	7.66	5.3	1.0	0.899	0.107	0.290	2.27	0.716	39.50	26.8	4.10	18.5
7	19	2117	141.3	1	B	7.68	6.0	0.8	0.740	0.048	0.159	NA	NA	26.33	25.9	4.60	19.5
7	19	2214	142.2	1	B	7.72	3.7	0.4	0.676	0.044	0.136	2.03	0.519	28.22	25.3	3.90	20.0
7	19	2310	143.2	1	B	7.69	3.5	0.4	0.683	0.087	0.267	NA	NA	24.45	25.9	4.05	20.0
7	2	12	144.2	1	B	7.68	3.3	0.4	0.511	0.062	0.232	3.97	0.530	33.86	25.5	3.50	19.1
7	2	113	145.2	1	B	7.63	4.1	0.6	0.531	0.033	0.133	NA	NA	36.68	26.0	4.20	19.0
7	2	215	146.3	1	B	7.56	5.0	1.2	0.667	0.033	0.114	1.91	0.499	31.98	27.0	3.90	17.0
7	2	315	147.3	1	B	7.55	6.1	2.0	0.899	0.057	0.247	NA	NA	39.50	27.0	4.30	16.0
7	2	411	148.2	1	B	7.51	7.3	3.2	0.744	0.028	0.122	3.22	1.270	43.26	27.0	3.60	15.9
7	2	515	149.3	1	B	7.58	5.7	2.4	0.856	0.062	0.208	NA	NA	33.86	27.0	3.10	16.0
7	2	614	150.2	1	B	7.48	6.2	2.6	0.907	0.057	0.232	4.09	0.806	48.91	27.0	2.50	15.8
7	2	709	151.1	1	B	7.45	6.4	2.0	0.898	0.081	0.281	NA	NA	52.67	27.0	2.90	15.9
7	2	819	152.3	1	B	7.47	5.7	0.6	0.992	0.115	0.313	2.45	0.716	54.55	27.2	2.70	17.9
7	2	914	153.3	1	B	7.55	6.0	0.4	0.666	0.057	0.174	NA	NA	41.38	26.8	2.80	18.1
7	2	1017	154.3	1	B	7.59	4.4	0.4	0.663	0.067	0.195	2.47	0.865	31.98	26.5	2.70	19.0
7	2	1121	155.3	1	B	7.58	3.7	0.4	0.603	0.076	0.237	NA	NA	33.86	28.1	2.80	18.3
7	2	1218	156.3	1	B	7.71	3.7	0.4	0.639	0.081	0.256	2.32	0.653	28.22	27.5	2.30	18.1
7	2	1317	157.3	1	B	7.55	4.3	0.6	0.796	0.096	0.280	NA	NA	24.45	27.1	2.00	18.5
7	2	1415	158.3	1	B	7.54	4.0	0.4	0.929	0.106	0.282	2.76	0.587	37.62	28.7	1.70	17.5
7	2	1516	159.3	1	B	7.51	4.4	0.4	0.965	0.072	0.230	NA	NA	56.43	28.0	1.90	17.0
7	2	1614	160.2	1	B	7.47	4.7	0.4	0.928	0.110	0.348	6.14	0.824	52.67	26.9	2.30	15.9
7	2	1714	161.2	1	B	7.43	4.3	0.4	0.915	0.101	0.355	NA	NA	39.50	26.8	2.20	16.6
7	2	1817	162.3	1	B	7.43	4.1	0.4	0.917	0.096	0.389	2.50	0.617	22.57	26.7	2.30	16.5
7	20	1912	163.2	1	B	7.47	4.7	0.4	1.030	0.091	0.321	NA	NA	28.22	26.4	2.90	16.3
7	20	2014	164.2	1	B	7.55	4.0	0.4	1.060	0.110	0.333	5.08	0.726	30.10	27.0	3.10	18.6

94510447

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	2	2115	165.3	1	B	7.55	5.0	0.4	0.918	0.052	0.153	NA	NA	26.33	26.5	2.90	19.0
7	21	2220	166.3	1	B	7.59	4.2	0.4	0.813	0.042	0.132	NA	NA	41.38	28.0	3.10	18.5
7	2	2315	167.3	1	B	7.59	3.8	0.4	0.828	0.096	0.283	NA	NA	30.10	27.6	2.70	18.5
7	21	4	168.1	1	B	7.58	4.3	0.4	0.660	0.057	0.233	2.19	0.736	24.45	27.5	2.50	18.5
7	21	118	169.3	1	B	7.57	4.1	0.4	0.494	0.028	0.079	NA	NA	18.81	26.5	3.00	20.0
7	21	215	170.3	1	B	7.50	3.8	0.4	1.010	0.086	0.334	2.23	0.650	28.22	27.0	2.10	17.0
7	21	312	171.2	1	B	7.44	4.5	0.4	0.968	0.091	0.397	NA	NA	52.67	26.8	1.80	14.5
7	21	419	172.3	1	B	7.44	4.3	0.4	0.811	0.072	0.297	2.03	0.554	28.22	27.5	0.90	12.0
7	21	521	173.3	1	B	7.40	4.9	0.4	0.989	0.096	0.366	NA	NA	45.14	27.8	0.20	9.8
7	21	609	174.1	1	B	7.34	5.3	0.4	1.060	0.125	0.375	3.02	0.737	62.07	26.0	0.80	12.5
7	21	710	175.2	1	B	7.22	5.2	0.4	1.230	0.076	0.274	NA	NA	32.92	26.8	0.90	15.2
7	21	816	176.3	1	B	7.20	17.0	4.6	0.986	0.086	0.281	3.22	0.832	18.81	26.1	1.65	18.1
7	21	915	177.3	1	B	7.40	5.3	2.8	1.120	0.103	0.237	NA	NA	16.19	27.6	1.80	17.9
7	21	1018	178.3	1	B	7.50	6.2	1.8	0.727	0.037	0.100	3.10	0.816	14.84	25.1	3.25	19.2
7	21	1120	179.3	1	B	7.50	4.2	1.8	0.804	0.067	0.195	NA	NA	13.49	25.0	3.20	19.6
7	21	1214	180.2	1	B	7.50	4.0	2.4	0.647	0.057	0.195	1.75	0.509	22.26	24.9	2.80	19.8
7	21	1316	181.3	1	B	7.40	5.2	3.6	0.552	0.047	0.155	NA	NA	45.14	24.8	2.50	19.8
7	21	1420	182.3	1	B	7.5[illegible]	3.5	1.8	0.546	0.033	0.102	2.20	0.664	20.69	25.1	2.05	19.2
7	21	1514	183.2	1	B	7.40	3.8	2.4	0.744	0.042	0.111	NA	NA	18.81	26.0	1.60	17.5
7	21	1611	184.2	1	B	7.50	3.9	1.5	1.110	0.102	0.273	2.60	0.675	17.53	26.0	1.40	18.9
7	21	1712	185.2	1	B	7.4[illegible]	4.7	1.5	0.675	0.042	0.424	NA	NA	15.51	25.9	1.30	19.0
7	21	1820	186.3	1	B	7.40	6.0	1.2	0.985	0.126	0.572	2.52	0.839	21.58	NA	1.45	15.5
7	21	1914	187.2	1	B	7.40	5.8	1.8	1.150	0.145	0.612	NA	NA	26.33	26.6	0.85	17.6
7	21	2023	188.4	1	B	7.40	5.1	1.6	1.350	0.126	0.360	NA	NA	20.69	25.8	3.65	18.1
7	21	2117	189.3	1	B	7.40	23.0	2.4	1.140	0.103	0.264	NA	NA	22.57	26.7	2.40	17.5
7	21	2213	190.2	1	B	7.40	4.7	3.0	0.923	0.080	0.218	2.60	0.653	30.10	25.6	2.81	19.6

946510448

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	21	2315	191.3	1	B	7.50	4.5	2.4	1.080	0.136	0.494	NA	NA	22.26	25.4	2.75	19.9
7	22	10	192.2	1	B	7.50	5.4	3.2	0.849	0.089	0.272	1.90	0.546	17.53	25.0	2.50	19.5
7	22	107	193.1	1	B	7.50	3.8	0.4	1.180	0.070	0.227	NA	NA	14.16	24.8	2.75	18.5
7	22	211	194.2	1	B	7.50	5.5	1.2	0.826	0.080	0.255	3.77	0.587	16.19	25.0	2.75	20.2
7	22	310	195.2	1	B	7.50	3.7	0.6	1.290	NA	NA	NA	NA	13.49	25.0	2.74	19.0
7	22	409	196.1	1	B	7.50	5.2	0.8	1.000	0.084	0.248	2.96	0.613	18.21	25.5	2.25	18.9
7	22	520	197.3	1	B	7.40	4.0	0.4	1.090	0.108	0.374	NA	NA	19.56	25.9	0.60	16.5
7	22	645	198.8	1	B	7.40	4.1	0.4	1.080	0.098	0.271	2.41	0.701	16.53	26.0	1.20	15.5
7	22	815	200.3	1	B	7.20	6.8	3.8	1.130	0.089	0.280	3.22	0.753	26.33	26.0	0.60	16.0
7	22	914	201.2	1	B	7.30	5.0	3.2	1.090	0.108	0.357	NA	NA	15.05	26.2	1.45	17.0
7	22	1016	202.3	1	B	7.40	6.5	4.5	0.972	0.075	0.366	1.99	0.526	28.22	25.8	1.80	18.2
7	22	1115	203.3	1	B	7.50	6.2	4.2	0.803	0.080	0.250	NA	NA	13.17	24.8	2.19	20.2
7	22	1218	204.3	1	B	7.50	4.4	4.2	0.797	0.080	0.355	1.95	0.593	13.17	24.8	2.20	20.1
7	22	1316	205.3	1	B	7.50	4.7	4.2	0.885	0.108	0.327	NA	NA	16.93	24.8	2.65	20.1
7	22	1417	206.3	1	B	7.50	3.6	4.2	0.806	0.080	0.297	6.02	0.502	11.29	24.8	2.70	20.2
7	22	1515	207.3	1	B	7.50	3.4	3.3	0.876	0.089	0.278	NA	NA	16.93	26.0	2.45	17.5
7	22	1614	208.2	1	B	7.40	3.4	3.3	0.947	0.080	0.241	2.23	0.572	13.17	25.1	1.80	19.0
7	22	1715	209.3	1	B	7.40	4.3	3.6	0.732	0.052	0.139	NA	NA	13.17	25.0	1.50	19.9
7	22	1816	210.3	1	B	7.40	3.9	3.4	0.932	0.080	0.234	3.05	0.578	13.17	25.5	1.40	18.5
7	22	1914	211.2	1	B	7.40	4.5	3.4	1.130	0.126	0.407	NA	NA	18.81	25.2	1.48	18.9
7	22	2017	212.3	1	B	7.40	3.7	4.0	1.160	0.080	0.292	2.97	0.710	18.81	25.2	1.10	19.0
7	22	2115	213.3	1	B	7.50	4.0	2.7	0.716	0.052	0.176	NA	NA	20.69	26.0	2.30	18.0
7	22	2213	214.2	1	B	7.50	3.2	2.4	0.566	0.033	0.124	2.78	0.439	15.05	25.7	2.10	18.9
7	22	2314	215.3	1	B	7.50	4.3	2.4	0.883	0.089	0.274	NA	NA	16.93	25.0	2.35	19.3
7	23	8	216.1	1	B	7.60	4.7	2.6	0.639	0.056	0.203	NA	NA	5.64	24.5	2.65	20.0
7	23	110	217.2	1	B	7.50	3.8	2.7	0.843	0.080	0.307	1.61	0.497	11.29	24.0	2.45	20.1

94510449

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	23	213	218.2	1	B	7.50	3.9	2.6	0.621	0.089	0.298	NA	NA	11.29	24.0	2.05	20.0
7	23	309	219.1	1	B	7.50	3.3	2.2	0.595	0.042	0.142	1.02	0.441	15.05	24.0	1.85	20.2
7	23	414	220.2	1	B	7.50	4.1	4.0	1.010	0.028	0.308	NA	NA	11.29	24.5	2.25	19.0
7	23	515	221.3	1	B	7.40	6.5	3.0	0.434	0.014	0.135	3.55	0.564	15.99	25.7	1.40	18.1
7	23	612	222.2	1	B	7.40	4.8	2.4	1.190	0.094	0.292	NA	NA	16.93	25.1	1.90	18.9
7	23	715	223.3	1	B	7.40	4.2	2.1	1.010	0.080	0.281	4.27	0.585	16.93	25.0	1.30	18.0
7	23	815	224.3	1	B	7.33	5.0	3.0	1.190	0.098	0.313	NA	NA	24.45	25.5	0.80	17.0
7	23	917	225.3	1	B	7.39	3.7	2.1	1.100	0.117	0.392	NA	NA	14.84	25.5	0.87	17.2
7	23	1014	226.2	1	B	7.43	3.9	2.6	1.120	0.145	0.373	NA	NA	16.93	25.6	1.60	18.1
7	23	1115	227.3	1	B	7.45	3.9	2.0	0.529	0.038	0.335	3.55	0.578	15.05	25.0	1.60	18.5
7	23	1216	228.3	1	B	7.54	12.0	2.4	0.863	0.089	0.270	NA	NA	28.22	24.9	2.72	18.8
7	23	1314	229.2	1	B	7.60	3.7	2.7	0.897	0.089	0.316	2.22	0.536	15.51	24.6	2.54	19.8
7	23	1415	230.3	1	B	7.56	5.4	2.2	0.884	0.089	0.284	NA	NA	13.17	24.5	2.42	20.1
7	23	1514	231.2	1	B	7.64	3.5	2.4	0.913	0.089	0.268	2.53	0.571	22.57	24.6	2.10	19.9
7	23	1617	232.3	1	B	7.57	3.3	0.4	0.941	0.098	0.307	NA	NA	18.81	25.4	2.20	18.2
7	23	1718	233.3	1	B	7.52	3.4	0.4	1.470	0.108	0.384	3.07	0.937	16.93	26.0	2.30	16.7
7	23	1820	234.3	1	B	7.46	3.4	1.4	1.150	0.119	0.433	2.16	0.764	NA	25.7	1.55	15.3
7	23	1922	235.4	1	B	7.46	3.6	0.8	1.140	0.094	0.281	5.20	0.779	15.04	25.3	1.20	17.8
7	23	2014	236.2	1	B	7.47	3.5	0.4	0.943	0.080	0.300	NA	NA	18.81	25.0	1.10	17.9
7	23	2116	237.3	1	B	7.45	4.0	0.8	1.050	0.117	0.450	2.41	0.729	22.57	25.2	1.80	18.5
7	23	2216	238.3	1	B	7.48	3.7	0.4	0.689	0.052	0.132	NA	NA	15.04	25.8	2.10	17.5
7	23	2314	239.3	1	B	7.51	3.6	0.4	0.706	0.075	0.287	4.68	0.518	14.16	26.0	2.00	18.1
7	24	11	240.2	1	B	7.52	4.3	0.6	1.050	0.056	0.217	NA	NA	16.93	25.3	2.30	18.1
7	4	112	241.2	1	B	7.55	4.3	0.8	0.671	0.089	0.298	3.18	0.523	12.81	25.0	2.40	18.5
7	4	213	242.3	1	B	7.54	3.6	0.4	0.858	0.089	0.316	NA	NA	14.84	25.0	2.45	18.5
7	24	317	243.3	1	B	7.56	3.3	0.4	0.727	0.052	0.197	3.58	0.589	11.46	24.8	2.00	18.9

946510450

KEARNY POINT - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	414	244.2	1	B	7.54	3.8	0.4	0.704	0.103	0.326	NA	NA	12.14	25.1	2.45	18.0
7	24	525	245.4	1	B	7.54	3.6	0.4	1.140	0.108	0.331	5.27	0.727	12.14	25.5	1.65	15.5
7	24	612	246.2	1	B	7.56	3.7	1.8	1.190	0.061	0.238	NA	NA	10.12	26.0	1.85	16.5
7	24	710	247.2	1	B	7.52	3.5	0.6	0.908	0.061	0.241	2.88	0.594	11.80	25.5	1.50	16.8
		AVERAGE READING				7.54	5.7	2.0	0.829	0.082	0.276	2.32	0.709	27.90	25.7	3.21	18.4

946510451

BASELINE

JACKSØN STREET

7-14/7-24-81

1/3 DEPTH

946510452

JACKSON STREET - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

PAGE NO. 1

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB (NTU)	BOD (PPM)	NH3 (PPM)	NO2 (PPM)	NO3 (PPM)	TKN (PPM)	TP (PPM)	CHLOR (PPB)	TEMP (°C)	D.O. (PPM)	SAL (PPT)
7	14	800	8.0	2	A	7.27	3.4	3.0	0.684	0.049	0.265	0.98	0.730	13.17	26.5	2.60	13.5
7	14	1055	10.9	2	A	7.30	5.9	2.8	1.060	0.106	0.822	NA	NA	24.44	26.0	3.00	15..
7	14	1352	13.9	2	A	7.35	5.2	3.8	0.960	0.058	0.589	0.62	0.439	28.22	27.5	3.40	7.5
7	14	1640	16.7	2	A	7.51	4.0	4.5	1.040	0.101	0.305	NA	NA	31.98	27.0	6.00	15.0
7	14	1935	19.6	2	A	7.55	3.5	3.0	0.721	0.060	0.385	0.60	0.438	28.28	26.9	5.00	17.5
7	14	2259	22.6	2	A	7.50	3.8	2.8	1.060	0.106	0.657	NA	NA	18.83	25.8	4.10	12.0
7	15	132	25.5	2	A	7.40	4.7	3.0	0.975	0.096	0.805	1.50	0.609	26.33	25.9	2.90	8.5
7	15	434	28.6	2	A	7.40	3.9	2.4	0.986	0.096	0.450	NA	NA	18.91	25.6	3.10	13.2
7	15	730	31.5	2	A	7.40	3.7	2.1	0.861	0.101	0.479	1.19	0.693	22.57	25.2	3.30	10.5
7	15	1035	34.6	2	A	7.37	3.8	1.4	1.070	0.101	0.560	1.17	0.602	31.98	25.0	3.90	12.0
7	15	1335	37.6	2	A	7.39	4.8	1.5	0.961	0.096	0.795	NA	NA	52.67	27.0	4.00	8.5
7	15	1630	40.5	2	A	7.52	4.6	3.0	0.640	0.025	0.262	0.51	0.593	48.91	27.0	6.50	9.0
7	15	1930	43.5	2	A	7.63	4.0	1.3	0.949	0.096	0.367	NA	NA	52.67	25.5	5.20	17.0
7	15	2230	46.5	2	A	7.49	5.7	2.0	1.020	0.101	0.503	1.19	0.808	35.74	25.8	4.40	14.5
7	16	132	49.5	2	A	7.41	7.0	1.8	0.798	0.060	0.516	NA	NA	35.74	25.5	3.30	10.0
7	16	429	52.5	2	A	7.41	5.6	1.8	0.922	0.101	0.844	0.99	0.526	45.19	26.1	2.70	8.1
7	16	731	55.1	2	A	7.40	6.0	1.5	0.928	0.077	0.383	NA	NA	30.10	25.2	3.30	15.2
7	16	1035	58.6	2	A	7.31	5.6	1.6	0.824	0.073	0.404	1.02	0.453	24.45	25.8	3.70	13.8
7	16	1335	61.6	2	A	7.38	5.4	2.0	0.929	0.101	0.757	NA	NA	30.10	26.5	6.20	9.5
7	16	1635	64.6	2	A	7.55	5.4	2.2	1.070	0.106	0.696	1.00	0.474	33.86	26.0	4.00	10.0
7	16	1931	67.5	2	A	7.51	4.7	2.2	1.050	0.101	0.917	NA	NA	45.14	25.9	7.00	10.1
7	16	2245	70.6	2	A	7.38	5.4	1.8	0.994	0.103	0.485	1.32	0.556	48.91	25.3	5.20	14.8
7	17	154	73.9	2	A	7.48	5.2	2.0	1.050	0.106	0.694	NA	NA	28.28	26.0	3.20	10.6
7	17	456	77.1	2	A	7.36	4.9	2.0	1.040	0.106	0.803	1.33	0.609	30.10	26.0	2.50	8.1
7	17	757	79.9	2	A	7.38	5.1	1.6	1.060	0.101	0.483	NA	NA	33.86	25.5	2.70	14.0
7	17	1.55	82.9	2	A	7.43	6.2	2.1	0.577	0.051	0.290	0.87	0.479	62.07	25.8	4.90	14.5

946510453

JACKSON STREET - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1355	85.9	2	A	7.40	7.7	2.0	0.921	0.090	0.719	NA	NA	58.31	26.5	4.40	9.5
7	17	1655	88.9	2	A	7.40	7.3	2.1	0.960	0.099	0.773	1.25	0.568	45.14	26.2	4.40	8.5
7	17	1955	91.9	2	A	7.50	9.0	2.2	1.010	0.042	0.333	NA	NA	58.31	25.8	5.70	15.9
7	17	2255	94.9	2	A	7.50	6.6	2.1	1.000	0.099	0.422	1.83	0.578	47.02	25.8	5.10	15.8
7	18	153	97.9	2	A	7.40	7.5	2.6	1.040	0.104	0.648	NA	NA	45.14	25.9	3.70	11.2
7	18	455	100.9	2	A	7.40	8.3	0.9	1.040	0.099	0.872	1.47	0.709	52.67	26.0	2.10	7.1
7	18	756	103.9	2	A	7.40	7.2	1.7	1.070	0.104	0.624	2.05	0.636	41.38	25.8	3.30	11.8
7	18	1045	106.8	2	A	7.30	5.8	3.0	0.566	0.042	0.202	0.77	0.459	47.03	25.5	3.60	15.0
7	18	1350	109.8	2	A	7.40	7.0	3.4	0.731	0.068	0.469	NA	NA	54.55	26.5	4.90	10.5
7	18	1650	112.8	2	A	7.40	7.8	3.3	0.968	0.099	0.856	1.47	0.501	77.12	26.9	4.20	8.0
7	18	1950	115.8	2	A	7.60	6.3	4.2	0.924	0.105	0.571	NA	NA	75.24	26.5	8.20	12.9
7	18	2250	118.8	2	A	7.50	6.0	3.0	0.577	0.049	0.232	4.41	0.485	107.20	26.1	6.10	15.5
7	19	153	121.9	2	A	7.50	6.7	2.8	0.986	0.107	0.611	NA	NA	82.76	25.5	4.80	12.2
7	19	455	124.9	2	A	7.40	9.2	2.8	0.830	0.066	0.613	1.43	0.675	97.81	26.0	2.95	7.3
7	19	750	127.8	2	A	7.40	8.2	3.2	1.010	0.105	0.782	NA	NA	63.95	25.8	3.30	8.0
7	19	1050	130.8	2	A	7.36	4.2	3.2	0.957	0.105	0.412	NA	NA	62.07	26.5	4.00	16.3
7	19	1355	133.9	2	A	7.41	5.1	1.6	0.759	0.101	0.623	3.35	0.678	107.90	27.0	5.60	11.8
7	19	1655	136.9	2	A	7.41	5.7	1.4	0.952	0.099	0.823	NA	NA	77.12	27.0	4.30	8.0
7	19	1955	139.9	2	A	7.47	5.0	1.6	0.815	0.094	0.603	1.44	0.576	79.00	26.5	6.55	10.0
7	19	2250	142.8	2	A	7.52	4.2	1.6	0.913	0.105	0.386	NA	NA	52.67	26.0	4.90	16.4
7	20	158	146.9	2	A	7.41	4.9	1.0	0.977	0.107	0.613	1.66	0.597	67.72	26.2	3.70	11.5
7	2	455	148.9	2	A	7.38	5.5	2.2	0.757	0.066	0.531	NA	NA	65.83	26.0	2.90	8.2
7	2	747	151.8	2	A	7.35	6.6	1.4	0.678	0.051	0.440	1.58	0.752	54.55	26.0	2.50	7.4
7	2	1050	154.8	2	A	7.44	5.1	0.6	0.729	0.099	0.478	NA	NA	48.91	25.5	3.30	16.0
7	2	1345	157.8	2	A	7.40	5.3	0.4	0.977	0.063	0.330	3.13	0.725	62.07	26.0	2.90	13.3
7	20	1650	160.8	2	A	7.37	7.0	2.6	0.821	0.066	0.554	NA	NA	54.55	27.5	3.40	7.0

946510454

JACKSON STREET - LEVEL A - DEPTH 1/3
BASELINE SAMPLING (DRY FLOW)

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB (NTU)	BOD (PPM)	NH3 (PPM)	NO2 (PPM)	NO3 (PPM)	TKN (PPM)	TP (PPM)	CHLOR (PPB)	TEMP (°C)	D.O. (PPM)	SAL (PPT)
7	20	1950	163.8	2	A	7.34	9.0	1.6	0.831	0.049	0.528	3.35	0.646	43.26	26.2	2.50	7.0
7	21	2250	166.8	2	A	7.40	4.3	0.4	0.593	0.042	0.206	NA	NA	34.84	25.8	0.80	25.0
7	21	151	169.8	2	A	7.36	5.0	0.4	1.080	0.139	0.709	1.63	0.545	33.86	26.0	0.20	8.0
7	21	448	172.8	2	A	7.49	11.0	4.6	1.010	0.136	0.974	NA	NA	73.36	26.0	NA	1.0
7	21	750	175.8	2	A	7.59	10.5	2.0	0.557	0.089	1.540	2.00	0.910	168.60	25.5	0.70	0.2
7	21	1045	178.8	2	A	7.20	8.2	2.6	0.925	0.193	0.159	NA	NA	24.45	25.8	1.10	8.6
7	21	1350	181.8	2	A	7.30	8.0	2.2	1.060	0.286	0.515	2.52	0.678	22.57	26.0	0.50	2.0
7	21	1650	184.8	2	A	7.50	14.0	3.2	0.561	0.122	1.570	NA	NA	39.50	26.5	1.20	2.0
7	21	1945	187.8	2	A	7.30	5.3	4.0	0.562	0.127	1.660	3.16	0.605	39.50	25.8	0.90	0.2
7	21	2240	190.7	2	A	7.40	9.2	1.0	1.150	0.136	0.697	NA	NA	26.33	26.5	0.90	13.5
7	22	150	193.8	2	A	7.30	5.6	1.6	1.000	0.134	1.030	4.34	0.741	30.10	25.9	0.35	6.0
7	22	540	197.0	2	A	7.30	6.1	2.4	0.796	0.094	1.070	NA	NA	69.60	25.5	NA	2.5
7	22	745	199.8	2	A	7.20	12.0	4.8	0.781	0.132	1.280	4.23	0.566	39.50	24.8	0.10	NA
7	22	1050	202.8	2	A	7.20	5.2	3.4	0.761	0.118	0.618	NA	NA	30.10	25.5	0.80	4.5
7	22	1349	205.7	2	A	7.30	4.2	3.0	1.515	0.139	0.311	4.38	0.478	20.69	26.0	1.10	15.8
7	22	1650	208.8	2	A	7.20	6.9	3.6	0.817	0.118	0.632	NA	NA	26.33	25.8	0.75	3.7
7	22	1945	211.8	2	A	7.20	7.4	4.2	0.803	0.172	1.010	2.80	0.526	31.98	25.5	0.60	1.0
7	23	2241	214.7	2	A	7.20	5.4	3.2	0.933	0.094	0.763	NA	NA	22.57	25.0	NA	0.5
7	23	145	217.8	2	A	7.36	4.0	3.2	1.010	0.149	0.536	4.15	0.707	28.22	25.5	0.95	12.8
7	23	440	220.8	2	A	7.20	5.5	3.8	0.985	0.132	0.749	NA	NA	24.45	25.0	0.30	5.5
7	23	737	223.6	2	A	7.20	6.5	4.0	1.162	0.134	1.070	4.75	0.530	31.98	25.0	0.35	2.1
7	23	1050	226.8	2	A	7.30	4.4	2.8	1.120	0.151	1.040	NA	NA	18.88	25.0	2.70	4.3
7	23	1345	229.8	2	A	7.40	3.8	3.4	1.040	0.125	0.519	3.77	0.673	39.56	25.3	1.00	16.5
7	23	1655	232.8	2	A	7.30	3.5	2.8	1.000	0.156	0.802	NA	NA	24.45	25.8	2.80	9.0
7	23	1945	235.8	2	A	7.43	4.8	0.4	1.050	0.196	1.220	3.48	0.543	28.21	26.0	2.10	3.4
7	24	2241	238.7	2	A	7.32	4.1	3.4	1.270	0.136	0.994	NA	NA	24.45	24.8	2.00	4.2

946510455

JACKSON STREET - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	134	241.6	2	A	7.32	3.2	0.4	1.100	0.113	0.511	4.95	0.695	20.69	25.0	1.50	12.0
7	24	455	244.9	2	A	7.34	3.4	0.4	1.280	0.127	0.817	NA	NA	12.14	25.3	0.90	8.2
7	24	748	247.9	2	A	7.35	5.0	0.4	1.100	0.127	1.120	4.30	0.575	15.05	25.2	0.90	4.2
		AVERAGE READING				7.39	5.9	2.2	0.908	0.101	0.656	2.26	0.599	44.12	25.9	3.14	9.7

946510456

BASELINE

JACKSON

STREET

7-14/7-24-81

2/3 DEPTH

946510457

JACKSON STREET - -LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	805	8.1	2	B	7.27	3.2	2.7	1.170	0.082	0.393	NA	NA	18.81	26.3	2.20	15.5
7	14	1100	11.0	2	B	7.27	5.0	3.2	0.954	0.111	0.768	1.38	0.607	16.93	26.8	2.90	13.5
7	14	1357	13.9	2	B	7.34	4.2	3.3	0.727	0.068	0.638	0.90	0.540	28.22	26.3	2.40	10.0
7	14	1645	16.8	2	B	7.29	3.6	2.1	0.886	0.068	0.306	NA	NA	13.17	26.5	6.25	13.0
7	14	1940	19.7	2	B	7.49	4.0	2.0	1.020	0.101	0.375	1.19	0.553	18.81	25.8	3.25	18.0
7	14	2300	23.0	2	B	7.38	3.7	2.2	1.090	0.106	0.597	NA	NA	22.57	25.8	4.00	12.5
7	15	138	25.6	2	B	7.33	5.9	3.2	0.958	0.092	0.740	1.50	0.736	22.57	26.0	2.50	15.0
7	15	440	28.7	2	B	7.40	3.6	2.0	1.080	0.096	0.419	NA	NA	18.21	25.6	2.80	14.0
7	15	742	31.7	2	B	7.41	3.7	1.8	1.070	0.096	0.404	1.39	0.591	14.16	25.3	2.90	16.5
7	15	1040	34.7	2	B	7.47	4.5	1.4	0.993	0.096	0.605	NA	0.402	31.98	25.5	3.80	12.3
7	15	1340	37.7	2	B	7.42	5.0	1.2	1.030	0.096	0.658	NA	NA	26.33	26.0	2.50	14.8
7	15	1635	40.6	2	B	7.46	8.5	1.1	1.040	0.106	0.641	1.54	0.671	33.86	26.9	4.90	10.5
7	15	1935	43.6	2	B	7.63	5.1	1.6	0.979	0.096	0.351	NA	NA	37.62	25.5	4.50	18.0
7	15	2235	46.6	2	B	7.60	5.4	1.4	1.000	0.096	0.372	1.54	0.751	43.26	25.9	4.30	15.1
7	16	140	49.7	2	B	7.47	8.0	1.2	1.060	0.106	0.750	NA	NA	39.50	25.7	3.00	11.0
7	16	437	52.6	2	B	7.44	7.2	1.4	1.030	0.106	0.839	1.19	0.578	33.86	26.2	2.60	8.7
7	16	742	55.7	2	B	7.47	7.5	1.2	1.090	0.101	0.452	NA	NA	28.22	25.2	3.10	16.1
7	16	1040	58.7	2	B	7.33	3.3	2.0	0.772	0.039	0.348	0.76	0.462	16.93	25.5	3.00	14.5
7	16	1340	61.7	2	B	7.31	3.8	2.0	0.621	0.068	0.468	NA	NA	30.10	26.0	3.40	11.5
7	16	1640	64.7	2	B	7.36	5.0	1.6	0.897	0.077	0.546	1.54	0.558	31.98	26.0	4.10	11.5
7	16	1935	67.6	2	B	7.46	6.1	2.8	1.010	0.096	0.392	NA	NA	41.38	25.8	5.40	16.5
7	16	2240	70.7	2	B	7.48	5.2	1.4	0.996	0.101	0.381	1.48	0.686	33.86	25.8	4.90	15.1
7	17	2[illegible]	74.[illegible]	2	B	7.40	5.5	1.8	1.030	0.106	0.710	NA	NA	35.74	26.0	3.10	11.0
7	17	536	77.1	2	B	7.33	4.8	1.2	1.070	0.106	0.742	2.00	0.786	39.50	26.0	2.30	9.8
7	17	8[illegible]	80.[illegible]	2	B	7.3[illegible]	6.6	2.2	0.922	0.070	0.339	3.25	0.949	39.50	24.8	3.30	15.0
7	17	1055	82.9	2	B	7.40	6.5	2.0	0.897	0.080	0.392	NA	NA	30.10	25.0	3.40	16.0

94510458

JACKSON STREET - -LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	17	1400	86.0	2	B	7.40	7.5	2.4	0.412	0.020	0.160	3.54	0.541	47.03	26.5	4.40	9.5
7	17	1700	89.3	2	B	7.30	7.8	2.2	0.922	0.105	0.730	NA	NA	56.43	26.3	4.50	9.0
7	17	2000	92.0	2	B	7.50	6.7	2.2	0.794	0.099	0.396	1.80	0.712	52.67	25.7	5.30	16.5
7	17	2300	95.0	2	B	7.50	6.3	2.2	0.997	0.085	0.335	NA	NA	54.55	25.8	4.90	16.9
7	18	201	98.0	2	B	7.40	7.5	2.6	1.010	0.105	0.612	2.06	0.728	39.50	25.9	3.60	11.1
7	18	504	101.1	2	B	7.30	8.8	2.7	0.841	0.099	0.842	NA	NA	52.67	26.2	2.30	7.8
7	18	758	104.0	2	B	7.40	7.0	2.1	0.908	0.094	0.496	2.03	0.724	77.12	25.5	3.70	13.3
7	18	1050	106.8	2	B	7.40	5.8	2.1	0.995	0.080	0.374	NA	NA	60.19	25.3	3.10	16.5
7	18	1355	109.9	2	B	7.40	7.0	2.2	0.966	0.099	0.642	2.43	0.545	67.72	26.5	4.90	10.5
7	18	1655	112.9	2	B	7.40	7.5	2.4	0.960	0.104	0.849	NA	NA	62.07	26.1	3.10	11.1
7	18	1955	115.9	2	B	7.34	8.3	3.0	0.925	0.104	0.555	1.99	0.647	NA	26.5	8.20	13.1
7	18	2255	118.9	2	B	7.60	6.2	2.4	0.885	0.104	0.386	NA	NA	75.24	26.0	6.10	16.0
7	19	201	122.0	2	B	7.50	6.4	2.2	0.960	0.109	0.559	1.56	0.552	62.07	25.7	4.70	12.3
7	19	504	125.1	2	B	7.40	9.1	2.7	0.974	0.104	0.855	NA	NA	43.26	26.1	2.70	8.0
7	19	758	128.0	2	B	7.40	8.2	2.8	0.952	0.104	0.715	1.50	0.590	48.91	25.8	3.20	8.5
7	19	1055	130.9	2	B	7.36	4.3	2.4	0.858	0.090	0.364	2.09	0.773	67.72	26.0	2.80	17.3
7	19	1400	134.0	2	B	7.38	4.6	2.0	0.542	0.070	0.383	NA	NA	54.55	26.8	5.60	11.8
7	19	1700	137.0	2	B	7.36	5.3	1.8	0.911	0.094	0.709	1.76	0.672	52.67	26.8	3.70	9.1
7	19	2000	140.0	2	B	7.42	5.0	2.8	0.937	0.104	0.573	NA	NA	101.10	26.5	6.55	10.4
7	19	2300	143.	2	B	7.52	3.9	1.0	0.681	0.075	0.263	1.37	0.623	62.07	26.1	4.80	17.0
7	20	213	146.2	2	B	7.40	5.2	1.6	0.949	0.109	0.543	NA	NA	71.48	26.2	3.60	11.6
7	20	503	149.	2	B	7.38	5.8	1.4	0.480	0.075	0.655	1.06	0.504	63.95	26.0	3.00	8.6
7	20	754	151.9	2	B	7.35	6.2	1.6	1.030	0.109	0.730	NA	NA	56.43	26.1	2.45	7.8
7	20	1053	154.9	2	B	7.39	5.0	0.6	0.932	0.096	0.353	3.86	0.715	77.12	25.8	2.50	16.5
7	20	1350	157.8	2	B	7.41	5.2	0.4	0.819	0.052	0.277	NA	NA	75.24	26.0	2.80	13.8
7	20	1655	161.9	2	B	7.38	7.3	2.6	1.050	0.096	0.825	4.09	0.652	24.45	27.0	2.20	8.0

946510459

JACKSON STREET - -LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	1955	163.9	2	B	7.40	5.7	1.8	1.000	0.070	0.474	NA	NA	26.33	26.2	2.10	7.5
7	20	2255	166.9	2	B	7.40	4.5	0.4	1.020	0.096	0.421	4.62	0.636	22.57	25.8	2.30	15.5
7	21	159	170.9	2	B	7.33	6.0	2.0	1.160	0.136	0.193	NA	NA	39.50	26.0	0.40	7.8
7	21	455	172.9	2	B	7.44	9.5	4.2	1.040	0.134	1.050	2.88	1.200	47.02	25.9	NA	1.4
7	21	755	175.9	2	B	7.59	11.5	10.6	0.660	0.099	1.520	NA	NA	94.42	25.4	0.30	0.2
7	21	1050	178.8	2	B	7.10	9.3	3.6	1.040	0.191	0.183	3.18	0.815	24.95	25.5	0.25	12.5
7	21	1355	181.9	2	B	7.30	4.6	1.8	0.984	0.070	0.336	NA	NA	13.49	26.0	0.25	5.0
7	21	1655	184.9	2	B	7.40	9.1	4.2	0.723	0.127	1.410	3.07	0.741	26.33	26.5	1.00	1.5
7	21	1950	187.8	2	B	7.40	8.3	3.6	0.634	0.127	1.690	NA	NA	33.86	25.9	0.35	0.3
7	21	2245	190.8	2	B	7.30	6.2	1.4	0.884	0.115	0.535	2.60	0.797	18.21	26.5	0.90	10.5
7	22	158	194.9	2	B	7.30	4.2	1.2	0.980	0.047	0.259	NA	NA	15.51	26.0	0.25	11.0
7	22	505	197.1	2	B	7.30	7.7	2.6	1.010	0.165	1.260	3.87	0.640	25.63	25.3	NA	2.5
7	22	755	199.9	2	B	7.20	14.0	2.4	0.878	0.184	1.090	NA	NA	22.60	24.9	NA	0.8
7	22	1055	202.9	2	B	7.30	5.5	4.4	1.090	0.172	0.670	3.95	0.808	16.93	25.5	0.40	6.0
7	22	1354	205.9	2	B	7.30	3.7	3.4	1.250	0.127	0.424	NA	NA	18.81	26.0	0.70	16.5
7	22	1655	208.9	2	B	7.20	6.2	4.6	0.719	0.153	0.653	1.82	0.607	41.38	25.8	0.60	3.5
7	22	1950	211.8	2	B	7.20	14.0	4.0	0.941	0.212	0.769	NA	NA	30.10	25.5	0.50	6.0
7	22	2245	214.8	2	B	7.30	5.3	3.6	1.090	0.130	0.444	4.38	0.746	16.93	25.0	NA	0.4
7	23	155	217.9	2	B	7.40	3.6	2.0	1.250	0.118	0.384	NA	NA	18.81	25.5	1.10	17.4
7	23	458	221.0	2	B	7.30	4.7	3.8	0.599	0.058	0.280	1.40	0.478	30.10	25.0	0.30	5.5
7	23	756	223.9	2	B	7.30	5.7	3.0	1.160	0.151	0.879	NA	NA	22.57	25.0	0.20	4.2
7	23	1055	226.9	2	B	7.25	3.5	0.9	0.948	0.134	0.723	4.75	0.607	11.46	25.0	1.60	5.3
7	23	1355	229.9	2	B	7.37	2.8	0.4	1.050	0.118	0.411	NA	NA	13.49	25.3	0.60	17.0
7	23	1655	232.9	2	B	7.25	3.1	0.4	1.160	0.115	0.423	3.28	0.690	15.51	25.8	2.70	9.5
7	23	1950	235.8	2	B	7.33	3.7	.4	0.870	0.085	0.663	NA	NA	14.16	26.0	2.00	4.5
7	23	2245	238.8	2	B	7.36	4.0	0.8	0.655	0.058	0.423	2.76	0.514	18.88	24.8	1.90	5.0

94510460

JACKSON STREET - -LEVEL P - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	143	241.7	2	B	7.32	3.3	0.4	1.220	0.118	0.523	NA	N_A	11.46	25.2	1.0_0	14.0
7	24	504	245.1	2	B	7.35	3.6	0.4	0.830	0.077	0.497	1.82	0.586	11.46	25.2	0.80	8.7
7	24	755	247.9	2	B	7.40	5.6	6.4	1.150	0.132	1.060	NA	NA	16.86	25.2	0.80	4.5
		AVERAGE READING				7.38	5.9	2.3	0.939	0.102	0.586	2.32	0.660	37.16	25.8	2.84	10.7

946510461

BASELINE

BELLEVILLE TURNPIKE

7-14/7-24-81

1/3 DEPTH

946510462

BELLVILLE TURNPIKE - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	14	933	9.5	3	A	7.35	6.0	2.2	0.564	0.073	0.937	2.43	0.368	30.10	27.5	3.00	3.8
7	14	1230	12.5	3	A	7.36	5.9	3.4	0.446	0.054	0.966	NA	NA	41.38	28.0	3.20	1.3
7	14	1536	15.6	3	A	7.43	5.5	2.2	0.557	0.087	1.130	1.81	0.436	47.02	28.5	3.40	1.3
7	14	1830	18.5	3	A	7.36	5.5	3.2	0.753	0.096	0.891	NA	NA	28.22	27.0	3.25	8.5
7	14	2125	21.4	3	A	7.39	5.1	2.2	0.849	0.092	0.958	3.41	0.555	28.22	27.0	3.70	4.5
7	15	28	24.5	3	A	7.41	9.5	2.8	0.719	0.087	1.070	NA	NA	35.74	27.0	2.80	1.5
7	15	325	27.4	3	A	7.38	7.8	2.0	0.777	0.087	1.060	2.99	0.611	45.14	26.9	2.20	1.5
7	15	625	30.4	3	A	7.30	5.9	3.6	0.774	0.096	0.868	NA	NA	37.62	26.2	2.20	5.7
7	15	930	33.5	3	A	7.38	5.3	2.6	0.844	0.087	0.873	2.20	0.481	37.62	26.3	3.40	4.5
7	15	1235	36.6	3	A	7.52	7.0	3.0	0.663	0.068	0.821	NA	NA	35.74	27.8	3.90	2.0
7	15	1540	39.7	3	A	7.47	7.6	3.8	0.428	0.086	1.250	1.75	0.564	37.62	27.3	2.60	1.8
7	15	1840	42.7	3	A	7.40	7.0	3.8	0.947	0.096	0.808	NA	NA	35.74	26.9	4.10	6.9
7	15	2140	45.7	3	A	7.42	6.4	2.6	0.935	0.095	0.955	2.50	0.497	45.14	26.5	4.00	6.0
7	16	41	48.7	3	A	7.40	6.1	2.6	0.794	0.086	1.140	NA	NA	35.74	26.8	2.90	2.8
7	16	340	51.7	3	A	7.46	7.4	2.8	0.779	0.090	1.210	1.90	0.466	41.38	26.2	2.20	1.3
7	16	638	54.6	3	A	7.35	7.5	1.8	0.912	0.090	1.040	NA	NA	35.74	26.5	2.00	4.3
7	16	940	57.7	3	A	7.28	4.2	1.4	0.673	0.076	0.800	2.10	0.530	20.69	26.5	2.20	5.5
7	16	1238	60.6	3	A	7.44	4.5	2.0	0.696	0.086	1.160	NA	NA	41.38	27.3	4.50	2.5
7	16	1535	63.6	3	A	7.40	4.8	1.8	0.818	0.086	1.180	3.84	0.664	35.74	27.0	2.80	1.8
7	16	1835	66.6	3	A	7.43	5.3	2.8	0.793	0.090	1.000	NA	NA	41.38	27.0	4.40	4.3
7	16	2135	69.6	3	A	7.36	5.2	1.8	0.986	0.100	0.868	3.47	0.607	41.38	26.2	2.80	8.1
7	17	50	72.8	3	A	7.43	5.7	1.4	0.735	0.086	1.110	NA	NA	52.67	26.5	3.00	3.4
7	17	345	75.8	3	A	7.45	6.3	2.0	0.835	0.086	1.170	3.18	0.651	45.14	26.5	1.90	1.0
7	17	651	78.8	3	A	7.33	5.7	1.2	0.954	0.090	1.040	NA	NA	45.14	26.3	2.00	3.8
7	17	945	81.8	3	A	7.30	8.7	0.6	0.812	NA	NA	2.38	0.545	30.10	26.3	2.30	9.0
7	17	1255	84.9	3	A	7.40	2.1	2.2	0.864	0.080	1.120	NA	NA	47.03	27.5	5.30	2.5

94510463

BELLVILLE TURNPIKE - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1545	87.8	3	A	7.40	9.5	2.2	0.855	0.075	1.210	2.41	0.660	37.62	27.0	2.40	1.5
7	17	1845	90.8	3	A	7.40	11.0	3.2	0.856	0.070	0.924	NA	NA	52.67	26.8	3.90	4.2
7	17	2145	93.8	3	A	7.30	9.7	1.8	1.000	0.089	0.900	4.04	0.625	47.03	26.4	3.00	7.3
7	18	49	96.8	3	A	7.30	10.0	1.8	0.893	0.080	1.030	NA	NA	45.14	26.2	3.10	4.0
7	18	351	99.8	3	A	7.40	14.0	2.0	0.884	0.080	1.220	3.84	0.653	35.74	26.5	2.10	1.5
7	18	650	102.8	3	A	7.40	12.0	2.4	0.923	0.080	1.130	NA	NA	58.31	26.4	1.80	2.5
7	18	955	105.9	3	A	7.30	12.0	2.8	1.020	0.089	0.921	4.14	0.698	82.76	26.3	2.20	6.0
7	18	1300	109.[illegible]	3	A	7.40	8.6	3.0	0.874	0.075	0.995	NA	NA	54.55	27.3	4.10	3.5
7	18	1548	111.8	3	A	7.40	12.0	3.0	0.855	0.057	0.943	3.50	0.591	37.62	27.0	2.40	2.3
7	18	1850	114.8	3	A	7.50	14.0	4.2	0.860	0.075	1.150	NA	NA	58.31	27.0	4.30	2.4
7	18	2150	117.8	3	A	7.40	15.0	3.2	0.866	0.098	0.855	3.61	0.793	62.07	26.8	3.50	8.0
7	19	49	120.8	3	A	7.40	12.0	4.2	0.934	0.084	0.986	NA	NA	50.79	26.4	2.80	5.9
7	19	352	123.9	3	A	7.40	12.0	2.8	0.931	0.084	1.206	3.47	0.655	50.79	26.8	2.35	1.8
7	19	652	126.9	3	A	7.40	13.0	3.1	0.817	0.080	1.230	NA	NA	65.84	26.1	2.10	1.5
7	19	945	129.8	3	A	7.33	6.3	3.2	1.050	0.066	0.768	5.66	1.240	57.32	26.8	2.60	5.8
7	19	1247	132.8	3	A	7.34	5.6	1.2	0.935	0.084	0.986	NA	NA	50.58	27.3	3.50	4.8
7	19	1545	135.8	3	A	7.40	6.3	1.2	0.827	0.066	1.000	3.98	0.800	21.39	28.0	3.70	2.0
7	19	1845	138.8	3	A	7.43	6.7	1.0	0.776	0.075	1.210	NA	NA	50.58	27.1	4.20	1.7
7	19	2145	141.8	3	A	7.33	7.2	1.8	1.000	0.094	0.896	4.30	1.250	80.93	26.5	3.10	6.5
7	20	48	144.8	3	A	7.35	6.6	1.0	0.980	0.098	0.885	4.59	0.653	74.18	26.3	2.60	6.5
7	20	352	147.9	3	A	7.41	6.8	1.0	0.942	0.084	1.090	NA	NA	15.56	26.5	2.15	2.2
7	20	651	150.9	3	A	7.44	7.5	1.2	0.569	0.043	0.734	NA	NA	60.69	26.2	1.70	1.0
7	20	950	153.8	3	A	7.39	9.6	2.8	0.810	0.094	0.956	4.24	0.722	43.26	26.8	1.60	4.8
7	20	1249	156.9	3	A	7.38	7.1	0.4	0.681	0.052	0.510	NA	NA	35.74	26.3	1.80	5.8
7	20	1545	159.8	3	A	7.42	8.3	0.4	1.030	0.084	1.130	4.33	0.796	54.55	26.3	1.70	2.5
7	20	1851	162.9	3	A	7.51	7.6	0.4	0.685	0.084	1.300	NA	NA	5.64	26.5	1.50	0.5

946510464

BELLVILLE TURNPIKE - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2150	165.8	3	A	7.34	7.3	2.8	1.250	0.084	0.996	4.56	0.912	28.22	26.5	1.00	0.0
7	21	44	168.7	3	A	7.40	7.0	6.8	1.080	0.098	1.190	NA	NA	12.14	25.8	1.30	1.0
7	21	345	171.[illegible]	3	A	7.62	11.0	3.4	0.424	0.089	1.440	NA	NA	45.14	25.7	2.60	0.0
7	21	650	174.8	3	A	7.57	13.5	5.8	0.480	0.122	1.770	4.63	1.220	34.80	25.0	3.90	0.0
7	21	940	177.7	3	A	7.30	28.0	10.0	0.810	0.118	1.650	9.29	1.070	33.86	25.3	2.70	0.5
7	21	1245	180.8	3	A	7.40	15.0	5.8	0.790	0.122	1.420	NA	NA	37.62	25.5	1.30	0.8
7	21	1547	183.8	3	A	7.30	25.0	4.2	0.419	0.118	1.300	3.18	0.881	24.28	25.5	3.30	0.8
7	21	1850	186.8	3	A	7.20	23.0	3.8	0.492	0.090	1.040	NA	NA	14.16	24.5	4.00	0.2
7	21	2150	189.8	3	A	7.10	27.0	4.0	0.536	0.090	1.160	3.79	0.855	26.30	26.0	3.10	0.5
7	22	45	192.8	3	A	7.10	15.0	3.2	0.620	0.109	1.200	NA	NA	22.93	25.0	0.90	0.0
7	22	358	196.[illegible]	3	A	7.10	22.0	3.4	0.606	0.090	1.110	6.12	1.330	27.65	24.5	2.50	0.0
7	22	648	198.8	3	A	7.40	18.0	4.8	0.983	0.172	1.330	NA	NA	21.58	25.5	4.20	0.0
7	22	945	201.8	3	A	7.60	17.0	5.4	0.938	0.168	1.340	4.52	0.842	31.98	25.5	4.10	0.0
7	22	1252	204.[illegible]	3	A	7.30	12.0	5.4	0.944	0.140	1.410	5.65	0.851	20.69	24.8	0.40	0.0
7	22	1545	207.[illegible]	3	A	7.40	16.0	5.2	0.914	0.131	1.230	3.84	0.660	45.14	25.5	2.50	0.0
7	22	1850	210.8	3	A	7.40	14.0	5.4	0.871	0.130	1.430	11.60	0.912	33.86	26.5	5.00	0.2
7	22	2150	213.8	3	A	7.50	15.0	5.2	0.757	0.124	1.400	11.10	0.671	24.45	26.0	4.40	0.2
7	23	48	216.[illegible]	3	A	7.30	14.0	6.4	1.020	0.145	1.360	4.56	0.651	31.98	25.5	1.20	0.0
7	23	349	219.[illegible]	3	A	7.40	13.0	4.4	0.707	0.140	1.500	11.70	0.576	31.98	25.5	3.00	0.0
7	23	650	222.8	3	A	7.40	25.0	5.2	0.707	0.135	1.410	11.20	1.260	9.44	24.7	4.00	0.0
7	23	945	225.[illegible]	3	A	7.6[illegible]	8.6	2.4	0.702	0.150	1.440	4.42	0.634	12.14	24.5	4.20	0.0
7	23	1247	228.8	3	A	7.42	8.8	2.0	NA	NA	NA	NA	NA	43.26	25.8	2.30	0.5
7	23	1545	231.[illegible]	3	A	7.43	7.6	2.6	0.789	0.140	1.340	5.96	0.530	14.84	25.5	2.20	0.5
7	23	1850	234.[illegible]	3	A	7.47	11.0	1.8	0.827	0.156	1.450	4.31	0.888	37.62	25.5	4.40	0.2
7	23	2150	237.[illegible]	3	A	7.52	10.5	2.1	1.200	0.171	1.480	4.28	0.717	20.69	25.0	5.00	0.0
7	24	44	240.7	3	A	7.37	10.0	1.8	1.320	0.124	1.290	4.33	0.772	31.96	25.3	2.40	0.8

946510465

BELLVILLE TURNPIKE - LEVEL A - DEPTH 1/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O. [PPM]	SAL [PPT]
7	24	358	244.9	3	A	7.38	6.3	2.2	1.330	0.130	1.290	4.04	0.497	41.38	25.0	2.20	0.5
7	24	644	246.7	3	A	7.45	11.5	3.4	1.300	0.176	1.510	4.42	1.040	84.30	25.0	3.70	0.0
		AVERAGE READING				7.39	10.3	2.9	0.829	0.098	1.129	4.54	0.742	39.16	26.3	2.90	2.5

946510466

BASELINE

BELLEVILLE TURNPIKE

7-14/7-24-81

2/3 DEPTH

946510467

BELLEVILLE TURNPIKE - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	935	9.6	3	B	7.32	4.7	1.4	0.801	0.077	0.783	2.33	0.489	26.33	27.5	1.70	4.8
7	14	1235	12.6	3	B	7.33	6.5	1.8	0.848	0.087	0.963	NA	NA	35.74	27.8	2.90	3.0
7	14	1541	15.7	3	B	7.44	7.5	2.2	0.600	0.058	0.777	2.55	0.515	39.50	28.0	3.90	1.8
7	14	1835	18.6	3	B	7.37	5.1	2.6	0.981	0.101	0.817	NA	NA	20.69	26.5	3.50	9.0
7	14	2130	21.5	3	B	7.35	6.2	2.0	0.743	0.087	0.867	2.87	0.424	35.74	26.5	3.60	5.0
7	15	37	24.6	3	B	7.43	7.5	2.6	0.821	0.087	0.953	NA	NA	35.74	27.0	2.60	2.0
7	15	336	27.6	3	B	7.40	6.5	2.0	0.784	0.087	1.010	3.77	0.567	37.62	27.1	1.70	2.3
7	15	637	30.6	3	B	7.31	7.5	2.4	0.979	0.096	0.830	NA	NA	16.93	26.2	2.10	6.0
7	15	935	33.6	3	B	7.36	6.0	4.0	0.835	0.073	0.669	2.28	0.421	31.98	26.3	2.40	5.3
7	15	1240	36.7	3	B	7.39	8.5	2.2	0.868	0.087	0.983	NA	NA	41.38	27.3	2.50	3.0
7	15	1545	39.8	3	B	7.41	7.6	1.4	0.822	0.077	0.948	2.56	0.492	48.91	27.0	1.20	3.3
7	15	1845	42.8	3	B	7.46	17.0	1.6	0.905	0.095	0.945	NA	NA	37.62	26.9	3.90	7.1
7	15	2145	45.8	3	B	7.42	11.0	1.4	0.535	0.048	0.527	2.33	0.468	28.22	26.8	3.70	7.3
7	16	48	48.8	3	B	7.44	10.0	2.6	0.726	0.086	1.190	NA	NA	35.74	26.8	2.80	3.1
7	16	345	51.8	3	B	7.45	12.0	2.0	0.806	0.086	1.180	4.00	0.586	41.38	26.5	1.70	4.0
7	16	644	54.7	3	B	7.37	15.0	2.2	0.653	0.081	0.949	NA	NA	35.74	26.3	2.00	4.5
7	16	945	57.8	3	B	7.28	4.5	1.8	0.949	0.095	0.990	3.86	0.564	NA	26.5	1.90	5.8
7	16	1243	60.7	3	B	7.32	4.3	3.8	0.810	0.086	1.100	NA	NA	39.40	27.0	4.10	3.0
7	16	1540	63.7	3	B	7.34	4.7	2.4	0.699	0.062	0.925	2.87	0.497	35.74	26.5	0.80	3.3
7	16	1840	66.7	3	B	7.39	5.5	3.0	0.963	0.090	1.040	NA	NA	58.31	27.0	4.20	5.0
7	16	2140	69.7	3	B	7.34	5.3	2.2	1.010	0.100	0.862	3.00	0.607	45.14	26.3	2.80	8.7
7	17	56	73.[illegible]	3	B	7.37	5.4	2.2	0.912	0.090	1.030	NA	NA	47.97	26.5	2.95	3.8
7	17	4[illegible]	76.[illegible]	3	B	7.36	4.7	2.8	0.872	0.081	1.170	2.41	0.497	67.49	26.4	1.40	3.0
7	17	65[illegible]	79.[illegible]	3	B	7.34	5.6	3.0	0.713	0.090	1.070	NA	NA	47.03	26.2	2.00	3.9
7	17	953	81.8	3	B	7.3	9.2	1.8	0.728	0.052	0.636	2.06	0.468	35.74	26.3	2.10	6.3
7	17	1300	85.[illegible]	3	B	7.30	7.2	2.0	0.898	0.075	1.020	NA	NA	45.14	26.8	2.60	3.3

946510468

BELLEVILLE TURNPIKE - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1550	87.6	3	B	7.40	12.0	1.8	0.828	0.080	1.190	2.77	0.586	28.22	26.8	1.40	2.5
7	17	1850	90.6	3	B	7.40	16.0	2.2	0.938	0.080	1.040	NA	NA	NA	26.9	3.90	4.2
7	17	2150	93.6	3	B	7.30	14.0	2.2	0.981	0.089	0.888	2.46	0.636	50.79	26.2	2.60	7.9
7	18	55	96.9	3	B	7.40	14.0	2.0	0.898	0.080	1.010	NA	NA	43.26	26.2	3.00	4.2
7	18	358	100.0	3	B	7.40	12.0	2.0	0.922	0.080	1.160	NA	NA	37.62	26.8	1.90	1.8
7	18	659	103.[illegible]	3	B	7.40	12.0	3.2	NA	NA	NA	NA	NA	67.72	26.4	1.70	2.7
7	18	1000	106.0	3	B	7.50	18.0	3.4	0.950	0.075	0.791	3.67	0.796	41.38	26.3	2.10	6.3
7	18	1305	109.1	3	B	7.50	14.0	4.6	0.913	0.080	1.030	NA	NA	8.09	27.0	3.10	3.8
7	18	1553	111.[illegible]	3	B	7.40	14.0	9.8	0.904	0.075	1.120	6.13	0.679	24.45	26.8	1.30	3.5
7	18	1855	114.9	3	B	7.50	17.0	4.2	0.848	0.080	1.150	NA	NA	50.79	27.2	4.20	2.4
7	18	2155	117.9	3	B	7.40	20.0	3.2	1.030	0.089	0.814	4.62	0.894	82.76	26.7	3.40	8.0
7	19	56	120.9	3	B	7.40	13.0	2.8	0.931	0.084	0.936	NA	NA	65.84	26.3	2.60	7.1
7	19	358	124.[illegible]	3	B	7.40	14.0	3.2	0.789	0.057	0.863	NA	NA	39.50	26.8	2.30	2.0
7	19	700	127.[illegible]	3	B	7.40	18.0	2.6	0.648	0.070	1.110	NA	NA	45.14	26.2	2.00	1.7
7	19	950	129.[illegible]	3	B	7.30	6.0	2.2	0.996	0.075	0.899	5.15	1.160	82.78	26.8	2.60	5.8
7	19	1252	132.9	3	B	7.44	6.4	2.0	0.838	0.075	0.902	NA	NA	NA	26.8	2.10	6.0
7	19	1550	135.[illegible]	3	B	7.39	6.4	1.8	0.934	0.080	1.180	6.19	0.918	57.32	27.5	2.40	3.0
7	19	1850	138.[illegible]	3	B	7.44	6.6	1.4	0.866	0.075	1.190	NA	NA	64.07	27.1	3.40	2.8
7	19	2150	141.[illegible]	3	B	7.32	7.8	3.0	1.020	0.094	0.926	4.85	1.530	43.84	26.5	3.10	6.8
7	20	59	145.0	3	B	7.34	6.5	1.0	0.939	0.103	0.867	NA	NA	84.64	26.5	2.70	6.5
7	20	400	146.[illegible]	3	B	7.37	6.5	1.6	0.831	0.057	0.835	NA	NA	50.58	26.5	2.15	2.3
7	20	657	150.[illegible]	3	B	7.44	7.5	1.4	0.946	0.084	1.280	3.52	0.719	60.69	26.2	1.30	1.0
7	21	955	153.[illegible]	3	B	7.39	12.5	2.6	0.923	0.047	0.510	3.79	1.420	206.91	26.8	1.70	5.0
7	21	1259	156.[illegible]	3	B	7.37	6.7	0.6	0.990	0.098	0.912	NA	NA	24.45	26.3	1.70	6.3
7	21	1559	159.[illegible]	3	B	7.44	9.6	1.8	1.060	0.084	1.070	4.54	0.925	87.67	26.5	1.40	3.0
7	21	1855	162.[illegible]	3	B	7.51	7.5	1.2	0.840	0.089	1.250	NA	NA	18.81	26.5	1.50	0.5

946510469

BELLEVILLE TURNPIKE - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2155	165.9	3	B	7.34	8.2	4.2	1.200	0.084	0.946	NA	NA	33.86	26.5	0.90	3.2
7	21	54	168.9	3	B	7.40	7.3	2.4	1.180	0.011	1.260	NA	NA	161.86	25.8	0.75	1.0
7	21	356	171.9	3	B	7.66	10.5	4.8	0.456	0.098	1.560	NA	NA	253.34	25.8	2.65	0.0
7	21	659	175.0	3	B	7.56	12.5	8.4	0.421	0.122	1.760	NA	NA	65.84	25.0	3.70	0.0
7	21	945	177.8	3	B	7.30	34.0	9.8	1.320	0.122	1.480	12.70	1.580	33.86	25.3	2.70	0.5
7	21	1250	180.8	3	B	7.40	15.0	6.2	0.793	0.127	1.370	NA	NA	22.57	25.3	0.90	0.8
7	21	1552	183.9	3	B	7.20	26.0	5.2	0.826	0.122	1.300	4.19	0.887	33.86	25.3	3.20	0.8
7	21	1855	186.9	3	B	7.20	24.0	4.8	0.591	0.090	0.980	NA	NA	12.81	24.0	5.00	3.9
7	21	2155	189.9	3	B	7.10	30.0	4.0	0.939	0.090	1.080	3.12	0.769	15.51	26.0	3.10	0.3
7	22	55	192.9	3	B	7.10	12.0	3.0	0.651	0.109	1.140	NA	NA	45.14	25.0	0.95	0.0
7	22	405	196.1	3	B	7.10	24.0	3.2	1.040	0.090	1.040	2.98	0.727	11.46	24.5	2.45	0.0
7	22	655	198.9	3	B	7.30	23.0	4.2	1.020	0.172	1.140	NA	NA	20.69	25.5	4.20	0.0
7	22	950	201.8	3	B	7.40	25.0	8.6	1.550	0.172	1.370	3.88	0.766	35.74	25.5	4.10	0.0
7	22	1257	204.9	3	B	7.20	13.0	6.0	1.310	0.145	1.320	5.59	0.829	26.33	24.5	0.50	0.0
7	22	1550	207.8	3	B	7.30	18.0	5.6	1.310	0.131	1.220	3.50	0.712	24.45	25.3	2.20	0.0
7	22	1855	210.9	3	B	7.40	21.0	4.8	1.160	0.135	1.360	9.26	0.600	30.10	26.5	4.90	0.1
7	22	2150	213.8	3	B	7.70	16.0	4.6	0.986	0.114	1.420	7.01	0.585	37.62	26.0	4.30	0.2
7	23	56	216.9	3	B	7.30	17.0	5.2	1.440	0.150	1.320	5.75	0.741	41.38	25.5	1.00	0.0
7	23	355	219.9	3	B	7.40	16.0	2.4	1.380	0.156	1.380	5.54	0.696	47.03	25.7	2.90	0.0
7	23	658	223.0	3	B	7.40	25.0	3.0	1.140	0.145	1.360	3.87	1.130	102.93	24.7	4.00	0.0
7	23	953	225.8	3	B	7.44	16.0	3.8	1.110	0.145	1.390	3.53	0.681	43.26	24.5	4.10	0.0
7	23	1252	228.9	3	B	7.38	18.0	5.6	NA	NA	NA	NA	NA	87.67	25.8	2.20	0.5
7	23	1550	231.8	3	B	7.37	10.0	3.8	1.320	0.145	1.310	4.72	0.538	33.85	25.5	1.80	1.0
7	23	1855	234.9	3	B	7.41	24.0	3.8	1.140	0.156	1.420	4.05	0.880	28.22	25.5	4.30	0.0
7	23	2155	237.9	3	B	7.44	19.0	3.4	1.150	0.176	1.500	3.24	0.697	47.02	25.0	4.90	0.0
7	24	54	240.8	3	B	7.36	19.0	4.6	1.230	0.135	1.300	4.21	0.804	39.50	25.3	2.30	0.8

946510470

BELLEVILLE TURNPIKE - LEVEL B - DEPTH 2/3
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	405	244.1	3	B	7.34	11.0	3.0	1.180	0.114	1.120	3.60	0.521	35.74	25.0	2.0_0	0.5
7	24	650	246.6	3	B	7.43	25.0	3.8	1.170	0.176	1.490	6.07	1.010	NA	25.0	3.70	0.5
		AVERAGE READING				7.38	12.6	3.2	0.936	0.097	1.083	4.22	0.747	48.95	26.2	2.60	3.0

946510471

BASELINE

UNION AVENUE

7-14/7-24-81

1/2 DEPTH

946510472

UNION AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	1000	10.0	S	C	7.75	8.9	4.4	0.330	0.096	1.270	3.74	0.731	48.91	28.0	4.30	0.2
7	14	1300	13.0	S	C	7.94	8.5	5.4	0.179	0.106	1.350	NA	NA	62.07	27.5	4.90	0.1
7	14	1600	16.0	S	C	NA	NA	NA	0.296	0.096	1.240	2.59	0.897	NA	28.0	6.50	NA
7	14	1900	19.0	S	C	7.75	9.5	4.2	0.418	0.092	1.180	3.59	0.756	60.19	27.5	5.00	NA
7	14	2155	21.9	S	C	7.75	13.0	5.0	0.368	0.096	1.170	NA	NA	56.43	27.5	4.80	NA
7	15	56	24.0	S	C	7.91	13.5	6.0	0.198	0.106	1.350	2.17	0.788	60.19	26.3	5.90	NA
7	15	358	28.[illegible]	S	C	7.84	11.5	5.0	0.234	0.106	1.330	NA	NA	58.31	26.2	5.10	NA
7	15	658	31.0	S	C	7.69	12.0	4.4	0.417	0.096	1.180	2.20	0.825	67.72	26.2	4.00	NA
7	15	1010	34.2	S	C	7.48	8.5	3.2	0.471	0.096	1.160	1.89	0.696	37.62	26.5	3.80	NA
7	15	1300	37.[illegible]	S	C	7.66	6.6	4.2	0.293	0.101	1.310	NA	NA	39.50	26.8	4.40	0.1
7	15	1555	39.9	S	C	7.82	7.0	3.6	0.323	0.106	1.330	2.58	0.650	41.38	26.5	4.40	NA
7	15	1900	43.[illegible]	S	C	7.63	16.0	4.2	0.434	0.090	1.340	NA	NA	35.74	27.0	4.10	NA
7	15	2200	46.0	S	C	7.64	6.7	4.2	0.480	0.095	1.390	3.00	0.738	45.14	26.1	3.90	NA
7	16	100	49.[illegible]	S	C	7.68	8.5	4.0	0.337	0.105	1.520	NA	NA	41.38	25.8	4.20	NA
7	16	402	52.	S	C	7.73	8.4	5.0	0.328	0.114	1.590	2.42	0.614	43.26	25.3	4.60	NA
7	16	705	55.1	S	C	7.59	7.1	3.2	0.425	0.100	1.420	NA	NA	39.50	26.2	2.90	NA
7	16	1005	58.1	S	C	7.65	6.8	1.4	0.398	0.095	1.420	2.71	0.636	47.03	26.5	2.30	NA
7	16	1309	61.1	S	C	7.72	7.9	4.0	0.419	0.114	1.560	NA	NA	5.06	25.3	3.30	0.1
7	16	1605	64.1	S	C	7.68	12.0	4.8	0.299	0.114	1.623	2.41	0.582	62.07	25.0	4.20	0.1
7	16	1900	67.[illegible]	S	C	7.69	13.0	4.2	0.487	0.105	1.430	NA	NA	5.25	26.9	3.20	NA
7	16	2155	69.9	S	C	7.68	9.7	0.5	0.477	0.095	1.390	1.50	0.497	54.55	27.0	2.70	NA
7	17	125	73.4	S	C	7.77	8.9	4.0	0.392	0.105	1.430	NA	NA	63.95	25.8	3.30	NA
7	17	427	76.4	S	C	7.86	9.3	3.6	0.302	0.114	1.510	1.97	0.636	45.14	25.4	5.00	NA
7	17	726	79.4	S	C	7.69	7.4	5.0	0.481	0.109	1.480	NA	NA	26.33	25.6	2.50	NA
7	17	1020	82.3	S	C	7.70	15.0	1.5	0.538	0.094	1.460	2.02	0.670	69.60	26.0	2.00	NA
7	17	1322	85.4	S	C	7.70	10.0	1.5	0.424	0.107	1.610	NA	NA	37.62	25.5	3.40	NA

946510473

UNION AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1620	88.3	5	C	7.80	16.0	1.4	0.364	0.107	1.660	2.22	0.723	52.67	25.3	4.40	NA
7	17	1920	91.3	5	C	7.70	20.0	1.8	0.521	0.098	1.510	NA	NA	33.86	26.0	3.20	NA
7	17	2220	94.3	5	C	7.60	15.0	1.2	0.545	0.094	1.440	2.94	0.699	56.43	26.3	2.30	NA
7	18	120	97.3	5	C	7.70	17.0	1.4	0.498	0.107	1.570	NA	NA	35.74	25.5	3.00	NA
7	18	422	100.4	5	C	7.90	18.0	2.6	0.403	0.107	1.630	3.30	1.120	37.62	25.4	3.95	NA
7	18	721	103.3	5	C	7.80	17.0	2.4	0.341	0.107	1.620	NA	NA	31.98	25.5	3.40	NA
7	18	1018	106.3	5	C	7.60	14.0	3.2	0.655	0.103	1.480	2.99	0.676	18.81	26.0	2.00	NA
7	18	1320	109.3	5	C	7.70	20.0	4.2	0.467	0.107	1.570	NA	NA	33.86	25.5	2.70	0.1
7	18	1620	112.3	5	C	7.90	15.0	3.8	NA	NA	NA	NA	NA	43.26	25.8	3.40	NA
7	18	1920	115.3	5	C	7.80	21.0	4.4	0.411	0.107	1.560	NA	NA	41.38	26.0	4.70	NA
7	18	2220	118.3	5	C	7.70	17.0	3.4	0.620	0.098	1.420	2.83	0.761	30.10	26.7	2.80	NA
7	19	121	121.3	5	C	7.73	14.0	3.2	0.596	0.112	1.590	NA	NA	10.79	25.5	3.90	NA
7	19	419	124.3	5	C	7.80	15.0	4.8	0.403	0.080	1.450	2.31	0.501	28.22	24.9	3.60	NA
7	19	720	127.3	5	C	7.70	17.0	3.0	0.678	0.103	1.510	NA	NA	43.26	24.8	3.80	NA
7	19	1015	130.3	5	C	7.54	5.2	3.6	0.598	0.094	1.480	2.72	0.782	47.21	26.5	2.60	NA
7	19	1310	133.2	5	C	7.55	5.2	3.6	0.663	0.103	1.520	NA	NA	53.95	26.3	2.50	0.1
7	19	1612	136.2	5	C	7.68	6.2	3.8	0.461	0.107	1.590	1.88	0.673	30.35	26.9	4.20	NA
7	19	1910	139.2	5	C	7.71	6.2	3.6	0.601	0.114	1.640	NA	NA	17.50	26.5	4.80	NA
7	19	2210	142.2	5	C	7.57	7.3	1.6	0.601	0.098	1.470	2.76	0.793	33.72	26.2	3.10	NA
7	20	118	145.3	5	C	7.61	8.5	1.6	0.518	NA	NA	NA	NA	67.44	26.0	3.35	NA
7	2	421	148.3	5	C	7.73	7.5	2.4	0.435	0.108	1.610	1.62	0.607	43.84	25.5	3.50	NA
7	2	714	151.2	5	C	7.72	8.0	2.4	0.560	0.107	1.580	NA	NA	40.46	25.3	3.40	NA
7	20	1010	154.2	5	C	7.59	12.0	3.6	0.550	0.098	1.560	2.71	0.636	22.57	26.0	2.50	NA
7	20	1315	157.1	5	C	7.61	16.5	6.6	0.551	0.103	1.470	NA	NA	41.38	26.0	2.40	NA
7	20	1615	160.3	5	C	7.68	10.0	4.0	0.482	0.098	1.590	NA	NA	16.93	25.8	3.40	NA
7	2	1920	163.3	5	C	7.70	11.5	4.6	0.489	0.103	1.670	2.41	0.564	161.68	25.8	3.40	NA

94651047

UNION AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	21	2229	166.3	5	C	7.62	10.1	2.8	0.610	0.098	1.540	NA	NA	155.11	24.5	2.60	0.3
7	21	121	169.3	5	C	7.72	12.0	8.4	0.554	0.117	1.560	2.56	0.635	244.53	25.0	5.70	NA
7	21	418	172.3	5	C	7.39	14.0	7.8	0.450	0.122	1.570	NA	NA	7.42	24.8	4.60	NA
7	21	720	175.3	5	C	7.71	13.5	7.0	0.437	0.126	1.490	2.38	0.607	141.62	24.9	4.60	NA
7	21	1010	178.2	5	C	7.30	42.0	7.6	0.748	0.122	1.010	2.29	0.582	14.16	24.0	4.60	0.3
7	21	1308	181.1	5	C	7.39	38.0	6.8	0.572	0.122	1.010	NA	NA	24.45	24.0	4.80	0.5
7	21	1615	184.3	5	C	7.53	16.0	7.0	0.832	0.131	1.240	2.42	0.521	NA	25.0	6.40	NA
7	21	1920	187.3	5	C	7.73	12.0	7.6	1.010	0.191	1.460	NA	NA	18.81	24.5	7.00	NA
7	21	2215	190.3	5	C	7.59	8.5	5.8	1.160	0.186	1.460	3.73	0.614	26.33	26.5	6.20	NA
7	22	120	193.3	5	C	7.60	8.0	4.8	1.060	0.186	1.470	NA	NA	30.10	26.2	5.40	NA
7	22	430	196.5	5	C	7.61	11.5	4.6	0.872	0.127	1.320	3.26	0.504	18.81	25.5	5.10	NA
7	22	715	199.3	5	C	7.51	11.0	4.4	0.956	0.122	1.200	NA	NA	20.39	25.5	5.00	NA
7	22	1010	202.2	5	C	7.60	18.0	6.0	0.910	0.141	1.340	2.68	0.490	24.45	25.0	5.00	NA
7	22	1315	205.3	5	C	7.60	16.0	6.4	0.710	0.141	1.330	NA	NA	22.57	25.3	4.50	NA
7	22	1615	208.3	5	C	7.60	18.0	6.8	0.853	0.156	1.590	3.88	0.564	18.81	25.0	5.30	0.1
7	22	1920	211.3	5	C	7.70	16.0	7.2	0.907	0.197	1.570	3.37	0.611	20.69	26.0	5.50	0.2
7	22	2215	214.3	5	C	7.70	14.0	6.8	0.923	0.208	1.590	3.24	0.568	30.10	26.0	6.70	0.3
7	23	118	217.3	5	C	7.70	15.0	5.8	0.941	0.187	1.540	3.71	0.625	28.22	25.0	5.80	NA
7	23	416	220.3	5	C	7.70	15.0	5.4	0.962	0.187	1.540	2.22	0.476	26.33	25.8	6.00	NA
7	23	717	223.3	5	C	7.70	17.0	6.8	0.911	0.213	1.610	5.14	0.599	28.22	24.5	6.20	NA
7	23	1008	226.1	5	C	7.47	12.0	1.4	0.716	0.187	1.630	4.80	0.641	43.26	24.3	4.60	0.1
7	23	1313	229.2	5	C	7.61	12.0	1.6	0.798	0.197	1.640	3.96	0.630	67.44	25.5	5.00	0.1
7	23	1619	232.2	5	C	7.52	11.0	2.8	0.691	0.197	1.640	NA	NA	28.21	25.5	6.30	0.2
7	23	1920	235.3	5	C	7.64	12.0	2.4	0.585	0.171	1.550	3.89	0.676	41.38	24.8	6.50	0.2
7	23	2215	238.3	5	C	7.72	12.0	2.4	0.508	0.156	1.500	3.62	0.608	62.07	25.0	7.80	NA
7	24	110	241.2	5	C	7.59	15.0	1.9	0.609	0.182	1.570	NA	0.723	67.44	24.5	5.50	NA

946510475

UNION AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NIU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	426	244.4	5	C	7.57	12.0	2.4	0.543	0.166	1.520	2.90	0.636	53.95	24.5	5.70	NA
7	24	715	247.3	5	C	7.53	16.0	2.6	0.648	0.197	1.580	NA	0.709	39.50	24.5	5.80	NA
		AVERAGE READING				7.67	12.8	4.1	0.560	0.124	1.466	2.85	0.658	45.30	25.7	4.31	NA

946510476

BASELINE

SECØND

RIVER

7-14/7-24-81

1/2 DEPTH

946510477

SECOND RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	920	9.3	4	C	8.55	1.3	3.0	0.031	0.039	1.880	0.97	0.238	5.84	23.5	9.80	NA
7	14	1220	12.3	4	C	9.08	1.1	3.0	0.010	0.035	1.850	NA	NA	4.28	25.3	11.30	NA
7	14	1518	15.3	4	C	9.22	1.3	2.2	0.052	0.035	1.720	1.80	0.249	3.50	26.5	11.70	NA
7	14	1800	18.0	4	C	8.99	1.4	7.4	0.049	0.044	1.820	NA	NA	3.11	24.5	9.00	NA
7	14	2100	21.0	4	C	8.67	1.4	4.0	0.073	0.077	1.810	2.32	0.241	2.33	22.0	7.25	NA
7	14	2350	23.8	4	C	8.18	1.7	2.4	0.050	0.030	1.890	NA	NA	1.94	21.0	7.80	NA
7	15	210	26.2	4	C	8.09	1.2	1.6	0.072	0.030	1.860	1.61	0.221	2.72	19.8	7.80	NA
7	15	508	29.1	4	C	8.08	1.3	1.6	0.066	0.030	1.850	NA	NA	1.75	19.5	7.40	NA
7	15	810	32.2	4	C	8.60	1.4	1.8	0.061	0.020	1.860	NA	NA	6.74	20.0	9.20	NA
7	15	1105	35.1	4	C	9.10	1.2	1.8	0.051	0.016	1.550	NA	NA	8.09	23.5	11.50	NA
7	15	1415	38.3	4	C	9.32	1.3	1.6	0.015	0.035	1.810	3.01	0.359	6.74	25.5	11.60	NA
7	15	1715	41.3	4	C	9.22	1.3	1.8	0.121	0.043	1.790	NA	NA	3.30	24.6	9.10	NA
7	15	2020	44.3	4	C	8.56	1.2	1.2	0.086	0.039	1.810	1.72	0.271	3.50	23.1	7.20	NA
7	15	2320	47.3	4	C	8.13	1.4	1.8	0.100	0.039	1.920	NA	NA	4.08	22.0	7.30	NA
7	16	215	50.3	4	C	8.10	1.3	1.0	0.053	0.025	1.850	1.50	0.231	1.75	20.7	7.70	NA
7	16	513	53.2	4	C	8.05	1.3	2.2	0.026	0.020	1.870	NA	NA	2.52	20.0	7.50	NA
7	16	815	56.3	4	C	8.28	0.9	1.4	0.041	0.020	1.900	0.88	0.207	9.44	20.3	9.30	NA
7	16	1115	59.2	4	C	8.94	1.0	1.6	0.022	0.020	1.870	NA	NA	12.81	23.5	11.50	NA
7	16	1415	62.1	4	C	9.05	1.2	1.6	0.022	0.029	1.850	1.13	0.188	8.77	26.0	13.80	NA
7	16	1715	65.1	4	C	9.03	1.1	7.2	0.044	0.039	1.970	NA	NA	5.40	24.0	9.70	NA
7	16	2015	68.1	4	C	8.48	1.1	1.2	0.078	0.034	1.790	1.75	0.284	8.77	23.4	7.00	NA
7	16	2315	71.1	4	C	8.16	1.1	1.2	0.069	0.039	1.890	NA	NA	4.05	22.2	6.60	NA
7	17	22	74.3	4	C	8.11	1.1	1.0	0.103	0.039	1.860	2.41	0.323	4.72	21.8	7.30	NA
7	17	324	77.4	4	C	8.11	1.8	0.8	0.260	0.029	1.870	NA	NA	3.37	21.0	7.60	NA
7	17	815	82.3	4	C	8.47	1.6	1.2	0.022	0.024	1.810	1.08	0.210	8.77	21.0	8.70	NA
7	17	1115	85.3	4	C	9.19	1.8	0.4	0.019	0.024	1.760	NA	NA	8.09	24.5	13.50	NA

94651047B

SECOND RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1420	86.3	4	C	9.40	1.5	0.6	0.012	0.038	1.860	0.91	NA	11.46	25.3	11.40	NA
7	17	1725	89.4	4	C	9.10	1.7	0.4	0.062	0.029	1.720	NA	NA	8.77	24.5	8.20	NA
7	17	2025	92.4	4	C	8.30	1.9	0.8	0.080	0.034	1.820	1.09	NA	6.74	24.0	6.90	NA
7	17	2325	95.4	4	C	8.10	1.4	0.8	0.075	0.038	1.860	NA	NA	2.72	23.0	7.00	NA
7	18	226	98.3	4	C	8.10	1.3	0.4	0.058	0.034	1.890	2.35	0.228	2.33	22.2	7.20	NA
7	18	526	101.4	4	C	8.10	1.4	0.4	0.010	0.034	1.920	NA	NA	3.50	21.7	7.50	NA
7	18	820	104.3	4	C	8.50	1.5	1.8	0.102	0.030	1.860	1.50	0.226	11.46	22.3	9.80	NA
7	18	1120	107.3	4	C	9.20	1.4	1.2	0.010	0.024	1.710	NA	NA	12.14	25.5	13.30	NA
7	18	1430	110.5	4	C	9.30	1.6	1.4	0.102	0.066	1.790	3.24	0.413	8.09	25.5	11.00	NA
7	18	1730	113.5	4	C	9.20	1.7	2.0	0.156	0.084	1.880	NA	NA	5.40	25.0	9.00	NA
7	18	2030	116.5	4	C	8.40	1.6	2.2	0.111	0.038	1.810	2.03	0.566	2.53	24.5	7.00	NA
7	18	2330	119.5	4	C	8.10	1.4	2.4	0.010	0.047	1.790	NA	NA	2.70	23.0	7.00	NA
7	19	226	122.4	4	C	8.20	1.2	2.0	0.086	0.038	1.700	2.46	0.302	3.37	22.0	6.80	NA
7	19	519	125.3	4	C	8.10	1.4	1.8	0.010	0.038	1.740	NA	NA	1.75	21.5	7.00	NA
7	19	815	128.3	4	C	8.33	0.8	1.6	0.031	0.020	1.320	0.88	0.258	5.84	22.3	9.30	NA
7	19	1130	131.5	4	C	9.36	0.9	1.4	0.010	0.020	1.630	NA	NA	8.75	26.3	12.10	NA
7	19	1430	134.5	4	C	9.32	0.8	2.4	0.051	0.454	1.620	1.97	0.389	8.75	25.8	8.80	NA
7	19	1730	137.5	4	C	9.90	0.9	2.4	0.010	0.047	1.760	NA	NA	3.89	25.2	8.00	NA
7	19	2030	140.5	4	C	7.77	4.6	8.8	NA	0.075	1.745	14.00	0.540	31.12	24.6	6.30	NA
7	19	2330	143.5	4	C	7.54	3.8	9.8	0.303	0.247	2.000	NA	NA	10.69	23.1	5.80	NA
7	2	230	146.5	4	C	7.56	2.9	10.6	0.116	0.275	1.430	1.75	0.356	6.81	22.1	5.00	NA
7	2	523	149.4	4	C	7.59	3.2	10.4	0.010	0.318	1.420	NA	NA	5.84	21.8	5.60	NA
7	2	820	152.3	4	C	7.64	2.5	12.4	0.074	0.196	1.130	1.62	0.290	30.10	22.8	6.40	NA
7	2	1130	155.5	4	C	7.09	15.0	10.0	0.839	0.117	1.600	NA	NA	10.12	23.5	5.70	NA
7	2	1425	158.4	4	C	7.14	12.5	12.6	0.500	0.066	1.220	NA	NA	10.12	23.3	7.30	NA
7	2	1730	161.5	4	C	7.17	9.5	8.8	0.479	0.052	1.430	1.90	0.253	10.79	25.0	7.80	NA

9465104 79

SECOND RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	21	2030	164.5	4	C	7.45	6.5	7.4	0.223	0.047	1.640	NA	NA	4.08	23.5	6.60	NA
7	21	2330	167.5	4	C	7.32	10.2	11.2	0.301	0.029	0.928	2.47	0.306	12.81	24.0	6.80	NA
7	21	215	170.3	4	C	7.17	11.5	9.0	0.252	0.019	0.504	NA	NA	18.81	23.0	8.00	NA
7	21	518	173.3	4	C	7.41	6.8	3.4	0.128	0.015	0.756	2.38	0.279	9.11	22.8	7.90	NA
7	21	815	176.3	4	C	7.70	4.2	4.4	0.345	0.013	0.950	16.00	0.342	7.42	22.8	8.70	NA
7	21	1135	179.6	4	C	7.80	4.4	4.0	0.044	0.013	1.210	NA	NA	6.07	24.5	8.80	NA
7	21	1430	182.5	4	C	8.80	3.4	2.2	0.425	0.018	1.360	1.90	0.233	NA	26.0	9.30	NA
7	21	1725	185.4	4	C	8.60	2.5	2.8	0.100	0.018	1.460	NA	NA	3.50	26.0	9.40	NA
7	21	2020	188.3	4	C	7.90	8.7	7.0	0.612	0.036	1.120	2.93	0.310	2.72	25.0	7.30	NA
7	21	2320	191.3	4	C	7.50	5.7	12.4	0.097	0.036	0.892	NA	NA	3.11	24.5	6.20	NA
7	22	215	194.3	4	C	7.60	5.6	4.6	0.467	0.027	1.050	1.78	0.268	NA	23.0	7.60	NA
7	22	525	197.4	4	C	7.70	3.2	2.6	0.090	0.027	1.230	NA	NA	2.14	22.0	7.00	NA
7	22	815	200.3	4	C	8.10	2.7	4.0	0.325	0.018	1.340	2.17	0.200	5.40	22.0	8.20	NA
7	22	1125	203.4	4	C	8.70	1.8	3.8	0.075	0.013	1.450	NA	NA	6.07	25.5	10.70	NA
7	22	1418	206.3	4	C	8.80	1.7	5.4	0.540	0.031	1.510	1.39	0.207	4.05	27.0	10.60	NA
7	22	1730	209.5	4	C	8.80	2.1	5.4	0.406	0.020	1.600	13.30	0.322	9.44	24.9	8.60	NA
7	22	2020	212.3	4	C	8.20	1.6	4.6	0.419	0.020	1.620	1.09	0.224	3.37	23.8	7.00	NA
7	22	2320	215.3	4	C	8.10	1.8	6.4	0.449	0.020	1.670	2.99	0.216	2.02	21.5	6.95	NA
7	23	215	218.3	4	C	8.10	1.3	3.0	0.378	0.020	1.750	1.08	0.210	6.07	20.5	7.50	NA
7	23	520	221.4	4	C	8.10	1.8	4.6	0.347	0.020	1.880	3.47	0.188	4.72	19.5	7.50	NA
7	23	810	224.2	4	C	8.20	4.0	2.6	0.305	0.020	1.840	0.46	0.182	6.07	19.3	8.90	NA
7	23	1115	227.3	4	C	8.83	2.0	2.6	0.262	0.020	1.910	2.01	0.171	8.09	23.8	11.50	NA
7	23	1420	230.3	4	C	9.89	2.1	2.2	0.276	0.020	1.830	14.00	0.181	4.47	25.3	11.60	NA
7	23	1720	233.3	4	C	8.77	1.9	1.8	0.471	0.020	1.920	12.50	0.183	5.39	24.5	8.80	NA
7	23	2030	236.5	4	C	8.15	2.0	1.2	1.110	0.030	1.900	14.10	0.446	2.53	22.8	7.30	NA
7	23	2320	239.3	4	C	8.06	1.5	0.6	0.498	0.030	1.940	2.33	0.219	1.75	21.5	7.20	NA

94651048O

SECOND RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	230	242.5	4	C	6.07	1.3	0.6	0.378	0.030	1.950	2.58	0.187	2.72	20.3	7.40	NA
7	24	530	245.5	4	C	6.06	1.3	0.4	0.305	0.025	1.970	1.62	0.160	5.39	19.8	7.70	NA
		AVERAGE READING				6.34	2.7	3.6	0.184	0.050	1.657	3.44	0.270	6.53	23.2	8.45	NA

946510481

BASELINE

SADDLE RIVER

7-14/7-24-81

1/2 DEPTH

946510482

SADDLE RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
7	14	950	9.8	7	C	7.63	2.4	5.6	3.030	0.900	3.380	3.92	1.310	10.12	25.0	6.50	N_A
7	14	1248	12.8	7	C	7.83	2.3	4.4	3.060	1.000	3.490	NA	NA	10.12	26.0	7.60	NA
7	14	1600	16.0	7	C	7.74	3.2	7.0	2.610	1.040	3.430	3.51	1.160	12.14	27.2	8.40	NA
7	14	1900	19.0	7	C	7.97	2.2	4.6	2.440	0.840	3.020	NA	NA	8.77	26.2	6.20	NA
7	14	2150	21.8	7	C	8.10	2.6	7.4	1.840	0.940	3.690	2.97	1.230	10.12	25.2	5.90	NA
7	15	100	25.0	7	C	7.79	3.5	11.4	1.380	0.840	4.150	NA	NA	22.93	23.5	4.40	NA
7	15	355	27.9	7	C	7.76	2.4	6.4	1.090	0.940	4.500	1.54	1.100	9.44	22.0	3.20	NA
7	15	655	30.9	7	C	7.69	2.8	5.4	1.450	0.940	4.080	NA	NA	19.56	21.0	2.60	NA
7	15	945	33.8	7	C	7.58	2.5	5.4	1.850	0.960	3.610	4.46	1.410	12.81	21.0	4.30	NA
7	15	1310	37.2	7	C	7.73	2.6	5.6	2.240	1.060	3.770	NA	NA	17.53	27.5	6.80	NA
7	15	1605	40.1	7	C	7.83	2.4	5.0	2.750	0.960	3.590	9.83	3.150	22.25	25.2	8.30	NA
7	15	1950	42.7	7	C	7.85	2.6	4.8	2.440	1.060	3.650	NA	NA	16.18	25.2	6.90	NA
7	15	2145	45.8	7	C	7.88	2.3	8.8	1.860	1.010	3.430	6.02	1.480	10.12	25.2	6.80	NA
7	16	50	48.8	7	C	7.79	2.8	8.4	1.420	1.010	3.960	NA	NA	NA	24.0	4.80	NA
7	16	350	51.8	7	C	7.70	2.6	6.0	1.200	0.960	3.740	3.25	1.470	16.86	23.2	3.00	NA
7	16	650	54.8	7	C	7.68	2.7	5.0	1.420	0.960	3.730	NA	NA	18.21	21.8	2.20	NA
7	16	940	57.7	7	C	7.75	2.6	4.6	1.590	0.960	3.550	3.76	1.640	16.93	23.0	4.20	NA
7	16	1240	60.7	7	C	7.99	2.7	5.0	1.820	1.060	3.550	NA	NA	15.05	24.0	7.00	NA
7	16	1605	64.1	7	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	25.8	8.50	NA
7	16	1840	66.7	7	C	7.97	2.2	5.0	2.230	1.060	3.630	5.19	1.550	8.77	25.8	7.00	NA
7	16	2140	69.7	7	C	8.09	3.1	10.0	1.770	1.060	3.760	NA	NA	NA	26.0	8.10	NA
7	17	40	72.7	7	C	7.94	2.7	8.2	1.460	0.960	3.820	6.20	1.510	24.45	25.0	5.00	NA
7	17	340	75.7	7	C	7.82	2.5	6.4	1.210	1.010	4.180	NA	NA	16.93	24.3	3.20	NA
7	17	640	78.7	7	C	7.75	3.9	8.4	1.350	1.010	3.870	3.10	1.750	NA	23.5	2.00	NA
7	17	955	81.9	7	C	7.80	2.7	4.6	1.320	0.970	3.860	6.22	1.910	2.92	23.5	4.80	NA
7	17	1245	84.7	7	C	8.00	3.0	4.4	1.530	1.020	4.030	NA	NA	24.45	26.0	8.40	NA

94651048 3

SADDLE RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1555	87.9	7	C	7.90	3.3	3.6	1.730	1.060	4.060	5.35	2.250	24.45	26.5	7.10	NA
7	17	1840	90.7	7	C	8.00	2.4	3.4	1.610	0.970	3.960	NA	NA	22.57	26.0	7.00	NA
7	17	2140	93.7	7	C	8.10	3.0	5.6	1.520	0.970	4.040	4.58	1.340	17.53	26.0	6.70	NA
7	18	40	96.7	7	C	8.10	3.2	5.2	1.320	0.920	3.820	NA	NA	13.49	25.0	5.00	NA
7	18	340	99.7	7	C	7.90	3.9	4.6	1.140	0.840	3.530	2.53	1.600	14.16	24.0	3.20	NA
7	18	640	102.7	7	C	7.80	2.8	3.6	1.390	0.850	3.540	NA	NA	22.57	23.0	1.90	NA
7	18	931	105.5	7	C	7.90	2.8	5.6	1.450	0.940	3.600	3.32	1.850	10.12	23.5	4.00	NA
7	18	1235	108.6	7	C	8.00	2.6	4.8	1.550	1.030	4.000	NA	NA	13.49	26.0	7.80	NA
7	18	1610	112.2	7	C	8.00	3.0	4.6	2.050	1.130	4.340	5.72	1.920	8.09	27.2	8.50	NA
7	18	1840	114.7	7	C	8.10	3.0	6.6	1.960	1.080	4.500	NA	NA	10.79	27.0	7.40	NA
7	18	2140	117.7	7	C	8.30	4.7	8.6	1.360	0.980	4.200	4.37	1.780	21.58	26.5	8.90	NA
7	19	55	120.9	7	C	8.00	4.3	7.8	0.802	0.890	4.580	NA	NA	16.86	26.5	5.60	NA
7	19	345	123.8	7	C	7.90	3.3	5.8	0.747	0.850	4.900	4.57	2.100	23.60	25.0	3.40	NA
7	19	645	126.8	7	C	7.80	2.8	4.8	2.490	0.940	5.220	NA	NA	14.16	24.0	2.00	NA
7	19	935	129.6	7	C	7.64	1.8	4.4	1.660	0.990	5.130	3.59	2.230	14.16	24.0	3.50	NA
7	19	1240	132.8	7	C	7.84	2.0	3.8	2.450	1.030	5.170	NA	NA	22.57	26.2	7.00	NA
7	19	1555	135.9	7	C	7.89	1.9	5.0	2.380	0.940	4.560	4.80	2.140	26.33	27.5	8.30	NA
7	19	1840	138.7	7	C	8.12	2.1	6.4	1.090	0.940	4.380	NA	NA	15.05	28.0	9.10	NA
7	19	2140	141.7	7	C	7.97	1.7	7.8	1.760	0.940	4.750	4.33	2.040	24.45	28.0	7.10	NA
7	2	135	145.1	7	C	7.68	2.1	3.2	0.928	0.940	5.600	NA	NA	16.93	26.0	4.60	NA
7	2	345	147.8	7	C	7.66	2.3	2.4	0.934	0.890	5.810	5.40	2.180	13.17	26.0	2.80	NA
7	2	645	150.8	7	C	7.65	2.1	3.6	1.370	0.940	5.490	NA	NA	13.15	25.0	1.80	NA
7	20	932	153.5	7	C	7.70	2.3	4.6	1.090	0.830	4.260	4.93	2.030	4.72	24.3	2.40	NA
7	2	1233	156.3	7	C	7.62	4.3	10.2	3.180	0.650	3.910	NA	NA	26.33	NA	3.20	NA
7	2	1605	160.1	7	C	7.46	6.0	11.2	3.604	0.280	2.450	2.07	0.972	5.39	23.8	5.60	NA
7	2	1840	162.7	7	C	7.41	6.4	11.2	3.970	0.330	2.430	NA	NA	12.14	24.1	4.70	NA

946510484

SADDLE RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	2[illegible]	2140	165.7	7	C	7.28	8.4	12.4	NA	NA	NA	NA	NA	12.14	24.0	4.40	NA
7	21	55	168.9	7	C	7.29	26.0	5.4	0.770	0.050	1.010	NA	NA	10.79	23.5	5.90	NA
7	21	345	171.8	7	C	7.26	35.0	6.2	0.035	0.020	0.841	1.91	0.584	8.09	23.0	5.50	NA
7	21	645	174.8	7	C	7.25	42.0	4.8	0.402	0.020	0.928	NA	NA	16.53	22.5	5.30	NA
7	21	938	177.6	7	C	7.32	23.5	6.2	0.361	0.055	0.908	2.88	0.476	10.12	24.0	6.00	NA
7	21	1230	180.5	7	C	7.34	14.5	6.0	0.456	0.069	1.000	NA	NA	4.86	24.7	6.20	NA
7	21	1555	183.9	7	C	7.51	13.5	6.6	0.649	0.091	1.070	2.63	0.583	6.22	26.8	6.80	NA
7	21	1840	186.7	7	C	7.50	11.0	7.0	0.800	0.101	1.180	NA	NA	16.86	26.2	5.60	NA
7	21	2140	189.7	7	C	7.55	10.5	8.6	1.150	0.155	1.320	3.25	0.736	8.09	25.0	5.50	NA
7	22	55	192.9	7	C	7.49	9.3	8.4	1.030	0.128	1.250	NA	NA	5.25	25.0	5.00	NA
7	22	340	195.7	7	C	7.55	9.0	8.4	1.040	0.137	1.240	4.35	0.703	7.42	23.0	4.20	NA
7	22	640	198.7	7	C	7.57	10.0	7.8	1.120	0.148	1.490	NA	NA	6.22	23.0	4.80	NA
7	22	933	201.6	7	C	7.60	9.3	8.4	1.130	0.157	1.500	NA	NA	13.17	23.8	5.00	NA
7	22	1225	204.4	7	C	7.70	8.6	7.6	0.958	0.161	1.540	3.47	0.743	13.17	25.0	5.30	NA
7	22	1605	208.1	7	C	7.80	7.0	7.4	0.664	0.165	1.640	NA	NA	13.17	27.2	6.30	NA
7	22	1840	210.7	7	C	7.80	6.3	8.8	1.020	0.191	1.660	3.22	0.763	15.05	27.0	5.80	NA
7	22	2140	213.7	7	C	7.70	6.7	8.6	1.390	0.200	1.630	3.68	0.778	16.93	26.0	4.80	NA
7	23	110	217.2	7	C	7.80	7.8	9.8	1.310	0.222	1.830	3.69	0.810	20.69	24.0	4.30	NA
7	23	345	219.8	7	C	7.80	7.4	7.2	1.910	0.262	1.900	NA	NA	8.77	22.5	4.00	NA
7	23	645	222.8	7	C	7.80	7.5	7.8	1.230	0.288	2.020	4.35	1.050	18.81	21.3	4.00	NA
7	23	935	225.6	7	C	7.55	4.0	3.2	2.000	0.288	2.100	NA	NA	NA	21.0	5.00	NA
7	23	1235	228.5	7	C	7.62	4.0	3.2	1.860	0.288	2.070	4.26	1.000	8.77	23.4	5.80	NA
7	23	1555	231.8	7	C	7.66	3.0	3.8	1.560	0.315	2.060	5.81	0.993	8.77	26.2	7.10	NA
7	23	1845	234.7	7	C	7.69	2.5	2.4	1.190	0.341	2.140	4.36	0.928	4.28	26.8	5.90	NA
7	23	2140	237.7	7	C	7.64	3.8	2.4	1.270	0.354	3.830	NA	NA	18.88	25.5	5.20	NA
7	24	55	240.9	7	C	7.64	4.9	3.2	2.010	0.345	3.800	3.33	1.040	10.79	24.2	4.00	NA

946510485

SADDLE RIVER - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	340	243.7	7	C	7.62	5.3	2.8	1.820	0.350	3.250	NA	NA	10.79	23.0	3.90	NA
7	24	640	246.7	7	C	7.65	5.0	2.4	1.490	0.306	2.190	3.61	0.944	10.79	21.5	3.80	NA
		AVERAGE READING				7.75	5.7	6.1	1.494	0.678	3.245	4.15	1.396	14.13	24.7	5.38	NA

946510486

BASELINE

MARKET

STREET

7-14/7-24-81

1/2 DEPTH

946510487

MARKET STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	1005	10.1	9	C	8.37	7.2	6.0	0.070	0.085	1.540	2.26	0.680	67.72	27.4	9.40	NA
7	14	1300	13.0	9	C	8.81	8.0	6.8	0.028	0.075	1.590	NA	NA	63.95	27.0	12.60	NA
7	14	1620	16.3	9	C	8.96	8.1	7.0	0.101	0.075	1.640	2.97	0.685	NA	27.8	13.60	NA
7	14	1920	19.3	9	C	8.94	6.9	5.8	0.042	0.075	1.660	NA	NA	48.91	27.2	11.40	NA
7	14	2205	22.1	9	C	8.84	7.5	6.6	0.044	0.070	1.650	2.51	0.732	69.60	26.5	10.80	NA
7	15	115	25.3	9	C	8.65	7.0	6.2	0.050	0.070	1.690	NA	NA	58.31	26.0	9.90	NA
7	15	415	28.3	9	C	8.56	7.0	6.0	0.030	0.070	1.690	1.21	0.630	26.33	25.5	8.80	NA
7	15	715	31.3	9	C	8.33	7.4	5.6	0.043	0.075	1.700	NA	NA	47.03	25.0	8.20	NA
7	15	1000	34.0	9	C	8.34	9.5	6.6	0.054	0.077	1.613	1.51	0.745	75.24	25.0	8.80	NA
7	15	1325	37.4	9	C	9.03	7.6	7.2	0.024	0.084	1.608	NA	NA	73.36	25.5	12.40	NA
7	15	1620	40.3	9	C	9.16	14.0	7.8	0.094	0.082	1.558	NA	NA	71.48	26.5	12.60	NA
7	15	1910	43.2	9	C	9.30	13.0	7.0	0.050	0.087	1.533	2.20	0.684	80.88	26.5	13.80	NA
7	15	2205	46.1	9	C	9.09	14.0	7.2	0.097	0.087	1.573	NA	NA	82.76	26.0	12.80	NA
7	16	105	49.1	9	C	8.93	13.0	6.8	0.035	0.096	1.604	2.07	0.732	63.95	25.5	13.20	NA
7	16	405	52.1	9	C	8.86	13.0	6.6	0.033	0.087	1.563	NA	NA	75.24	25.0	11.60	NA
7	16	705	55.1	9	C	8.59	15.0	6.4	0.063	0.096	1.594	1.69	0.782	71.48	24.0	9.70	NA
7	16	959	57.9	9	C	8.85	8.7	6.2	0.040	0.096	1.514	NA	NA	NA	25.1	10.00	NA
7	16	1252	60.9	9	C	9.32	8.8	5.0	0.017	0.110	1.530	2.33	0.743	41.38	25.2	16.80	NA
7	16	1620	64.3	9	C	9.50	9.8	7.2	0.030	0.106	1.474	NA	NA	75.24	26.0	19.80	NA
7	16	1850	66.7	9	C	9.66	11.0	8.6	0.028	0.101	1.439	2.32	0.678	55.49	26.2	18.40	NA
7	16	2150	69.8	9	C	9.59	9.9	5.4	0.028	0.101	1.459	NA	NA	37.62	26.5	17.60	NA
7	17	55	72.3	9	C	9.56	9.3	5.6	0.034	0.096	1.514	1.44	0.571	35.74	26.5	18.80	NA
7	17	355	75.1	9	C	9.28	9.7	5.8	0.021	0.101	1.608	NA	NA	80.88	26.0	16.20	NA
7	17	655	78.0	9	C	9.03	11.0	5.2	0.030	0.106	1.654	1.83	0.659	NA	25.0	13.30	NA
7	17	1002	82.1	9	C	9.00	14.0	4.4	0.052	0.106	1.773	3.87	0.744	97.79	25.0	12.00	NA
7	17	1255	84.4	9	C	9.39	12.0	5.4	0.115	0.115	1.790	NA	NA	169.93	26.5	19.90	NA

946510488

MARKET STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [S.TU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1610	88.2	9	C	9.50	15.0	4.8	0.022	0.102	1.780	3.37	0.615	111.28	27.0	17.80	NA
7	17	1850	90.8	9	C	9.50	12.0	10.8	0.010	0.097	1.790	NA	NA	25.29	26.8	17.40	NA
7	17	2150	93.8	9	C	9.40	16.0	4.6	0.070	0.102	1.660	3.53	0.661	94.42	26.2	16.80	NA
7	18	55	96.9	9	C	9.30	17.0	4.6	0.027	0.099	1.650	NA	NA	101.16	26.5	17.60	NA
7	18	355	99.9	9	C	9.20	14.0	4.2	0.051	0.111	1.780	3.15	0.558	118.02	26.0	16.60	NA
7	18	655	102.9	9	C	9.00	18.0	4.8	0.036	0.103	1.640	NA	NA	121.39	25.0	9.40	NA
7	18	945	105.8	9	C	9.00	14.0	4.8	0.037	0.098	1.460	2.81	0.652	60.19	25.5	13.40	NA
7	18	1250	108.8	9	C	9.40	13.0	5.4	0.031	0.098	1.370	NA	NA	97.81	26.0	20.00	NA
7	18	1625	112.4	9	C	9.50	17.0	5.2	0.058	0.103	1.280	3.78	0.720	58.31	27.0	18.60	NA
7	18	1850	114.8	9	C	9.50	15.0	8.2	0.022	0.094	1.460	NA	NA	80.88	26.2	15.20	NA
7	18	2150	117.8	9	C	9.50	18.0	7.0	0.061	0.094	1.450	3.48	0.697	86.53	26.5	14.60	NA
7	19	115	121.3	9	C	9.40	19.0	6.6	0.023	0.094	1.330	NA	NA	77.12	27.0	17.90	NA
7	19	400	124.0	9	C	9.30	14.0	5.6	0.020	0.089	1.670	2.76	0.622	75.24	27.0	16.40	NA
7	19	700	127.0	9	C	9.30	14.0	5.4	0.066	0.094	1.390	NA	NA	107.90	27.0	15.40	NA
7	19	950	129.5	9	C	9.31	9.4	7.4	0.074	0.094	1.496	3.50	0.657	77.56	27.0	15.00	NA
7	19	1300	133.0	9	C	10.05	11.0	9.2	0.026	0.099	1.301	NA	NA	141.10	27.0	17.20	NA
7	19	1610	136.2	9	C	9.93	13.0	10.6	0.066	0.118	1.352	5.04	0.690	122.30	27.5	17.80	NA
7	19	1850	138.8	9	C	9.71	15.1	9.0	0.265	0.113	1.360	NA	NA	112.90	27.0	14.50	NA
7	19	2150	141.8	9	C	9.44	10.3	8.0	0.046	0.537	1.440	3.89	0.838	91.04	27.0	14.10	NA
7	2	120	145.3	9	C	9.45	11.5	7.2	0.018	0.112	1.420	NA	NA	87.67	27.0	19.80	NA
7	2	420	148.	9	C	9.30	11.5	7.4	0.049	0.113	1.530	3.29	0.732	67.44	27.0	18.80	NA
7	2	700	151.0	9	C	9.35	12.0	6.0	0.032	0.113	1.650	NA	NA	94.42	27.0	16.00	NA
7	20	944	153.7	9	C	9.18	13.5	5.8	0.076	0.115	1.890	3.28	0.645	197.51	27.8	14.80	NA
7	20	1245	156.	9	C	8.14	14.5	14.2	0.615	0.143	1.780	NA	NA	150.48	26.0	9.40	NA
7	20	1625	159.3	9	C	8.74	14.0	10.8	0.364	0.129	2.030	12.10	0.662	74.18	26.2	10.30	NA
7	20	1850	162.0	9	C	8.28	19.5	7.6	0.221	0.125	2.090	NA	NA	91.04	26.4	9.60	NA

94510489

MARKET STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	2[illegible]	2150	165.8	9	C	7.51	9.5	7.0	0.623	0.148	2.260	2.64	0.756	30.35	25.8	4.80	NA
7	21	110	169.2	9	C	7.25	30.0	8.6	0.866	0.115	1.260	NA	NA	23.34	24.5	5.00	NA
7	21	400	172.0	9	C	7.33	27.5	7.6	0.252	0.115	1.250	3.32	0.639	17.51	24.7	4.80	NA
7	21	700	175.0	9	C	7.55	15.0	8.8	1.170	0.217	1.650	NA	NA	22.37	24.5	5.80	NA
7	21	950	177.8	9	C	7.69	10.0	9.2	1.410	0.248	1.440	3.04	0.661	22.26	25.5	6.80	NA
7	21	1245	180.8	9	C	7.61	8.8	8.8	1.070	0.173	1.310	NA	NA	26.30	26.0	6.60	NA
7	21	1610	184.2	9	C	7.58	14.5	7.8	0.636	0.128	1.130	3.51	0.516	12.14	26.5	7.00	NA
7	21	1850	186.8	9	C	7.47	19.5	6.8	0.742	0.139	1.200	NA	NA	14.16	26.2	6.70	NA
7	21	2150	189.8	9	C	7.49	10.5	7.4	0.923	0.191	1.350	3.22	0.560	8.77	26.0	6.30	NA
7	22	110	193.2	9	C	7.47	9.5	6.8	0.770	0.209	1.400	NA	NA	11.46	26.0	4.90	NA
7	22	355	195.9	9	C	7.52	9.0	7.2	1.080	0.228	1.470	3.01	0.568	8.09	24.5	4.50	NA
7	22	655	198.9	9	C	7.49	10.0	7.2	1.170	0.237	1.470	NA	NA	15.85	25.0	4.70	NA
7	22	944	201.7	9	C	7.60	17.0	7.8	0.943	0.228	1.470	2.57	0.546	15.05	25.0	5.80	NA
7	22	1240	204.7	9	C	7.70	13.0	8.0	0.816	0.223	1.470	3.13	0.597	22.57	25.0	6.30	NA
7	22	1620	208.3	9	C	7.80	12.0	7.8	0.649	0.200	1.470	2.49	0.513	28.22	26.0	7.40	NA
7	22	1850	210.8	9	C	7.70	14.0	8.0	0.527	0.183	1.400	NA	NA	33.86	26.2	7.50	NA
7	22	2150	213.8	9	C	7.80	15.0	7.0	0.467	0.143	1.430	2.40	0.564	35.74	26.0	7.00	NA
7	23	125	217.4	9	C	7.50	14.0	6.2	0.385	0.155	1.200	NA	NA	24.45	25.0	6.80	NA
7	23	400	220.[illegible]	9	C	7.73	16.0	7.0	0.434	0.164	1.150	2.31	0.487	31.98	25.0	5.10	NA
7	23	700	223.[illegible]	9	C	7.6[illegible]	13.0	6.6	0.487	0.155	1.160	NA	NA	31.04	24.5	5.00	NA
7	23	950	225.[illegible]	9	C	7.47	9.2	3.4	0.456	0.165	1.290	2.60	0.483	28.21	24.5	5.40	NA
7	23	1245	228.[illegible]	9	C	7.52	7.6	3.4	0.400	0.157	1.300	NA	NA	17.53	25.0	6.20	NA
7	23	161[illegible]	232.2	9	C	7.71	6.7	5.0	0.332	0.157	1.360	1.73	0.443	43.26	24.8	7.70	NA
7	23	18[illegible]	234.	9	C	7.70	7.3	4.6	0.367	0.160	1.270	3.17	0.471	24.45	25.1	7.40	NA
7	23	2150	237.8	9	C	7.66	7.4	3.8	0.280	0.157	1.390	2.76	0.506	26.33	25.0	6.80	NA
7	24	116	241.2	9	C	7.60	9.2	4.2	0.319	0.157	1.440	6.07	0.460	37.62	25.5	8.20	NA

9465104[illegible]90

MARKET STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	355	243.9	9	C	7.61	7.8	4.0	0.309	0.157	1.490	2.23	0.473	24.45	25.5	7.80	NA
7	24	655	246.9	9	C	7.55	9.0	3.6	NA	0.165	1.460	3.82	0.486	21.33	25.0	6.70	NA
		AVERAGE READING				8.60	12.2	6.7	0.267	0.130	1.519	3.10	0.626	61.72	25.9	11.52	NA

946510491

BASELINE

LINCØLN

AVENUE

7-14/7-24-81

1/2 DEPTH

946510492

LINCOLN AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	855	8.9	10	C	7.54	4.9	5.2	0.110	0.168	2.150	1.77	0.864	35.74	26.0	4.60	NA
7	14	1153	11.9	10	C	7.80	6.2	6.4	0.110	0.168	2.170	NA	NA	50.79	26.5	8.20	NA
7	14	1515	15.3	10	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.0	14.20	NA
7	14	1815	18.3	10	C	8.85	8.4	6.6	0.074	0.152	2.260	2.44	0.720	63.95	28.0	14.00	NA
7	14	2110	21.2	10	C	8.60	7.9	6.4	0.096	0.168	2.350	NA	NA	54.55	27.5	9.50	NA
7	15	15	24.3	10	C	7.88	6.9	5.8	0.128	0.168	2.210	2.12	0.865	39.50	26.0	6.60	NA
7	15	315	27.3	10	C	7.62	7.8	5.0	0.175	0.188	2.320	NA	NA	54.55	24.5	4.00	NA
7	15	605	30.1	10	C	7.51	6.5	5.2	0.194	0.188	2.360	1.36	0.768	24.45	24.0	3.10	NA
7	15	853	32.9	10	C	7.48	6.8	5.2	0.248	0.196	2.176	1.43	0.657	50.79	23.9	4.20	NA
7	15	1150	35.8	10	C	7.81	7.8	6.0	0.148	0.196	2.088	NA	NA	54.54	25.5	6.00	NA
7	15	1450	38.8	10	C	8.58	8.0	8.2	0.056	0.196	2.284	NA	NA	NA	26.5	10.50	NA
7	15	1805	42.1	10	C	8.83	9.0	7.2	0.086	0.196	2.312	1.87	0.730	71.48	28.0	12.20	NA
7	15	2100	45.3	10	C	8.42	9.3	6.8	0.143	0.216	2.436	NA	NA	82.76	27.5	10.50	NA
7	16	15	48.3	10	C	7.88	8.6	7.2	0.206	0.216	2.420	2.08	0.818	69.19	26.0	7.60	NA
7	16	305	51.1	10	C	7.65	8.3	5.8	0.288	0.236	2.456	NA	NA	48.91	25.0	4.30	NA
7	16	600	54.0	10	C	7.47	6.0	4.6	0.347	NA	NA	2.02	0.756	37.62	23.7	2.80	NA
7	16	855	56.9	10	C	7.61	7.2	4.6	0.249	0.196	2.180	1.42	0.731	17.53	23.7	3.60	NA
7	16	1155	59.9	10	C	7.79	6.3	5.4	0.176	0.216	2.392	NA	NA	41.38	25.0	7.40	NA
7	16	1455	62.9	10	C	8.73	7.1	5.4	0.095	0.216	2.452	1.50	0.672	43.26	26.5	12.00	NA
7	16	1755	65.9	10	C	8.46	8.3	6.0	0.066	0.196	2.504	NA	NA	48.91	27.0	13.40	NA
7	16	2058	68.9	10	C	8.01	7.9	6.6	0.105	0.196	2.464	2.06	0.914	63.95	26.8	11.40	NA
7	17	5	72.1	10	C	8.10	8.1	5.8	0.146	0.196	2.480	NA	NA	47.03	26.0	8.40	NA
7	17	255	74.9	10	C	7.82	7.8	5.8	0.199	0.196	2.484	1.59	0.813	58.31	25.3	5.40	NA
7	17	555	77.9	10	C	7.65	6.7	5.8	0.214	0.206	2.503	NA	NA	35.74	24.5	3.20	NA
7	17	857	80.9	10	C	7.78	8.0	4.4	0.027	0.204	2.580	3.16	0.611	53.95	24.0	4.20	NA
7	17	1157	84.	10	C	7.91	7.6	5.2	0.203	0.184	2.610	NA	NA	64.07	25.0	7.60	NA

94510493

LINCOLN AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1505	87.1	10	C	8.50	8.4	5.2	0.132	0.184	2.630	2.30	0.561	50.58	26.2	13.20	NA
7	17	1755	89.9	10	C	8.70	9.8	4.8	0.030	0.204	2.760	NA	NA	87.67	26.8	13.80	NA
7	17	2055	92.9	10	C	8.50	9.6	3.8	0.220	0.184	2.750	2.75	0.520	77.56	26.2	12.90	NA
7	17	2350	95.8	10	C	8.50	12.0	3.6	0.171	0.188	2.430	NA	NA	64.07	26.3	8.80	NA
7	18	250	98.8	10	C	7.90	12.0	3.4	0.269	0.204	2.880	3.06	0.736	9.73	26.0	5.60	NA
7	18	550	101.8	10	C	7.70	8.0	3.4	0.161	0.228	2.310	NA	NA	27.23	24.5	2.80	NA
7	18	852	104.9	10	C	7.70	6.9	4.6	0.294	0.264	2.310	3.25	0.679	58.31	25.0	3.60	NA
7	18	1155	107.9	10	C	8.00	7.2	4.8	0.141	0.264	2.500	NA	NA	41.38	26.5	9.00	NA
7	18	1448	110.8	10	C	8.60	8.0	5.4	0.094	0.264	2.550	3.95	0.629	62.07	28.5	9.20	NA
7	18	1755	113.9	10	C	8.90	9.3	6.2	0.084	0.264	2.560	NA	NA	67.71	28.5	13.70	NA
7	18	2055	116.9	10	C	8.50	15.0	6.6	0.150	0.228	2.590	3.01	0.538	62.07	28.3	13.00	NA
7	19	15	120.3	10	C	8.20	8.4	5.0	0.154	0.224	2.430	NA	NA	75.24	27.5	9.60	NA
7	19	255	122.9	10	C	8.00	9.2	4.4	0.204	0.224	2.600	3.24	0.593	65.84	27.0	5.60	NA
7	19	555	125.9	10	C	7.80	8.0	4.2	0.273	0.264	2.730	NA	NA	63.95	26.0	3.00	NA
7	19	853	128.8	10	C	7.62	6.4	4.2	0.284	0.284	2.760	11.10	0.984	54.55	25.8	3.50	NA
7	19	1155	131.9	10	C	7.81	8.7	4.4	0.194	0.300	2.620	NA	NA	73.36	26.6	8.20	NA
7	19	1510	135.2	10	C	8.75	10.0	6.6	0.076	0.264	2.690	4.09	0.806	121.40	28.3	15.20	NA
7	19	1755	137.9	10	C	8.76	8.4	5.8	0.044	0.264	2.610	NA	NA	114.70	28.0	13.70	NA
7	19	2055	140.9	10	C	8.55	9.6	4.6	0.120	0.244	2.790	3.23	0.690	50.78	28.0	12.40	NA
7	20	15	144.3	10	C	8.05	6.2	4.8	0.191	0.228	2.810	NA	NA	56.43	27.5	8.80	NA
7	20	255	146.9	10	C	7.83	5.5	4.0	0.152	0.224	3.050	2.36	0.633	71.48	26.8	5.60	NA
7	20	555	149.9	10	C	7.63	6.4	4.0	0.214	0.228	2.810	NA	NA	52.67	26.5	2.40	NA
7	20	853	152.8	10	C	7.54	6.2	3.8	0.223	0.224	2.940	1.61	0.490	67.44	26.2	2.40	NA
7	20	1148	155.8	10	C	7.59	6.6	4.4	0.246	0.240	2.980	NA	NA	118.02	25.8	3.50	NA
7	20	1458	159.0	10	C	7.61	7.3	12.0	1.080	0.240	3.010	1.98	0.607	128.14	25.8	4.80	NA
7	20	1755	161.9	10	C	7.27	11.0	3.4	0.694	0.276	2.580	NA	NA	23.34	25.8	2.40	NA

946510494

LINCOLN AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2055	164.9	10	C	7.14	20.0	11.8	1.070	0.092	1.340	17.70	0.900	12.64	25.0	6.30	NA
7	21	5	168.1	10	C	7.40	31.0	10.6	1.340	0.092	1.360	NA	NA	5.84	24.0	7.30	NA
7	21	250	170.8	10	C	7.62	17.0	10.6	1.080	0.224	1.860	4.67	0.932	22.37	24.7	7.40	NA
7	21	550	173.8	10	C	7.73	14.5	10.8	1.020	0.224	1.860	NA	NA	27.24	25.0	7.60	NA
7	21	855	176.9	10	C	7.48	22.0	7.0	1.110	0.146	1.250	3.61	0.840	16.19	25.5	8.00	NA
7	21	1155	179.9	10	C	7.47	21.5	6.4	0.625	0.119	1.100	NA	NA	20.91	24.5	8.10	NA
7	21	1455	182.9	10	C	7.46	17.0	6.4	0.733	0.155	1.240	4.09	0.636	13.49	26.0	7.20	NA
7	21	1755	185.9	10	C	7.54	10.5	7.4	1.070	0.219	1.420	NA	NA	11.46	26.0	8.60	NA
7	21	2055	188.9	10	C	7.58	10.5	7.4	1.130	0.228	1.420	3.47	0.667	10.12	26.1	7.40	NA
7	22	5	192.1	10	C	7.65	10.0	7.0	1.100	0.246	1.450	NA	NA	12.81	25.2	6.40	NA
7	22	250	194.8	10	C	7.61	13.5	7.4	1.010	0.228	1.400	3.78	0.757	11.46	24.5	6.80	NA
7	22	550	197.8	10	C	7.64	9.5	7.6	0.966	0.237	1.450	NA	NA	9.44	23.5	6.50	NA
7	22	854	200.9	10	C	7.80	17.0	7.2	NA	0.214	1.480	3.99	0.618	18.81	25.3	7.30	NA
7	22	1145	203.8	10	C	7.80	16.0	6.8	0.594	0.192	1.400	NA	NA	20.69	25.5	8.30	NA
7	22	1448	206.9	10	C	7.90	16.0	6.8	0.449	0.173	1.170	2.48	0.551	35.74	26.0	8.00	NA
7	22	1755	209.9	10	C	7.80	17.0	7.8	0.549	0.148	1.240	NA	NA	30.10	26.0	7.80	NA
7	22	2055	212.9	10	C	7.80	16.0	7.6	0.662	0.170	1.250	3.35	0.553	31.98	25.8	7.00	NA
7	23	15	216.2	10	C	7.73	15.0	7.2	0.495	0.165	1.240	NA	NA	24.45	25.0	6.40	NA
7	23	254	218.8	10	C	7.80	16.0	7.4	0.512	0.178	1.220	2.49	0.564	18.81	24.5	6.70	NA
7	23	550	221.8	10	C	7.80	14.0	7.1	0.528	0.174	1.300	NA	NA	18.81	24.0	6.40	NA
7	23	849	224.7	10	C	7.53	7.0	4.4	0.499	0.174	1.340	2.38	0.657	14.16	24.0	7.00	NA
7	23	1150	227.8	10	C	7.66	7.6	4.6	0.473	0.288	1.460	2.84	0.619	12.81	24.9	7.80	NA
7	23	1450	230.8	10	C	7.74	6.4	3.6	0.349	0.187	1.300	2.19	0.517	20.69	25.9	8.80	NA
7	23	1755	233.9	10	C	7.63	5.7	3.4	0.466	0.183	1.390	NA	NA	17.53	25.8	9.10	NA
7	23	2055	236.9	10	C	7.77	6.0	3.2	0.447	0.192	1.420	2.49	0.525	29.69	24.8	7.30	NA
7	24	5	240.1	10	C	7.55	6.3	3.6	0.501	0.192	1.430	NA	NA	26.33	24.0	5.80	NA

946510495

LINCOLN AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	250	242.8	10	C	7.53	6.4	3.2	0.497	0.192	1.430	2.55	0.510	15.51	24.0	5.40	NA
7	24	550	245.8	10	C	7.52	6.2	3.4	0.503	0.192	1.390	2.35	0.524	18.81	24.0	5.30	NA
		AVERAGE READING				7.90	10.0	5.8	0.379	0.206	2.115	3.22	0.685	44.48	25.8	7.59	NA

946510496

BASELINE

MARKET ISLAND

7-14/7-24-81

1/2 DEPTH

946510497

MARKET ISLAND - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	843	8.7	11	C	7.80	5.4	6.0	0.579	0.244	1.990	1.59	0.792	33.86	25.5	7.00	NA
7	14	1142	11.7	11	C	7.95	5.8	6.2	0.570	0.264	2.020	NA	NA	31.98	26.5	8.20	NA
7	14	1455	14.9	11	C	7.99	7.1	7.0	0.516	0.264	2.140	3.07	0.804	33.86	27.0	8.40	NA
7	14	1755	17.9	11	C	7.84	8.2	6.8	0.496	0.264	2.120	NA	NA	45.14	27.0	7.40	NA
7	14	2055	20.9	11	C	7.69	7.5	7.4	0.519	0.264	2.140	1.88	0.700	41.38	26.5	6.50	NA
7	14	2410	24.9	11	C	7.82	7.9	7.8	0.598	0.264	2.130	NA	NA	39.50	26.0	6.60	NA
7	15	300	27.5	11	C	7.77	8.3	6.6	0.578	0.264	2.170	2.24	0.860	48.91	25.5	7.60	NA
7	15	545	29.8	11	C	7.78	8.0	6.4	0.605	0.270	2.190	NA	NA	50.79	25.0	6.40	NA
7	15	840	32.7	11	C	7.78	8.7	7.2	0.632	0.292	2.116	2.41	0.804	47.02	25.0	7.40	NA
7	15	1138	35.6	11	C	7.82	8.0	7.2	0.651	0.308	2.216	NA	NA	33.86	26.0	8.20	NA
7	15	1440	38.7	11	C	8.00	7.4	6.2	0.617	0.308	2.252	2.51	0.884	52.67	26.5	8.30	NA
7	15	1750	41.8	11	C	7.81	7.3	6.0	0.613	0.308	2.284	NA	NA	50.79	26.5	7.20	NA
7	15	2050	44.8	11	C	7.67	7.6	6.2	0.631	0.292	2.252	2.81	1.050	50.79	26.0	6.60	NA
7	15	2356	47.8	11	C	7.67	7.7	5.8	0.643	0.308	2.288	NA	NA	48.91	25.2	6.40	NA
7	16	245	50.7	11	C	7.69	7.9	5.8	0.691	0.292	2.272	2.32	0.818	43.26	24.5	6.70	NA
7	16	535	53.6	11	C	7.72	7.6	6.4	0.662	0.292	2.240	NA	NA	41.38	24.0	6.20	NA
7	16	843	56.7	11	C	7.83	6.6	7.2	0.613	0.272	2.112	1.92	0.855	31.98	24.0	6.90	NA
7	16	1142	59.7	11	C	7.93	7.0	6.8	0.519	0.272	2.252	NA	NA	43.26	25.0	8.40	NA
7	16	1443	62.7	11	C	8.01	7.4	5.8	0.528	0.272	2.340	2.06	0.730	45.14	26.0	7.80	NA
7	16	1740	65.7	11	C	8.00	7.8	8.0	0.479	0.272	2.388	NA	NA	47.03	26.5	7.00	NA
7	16	2046	68.7	11	C	7.85	7.7	5.8	0.546	0.272	2.376	1.97	0.623	45.14	26.0	6.20	NA
7	16	2345	71.6	11	C	7.81	7.1	6.8	0.486	0.292	2.376	NA	NA	30.10	25.2	6.20	NA
7	17	235	74.6	11	C	7.81	7.3	6.8	0.549	0.308	2.368	2.45	0.514	18.81	25.0	6.70	NA
7	17	535	77.6	11	C	7.85	6.8	7.4	0.527	0.309	2.408	NA	NA	33.86	24.5	6.60	NA
7	17	844	80.7	11	C	7.93	10.0	4.4	0.740	0.296	2.470	2.68	0.472	57.32	24.0	7.60	NA
7	17	1142	83.7	11	C	8.00	9.4	3.8	NA	NA	NA	NA	NA	40.45	25.7	8.50	NA

946510498

MARKET ISLAND - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1450	86.8	11	C	8.10	9.7	4.8	0.612	0.296	2.590	3.63	0.664	33.72	25.0	8.50	NA
7	17	1740	89.7	11	C	8.00	9.3	5.0	0.651	0.316	2.670	NA	NA	37.09	26.8	7.00	NA
7	17	2040	92.7	11	C	8.00	9.5	5.4	0.592	0.316	2.670	3.97	0.823	53.95	26.5	6.30	NA
7	17	2345	95.8	11	C	7.90	9.7	5.2	0.589	0.324	2.690	NA	NA	15.56	25.8	6.30	NA
7	18	235	98.6	11	C	7.90	9.0	5.8	0.631	0.336	2.480	3.26	0.731	47.21	25.5	6.30	NA
7	18	540	101.7	11	C	7.90	8.4	4.8	0.780	0.356	2.530	NA	NA	60.70	25.0	6.40	NA
7	18	838	104.6	11	C	7.80	7.5	5.4	0.862	0.128	2.872	3.10	0.641	31.98	25.3	7.40	NA
7	18	1139	107.6	11	C	8.00	7.3	5.4	0.828	0.128	2.872	NA	NA	31.98	27.0	8.40	NA
7	18	1435	110.6	11	C	8.10	7.7	4.8	0.795	0.352	2.840	2.58	0.634	43.26	28.0	8.00	NA
7	18	1740	113.7	11	C	8.00	8.5	6.2	0.502	0.380	2.780	NA	NA	58.31	28.2	7.00	NA
7	18	2040	116.7	11	C	7.90	8.3	6.0	0.612	0.380	2.850	8.64	1.160	33.86	27.8	5.90	NA
7	19	[illegible]	120.[illegible]	11	C	7.80	8.2	6.2	0.633	0.336	2.590	NA	NA	24.45	27.0	5.60	NA
7	19	240	122.7	11	C	7.90	7.8	5.4	0.766	0.376	2.600	3.27	0.734	45.14	26.0	5.80	NA
7	19	540	125.7	11	C	7.90	7.6	5.6	0.743	0.330	2.740	NA	NA	33.86	26.0	5.80	NA
7	19	840	128.7	11	C	7.79	7.5	6.2	0.684	0.356	2.610	4.91	0.644	54.55	26.0	7.00	NA
7	19	1139	131.6	11	C	7.87	5.8	5.6	0.583	0.336	2.640	NA	NA	50.79	27.0	7.80	NA
7	19	1445	134.9	11	C	7.95	6.3	5.6	0.541	0.336	2.760	3.77	0.709	73.36	28.2	7.50	NA
7	19	1740	137.7	11	C	7.88	7.7	5.8	0.504	0.336	2.890	NA	NA	79.00	28.5	6.20	NA
7	19	2040	140.7	11	C	7.81	7.0	5.6	0.491	0.280	2.850	3.61	0.647	94.42	27.8	5.20	NA
7	2[illegible]	[illegible]	144.[illegible]	11	C	7.77	6.9	6.2	0.613	0.336	2.810	NA	NA	62.07	27.0	6.00	NA
7	2[illegible]	235	146.[illegible]	11	C	7.74	6.0	5.6	0.580	0.280	2.690	3.52	0.625	69.59	26.5	6.10	NA
7	2[illegible]	535	149.6	11	C	7.76	6.1	5.2	0.607	0.280	2.790	NA	NA	63.95	26.2	6.10	NA
7	2[illegible]	841	152.7	11	C	7.80	6.8	5.8	0.701	0.331	2.760	3.37	0.586	225.72	26.2	6.80	NA
7	2[illegible]	1140	155.7	11	C	7.79	7.8	5.6	0.805	0.332	2.760	NA	NA	178.70	26.0	6.60	NA
7	2[illegible]	1440	158.7	11	C	7.84	8.2	7.8	0.866	0.332	2.670	2.81	0.601	94.42	26.1	7.20	NA
7	3[illegible]	1740	161.7	11	C	7.81	7.9	8.2	0.987	0.332	2.610	NA	NA	159.89	26.2	7.40	NA

946510499

MARKET ISLAND - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2040	164.7	11	C	7.57	26.0	12.4	1.040	0.184	1.700	3.69	0.891	67.44	25.1	8.10	NA
7	21	2340	167.7	11	C	7.69	21.0	11.4	1.140	0.240	2.100	NA	NA	60.70	24.8	8.80	NA
7	21	235	170.6	11	C	7.89	15.0	12.0	1.700	0.276	1.890	4.40	0.817	17.51	25.5	8.60	NA
7	21	535	173.6	11	C	7.71	25.0	10.4	1.340	0.168	1.610	NA	NA	9.73	24.5	8.80	NA
7	21	840	176.7	11	C	7.60	28.0	7.2	0.776	0.119	1.070	3.41	0.662	20.23	24.0	8.90	NA
7	21	1139	179.6	11	C	7.59	23.0	6.8	0.783	0.146	1.110	NA	NA	18.88	23.5	8.30	NA
7	21	1443	182.7	11	C	7.69	12.0	6.4	1.160	0.205	1.280	3.32	0.563	16.86	26.5	8.60	NA
7	21	1740	185.7	11	C	7.67	11.0	6.4	0.968	0.228	1.340	NA	NA	11.46	25.8	8.50	NA
7	21	2040	188.7	11	C	7.73	15.0	6.8	1.250	0.246	1.340	2.79	0.608	12.14	25.8	8.50	NA
7	21	2350	191.8	11	C	7.75	12.5	6.4	1.110	0.228	1.340	NA	NA	14.84	24.8	7.30	NA
7	22	235	194.6	11	C	7.74	10.0	7.0	1.040	0.228	1.240	3.17	0.863	12.14	25.0	8.20	NA
7	22	535	197.6	11	C	7.78	11.0	6.4	0.968	0.219	1.260	NA	NA	14.17	23.5	7.80	NA
7	22	840	200.7	11	C	7.80	19.0	8.0	1.200	0.210	1.270	2.27	0.569	9.41	24.5	8.90	NA
7	22	1136	203.6	11	C	7.90	17.0	7.6	0.651	0.178	1.090	2.30	0.542	22.57	25.0	9.00	NA
7	22	1435	206.6	11	C	7.90	21.0	7.0	0.742	0.164	1.010	2.24	0.430	15.05	25.6	8.80	NA
7	22	1740	209.7	11	C	7.80	17.0	7.6	0.449	0.165	1.220	NA	NA	30.10	26.0	8.70	NA
7	22	2040	212.7	11	C	7.80	18.0	7.8	0.689	0.152	1.260	1.89	0.364	22.57	25.8	8.40	NA
7	23	"	216..	11	C	7.90	16.0	7.6	0.671	0.174	1.220	NA	NA	18.81	25.0	8.60	NA
7	23	235	218.6	11	C	7.80	17.0	7.6	0.723	0.183	1.250	2.96	0.430	18.81	24.7	8.60	NA
7	23	535	221.6	11	C	7.90	14.0	6.8	0.679	0.187	1.280	NA	NA	19.22	24.0	8.00	NA
7	23	836	224.6	11	C	7.62	7.6	3.8	0.542	0.187	1.280	2.32	0.470	13.49	24.0	8.70	NA
7	23	1139	227.6	11	C	7.73	7.2	3.8	0.686	NA	NA	NA	NA	20.69	24.3	7.70	NA
7	23	144..	230.7	11	C	7.71	6.5	3.2	0.712	0.196	1.310	2.46	0.456	16.93	24.5	8.40	NA
7	23	174..	233.7	11	C	NA	NA	NA	NA	NA	NA	NA	NA	NA	24.8	8.40	NA
7	23	2040	236.7	11	C	7.66	6.8	4.0	0.677	0.196	1.320	NA	NA	17.53	24.8	7.80	NA
7	23	2350	239..	11	C	7.73	7.9	4.4	0.776	0.200	1.330	3.06	0.456	13.49	24.8	7.80	NA

946510500

MARKET ISLAND - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O. [PPM]	SAL [PPT]
7	24	235	242.6	11	C	7.77	8.3	4.2	0.714	0.192	1.310	NA	NA	19.56	25.0	7.70	NA
7	24	535	245.6	11	C	7.82	9.0	2.8	0.809	0.200	1.330	2.92	0.562	24.45	24.8	7.80	NA
		AVERAGE READING				7.82	10.1	6.4	0.720	0.264	2.095	3.01	0.678	43.08	25.7	7.44	NA

946510501

BASELINE

MCBRIDE AVENUE

7-14/7-24-81

1/2 DEPTH

946510502

MCBRIDE AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	831	8.5	12	C	7.51	5.8	9.0	0.851	0.224	1.720	1.92	0.855	71.48	27.0	5.40	NA
7	14	1130	11.5	12	C	7.72	6.7	6.2	0.673	0.224	1.800	NA	NA	86.53	26.9	6.20	NA
7	14	1445	14.6	12	C	7.95	6.6	7.6	0.815	0.264	1.960	3.03	0.615	90.29	27.5	8.20	NA
7	14	1745	17.8	12	C	8.12	7.6	7.8	0.815	0.264	1.930	NA	NA	92.17	28.0	8.20	NA
7	14	2045	20.8	12	C	7.88	7.9	8.4	0.756	0.264	1.950	2.24	0.589	67.72	27.5	8.20	NA
7	14	2350	23.8	12	C	7.73	8.3	6.8	0.799	0.264	1.940	NA	NA	65.84	26.8	7.00	NA
7	15	240	26.7	12	C	7.63	7.7	7.4	0.840	0.264	1.890	1.97	0.808	63.95	26.0	5.40	NA
7	15	530	29.5	12	C	7.57	9.0	6.2	0.912	0.264	2.010	NA	NA	35.74	26.0	5.40	NA
7	15	828	32.5	12	C	7.51	8.4	7.0	1.210	0.272	1.928	2.30	0.612	67.71	25.5	5.40	NA
7	15	1130	35.5	12	C	7.67	8.3	6.6	0.565	0.308	2.024	NA	NA	63.95	26.0	6.10	NA
7	15	1425	38.4	12	C	8.05	7.8	7.0	0.918	0.292	2.076	2.07	0.526	65.84	26.2	7.40	NA
7	15	1740	41.7	12	C	8.24	8.0	7.4	0.837	0.272	2.028	NA	NA	71.48	27.5	8.80	NA
7	15	2040	44.7	12	C	8.27	7.6	6.6	0.692	0.272	2.076	1.98	0.626	54.54	27.0	9.80	NA
7	15	2340	47.7	12	C	7.79	8.4	5.8	0.775	0.272	2.044	NA	NA	45.14	26.0	7.60	NA
7	16	230	50.5	12	C	7.59	9.0	6.2	0.887	0.272	1.944	2.58	0.513	41.38	25.0	6.20	NA
7	16	520	53.3	12	C	7.56	9.1	5.4	0.736	0.272	2.012	NA	NA	35.74	25.0	4.20	NA
7	16	832	56.5	12	C	7.64	7.4	4.6	0.878	0.272	2.032	3.16	0.560	39.50	24.5	5.20	NA
7	16	1130	59.5	12	C	7.84	7.2	6.2	0.907	0.272	2.080	NA	NA	35.74	25.2	7.20	NA
7	16	1431	62.5	12	C	8.24	7.9	7.4	0.770	0.272	2.116	3.52	0.752	47.02	27.0	9.80	NA
7	16	1730	65.5	12	C	8.23	8.8	7.0	0.729	0.272	2.072	NA	NA	62.07	27.0	11.00	NA
7	16	2030	68.5	12	C	8.02	8.7	7.2	0.699	0.292	2.200	3.48	0.642	52.67	26.5	9.80	NA
7	16	2330	71.5	12	C	7.86	8.5	5.6	0.663	0.292	2.108	NA	NA	47.02	26.0	9.10	NA
7	17	220	74.3	12	C	7.77	7.6	6.8	0.914	0.292	2.116	2.82	0.715	35.74	25.0	6.90	NA
7	17	520	77.3	12	C	7.66	7.8	7.0	0.701	0.272	2.146	NA	NA	28.22	25.0	5.40	NA
7	17	833	80.5	12	C	7.66	9.3	5.0	0.685	0.260	2.070	2.96	0.615	50.58	24.3	5.20	NA
7	17	1140	83.5	12	C	7.91	9.6	4.8	0.891	0.296	2.320	NA	NA	50.58	25.7	8.50	NA

946510503

MCBRIDE AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1440	86.7	12	C	8.50	9.2	5.0	0.819	0.316	2.630	4.48	0.734	67.44	24.9	8.60	NA
7	17	1730	89.5	12	C	8.90	9.0	4.2	0.746	0.316	2.440	NA	NA	64.07	26.2	11.20	NA
7	17	2030	92.5	12	C	8.70	9.4	5.0	0.843	0.316	2.420	2.24	0.417	33.72	26.0	9.50	NA
7	17	2330	95.5	12	C	8.40	8.5	4.2	0.810	0.332	2.460	NA	NA	64.07	26.8	10.50	NA
7	18	220	98.3	12	C	8.00	8.0	3.4	1.100	0.280	2.440	2.88	0.562	50.58	25.0	4.00	NA
7	18	525	101.4	12	C	7.80	7.9	3.6	1.210	0.316	2.320	NA	NA	40.46	26.0	7.00	NA
7	18	829	104.5	12	C	7.70	8.2	5.0	1.350	0.280	2.420	3.59	0.589	54.55	26.0	6.40	NA
7	18	1130	107.5	12	C	7.80	8.6	4.6	1.290	0.336	2.340	NA	NA	20.69	26.2	6.40	NA
7	18	1425	110.4	12	C	8.20	8.3	4.6	1.240	0.330	2.590	5.44	0.615	47.03	28.5	11.60	NA
7	18	1730	113.5	12	C	8.20	9.4	6.2	1.190	0.356	2.530	NA	NA	35.74	28.5	13.00	NA
7	18	2030	116.5	12	C	8.40	8.5	5.0	0.843	0.330	2.670	2.81	0.496	2.14	28.0	12.80	NA
7	18	2330	119.5	12	C	8.10	7.7	4.2	1.020	0.376	2.560	NA	NA	31.98	27.0	8.70	NA
7	19	225	122.4	12	C	8.00	7.6	4.2	1.120	0.330	2.600	4.30	0.562	19.56	26.5	7.90	NA
7	19	525	125.4	12	C	7.80	7.9	4.0	1.170	0.280	2.530	NA	NA	26.33	26.5	6.60	NA
7	19	830	128.5	12	C	7.54	6.4	6.0	1.150	0.280	2.500	3.81	0.483	225.70	25.8	3.40	NA
7	19	1129	131.5	12	C	7.82	6.7	5.0	1.140	0.280	2.590	NA	NA	150.50	26.5	6.40	NA
7	19	1440	134.7	12	C	8.40	7.7	5.8	0.862	0.336	2.630	3.49	0.456	50.78	28.0	7.40	NA
7	19	173[illegible]	137.5	12	C	8.62	8.4	7.8	0.762	0.280	2.740	NA	NA	20.69	28.8	13.40	NA
7	19	2030	140.5	12	C	8.61	8.6	4.4	0.667	0.336	2.650	3.77	0.502	159.90	27.5	7.30	NA
7	19	2330	143.5	12	C	8.33	7.4	5.8	0.755	0.280	2.610	NA	NA	121.40	27.0	7.10	NA
7	2	220	146.3	12	C	8.09	7.2	5.4	0.812	0.280	2.550	3.24	0.602	84.30	26.5	9.00	NA
7	2	520	149.3	12	C	7.80	7.1	5.0	0.930	0.336	2.470	NA	NA	64.07	26.5	7.60	NA
7	2	834	152.6	12	C	7.71	7.7	7.2	0.805	0.316	2.420	3.02	0.549	4.86	26.5	5.80	NA
7	2	1134	155.5	12	C	7.64	8.0	6.8	1.070	0.316	2.510	NA	NA	101.16	26.7	6.80	NA
7	2	1430	158.5	12	C	7.79	8.3	8.2	1.070	0.332	2.610	2.88	0.404	87.67	26.0	4.50	NA
7	2	173[illegible]	161.5	12	C	7.73	9.0	7.4	0.931	0.316	2.450	NA	NA	27.23	26.2	7.70	NA

946510504

MCBRIDE AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2030	164.5	12	C	7.48	9.7	10.0	1.240	0.260	2.080	2.97	0.562	28.20	25.3	4.40	NA
7	20	2330	167.5	12	C	7.49	14.0	9.8	0.801	0.276	2.080	NA	NA	19.45	26.0	5.20	NA
7	21	225	170.4	12	C	7.62	14.0	9.2	1.570	0.260	1.810	3.17	0.509	12.64	25.5	5.60	NA
7	21	521	173.3	12	C	7.44	29.0	8.8	1.340	0.148	1.480	NA	NA	27.23	25.0	5.80	NA
7	21	829	176.5	12	C	7.45	28.0	8.2	0.739	0.119	0.991	4.73	0.642	14.84	24.0	6.30	NA
7	21	1128	179.5	12	C	7.37	18.0	7.0	0.884	0.146	1.090	NA	NA	14.16	24.0	6.50	NA
7	21	1435	182.6	12	C	7.36	14.0	8.0	1.230	0.200	1.220	2.17	0.443	10.12	25.8	5.80	NA
7	21	1730	185.5	12	C	7.40	10.5	8.6	1.360	0.223	1.270	NA	NA	10.79	26.2	6.20	NA
7	21	2030	188.5	12	C	7.45	11.5	8.6	1.340	0.157	1.570	3.59	0.456	12.14	26.0	5.60	NA
7	21	2330	191.5	12	C	7.40	10.0	6.8	1.230	0.228	1.300	NA	NA	10.12	25.2	5.20	NA
7	22	225	194.4	12	C	7.42	9.2	6.8	1.160	0.219	1.290	4.02	0.443	11.46	25.0	4.40	NA
7	22	525	197.4	12	C	7.41	9.0	4.6	0.586	0.200	1.240	2.14	0.456	14.84	23.5	4.20	NA
7	22	830	200.5	12	C	7.60	15.0	6.4	0.778	0.196	1.150	NA	NA	21.58	25.0	5.30	NA
7	22	1128	203.5	12	C	7.50	16.0	6.2	0.629	0.165	1.140	2.14	0.430	13.49	25.0	5.40	NA
7	22	1425	206.4	12	C	7.60	16.0	6.0	0.642	0.165	1.100	NA	NA	9.44	26.0	5.70	NA
7	22	1730	209.5	12	C	7.50	18.0	6.4	0.753	0.164	1.010	1.96	0.351	18.88	26.2	5.70	NA
7	22	2030	212.5	12	C	7.50	17.0	7.6	0.748	0.164	1.030	NA	NA	12.14	26.0	4.90	NA
7	22	2335	215.6	12	C	7.52	15.0	7.2	0.978	0.164	1.060	4.66	0.337	4.67	25.2	4.00	NA
7	23	225	218.4	12	C	7.50	14.0	7.0	0.878	0.173	1.090	3.95	0.483	16.19	25.0	3.70	NA
7	23	525	221.4	12	C	7.50	12.0	7.4	0.890	0.178	1.100	2.35	0.390	10.79	24.5	3.00	NA
7	23	827	224.3	12	C	7.15	5.2	6.4	0.803	0.174	1.200	NA	NA	12.81	24.5	2.80	NA
7	23	1128	227.5	12	C	7.21	4.9	6.4	1.160	0.165	1.240	3.10	0.404	10.12	24.2	3.20	NA
7	23	1430	230.5	12	C	7.30	5.1	6.4	0.742	0.161	1.260	NA	NA	11.46	24.6	4.40	NA
7	23	1730	233.5	12	C	7.35	5.4	2.4	0.884	0.174	1.250	2.07	0.430	19.56	25.2	5.80	NA
7	23	2030	236.5	12	C	7.41	5.4	2.6	0.946	0.183	1.220	NA	NA	20.69	25.2	5.60	NA
7	23	2330	239.5	12	C	7.37	6.8	3.2	0.926	0.174	1.210	3.45	0.351	18.81	25.5	5.00	NA

946510505

MCBRIDE AVENUE - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	225	242.4	12	C	7.49	6.2	4.4	0.853	0.178	1.210	NA	NA	37.62	25.8	4.90	NA
7	24	525	245.4	12	C	7.41	6.6	3.4	0.828	0.178	1.210	3.31	0.324	24.45	25.0	4.30	NA
		AVERAGE READING				7.78	9.5	6.0	0.918	0.255	1.927	3.09	0.534	44.67	26.0	6.71	NA

946510506

BASELINE

HILLARY

STREET

7-14/7-24-81

1/2 DEPTH

946510507

HILLARY STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	14	817	8.3	13	C	7.45	7.1	9.0	0.974	0.264	1.740	2.42	0.753	80.88	26.0	3.20	NA
7	14	1120	11.3	13	C	7.50	6.5	8.8	1.080	0.300	1.920	NA	NA	62.07	26.0	5.20	NA
7	14	1420	14.3	13	C	7.64	6.8	7.4	1.370	0.300	2.080	1.83	0.793	50.79	27.0	7.80	NA
7	14	1720	17.3	13	C	7.82	7.2	8.6	1.090	0.300	2.100	NA	NA	48.91	28.5	8.80	NA
7	14	2020	20.3	13	C	7.80	6.3	6.6	1.100	0.300	2.180	3.58	0.984	37.62	28.0	6.80	NA
7	14	2320	23.3	13	C	7.62	8.0	6.0	1.100	0.300	2.220	NA	NA	37.62	26.2	5.70	NA
7	15	220	26.3	13	C	7.50	7.4	7.8	0.968	0.300	2.200	1.72	0.862	43.26	25.0	4.40	NA
7	15	515	29.3	13	C	7.48	8.4	7.4	0.974	0.300	2.190	NA	NA	67.72	24.0	3.20	NA
7	15	817	32.3	13	C	7.35	7.9	6.0	0.822	0.252	1.876	2.71	1.040	37.62	24.0	3.50	NA
7	15	1120	35.3	13	C	7.42	7.4	6.2	0.909	0.272	1.964	NA	NA	30.10	24.2	5.20	NA
7	15	1415	38.3	13	C	7.65	7.6	5.0	1.030	0.272	2.088	3.00	0.636	28.22	26.0	7.40	NA
7	15	1720	41.3	13	C	7.74	7.1	5.4	0.898	0.272	2.116	NA	NA	31.98	27.5	7.50	NA
7	15	2020	44.3	13	C	7.76	8.0	5.0	0.928	0.272	2.168	2.67	0.554	28.22	27.3	8.30	NA
7	15	2320	47.3	13	C	7.74	8.0	6.4	0.412	0.308	2.280	NA	NA	41.38	26.5	7.10	NA
7	16	215	50.3	13	C	7.65	8.3	6.4	0.947	0.328	2.360	2.97	0.642	37.52	25.0	4.80	NA
7	16	510	53.2	13	C	7.43	14.0	7.0	1.060	0.348	2.388	NA	NA	58.31	24.0	3.40	NA
7	16	820	56.3	13	C	7.55	7.4	5.0	0.900	0.364	2.416	2.24	0.734	30.10	23.5	3.40	NA
7	16	1120	59.3	13	C	7.60	7.8	5.4	0.898	0.328	2.156	NA	NA	39.50	28.5	4.80	NA
7	16	1417	62.3	13	C	7.66	6.9	6.0	1.200	0.328	2.220	4.48	0.615	30.10	26.2	7.20	NA
7	16	1720	65.3	13	C	7.82	7.7	9.0	1.220	0.348	2.352	NA	NA	26.33	26.2	7.60	NA
7	16	2020	68.3	13	C	7.82	8.2	7.4	1.070	0.348	2.328	2.97	0.589	35.74	25.8	7.80	NA
7	16	2320	71.3	13	C	7.79	7.8	8.4	1.190	0.364	2.512	NA	NA	60.19	26.8	7.40	NA
7	17	210	74.2	13	C	7.65	7.7	8.0	1.150	0.384	2.636	2.88	0.615	20.69	26.0	5.20	NA
7	17	51	77.1	13	C	7.62	8.5	8.5	1.270	0.424	2.608	NA	NA	31.98	25.0	3.50	NA
7	17	820	80.3	13	C	7.60	8.7	4.6	0.833	0.360	2.350	2.71	0.758	67.44	24.2	3.30	NA
7	17	1118	83.3	13	C	7.60	8.4	4.8	1.120	0.352	2.160	NA	NA	43.84	25.2	6.40	NA

946510508

HILLARY STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	17	1418	86.3	13	C	7.70	8.6	5.0	1.590	0.332	2.250	3.15	0.536	24.31	26.0	6.60	NA
7	17	1720	89.3	13	C	7.70	8.3	6.0	1.380	0.332	2.370	NA	NA	25.29	28.5	10.10	NA
7	17	2020	92.3	13	C	7.70	12.0	5.8	1.420	0.332	2.400	4.07	0.750	28.20	28.0	7.90	NA
7	17	2320	95.3	13	C	7.80	9.0	6.4	1.410	0.368	2.590	NA	NA	43.84	27.5	7.00	NA
7	18	210	98.2	13	C	7.80	11.0	4.8	1.310	0.388	2.740	3.41	0.985	40.46	26.5	5.20	NA
7	18	510	101.2	13	C	7.70	13.0	5.2	1.350	0.396	2.680	NA	NA	40.46	25.0	3.40	NA
7	18	819	104.3	13	C	7.50	9.3	5.8	1.290	0.380	2.650	2.82	0.602	30.10	25.0	3.20	NA
7	18	1115	107.3	13	C	7.60	7.8	4.8	1.300	0.380	2.470	NA	NA	26.33	25.8	5.60	NA
7	18	1417	110.3	13	C	7.70	8.3	4.4	1.440	0.280	2.650	3.87	0.715	22.57	26.4	5.80	NA
7	18	1720	113.3	13	C	7.80	9.0	5.0	1.300	0.336	2.650	NA	NA	24.45	27.0	7.30	NA
7	18	2020	116.3	13	C	7.90	8.4	5.2	1.070	0.356	2.720	3.39	0.788	28.22	28.0	8.70	NA
7	18	2320	119.3	13	C	7.80	8.8	5.6	0.929	0.336	2.780	NA	NA	24.45	28.2	8.40	NA
7	19	215	122.3	13	C	7.70	9.5	5.2	1.060	0.356	2.770	2.39	0.668	47.03	27.1	5.90	NA
7	19	515	125.3	13	C	7.70	9.0	5.4	1.130	0.330	2.720	NA	NA	33.86	26.0	3.70	NA
7	19	820	128.3	13	C	7.45	6.5	5.8	0.878	0.280	2.660	4.53	0.979	56.43	25.0	3.20	NA
7	19	1118	131.3	13	C	7.49	6.3	5.6	1.330	0.336	2.250	NA	NA	58.31	25.4	3.70	NA
7	19	1419	134.3	13	C	7.62	6.5	5.0	1.140	0.280	2.670	3.00	0.651	37.62	27.5	7.10	NA
7	19	1720	137.3	13	C	7.67	6.8	5.6	1.440	0.320	2.450	NA	NA	47.02	28.0	9.40	NA
7	19	2020	140.3	13	C	7.64	7.5	5.6	1.100	0.336	2.480	3.10	0.715	56.43	27.2	7.40	NA
7	19	2320	143.3	13	C	7.63	8.2	6.6	1.700	0.376	2.680	NA	NA	48.91	27.0	7.20	NA
7	20	215	146.2	13	C	7.60	7.2	6.0	0.978	0.380	3.050	3.74	1.060	52.67	26.5	5.60	NA
7	20	515	149.2	13	C	7.49	9.3	6.4	1.330	0.376	2.490	NA	NA	69.59	26.0	3.50	NA
7	20	820	152.3	13	C	7.49	8.3	7.2	1.170	0.388	2.620	2.74	0.700	169.29	25.8	2.90	NA
7	20	1118	155.3	13	C	7.53	8.8	5.0	1.260	0.368	2.430	NA	NA	131.67	26.0	3.80	NA
7	20	1419	158.3	13	C	7.58	8.9	6.8	1.140	0.332	2.350	3.37	0.899	150.48	26.0	5.20	NA
7	20	1720	161.3	13	C	7.53	10.4	10.8	1.410	0.352	2.520	NA	NA	25.29	24.8	6.40	NA

946510509

HILLARY STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	20	2020	164.3	13	C	7.56	9.6	9.2	1.410	0.332	2.090	3.31	0.791	37.09	21.5	5.70	NA
7	20	2320	167.3	13	C	7.57	10.5	9.2	1.660	0.352	1.680	NA	NA	23.34	25.8	6.40	NA
7	21	215	170.3	13	C	7.52	21.0	9.8	1.780	0.204	1.650	2.68	0.493	18.48	25.0	6.30	NA
7	21	515	173.3	13	C	7.56	40.0	7.1	0.740	0.092	1.200	NA	NA	26.26	24.1	7.20	NA
7	21	817	176.3	13	C	7.38	21.0	5.8	0.945	0.132	1.130	3.28	0.594	13.49	23.5	6.20	NA
7	21	1115	179.3	13	C	7.37	14.0	7.6	1.250	0.200	1.300	NA	NA	8.77	23.0	4.00	NA
7	21	1418	182.3	13	C	7.42	11.0	6.6	1.350	0.219	1.280	2.89	0.668	12.81	26.0	6.40	NA
7	21	1720	185.3	13	C	7.45	12.0	8.8	1.290	0.253	1.570	NA	NA	12.81	24.8	5.50	NA
7	21	2020	188.3	13	C	7.44	10.0	6.8	1.250	0.223	1.320	2.44	0.707	26.33	24.5	4.90	NA
7	21	2320	191.3	13	C	7.43	9.0	6.8	1.180	0.219	1.360	NA	NA	20.23	24.0	4.20	NA
7	22	215	194.3	13	C	7.50	8.8	7.0	0.956	0.200	1.330	NA	NA	13.49	25.0	4.80	NA
7	22	515	197.3	13	C	7.45	10.0	7.2	0.803	0.187	1.090	NA	NA	10.79	23.1	4.70	NA
7	22	820	200.3	13	C	7.50	25.0	6.4	0.592	0.160	0.980	NA	NA	NA	24.5	6.00	NA
7	22	1118	203.3	13	C	7.50	22.0	7.2	0.710	0.164	1.010	2.67	0.618	14.16	25.1	5.90	NA
7	22	1417	206.3	13	C	7.50	20.0	6.6	0.776	0.160	0.970	NA	NA	8.77	26.0	3.60	NA
7	22	1720	209.3	13	C	7.50	19.0	7.4	0.851	0.164	1.050	2.46	0.564	2.33	26.2	4.10	NA
7	22	2020	212.3	13	C	7.50	18.0	7.2	0.839	0.174	1.220	NA	NA	12.14	26.1	3.30	NA
7	22	2320	215.3	13	C	7.40	18.0	5.4	0.884	0.178	1.260	3.21	0.553	10.79	25.2	2.90	NA
7	23	215	218.3	13	C	7.50	17.0	6.6	0.833	0.178	1.120	NA	NA	20.69	24.5	3.60	NA
7	23	515	221.3	13	C	7.50	15.0	6.4	1.280	0.183	1.230	2.19	0.624	37.62	24.0	3.20	NA
7	23	815	224.3	13	C	7.14	5.4	3.0	0.851	0.178	1.200	2.13	0.725	8.77	23.5	4.00	NA
7	23	1117	227.3	13	C	7.29	6.2	2.2	0.974	0.178	1.180	NA	NA	6.07	24.0	4.70	NA
7	23	1418	230.3	13	C	7.34	5.7	4.6	0.987	0.174	1.180	5.60	0.608	13.49	25.4	5.40	NA
7	23	1720	233.3	13	C	7.79	5.7	2.4	0.877	0.183	1.250	NA	NA	24.45	27.0	5.40	NA
7	23	2020	236.3	13	C	7.46	6.4	4.0	0.922	0.183	1.270	1.93	0.562	16.19	26.0	4.60	NA
7	23	2320	239.3	13	C	7.36	6.7	3.4	0.835	0.183	1.230	NA	NA	31.98	24.5	4.30	NA

946510510

HILLARY STREET - LEVEL C - DEPTH 1/2
BASELINE SAMPLING LOW FLOW

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
7	24	215	242.3	13	C	7.30	7.0	3.2	0.800	0.174	1.210	2.40	0.554	45.14	24.2	4.00	NA
7	24	515	245.3	13	C	7.29	7.4	4.4	0.773	0.174	1.250	2.21	0.577	33.86	24.0	3.70	NA
		AVERAGE READING				7.57	10.2	6.2	1.097	0.284	2.004	2.98	0.707	37.49	25.7	5.48	NA

946510511

BASELINE

DUNDEE DAM

UPSTREAM

7-14/7-24-81

1/2 DEPTH

946510512

RIVER SAMPLING BASELINE - LOW FLOW
DUNDEE DAM UPSTREAM - LEVEL 8C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
7	14	0925	8	C	27.5	9.8
7	14	1210	8	C	27.3	10.0
7	14	1535	8	C	27.5	11.1
7	14	1835	8	C	27.2	10.5
7	14	2130	8	C	27.0	10.0
7	15	0035	8	C	26.0	9.8
7	15	0335	8	C	25.5	8.6
7	15	0630	8	C	25.0	9.0
7	15	0907	8	C	25.0	8.8
7	15	1215	8	C	25.5	11.2
7	15	1530	8	C	26.0	13.0
7	15	1825	8	C	26.5	12.8
7	15	2120	8	C	26.0	10.2
7	16	0030	8	C	26.0	12.2
7	16	0320	8	C	25.2	12.4
7	16	0620	8	C	24.0	9.9
7	16	0913	8	C	24.8	9.4
7	16	1220	8	C	25.0	8.0
7	16	1525	8	C	24.9	9.8
7	16	1820	8	C	25.5	15.1
7	16	2120	8	C	25.0	12.5
7	17	0020	8	C	26.0	18.2
7	17	0315	8	C	26.0	15.0
7	17	0615	8	C	25.5	15.4
7	17	0923	8	C	24.5	8.5
7	17	1218	8	C	25.2	10.6
7	17	1524	8	C	25.2	6.6
7	17	1820	8	C	25.2	12.4
7	17	2120	8	C	26.0	16.5
7	18	0010	8	C	26.5	18.2
7	18	0310	8	C	26.5	17.6
7	18	0610	8	C	26.0	16.0
7	18	0905	8	C	25.2	6.6
7	18	1210	8	C	26.0	7.0
7	18	1520	8	C	25.7	10.3
7	18	1820	8	C	26.5	18.6
7	18	2120	8	C	27.2	17.8
7	19	0030	8	C	28.0	20.0
7	19	0320	8	C	27.5	20.0
7	19	0620	8	C	26.5	14.8
7	19	0912	8	C	26.0	9.5

946510513

RIVER SAMPLING BASELINE - LOW FLOW
DUNDEE DAM UPSTREAM - LEVEL BC - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
7	19	1215	B	C	26.0	9.5
7	19	1530	B	C	26.5	13.5
7	19	1820	B	C	26.2	8.6
7	19	2120	B	C	26.5	13.2
7	2[illegible]	0035	B	C	27.0	20.0
7	2	0315	B	C	27.5	19.6
7	2[illegible]	0615	B	C	26.0	15.8
7	2[illegible]	0910	B	C	26.0	6.8
7	2[illegible]	1205	B	C	26.7	3.2
7	2[illegible]	1515	B	C	26.6	13.2
7	2[illegible]	1820	B	C	26.5	12.4
7	2	2120	B	C	26.2	8.5
7	21	0030	B	C	25.0	2.8
7	21	0315	B	C	24.5	4.6
7	21	0615	B	C	24.0	5.0
7	21	0915	B	C	25.1	6.2
7	21	1209	B	C	25.8	6.8
7	21	1520	B	C	26.5	6.7
7	21	1820	B	C	26.5	6.6
7	21	2120	B	C	26.1	6.3
7	22	0025	B	C	26.0	5.4
7	22	0310	B	C	24.5	3.9
7	22	0610	B	C	24.0	4.0
7	22	0910	B	C	25.0	5.2
7	22	1200	B	C	25.0	5.5
7	22	1515	B	C	25.5	6.5
7	22	1820	B	C	26.0	7.3
7	22	2120	B	C	26.0	7.1
7	23	0040	B	C	25.5	6.8
7	23	0315	B	C	25.0	6.8
7	23	0615	B	C	24.7	4.9
7	23	0910	B	C	24.5	5.0
7	23	1208	B	C	24.5	4.8
7	23	1520	B	C	24.5	6.4
7	23	1820	B	C	25.5	8.3
7	23	2120	B	C	24.9	7.1
7	24	0025	B	C	24.5	6.3
7	24	0310	B	C	24.0	5.4
7	24	0610	B	C	24.8	6.8

946510514

BASELINE

DUNDEE DAM

DØWNSTREAM

7-14/7-24-81

1/2 DEPTH

946510515

RIVER SAMPLING BASELINE - LOW FLOW
DUNDEE DAM DOWNSTREAM - LEVEL 6C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
7	14	0930	6	C	26.0	8.7
7	14	1220	6	C	27.5	8.9
7	14	1545	6	C	27.2	9.1
7	14	1845	6	C	26.2	8.2
7	14	2140	6	C	25.0	6.3
7	15	0050	6	C	24.5	6.3
7	15	0345	6	C	24.0	6.4
7	15	0640	6	C	24.0	6.4
7	15	0920	6	C	24.5	8.3
7	15	1300	6	C	26.5	9.1
7	15	1550	6	C	27.5	9.2
7	15	1835	6	C	26.8	8.0
7	15	2130	6	C	25.2	6.5
7	16	0040	6	C	25.0	6.4
7	16	0335	6	C	24.5	5.4
7	16	0635	6	C	24.0	6.3
7	16	0925	6	C	25.0	8.2
7	16	1230	6	C	27.2	9.6
7	16	1545	6	C	27.0	9.1
7	16	1830	6	C	27.5	8.2
7	16	2130	6	C	26.0	5.9
7	17	0030	6	C	24.5	6.4
7	17	0330	6	C	24.0	6.4
7	17	0630	6	C	24.0	6.6
7	17	0930	6	C	25.3	9.3
7	17	1230	6	C	28.0	10.5
7	17	1545	6	C	28.0	8.2
7	17	1830	6	C	27.8	6.9
7	17	2130	6	C	26.0	6.7
7	18	0025	6	C	25.0	6.2
7	18	0325	6	C	25.0	6.2
7	18	0625	6	C	25.0	6.4
7	18	0918	6	C	25.8	8.7
7	18	1220	6	C	28.5	10.2
7	18	1550	6	C	29.2	9.1
7	18	1830	6	C	26.2	8.3
7	18	2130	6	C	25.0	6.3
7	19	0040	6	C	26.0	4.8
7	19	0335	6	C	27.0	5.1
7	19	0635	6	C	25.0	5.8
7	19	0924	6	C	26.0	8.5
7	19	1238	6	C	29.0	9.8
7	19	1545	6	C	30.5	9.4
7	19	1830	6	C	29.0	7.2
7	19	2130	6	C	28.0	5.4
7	20	0050	6	C	26.0	5.4
7	20	0330	6	C	26.5	5.1
7	20	0630	6	C	26.5	5.6
7	20	0919	6	C	27.0	7.2
7	20	1220	6	C	26.0	6.6
7	20	1545	6	C	26.0	7.5
7	20	1830	6	C	26.2	8.4
7	20	2130	6	C	26.1	8.2

946510516

RIVER SAMPLING BASELINE - LOW FLOW

7	21	0345	6	C	25.0	6.7
7	21	0330	6	C	24.5	7.0
7	21	0630	6	C	24.0	7.8
7	21	0926	6	C	25.0	8.0
7	21	1215	6	C	25.5	8.0
7	21	1545	6	C	26.5	7.6
7	21	1830	6	C	26.8	7.5
7	21	2130	6	C	26.2	7.9
7	22	0040	6	C	26.0	7.7
7	22	0325	6	C	24.5	7.2
7	22	0625	6	C	23.8	6.8
7	22	0920	6	C	25.0	7.8
7	21	1215	6	C	25.5	7.5
7	22	1545	6	C	26.5	7.3
7	22	1830	6	C	25.8	7.7
7	22	2130	6	C	25.5	7.1
7	23	0055	6	C	25.0	7.7
7	23	0330	6	C	25.0	7.4
7	23	0630	6	C	24.0	7.5
7	23	0925	6	C	24.9	8.3
7	23	1219	6	C	25.8	8.3
7	23	1545	6	C	28.6	8.4
7	23	1830	6	C	25.8	8.3
7	23	2130	6	C	25.5	7.2
7	24	0040	6	C	24.5	7.4
7	24	0325	6	C	24.0	7.2
7	24	0625	6	C	24.0	7.4

946510517

Storm Sampling
September 1981

946510518

STØRM #2

KEARNY

PØINT

9-15/9-25-81

1/3 DEPTH

946510519

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1257	12.9	1	A	7.20	5.4	3.2	1.690	0.139	0.482	2.96	0.478	9.44	24.1	2.30	17.8
9	15	1352	13.9	1	A	7.30	5.4	2.4	1.480	0.107	0.451	0.00	0.000	6.07	24.2	2.05	17.2
9	15	1459	15.0	1	A	7.30	4.7	1.6	1.310	0.089	0.416	2.54	0.504	8.77	24.0	1.75	16.2
9	15	1600	16.0	1	A	7.20	5.3	2.4	1.390	0.084	0.516	0.00	0.000	7.42	23.7	1.20	13.2
9	15	1656	16.9	1	A	7.20	5.4	1.4	1.600	0.125	0.810	2.90	0.487	12.14	23.4	1.10	13.6
9	15	1759	18.0	1	A	7.20	4.5	1.6	1.710	0.139	0.817	0.00	0.000	10.80	23.3	1.30	13.4
9	15	1858	19.0	1	A	7.30	6.4	4.0	1.520	0.093	0.381	2.45	0.510	9.44	24.9	2.05	16.4
9	15	1955	19.9	1	A	7.30	7.5	2.4	2.040	0.148	0.494	0.00	0.000	3.37	24.2	2.20	17.4
9	15	2057	20.9	1	A	7.40	4.7	1.8	0.690	0.093	0.339	1.24	0.278	4.72	23.6	2.30	18.6
9	15	2212	22.2	1	A	7.50	6.6	2.6	1.410	0.125	0.391	0.00	0.000	8.77	23.2	2.00	19.7
9	15	2259	23.0	1	A	7.40	4.6	2.0	1.130	0.080	0.436	2.00	0.373	6.07	23.3	2.20	18.3
9	15	2355	23.9	1	A	7.20	4.1	2.2	1.350	0.089	0.301	0.00	0.000	5.40	24.1	1.45	17.0
9	16	59	25.0	1	A	7.30	4.0	1.6	1.710	0.130	0.470	2.74	0.553	6.07	24.2	0.80	16.8
9	16	210	26.2	1	A	7.30	3.3	2.0	1.810	0.134	0.549	0.00	0.000	5.40	24.0	0.76	16.4
9	16	309	27.1	1	A	7.30	3.4	1.0	1.730	0.134	0.591	2.84	0.555	5.40	23.8	0.70	14.2
9	16	358	28.0	1	A	7.20	3.5	1.8	1.120	0.061	0.287	0.00	0.000	7.42	23.2	0.68	12.1
9	16	456	28.9	1	A	7.30	6.6	1.2	1.290	0.116	0.641	0.00	0.000	0.00	23.0	0.66	10.4
9	16	559	30.0	1	A	7.20	3.6	1.8	1.690	0.130	0.784	0.00	0.000	11.47	22.5	0.60	9.2
9	16	658	31.0	1	A	7.30	3.7	4.0	1.240	0.098	0.334	2.06	0.432	11.47	23.0	0.87	10.6
9	16	800	32.9	1	A	7.30	6.7	4.0	1.700	0.144	0.498	0.00	0.000	10.12	24.0	0.67	15.3
9	16	930	33.5	1	A	7.40	5.3	3.2	0.631	0.075	0.420	1.01	0.238	7.42	23.0	1.65	18.0
9	16	1035	34.6	1	A	7.40	6.5	4.2	1.420	0.130	0.407	0.00	0.000	6.07	23.0	1.46	18.8
9	16	1220	36.3	1	A	7.40	7.3	3.4	1.550	0.130	0.459	2.57	0.472	8.77	22.8	1.80	17.9
9	16	1318	37.3	1	A	7.40	5.0	2.0	1.740	0.144	0.518	0.00	0.000	8.09	23.4	1.10	15.7
9	16	1415	38.3	1	A	7.30	4.7	1.8	1.720	0.144	0.518	3.11	0.574	10.12	23.4	0.90	14.9
9	16	1516	39.3	1	A	7.30	5.2	2.6	1.650	0.116	0.693	0.00	0.000	16.18	23.2	1.00	13.5

946510520

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	16	1620	40.5	1	A	7.30	5.0	2.2	1.600	0.134	0.790	2.63	0.520	16.86	23.9	1.05	9.8
9	16	1723	41.4	1	A	7.20	5.4	2.2	1.630	0.134	0.966	0.00	0.000	12.81	22.5	1.15	8.2
9	16	1822	42.4	1	A	7.20	7.5	2.6	1.580	0.139	1.070	3.72	0.919	13.49	22.4	1.25	7.6
9	16	1927	43.4	1	A	7.30	5.5	1.8	1.720	0.148	0.661	0.00	0.000	13.49	23.2	1.20	12.9
9	16	2026	44.4	1	A	7.30	4.9	1.8	1.470	0.112	0.488	2.33	0.529	5.49	23.5	1.10	14.9
9	16	2130	45.5	1	A	7.40	4.2	1.4	1.670	0.121	0.541	0.00	0.000	6.22	22.6	1.80	16.9
9	16	2237	46.6	1	A	7.40	4.0	1.4	1.660	0.153	0.604	2.75	0.646	1.94	22.8	1.65	16.6
9	16	2336	47.6	1	A	7.30	3.2	1.2	1.350	0.130	0.428	0.00	0.000	5.06	22.0	1.60	18.0
9	17	35	48.6	1	A	7.30	3.3	0.4	0.830	0.103	0.392	1.17	0.243	4.28	22.8	1.10	16.0
9	17	134	49.6	1	A	7.20	2.9	0.4	1.510	0.125	0.454	0.00	0.000	7.00	23.2	0.65	15.7
9	17	234	50.6	1	A	7.20	5.0	1.0	1.370	0.093	0.402	2.29	0.667	5.06	22.7	0.40	13.3
9	17	335	51.6	1	A	7.20	3.4	0.4	1.670	0.139	0.754	0.00	0.000	10.12	22.0	0.29	10.0
9	17	436	52.6	1	A	7.20	3.7	2.8	1.530	0.134	0.822	2.17	0.509	7.42	22.0	0.28	8.5
9	17	533	53.5	1	A	7.20	3.4	0.4	1.390	0.098	0.837	0.00	0.000	10.79	22.0	0.21	7.7
9	17	634	54.6	1	A	7.30	4.0	0.6	0.882	0.075	0.546	1.42	0.299	12.81	21.8	0.18	7.2
9	17	737	55.6	1	A	7.20	4.1	0.4	0.955	0.057	0.438	0.00	0.000	12.14	22.2	0.35	13.1
9	17	839	56.6	1	A	7.30	4.0	0.4	1.680	0.153	0.530	2.64	0.531	10.79	23.0	0.68	15.2
9	17	937	57.6	1	A	7.40	3.2	0.4	0.756	0.134	0.078	0.00	0.000	9.44	22.0	1.25	17.2
9	17	1035	58.6	1	A	7.30	2.7	0.4	0.665	0.089	0.400	2.11	0.418	7.42	22.0	1.30	17.5
9	17	1232	60.5	1	A	7.30	4.1	3.0	1.370	0.144	0.550	2.29	0.448	6.42	22.5	1.45	16.8
9	17	1335	61.6	1	A	7.30	3.3	1.8	1.170	0.109	0.590	0.00	0.000	7.58	22.9	1.45	15.8
9	17	1432	62.5	1	A	7.30	3.4	2.0	1.680	0.144	0.581	2.77	0.545	14.84	23.0	1.30	15.1
9	17	1535	63.6	1	A	7.30	3.3	2.4	1.810	0.142	0.701	0.00	0.000	12.14	22.9	1.15	13.9
9	17	1637	64.6	1	A	7.20	3.6	2.2	1.620	0.153	0.845	2.55	0.532	13.49	22.5	1.00	12.2
9	17	1733	65.5	1	A	7.20	4.1	5.4	1.050	0.096	0.771	0.00	0.000	11.46	22.2	1.10	10.5
9	17	1837	66.6	1	A	7.20	4.2	2.4	0.890	0.096	0.678	1.47	0.329	10.79	22.0	1.10	9.4

946510521

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	17	1934	67.6	1	A	7.20	6.2	3.4	1.630	0.153	1.090	0.00	0.000	18.21	21.9	0.90	9.2
9	17	2033	68.5	1	A	7.30	4.7	2.8	1.980	0.162	0.731	3.38	0.610	10.12	23.4	1.30	15.9
9	17	2132	69.5	1	A	7.30	7.4	2.2	1.510	0.125	0.443	0.00	0.000	8.77	23.9	1.40	16.0
9	17	2237	70.6	1	A	7.30	3.5	1.9	0.640	0.064	0.238	1.33	0.329	3.11	22.5	1.60	16.5
9	17	2350	71.8	1	A	7.10	4.0	2.8	1.000	0.100	0.359	0.00	0.000	1.66	22.1	1.40	19.0
9	18	53	72.9	1	A	7.30	3.4	1.8	1.290	0.132	0.438	2.32	0.392	5.06	22.0	1.20	19.0
9	18	200	74.0	1	A	7.30	5.0	1.8	2.190	0.146	0.553	0.00	0.000	3.50	22.9	0.60	17.0
9	18	304	75.1	1	A	7.20	4.7	1.2	1.600	0.146	0.817	2.88	0.536	6.81	22.6	0.55	15.1
9	18	406	76.1	1	A	7.20	3.2	1.6	1.100	0.142	0.938	0.00	0.000	2.33	22.2	0.48	13.0
9	18	504	77.1	1	A	7.30	3.0	2.8	0.549	0.045	0.341	1.14	0.267	3.11	22.0	0.38	12.0
9	18	603	78.0	1	A	7.30	4.0	2.0	1.040	0.054	0.188	0.00	0.000	2.72	21.8	0.30	9.8
9	18	705	79.1	1	A	7.30	3.1	1.6	0.605	0.082	0.593	1.16	0.223	7.58	21.7	0.25	8.2
9	18	805	80.1	1	A	7.30	2.8	1.0	0.853	0.054	0.248	3.40	0.606	7.58	22.0	0.80	15.1
9	18	904	81.1	1	A	7.30	7.0	1.8	1.760	0.146	0.493	0.00	0.000	5.45	23.0	0.75	17.0
9	18	1006	82.1	1	A	7.30	3.6	1.6	1.760	0.146	0.577	0.00	0.000	4.28	23.0	0.35	17.3
9	18	1057	82.9	1	A	7.30	4.8	1.8	1.340	0.142	0.509	2.41	0.467	2.92	22.2	1.30	17.9
9	18	1228	84.5	1	A	7.30	3.8	7.0	0.528	0.142	0.701	1.88	0.327	4.72	22.0	1.35	18.0
9	18	1330	85.5	1	A	7.40	4.5	2.8	1.660	0.142	0.593	0.00	0.000	6.74	22.3	1.65	17.9
9	18	1431	86.5	1	A	7.30	3.7	1.4	1.630	0.146	0.601	2.74	0.471	6.74	23.0	1.15	16.5
9	18	1532	87.5	1	A	7.40	4.1	1.6	1.780	0.142	0.581	0.00	0.000	12.81	23.0	1.10	15.9
9	18	1634	88.6	1	A	7.30	3.7	1.2	1.480	0.151	0.740	3.10	0.649	12.14	22.5	1.10	14.5
9	18	1733	89.5	1	A	7.30	3.5	1.8	1.560	0.142	0.845	0.00	0.000	11.47	22.1	1.35	12.0
9	18	1829	90.5	1	A	7.30	4.6	1.6	1.450	0.137	0.923	2.13	0.441	9.44	22.0	1.95	10.0
9	18	1932	91.5	1	A	7.30	9.7	1.6	0.666	0.082	0.725	0.00	0.000	16.93	21.9	1.65	9.3
9	18	2036	92.6	1	A	7.30	4.2	2.8	1.270	0.119	0.796	2.06	0.590	6.07	22.1	1.55	12.0
9	18	2137	93.6	1	A	7.30	5.3	2.0	1.420	0.091	0.416	0.00	0.000	13.49	22.9	1.30	16.2

946510522

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	2235	94.6	1	A	7.40	5.4	1.5	0.717	0.096	0.471	0.00	0.000	12.14	22.7	1.35	16.9
9	19	35	96.6	1	A	7.30	6.3	1.0	1.350	0.129	0.438	0.00	0.000	4.05	21.8	1.65	18.4
9	19	154	97.9	1	A	7.40	3.7	0.4	1.230	0.124	0.420	2.10	0.325	4.05	21.5	1.60	19.0
9	19	306	99.1	1	A	7.40	3.5	0.4	1.380	0.086	0.337	0.00	0.000	4.72	22.0	1.30	17.6
9	19	405	100.1	1	A	7.30	3.3	0.6	0.676	0.105	0.639	1.35	0.323	4.05	22.0	1.00	15.9
9	19	507	101.1	1	A	7.30	3.4	0.4	1.020	0.072	0.417	0.00	0.000	7.42	21.6	1.00	14.3
9	19	606	102.1	1	A	7.40	4.0	0.4	1.480	0.100	0.563	2.30	0.448	5.40	21.8	1.35	16.0
9	19	710	103.2	1	A	7.30	3.7	0.4	1.680	0.151	0.776	0.00	0.000	7.42	21.2	1.25	15.0
9	19	806	104.1	1	A	7.30	3.4	0.4	0.940	0.073	0.518	1.44	0.317	5.40	21.0	1.45	12.2
9	19	907	105.1	1	A	7.40	3.8	0.4	1.920	0.169	0.698	0.00	0.000	9.44	21.7	1.95	17.2
9	19	1008	106.1	1	A	7.40	4.7	0.4	1.780	0.167	0.589	2.68	0.444	7.42	22.0	1.70	17.2
9	19	1054	106.9	1	A	7.40	5.3	0.4	0.759	0.040	0.178	0.00	0.000	6.07	21.5	1.60	18.0
9	19	1207	108.1	1	A	7.30	4.0	0.4	1.450	0.152	0.470	2.22	0.378	3.70	21.0	0.00	19.0
9	19	1305	109.1	1	A	7.30	2.7	0.6	1.210	0.128	0.595	0.00	0.000	0.00	22.0	2.15	19.0
9	19	1405	110.1	1	A	7.30	2.9	0.4	1.340	0.133	0.478	2.21	0.401	4.47	22.0	2.00	19.8
9	19	1505	111.1	1	A	7.30	3.0	0.8	1.630	0.140	0.491	0.00	0.000	5.25	21.8	2.25	18.0
9	19	1604	112.1	1	A	7.30	3.0	1.0	1.530	0.162	0.660	2.42	0.423	5.06	22.0	1.75	17.1
9	19	1708	113.1	1	A	7.30	3.1	1.2	1.580	0.152	0.736	0.00	0.000	4.67	22.5	1.55	15.5
9	19	1802	114.0	1	A	7.30	5.6	1.0	1.530	0.138	0.706	2.66	0.559	6.03	22.5	1.35	15.0
9	19	1905	115.1	1	A	7.20	2.8	0.4	1.450	0.129	0.782	0.00	0.000	3.89	22.0	1.05	14.0
9	19	2011	116.2	1	A	7.20	5.0	0.4	1.310	0.124	0.886	2.24	0.467	5.84	22.0	1.00	13.0
9	19	2105	117.1	1	A	7.20	3.6	0.8	1.570	0.137	0.933	0.00	0.000	3.50	21.0	1.25	14.5
9	19	2204	118.1	1	A	7.20	2.8	0.8	0.476	0.133	0.734	1.00	0.242	4.47	21.0	1.80	14.0
9	19	2307	119.1	1	A	7.30	3.7	1.4	1.870	0.162	0.516	0.00	0.000	4.67	22.5	1.75	17.0
9	20	16	120.3	1	A	7.40	5.6	0.0	1.530	0.000	0.000	0.00	0.000	6.07	21.3	1.45	18.9
9	20	111	121.2	1	A	7.10	3.8	0.4	0.977	0.104	0.539	0.00	0.000	2.72	21.1	1.35	18.1

946510523

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POO [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	21	209	122.1	1	A	7.30	6.4	1.0	1.430	0.135	0.496	2.38	0.486	3.11	20.9	2.25	19.2
9	2	310	123.2	1	A	7.30	4.4	0.4	1.350	0.131	0.451	0.00	0.000	1.36	21.1	1.75	19.0
9	2	402	124.0	1	A	7.30	3.1	0.4	1.470	0.135	0.508	2.45	0.476	2.33	21.4	2.15	17.5
9	2	508	125.1	1	A	7.40	3.2	0.4	1.650	0.149	0.746	0.00	0.000	4.86	20.0	2.30	13.5
9	20	605	126.1	1	A	7.30	3.0	0.4	1.550	0.149	0.911	2.93	0.556	4.28	20.8	1.85	12.8
9	2	707	127.1	1	A	7.30	2.8	0.4	1.350	0.131	1.010	0.00	0.000	6.03	20.7	1.60	12.1
9	2	808	128.1	1	A	7.20	4.8	0.4	1.630	0.140	0.647	2.72	0.544	8.09	20.9	1.25	11.9
9	2	918	129.3	1	A	7.30	3.4	0.4	1.620	0.144	1.400	0.00	0.000	7.42	20.7	1.35	11.4
9	2	1008	130.1	1	A	7.20	3.7	0.4	1.120	0.085	0.546	1.91	0.433	1.75	20.9	1.60	12.0
9	2	1104	131.1	1	A	7.40	5.2	0.6	1.480	0.104	0.358	0.00	0.000	14.84	22.0	1.75	16.7
9	2	1204	132.1	1	A	7.40	18.0	1.0	1.610	0.149	0.554	3.42	0.646	6.74	21.5	2.65	16.9
9	2	1307	133.1	1	A	7.40	6.5	1.6	1.440	0.131	0.500	0.00	0.000	5.40	21.0	3.10	18.0
9	20	1407	134.1	1	A	7.40	4.4	1.6	1.180	0.099	0.363	1.77	0.394	3.37	21.0	3.65	17.0
9	2	1503	135.0	1	A	7.40	4.0	1.4	1.400	0.000	0.000	0.00	0.000	4.05	21.0	2.95	18.0
9	2	1607	136.1	1	A	7.40	4.6	1.4	1.660	0.149	0.578	2.76	0.495	8.77	21.0	3.05	17.0
9	2	1702	137.0	1	A	7.40	4.1	1.2	1.770	0.149	0.617	2.77	0.537	6.07	21.0	2.75	16.8
9	2	1806	138.1	1	A	7.40	3.6	1.6	1.710	0.144	0.723	0.00	0.000	8.77	21.0	2.90	15.5
9	2	1908	139.1	1	A	7.30	3.4	1.4	1.450	0.117	0.658	1.96	0.405	5.40	21.0	2.35	14.5
9	2	2005	140.1	1	A	7.40	3.6	1.6	1.670	0.149	0.812	0.00	0.000	5.40	21.0	1.55	13.0
9	2	2105	141.1	1	A	7.30	3.4	0.8	1.460	0.000	0.000	0.00	0.000	5.40	20.5	1.50	13.2
9	2	2208	142.1	1	A	7.30	3.3	1.0	1.530	0.149	1.080	2.47	0.468	5.40	21.0	1.35	11.0
9	20	2303	143.0	1	A	7.40	4.0	1.6	0.969	0.090	0.460	0.00	0.000	3.37	21.0	1.40	13.0
9	21	7	144.1	1	A	7.50	4.5	3.8	1.920	0.158	0.518	0.00	0.000	1.75	21.4	2.45	17.4
9	21	109	145.1	1	A	7.40	13.0	1.4	1.480	0.131	0.451	2.31	0.546	3.50	20.7	2.30	18.6
9	21	212	146.2	1	A	7.40	11.0	2.4	1.440	0.126	0.432	0.00	0.000	2.53	20.6	2.40	19.0
9	21	307	147.1	1	A	7.40	17.0	1.8	0.893	0.114	0.588	2.10	0.445	10.79	20.5	2.25	18.9

946510524

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	21	407	148.1	1	A	7.40	7.1	0.6	1.520	0.131	0.476	0.00	0.000	4.28	20.5	2.30	18.9
9	21	515	149.3	1	A	7.40	6.1	0.4	1.250	0.099	0.363	1.42	0.457	2.92	20.9	1.90	17.5
9	21	605	150.1	1	A	7.40	4.2	0.4	1.110	0.076	0.386	0.00	0.000	3.89	20.6	1.65	15.6
9	21	706	151.1	1	A	7.30	3.3	0.4	1.610	0.140	0.515	2.38	0.456	4.47	20.2	1.35	13.8
9	21	805	152.1	1	A	7.40	4.0	0.8	1.630	0.135	0.616	0.00	0.000	2.92	20.5	1.25	15.1
9	21	904	153.1	1	A	7.40	3.6	0.6	0.843	0.076	0.386	1.31	0.393	4.09	20.2	1.20	14.4
9	21	1004	154.1	1	A	7.30	6.7	0.6	1.360	0.140	0.980	0.00	0.000	2.72	20.2	1.25	13.2
9	21	1102	155.0	1	A	7.40	5.5	0.4	1.180	0.128	0.586	3.51	0.618	3.11	20.6	1.55	17.0
9	21	1205	156.1	1	A	7.30	18.0	1.8	1.600	0.126	0.493	2.59	0.621	14.84	21.0	2.50	17.0
9	21	1306	157.1	1	A	7.30	5.2	1.2	1.730	0.152	0.539	0.00	0.000	5.06	21.5	2.50	17.0
9	21	1404	158.1	1	A	7.30	14.0	1.8	1.160	0.123	0.423	3.21	0.727	7.42	21.0	3.00	17.5
9	21	1506	159.1	1	A	7.30	4.5	1.2	1.450	0.140	0.491	0.00	0.000	2.53	21.0	2.25	17.0
9	21	1607	160.1	1	A	7.40	3.6	0.4	1.330	0.137	0.483	2.57	0.474	4.67	21.0	3.05	18.5
9	21	1705	161.1	1	A	7.40	5.2	0.8	1.590	0.142	0.572	0.00	0.000	4.67	21.0	3.35	17.0
9	21	1804	162.1	1	A	7.30	4.5	0.4	1.610	0.124	0.498	0.00	0.000	2.14	21.5	3.00	16.0
9	21	1905	163.1	1	A	7.30	4.0	2.0	1.630	0.123	0.568	0.00	0.000	5.25	22.0	2.65	15.0
9	21	2006	164.1	1	A	7.30	6.2	0.6	0.980	0.067	0.419	1.63	0.414	6.03	21.5	2.20	15.0
9	21	2107	165.1	1	A	7.30	3.2	1.2	1.570	0.140	0.780	0.00	0.000	2.72	20.5	2.45	13.5
9	21	2205	166.1	1	A	7.30	3.0	0.4	1.540	0.138	0.806	2.05	0.487	2.92	20.5	2.00	13.0
9	21	2250	166.8	1	A	7.30	2.9	1.0	1.560	0.142	0.855	0.00	0.000	3.11	20.0	1.95	13.5
9	21	2347	167.8	1	A	7.30	15.0	2.8	1.200	0.123	0.544	2.86	0.677	5.40	20.8	2.10	14.1
9	22	48	168.8	1	A	7.40	6.3	1.6	1.660	0.067	0.235	0.00	0.000	6.07	21.0	2.35	18.0
9	22	149	169.8	1	A	7.40	5.3	0.8	1.030	0.100	0.332	2.51	0.479	4.05	21.3	2.65	17.9
9	22	250	170.8	1	A	7.40	5.4	0.8	0.787	0.076	0.285	0.00	0.000	4.05	20.9	2.70	18.5
9	22	354	171.9	1	A	7.40	5.1	0.6	1.070	0.095	0.325	2.20	0.419	5.40	20.6	2.70	19.2
9	22	453	172.9	1	A	7.40	6.2	1.4	0.975	0.095	0.478	0.00	0.000	8.77	20.8	2.65	18.2

946510525

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	22	553	173.9	1	A	7.40	4.6	1.0	1.230	0.104	0.398	2.36	0.456	5.40	20.9	2.35	17.8
9	22	652	174.9	1	A	7.40	5.5	1.6	0.674	0.090	0.365	0.00	0.000	4.72	20.8	2.20	16.9
9	22	747	175.8	1	A	7.40	4.3	0.8	0.830	0.062	0.228	2.05	0.475	5.40	20.5	1.85	15.3
9	22	846	176.8	1	A	7.40	4.1	0.8	0.889	0.039	0.227	0.00	0.000	4.05	20.5	1.85	16.2
9	22	945	177.8	1	A	7.40	3.8	0.6	0.492	0.053	0.237	1.41	0.356	4.05	20.5	1.65	16.0
9	22	1046	178.8	1	A	7.40	4.2	0.5	0.961	0.072	0.407	0.00	0.000	5.4[illegible]	20.4	1.65	13.4
9	22	1203	180.0	1	A	7.30	7.5	4.2	1.500	0.142	0.714	2.64	0.528	3.89	21.0	2.35	14.5
9	22	1306	181.1	1	A	7.40	4.7	1.6	0.873	0.076	0.473	0.00	0.000	3.70	21.5	2.50	17.0
9	22	1405	182.1	1	A	7.40	4.8	1.2	1.560	0.152	0.515	2.61	0.501	3.31	21.5	2.95	18.0
9	22	1502	183.0	1	A	7.40	4.4	1.2	1.380	0.142	0.596	0.00	0.000	4.67	21.0	3.30	19.0
9	22	1608	184.1	1	A	7.40	4.6	0.6	1.280	0.142	0.478	3.05	0.568	3.70	21.0	3.45	19.5
9	22	1704	185.1	1	A	7.40	4.7	0.6	1.340	0.142	0.478	0.00	0.000	4.09	21.0	3.25	19.8
9	22	1803	186.0	1	A	7.60	4.9	1.0	1.470	0.152	0.586	3.15	0.596	3.11	21.0	3.05	18.0
9	22	1908	187.1	1	A	7.40	5.5	2.4	1.580	0.152	0.610	0.00	0.000	3.89	21.0	3.00	17.0
9	22	2006	188.1	1	A	7.40	6.0	4.0	1.380	0.147	0.638	3.12	0.771	3.31	21.0	2.85	16.5
9	22	2104	189.1	1	A	7.40	4.7	1.0	1.550	0.147	0.567	0.00	0.000	4.48	20.5	2.95	15.2
9	22	2204	190.1	1	A	7.40	4.8	1.2	1.150	0.142	0.678	3.00	0.615	3.70	20.5	2.05	14.2
9	22	2247	190.8	1	A	7.40	4.7	1.2	1.600	0.142	0.620	0.00	0.000	2.92	20.5	2.00	0.0
9	22	2349	191.8	1	A	7.30	4.8	0.8	0.670	0.114	0.906	1.51	0.389	3.70	20.5	1.75	13.3
9	23	47	192.8	1	A	7.30	4.7	0.8	1.380	0.119	0.595	0.00	0.000	3.37	20.5	1.70	13.6
9	23	148	193.8	1	A	7.40	4.5	1.8	1.400	0.161	0.577	3.40	0.707	3.50	20.9	2.35	14.6
9	23	249	194.8	1	A	7.40	4.8	0.6	1.460	0.133	0.440	0.00	0.000	2.72	21.9	2.55	17.1
9	23	350	195.8	1	A	7.40	4.7	0.6	1.380	0.104	0.351	2.65	0.485	4.72	21.1	2.65	18.0
9	23	448	196.8	1	A	7.40	5.3	3.0	0.829	0.067	0.211	0.00	0.000	3.37	20.9	2.10	18.5
9	23	546	197.8	1	A	7.40	4.2	0.8	1.050	0.119	0.407	3.56	0.671	3.31	20.8	2.55	18.9
9	23	647	198.8	1	A	7.30	4.2	1.0	1.090	0.095	0.348	0.00	0.000	4.28	21.2	2.10	17.8

94510526

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	23	747	199.8	1	A	7.30	4.2	1.2	1.070	0.095	0.395	3.87	0.958	2.53	20.8	2.00	17.1
9	23	845	200.8	1	A	7.40	4.3	0.6	1.420	0.133	0.499	0.00	0.000	2.02	20.5	1.95	15.5
9	23	947	201.9	1	A	7.40	4.8	0.4	1.340	0.147	0.567	4.23	0.713	2.70	19.9	2.15	13.9
9	23	1048	202.8	1	A	7.40	4.6	1.9	0.687	0.114	0.706	0.00	0.000	3.89	19.9	2.25	13.0
9	23	1203	204.0	1	A	7.40	5.4	1.0	0.544	0.094	0.772	2.21	0.401	3.50	21.0	2.85	0.0
9	23	1305	205.1	1	A	7.40	5.4	1.2	1.440	0.136	0.622	0.00	0.000	1.56	20.0	2.35	13.0
9	23	1404	206.1	1	A	7.40	5.5	1.0	1.470	0.146	0.617	2.75	0.666	2.33	20.5	2.50	16.5
9	23	1506	207.1	1	A	7.50	5.5	1.6	1.640	0.155	0.593	0.00	0.000	2.33	21.0	3.65	17.0
9	23	1603	208.0	1	A	7.50	6.6	1.2	1.270	0.146	0.517	2.87	0.726	2.92	20.0	3.50	18.0
9	23	1708	209.1	1	A	7.50	5.5	1.0	1.400	0.146	0.508	0.00	0.000	1.56	20.0	3.60	19.0
9	23	1806	210.1	1	A	7.50	5.8	3.0	1.520	0.146	0.552	2.59	0.763	1.75	20.0	3.75	18.0
9	23	1904	211.1	1	A	7.60	5.5	1.2	0.000	0.000	0.000	0.00	0.000	4.47	20.0	3.50	18.0
9	23	2035	212.6	1	A	7.40	4.8	1.0	1.420	0.108	0.554	1.91	0.564	1.36	19.5	3.25	16.5
9	23	2205	214.1	1	A	7.40	4.8	1.0	1.480	0.146	0.764	0.00	0.000	2.05	19.5	3.15	15.0
9	23	2343	215.7	1	A	7.50	5.0	0.8	0.908	0.080	0.359	1.98	0.594	7.42	19.5	2.47	14.1
9	24	112	217.2	1	A	7.30	5.2	1.0	0.760	0.080	0.457	0.00	0.000	6.74	19.0	2.25	11.8
9	24	244	218.7	1	A	7.40	4.8	0.8	1.390	0.136	0.514	2.27	0.627	9.44	20.7	3.30	16.9
9	24	342	219.7	1	A	7.40	4.8	0.8	1.120	0.080	0.294	0.00	0.000	9.44	20.4	4.15	17.6
9	24	445	220.8	1	A	7.50	5.5	0.6	0.778	0.089	0.322	1.68	0.478	8.09	19.9	3.60	19.2
9	24	544	221.7	1	A	7.50	5.3	1.2	0.846	0.070	0.277	0.00	0.000	6.74	19.5	3.65	19.6
9	24	644	222.7	1	A	7.40	5.3	1.0	0.991	0.099	0.342	2.02	0.504	9.44	19.6	3.80	18.9
9	24	742	223.7	1	A	7.40	5.3	1.2	1.170	0.099	0.416	0.00	0.000	7.42	19.3	3.65	16.6
9	24	845	224.9	1	A	7.40	5.2	1.0	1.090	0.080	0.356	1.74	0.532	6.07	19.6	3.25	16.4
9	24	942	225.7	1	A	7.40	5.0	0.8	1.060	0.127	0.600	0.00	0.000	5.40	19.5	3.00	16.0
9	24	1042	226.7	1	A	7.40	5.5	0.7	1.450	0.136	0.740	1.73	0.482	8.77	19.2	2.85	14.7
9	24	1203	228.0	1	A	7.30	5.0	2.2	1.500	0.146	0.810	1.85	0.502	4.47	20.5	3.75	13.0

946510527

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	24	1305	229.1	1	A	7.40	4.6	2.0	1.080	0.127	0.755	0.00	0.000	5.84	19.5	3.05	13.5
9	24	1402	230.[illegible]	1	A	7.30	5.5	1.8	1.430	0.146	0.964	1.86	0.533	3.89	19.5	2.85	13.0
9	24	1507	231.1	1	A	7.40	5.0	2.0	1.660	0.165	0.632	0.00	0.000	4.72	19.5	3.25	17.0
9	24	1606	232.1	1	A	7.50	5.2	2.0	1.520	0.160	0.583	2.54	0.518	7.42	19.5	4.15	18.0
9	24	1704	233.1	1	A	7.60	5.6	1.6	1.410	0.151	0.517	0.00	0.000	6.74	19.5	4.50	19.0
9	24	1802	234.[illegible]	1	A	7.60	4.4	2.0	1.320	0.151	0.533	1.91	0.514	6.74	19.5	4.25	19.0
9	24	1907	235.1	1	A	7.60	5.3	1.6	1.360	0.151	0.516	0.00	0.000	4.72	19.0	4.05	19.5
9	24	2035	236.6	1	A	7.50	4.3	1.4	1.670	0.155	0.603	2.43	0.552	4.72	19.0	4.05	19.5
9	24	2205	238.1	1	A	7.50	4.7	1.8	1.530	0.155	0.602	0.00	0.000	5.06	19.0	3.90	18.5
9	24	2335	239.6	1	A	7.60	5.0	3.7	1.400	0.156	0.744	0.00	0.000	3.38	18.9	3.35	15.8
9	25	106	241.1	1	A	7.40	5.0	1.2	1.370	0.151	0.889	3.05	0.716	3.37	18.7	2.75	14.4
9	25	237	242.6	1	A	7.30	5.4	2.8	1.420	0.146	0.629	0.00	0.000	4.05	18.6	2.75	13.9
9	25	335	243.6	1	A	7.40	5.3	2.0	1.370	0.160	0.764	3.77	1.270	2.70	19.0	3.15	16.8
9	25	434	244.6	1	A	7.60	4.8	1.6	1.040	0.127	0.535	1.71	0.534	4.72	19.2	4.05	18.9
9	25	538	245.6	1	A	7.60	4.7	1.6	0.000	0.000	0.000	0.00	0.000	3.37	18.8	4.30	19.4
9	25	637	246.6	1	A	7.60	4.8	2.0	0.980	0.103	0.364	0.00	0.000	5.40	18.5	3.85	19.7
9	25	736	247.6	1	A	7.50	4.4	2.8	1.230	0.151	0.300	2.24	0.550	4.72	18.4	3.30	20.0
9	25	834	248.6	1	A	7.60	4.8	1.2	1.380	0.156	0.525	0.00	0.000	2.02	18.5	4.00	19.5
9	25	936	249.6	1	A	7.60	5.0	2.0	0.844	0.066	0.249	1.53	0.450	4.05	19.0	4.00	19.1
9	25	1035	250.6	1	A	7.70	4.7	2.2	0.865	0.108	0.415	0.00	0.000	6.07	19.0	3.65	18.4
		AVERAGE READING				7.35	4.9	1.5	1.333	0.122	0.559	2.37	0.511	6.07	21.4	2.02	15.6

94510528

STØRM #2

KEARNY

PØINT

9-15/9-25-81

2/3 DEPTH

946510529

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1250	12.8	1	B	7.40	4.5	1.2	1.610	0.144	0.466	2.54	0.484	7.42	24.0	2.40	18.1
9	15	1345	13.8	1	B	7.40	4.6	2.4	1.430	0.125	0.454	NA	NA	14.16	24.2	2.15	17.5
9	15	1452	14.9	1	B	7.40	5.0	1.2	1.730	0.134	0.591	NA	NA	6.74	24.2	2.05	17.2
9	15	1554	15.9	1	B	7.30	4.3	0.6	1.760	0.134	0.665	NA	NA	11.46	23.8	1.25	14.6
9	15	1701	17.0	1	B	7.30	4.2	1.0	1.540	0.125	0.747	NA	NA	15.50	23.9	1.35	15.1
9	15	1753	17.9	1	B	7.20	6.0	1.2	1.290	0.080	0.562	NA	NA	8.09	23.9	1.60	15.0
9	15	1852	18.9	1	B	7.40	6.3	1.2	1.910	0.162	0.480	NA	NA	8.09	24.7	2.30	17.6
9	15	1950	19.8	1	B	7.40	13.0	2.4	1.000	0.093	0.465	NA	NA	4.72	24.0	2.40	18.0
9	15	2052	20.9	1	B	7.40	5.6	2.2	1.290	0.121	0.458	2.43	0.499	8.77	23.3	2.60	18.9
9	15	2207	22.1	1	B	7.50	5.4	4.0	1.560	0.139	0.440	NA	NA	9.44	23.0	2.10	19.8
9	15	2250	22.8	1	B	7.50	3.9	2.4	0.873	0.080	0.279	1.57	0.320	8.77	23.0	2.50	19.0
9	15	2355	23.9	1	B	7.50	3.5	1.6	1.270	0.102	0.330	NA	NA	4.72	24.0	2.00	17.2
9	16	106	25.1	1	B	7.30	5.3	1.8	0.994	0.070	0.226	1.77	0.388	7.42	24.0	1.30	17.8
9	16	201	26.0	1	B	7.30	4.1	2.2	1.460	0.130	0.491	NA	NA	8.09	24.0	0.75	17.6
9	16	303	27.0	1	B	7.30	3.7	1.8	1.740	0.144	0.581	2.80	0.510	4.05	24.0	0.62	15.0
9	16	405	28.1	1	B	7.40	6.8	1.8	1.480	0.134	0.445	NA	NA	5.64	24.0	0.75	17.0
9	16	504	29.1	1	B	7.20	3.7	2.0	1.640	0.130	0.836	NA	NA	NA	23.8	0.83	17.2
9	16	607	30.1	1	B	7.30	4.4	2.4	1.370	0.130	0.532	2.29	0.424	6.07	23.2	0.95	17.8
9	16	705	31.1	1	B	7.30	7.8	2.2	1.420	0.144	0.456	NA	NA	2.02	23.2	1.00	17.5
9	16	806	32.1	1	B	7.30	8.2	2.8	1.480	0.144	0.456	3.91	0.621	6.07	23.8	1.20	17.0
9	16	923	33.4	1	B	7.40	9.6	3.6	1.280	0.134	0.413	NA	NA	5.64	23.0	1.80	18.6
9	16	1039	34.6	1	B	7.40	5.7	2.8	0.945	0.098	0.324	1.62	0.373	6.07	22.9	1.60	19.2
9	16	1215	36.3	1	B	7.50	6.3	1.6	1.170	0.139	0.419	2.13	0.425	7.42	22.5	1.80	17.8
9	16	1314	37.2	1	B	7.40	5.2	2.0	1.300	0.144	0.456	NA	NA	5.45	23.2	1.40	16.2
9	16	1410	38.2	1	B	7.40	5.6	2.2	1.120	0.070	0.278	1.97	0.411	10.79	23.4	0.75	15.6
9	16	1509	39.1	1	B	7.30	5.2	2.2	1.260	0.084	0.390	NA	NA	10.79	23.4	1.00	13.7

946510530

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PP	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	16	1615	40.3	1	B	7.30	5.2	2.0	1.560	0.144	0.550	2.52	0.486	10.12	23.2	1.15	15.0
9	16	1716	41.3	1	B	7.30	4.8	2.4	1.640	0.153	0.708	NA	NA	12.14	23.1	0.85	13.8
9	16	1817	42.3	1	B	7.30	5.3	2.2	0.699	0.093	0.632	1.36	0.425	16.86	22.9	0.90	11.9
9	16	1922	43.4	1	B	7.40	5.3	2.2	1.370	0.098	0.366	NA	NA	9.44	23.6	1.70	15.4
9	16	2020	44.3	1	B	7.30	5.6	1.8	0.931	0.048	0.227	1.43	0.370	8.09	23.5	1.30	15.9
9	16	2125	45.4	1	B	7.40	7.2	2.0	1.150	0.107	0.357	NA	NA	6.07	22.4	1.75	17.0
9	16	2230	46.5	1	B	7.40	5.6	2.6	0.624	0.057	0.354	1.24	0.297	10.12	22.5	1.90	17.2
9	16	2330	47.5	1	B	7.40	4.0	0.4	1.360	0.102	0.330	NA	NA	5.40	22.2	1.50	16.9
9	17	30	48.5	1	B	7.30	3.5	0.4	1.210	0.134	0.413	2.10	0.414	6.74	22.5	1.70	17.8
9	17	128	49.5	1	B	7.30	5.2	1.6	1.450	0.153	0.520	NA	NA	11.46	23.1	1.00	16.9
9	17	229	50.5	1	B	7.30	5.5	1.0	1.750	0.144	0.581	2.89	0.831	5.45	23.1	0.55	15.1
9	17	328	51.5	1	B	7.30	4.6	0.8	1.270	0.093	0.391	NA	NA	7.39	22.8	0.30	13.0
9	17	432	52.5	1	B	7.30	6.5	3.0	1.500	0.139	0.513	2.99	0.898	14.16	22.8	0.50	13.0
9	17	527	53.4	1	B	7.20	4.4	4.4	1.610	0.139	0.450	NA	NA	11.46	22.3	0.47	13.2
9	17	629	54.5	1	B	7.20	4.2	0.8	1.490	0.153	1.140	2.91	0.583	11.46	22.0	0.40	13.9
9	17	732	55.5	1	B	7.20	4.7	1.0	1.440	0.102	0.445	NA	NA	10.12	22.8	0.50	15.3
9	17	833	56.5	1	B	7.30	7.3	0.6	1.220	0.107	0.346	2.35	0.493	13.49	23.0	0.80	15.8
9	17	932	57.5	1	B	7.30	3.2	0.4	1.580	0.144	0.456	NA	NA	5.40	22.0	1.30	17.4
9	17	1029	58.5	1	B	7.40	3.0	0.4	NA	NA	NA	NA	NA	4.67	22.0	1.45	17.8
9	17	1225	60.4	1	B	7.10	1.7	4.6	1.170	0.125	0.485	1.78	0.426	5.40	22.1	1.60	17.9
9	17	1330	61.5	1	B	7.20	2.0	2.6	1.450	0.144	0.498	NA	NA	10.12	22.6	1.65	16.1
9	17	1426	62.4	1	B	7.20	2.2	2.8	1.290	0.137	0.610	NA	NA	12.14	22.9	1.35	15.6
9	17	1530	63.5	1	B	7.20	2.4	2.6	1.700	0.119	0.508	NA	NA	9.44	22.8	1.35	14.0
9	17	1634	64.6	1	B	7.20	2.6	2.6	1.640	0.148	0.682	2.56	0.558	12.14	22.7	1.15	13.0
9	17	1727	65.4	1	B	7.20	2.6	2.8	1.480	0.153	0.887	NA	NA	8.09	22.5	0.95	13.5
9	17	1830	66.5	1	B	7.20	2.8	2.6	1.300	0.080	0.760	2.41	0.475	13.49	22.0	1.10	10.5

946510531

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	17	1928	67.5	1	B	7.20	2.9	3.2	1.600	0.151	0.949	NA	NA	19.56	22.3	1.05	11.4
9	17	2026	68.4	1	B	7.30	2.8	2.2	1.920	0.132	0.543	3.08	0.559	10.12	23.2	1.45	16.0
9	17	2126	69.4	1	B	7.30	3.4	3.0	0.836	0.112	0.571	NA	NA	6.74	23.9	1.55	16.8
9	17	2234	70.6	1	B	7.30	2.7	3.0	0.768	0.073	0.277	1.16	0.296	2.33	22.1	1.85	18.1
9	17	2345	71.8	1	B	7.40	4.4	2.0	1.340	0.137	0.442	NA	NA	2.72	22.0	1.70	19.0
9	18	47	72.8	1	B	7.40	3.4	1.8	1.000	0.119	0.460	1.62	0.346	1.94	21.8	1.30	18.9
9	18	154	73.9	1	B	7.30	5.4	2.0	1.410	0.137	0.466	NA	NA	6.74	22.1	1.00	18.7
9	18	257	74.9	1	B	7.30	3.4	2.2	1.220	0.109	0.686	1.34	0.300	8.77	22.5	0.78	15.7
9	18	357	75.9	1	B	7.30	3.0	1.8	1.250	0.096	0.435	NA	NA	9.44	22.5	0.50	14.3
9	18	457	76.9	1	B	7.30	2.8	0.8	1.430	0.142	0.485	2.18	0.418	10.12	22.1	0.40	17.0
9	18	557	77.9	1	B	7.30	4.7	1.8	1.450	0.132	0.459	NA	NA	12.81	22.2	0.50	15.4
9	18	659	79.0	1	B	7.30	3.6	1.0	1.500	0.155	0.955	2.62	0.487	9.44	22.0	0.65	18.0
9	18	750	79.8	1	B	7.30	1.9	1.2	1.480	0.132	0.471	NA	NA	8.77	21.9	1.00	17.5
9	18	858	81.0	1	B	7.30	5.3	1.4	0.982	0.091	0.476	2.36	NA	11.46	23.0	0.78	17.8
9	18	957	81.9	1	B	7.30	5.0	1.0	1.300	0.114	0.525	NA	NA	4.28	22.8	0.80	17.2
9	18	1050	82.8	1	B	7.40	5.1	1.3	1.180	0.137	0.430	2.45	0.632	5.45	22.1	1.25	18.7
9	18	1220	84.3	1	B	7.20	5.5	2.4	1.090	0.114	0.345	1.85	0.450	6.74	21.9	1.50	18.9
9	18	1323	85.4	1	B	7.30	4.2	1.8	1.310	0.132	0.411	NA	NA	4.72	22.0	1.80	18.5
9	18	1425	86.4	1	B	7.30	3.8	0.8	0.584	0.146	0.529	1.19	0.315	13.49	22.5	1.35	17.8
9	18	1526	87.4	1	B	7.20	4.0	1.4	1.690	0.146	0.541	NA	NA	15.51	23.0	1.10	16.8
9	18	1626	88.4	1	B	7.30	3.2	1.6	1.560	0.146	0.613	2.60	0.531	10.79	22.5	0.90	14.0
9	18	1725	89.4	1	B	7.30	3.8	1.6	1.410	0.109	0.470	NA	NA	12.14	22.3	0.85	16.0
9	18	1824	90.4	1	B	7.20	3.7	1.8	1.610	0.155	0.688	2.37	0.466	11.47	22.1	1.45	14.0
9	18	1925	91.4	1	B	7.20	5.4	2.4	1.160	0.082	0.473	NA	NA	14.16	22.0	1.15	14.0
9	18	2029	92.5	1	B	7.20	4.2	3.0	1.390	0.137	0.694	2.49	0.735	11.47	22.0	1.20	17.0
9	18	2133	93.5	1	B	7.30	4.0	2.0	1.670	0.151	0.500	NA	NA	7.42	22.9	1.35	17.4

946510532

KEARNY POINT-LEVEL 5-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	2230	94.5	1	B	7.30	5.6	2.5	0.592	0.059	0.303	0.92	0.297	14.84	22.3	1.65	17.9
9	19	30	96.5	1	B	7.30	8.8	0.4	1.100	0.105	0.328	NA	NA	5.40	21.7	1.75	17.6
9	19	147	97.8	1	B	7.30	39.0	1.4	1.140	0.128	0.379	2.06	0.487	11.29	21.2	1.45	19.5
9	19	300	99.0	1	B	7.40	22.0	0.4	0.675	0.082	0.341	NA	NA	6.74	21.8	1.60	18.7
9	19	359	100.0	1	B	7.40	14.0	3.6	NA	NA	NA	NA	NA	8.09	22.0	1.20	15.3
9	19	501	101.0	1	B	7.30	12.0	1.4	1.330	0.133	0.489	NA	NA	10.79	21.9	1.00	15.4
9	19	600	102.0	1	B	7.30	4.2	0.4	1.380	0.132	0.483	2.22	0.581	6.74	21.5	1.37	18.5
9	19	702	103.0	1	B	7.30	6.6	3.0	1.480	0.128	0.403	NA	NA	5.40	21.5	1.37	18.2
9	19	759	104.0	1	B	7.20	5.6	0.8	1.540	0.138	0.506	2.37	0.565	6.74	21.3	1.45	18.7
9	19	901	105.0	1	B	7.30	3.8	0.6	1.570	0.142	0.521	NA	NA	6.74	21.5	1.60	17.5
9	19	1000	106.0	1	B	7.30	6.8	0.6	1.500	0.137	0.442	2.53	0.656	8.77	21.7	1.55	18.0
9	19	1048	106.8	1	B	7.40	7.9	0.9	0.997	0.073	0.338	NA	NA	11.47	21.5	1.50	18.7
9	19	1203	108.0	1	B	7.30	5.5	0.4	1.280	0.133	0.423	1.92	0.449	4.86	21.0	2.05	19.5
9	19	1302	109.0	1	B	7.40	4.4	0.6	1.280	0.133	0.411	NA	NA	19.56	21.5	2.00	19.8
9	19	1403	110.0	1	B	7.30	4.2	0.4	1.060	0.124	0.409	2.03	0.440	3.31	21.2	1.85	20.0
9	19	1500	111.0	1	B	7.40	3.5	1.0	1.270	0.131	0.439	NA	NA	5.40	21.0	1.95	19.5
9	19	1601	112.0	1	B	7.30	3.3	1.0	0.351	0.105	0.517	1.30	0.294	8.77	22.2	1.50	19.0
9	19	1704	113.1	1	B	7.30	3.3	0.4	1.620	0.133	0.556	NA	NA	11.46	22.0	1.45	17.0
9	19	1800	114.0	1	B	7.40	3.5	0.6	1.530	0.148	0.496	2.05	0.424	5.84	22.5	1.05	18.5
9	19	1902	115.0	1	B	7.30	3.7	1.0	1.450	0.100	0.455	NA	NA	3.69	21.5	1.15	19.0
9	19	2008	116.1	1	B	7.30	4.7	1.4	0.872	0.067	0.444	1.41	0.344	4.47	22.0	1.10	17.2
9	19	2102	117.0	1	B	7.20	6.5	1.0	1.400	0.138	0.484	NA	NA	5.64	21.0	1.55	16.5
9	19	2201	118.0	1	B	7.30	5.4	1.6	0.406	0.052	0.481	0.35	0.251	14.16	21.5	1.50	17.0
9	19	2303	119.0	1	B	7.30	4.6	1.4	1.400	0.148	0.474	NA	NA	5.25	22.0	1.50	19.0
9	20	14	120.2	1	B	7.40	18.0	NA	NA	NA	NA	NA	NA	NA	21.2	1.40	19.1
9	20	109	121.1	1	B	7.40	5.1	0.8	1.470	NA	0.691	NA	NA	3.89	21.1	1.60	19.1

946510533

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O. [PPM]	SAL [PPT]
9	20	208	122.1	1	B	7.40	4.0	0.4	0.939	0.140	0.491	1.82	0.369	1.75	21.0	2.05	19.2
9	20	308	123.1	1	B	7.50	8.5	1.0	1.390	0.135	0.447	NA	NA	4.08	20.9	1.80	19.9
9	20	400	124.0	1	B	7.40	6.2	0.4	1.200	0.140	0.467	2.85	0.493	2.72	21.0	2.10	19.4
9	20	506	125.1	1	B	7.40	3.8	0.4	1.500	0.140	0.491	NA	NA	3.11	21.0	2.30	16.3
9	20	603	126.0	1	B	7.40	4.0	2.4	1.680	0.154	0.585	3.02	0.531	4.08	21.2	1.65	14.1
9	20	705	127.1	1	B	7.30	3.4	0.4	1.670	0.135	0.652	NA	NA	2.92	21.1	1.40	13.3
9	20	805	128.1	1	B	7.30	5.4	0.4	0.974	0.081	0.345	1.74	0.336	6.07	21.5	1.45	16.1
9	20	916	129.3	1	B	7.10	7.0	0.4	1.700	0.131	0.476	NA	NA	5.40	21.5	1.55	16.9
9	20	1006	130.1	1	B	7.30	5.0	0.4	1.610	0.140	0.563	2.51	0.539	2.72	21.3	1.60	17.0
9	20	1102	131.0	1	B	7.40	5.6	0.4	1.670	0.140	0.491	NA	NA	2.14	21.9	1.55	18.1
9	20	1201	132.0	1	B	7.40	5.0	NA	1.510	0.140	0.479	NA	NA	4.05	21.0	2.45	18.0
9	20	1304	133.1	1	B	7.40	7.6	1.4	1.440	0.135	0.460	NA	NA	5.06	21.0	3.25	18.1
9	20	1405	134.1	1	B	7.50	6.1	1.4	1.240	0.122	0.400	2.02	0.453	3.50	21.0	3.75	19.0
9	20	1500	135.0	1	B	7.40	5.6	2.0	1.370	NA	NA	NA	NA	4.86	20.5	3.00	18.5
9	20	1605	136.1	1	B	7.50	5.4	1.6	1.360	0.131	0.451	2.29	0.438	3.11	20.5	2.85	18.5
9	20	1700	137.0	1	B	7.40	5.0	1.2	1.580	0.140	0.503	NA	NA	6.22	21.0	2.50	17.0
9	20	1804	138.1	1	B	7.40	4.5	1.4	1.320	0.135	0.508	2.44	0.506	2.53	21.0	2.95	19.0
9	20	1905	139.1	1	B	7.40	4.4	1.8	NA	NA	NA	NA	NA	4.47	21.0	2.65	18.5
9	20	2001	140.0	1	B	7.40	5.1	2.4	0.632	0.067	0.459	1.64	0.396	5.45	21.0	2.05	17.2
9	20	2103	141.0	1	B	7.40	6.0	1.2	0.819	0.072	0.282	NA	NA	5.06	20.5	1.92	18.8
9	20	2204	142.1	1	B	7.40	6.9	2.0	1.460	0.131	0.464	2.86	0.591	1.95	21.0	1.60	16.1
9	20	2300	143.0	1	B	7.40	6.3	1.8	0.981	0.122	0.485	NA	NA	1.95	20.5	1.65	17.8
9	21	5	144.1	1	B	7.30	4.2	1.0	1.570	0.144	0.559	2.51	0.544	4.67	21.0	2.55	18.0
9	21	106	145.1	1	B	7.40	7.7	0.8	0.880	0.072	0.312	NA	NA	2.92	20.5	2.55	19.8
9	21	211	146.2	1	B	7.30	14.0	1.2	1.570	0.090	0.318	2.51	0.573	4.72	20.3	2.30	19.2
9	21	305	147.1	1	B	7.40	13.0	0.8	1.390	0.131	0.427	NA	NA	7.42	20.1	2.40	19.7

946510534

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	21	405	148.1	1	B	7.40	7.1	0.6	1.220	0.144	0.414	2.70	0.504	4.67	20.3	2.40	19.9
9	21	513	149.2	1	B	7.30	7.6	1.6	1.120	0.144	0.679	NA	NA	3.89	20.6	2.05	19.0
9	21	603	150.0	1	B	7.30	3.6	0.4	1.590	0.140	0.539	3.31	0.535	3.70	20.5	1.75	16.5
9	21	704	151.1	1	B	7.30	4.1	0.4	1.530	0.135	0.736	NA	NA	1.95	20.4	1.60	15.9
9	21	803	152.0	1	B	7.30	5.0	1.4	0.774	0.058	0.260	1.59	0.482	4.86	20.5	1.65	18.3
9	21	901	153.0	1	B	7.30	6.0	1.0	0.617	0.058	0.176	NA	NA	2.72	20.6	1.85	18.9
9	21	1002	154.0	1	B	7.40	6.5	0.4	0.957	0.062	0.184	1.36	0.412	3.89	20.8	1.75	18.5
9	21	1100	155.0	1	B	7.30	7.9	1.3	1.520	0.076	0.308	NA	NA	4.67	20.6	1.75	18.8
9	21	1202	156.0	1	B	7.40	14.0	1.2	1.740	0.144	0.463	2.90	0.565	1.17	21.0	2.75	18.6
9	21	1304	157.1	1	B	7.40	17.0	1.0	1.430	0.142	0.502	NA	NA	3.11	21.0	2.40	18.0
9	21	1400	158.0	1	B	7.40	6.7	1.2	1.210	0.131	0.415	2.50	0.471	3.70	21.0	2.85	19.5
9	21	1503	159.0	1	B	7.40	6.7	0.8	1.270	0.137	0.507	NA	NA	2.14	21.0	2.45	20.0
9	21	1604	160.1	1	B	7.40	4.4	0.6	1.240	0.137	0.518	2.57	0.444	1.95	21.0	3.00	19.5
9	21	1700	161.0	1	B	7.40	4.3	0.4	1.340	0.137	0.483	NA	NA	3.50	21.0	2.75	19.5
9	21	1801	162.0	1	B	7.30	4.2	0.4	1.280	0.142	0.537	3.21	0.516	2.14	21.5	2.85	18.0
9	21	1902	163.0	1	B	7.30	4.6	0.4	0.764	0.099	0.339	NA	NA	1.95	22.0	2.40	17.1
9	21	2003	164.0	1	B	7.30	3.9	0.4	0.705	0.088	0.434	1.57	0.413	3.31	21.5	2.00	15.5
9	21	2104	165.1	1	B	7.30	5.4	1.0	1.350	0.140	0.467	NA	NA	3.70	20.5	1.95	17.1
9	21	2202	166.0	1	B	7.30	4.4	1.0	1.440	0.140	0.515	2.76	0.492	4.05	20.5	1.85	16.0
9	21	2245	166.8	1	B	7.30	4.8	1.9	1.510	0.135	0.496	NA	NA	5.40	20.0	1.50	16.5
9	21	2345	167.8	1	B	7.40	3.4	1.6	0.967	0.094	0.344	3.08	0.693	8.10	20.6	1.95	18.5
9	22	46	168.8	1	B	7.40	6.3	1.0	0.896	0.057	0.257	NA	NA	6.07	21.1	2.30	18.1
9	22	147	169.8	1	B	7.40	14.0	1.8	0.867	0.081	0.303	3.25	0.725	6.74	21.3	2.60	18.2
9	22	248	170.8	1	B	7.40	12.0	5.0	0.781	0.067	0.365	NA	NA	8.77	21.7	2.80	19.0
9	22	352	171.9	1	B	7.40	14.0	6.4	1.070	0.109	0.417	2.34	0.421	4.72	20.3	2.25	19.9
9	22	459	172.9	1	B	7.50	8.5	0.4	0.757	0.062	0.240	NA	NA	5.40	20.5	2.60	19.9

946510535

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	22	550	173.8	1	B	7.50	5.5	0.6	1.070	0.081	0.309	1.95	0.416	2.02	20.9	2.45	18.1
9	22	650	174.8	1	B	7.40	4.8	0.4	1.530	0.095	0.407	NA	NA	6.74	20.9	2.20	17.5
9	22	746	175.8	1	B	7.40	6.1	0.4	0.925	0.076	0.354	1.61	0.396	6.07	20.8	2.45	19.0
9	22	845	176.8	1	B	7.40	13.0	0.4	0.745	0.067	0.317	NA	NA	6.74	20.8	1.90	18.9
9	22	944	177.7	1	B	7.40	6.8	0.4	1.030	0.067	0.329	2.23	0.386	7.42	20.9	1.95	18.2
9	22	1045	178.8	1	B	7.40	4.2	0.4	1.440	0.114	0.553	NA	NA	6.74	20.9	1.75	18.0
9	22	1200	180.0	1	B	7.40	6.2	1.4	1.350	0.133	0.581	3.48	0.599	7.42	21.0	2.15	18.5
9	22	1303	181.0	1	B	7.40	4.8	1.6	1.590	0.142	0.596	NA	NA	6.74	21.5	2.60	18.5
9	22	1401	182.0	1	B	7.40	5.4	1.2	1.350	0.147	0.520	3.16	0.574	5.40	21.0	3.00	18.5
9	22	1500	183.0	1	B	7.40	7.2	2.0	1.440	0.076	0.308	NA	NA	4.72	21.0	3.15	19.5
9	22	1606	184.1	1	B	7.40	4.3	1.0	1.290	0.133	0.487	2.40	0.409	4.72	21.0	2.85	19.5
9	22	1700	185.0	1	B	7.40	3.7	0.8	1.250	0.133	0.534	NA	NA	4.05	21.0	3.35	20.0
9	22	1800	186.0	1	B	7.50	5.0	3.0	1.240	0.142	0.513	4.32	0.817	5.40	21.0	3.25	19.5
9	22	1905	187.1	1	B	7.40	3.7	1.2	1.480	0.142	0.525	NA	NA	3.37	21.0	2.85	18.5
9	22	2002	188.0	1	B	7.40	3.7	1.2	1.360	0.133	0.487	3.95	0.777	3.37	21.0	2.95	18.0
9	22	2101	189.0	1	B	7.40	3.9	1.0	1.630	0.133	0.487	NA	NA	3.50	20.5	2.85	19.8
9	22	2200	190.0	1	B	7.40	4.1	1.0	1.290	0.133	0.487	3.07	0.609	2.92	20.5	2.50	19.0
9	22	2244	190.7	1	B	7.40	4.1	1.1	1.480	0.114	0.506	NA	NA	4.09	20.5	2.45	18.9
9	22	2347	191.8	1	B	7.40	6.5	0.6	0.820	0.067	0.241	NA	NA	4.72	20.5	2.30	16.4
9	23	45	192.8	1	B	7.30	5.5	0.8	1.130	0.086	0.510	NA	NA	2.70	20.8	2.00	14.8
9	23	146	193.8	1	B	7.40	6.7	2.4	0.994	0.076	0.308	2.32	0.429	6.74	21.2	2.45	16.9
9	23	247	194.8	1	B	7.40	8.2	2.8	1.210	0.100	0.367	NA	NA	4.72	21.7	2.70	17.9
9	23	348	195.8	1	B	7.40	9.6	1.6	0.632	0.062	0.311	1.43	0.380	8.10	21.0	2.50	19.0
9	23	445	196.8	1	B	7.40	5.0	0.4	1.870	0.133	0.487	NA	NA	4.47	20.8	2.60	18.9
9	23	544	197.7	1	B	7.40	5.0	1.8	0.902	0.067	0.247	3.15	0.621	2.53	20.7	2.80	19.2
9	23	645	198.8	1	B	7.40	4.7	1.0	1.390	0.137	0.283	NA	NA	2.53	20.4	2.70	19.8

946510536

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	CFP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	23	745	199.8	1	B	7.40	5.3	0.6	1.090	0.086	0.298	2.95	0.531	2.70	20.7	2.55	19.8
9	23	843	200.7	1	B	7.40	5.6	0.4	1.050	0.123	0.450	NA	NA	2.70	20.9	2.40	19.5
9	23	945	201.8	1	B	7.40	4.6	0.6	0.900	0.100	0.390	2.90	0.477	4.05	20.8	2.40	19.3
9	23	1045	202.8	1	B	7.40	4.9	0.4	0.924	0.086	0.322	NA	NA	2.70	20.6	2.10	19.2
9	23	1200	204.0	1	B	7.30	7.0	1.2	1.450	0.137	0.477	2.41	0.553	2.14	21.0	3.25	19.0
9	23	1302	205.0	1	B	7.30	5.7	0.6	1.400	0.137	0.461	NA	NA	2.53	20.5	2.50	19.0
9	23	1400	206.0	1	B	7.40	6.6	0.4	1.390	0.146	0.518	1.87	0.504	1.56	20.5	2.55	18.0
9	23	1502	207.0	1	B	7.40	9.2	1.2	1.270	0.142	0.478	NA	NA	4.67	21.0	3.25	17.0
9	23	1601	208.0	1	B	7.40	15.0	3.6	1.280	0.142	0.503	2.65	0.665	5.40	20.0	3.75	19.0
9	23	1705	209.1	1	B	7.50	8.0	1.2	1.400	0.146	0.537	NA	NA	2.33	20.0	3.10	19.0
9	23	1803	210.0	1	B	7.50	7.0	0.8	1.220	0.142	0.515	2.15	0.482	3.89	20.0	3.85	19.0
9	23	1900	211.0	1	B	7.50	8.0	2.2	1.630	0.146	0.524	NA	NA	2.33	20.0	3.35	18.0
9	23	2030	212.5	1	B	7.50	6.0	1.4	0.968	0.089	0.377	NA	NA	2.92	19.5	3.10	17.0
9	23	2200	214.0	1	B	7.50	7.0	0.8	1.300	0.142	0.462	NA	NA	2.92	19.5	2.95	18.0
9	23	2340	215.7	1	B	7.40	10.0	4.6	0.748	0.075	0.319	1.50	0.475	6.74	20.1	2.30	19.0
9	24	110	217.2	1	B	7.10	7.4	2.0	1.440	0.094	0.332	NA	NA	6.74	20.1	2.35	17.0
9	24	242	218.7	1	B	7.30	6.0	2.2	0.804	0.118	0.431	2.20	0.376	2.70	20.5	3.20	17.9
9	24	340	219.7	1	B	7.40	5.5	1.6	0.702	0.089	0.316	NA	NA	5.40	20.1	3.80	18.8
9	24	443	220.7	1	B	7.50	5.8	1.0	0.986	0.104	0.342	2.26	0.491	7.42	19.8	3.75	19.4
9	24	542	221.7	1	B	7.50	9.7	2.4	0.888	0.085	0.300	NA	NA	6.74	19.7	3.65	19.6
9	24	641	222.7	1	B	7.50	8.5	2.4	0.764	0.075	0.260	2.20	0.579	3.37	19.3	3.80	19.2
9	24	740	223.7	1	B	7.40	5.5	1.8	1.370	0.146	0.513	NA	NA	33.86	19.6	3.50	17.8
9	24	843	224.7	1	B	7.50	5.2	0.8	0.863	0.108	0.413	1.65	0.376	31.98	19.9	3.30	17.2
9	24	940	225.7	1	B	7.40	5.7	1.0	1.340	0.146	0.603	NA	NA	30.10	19.7	3.00	16.4
9	24	1040	226.7	1	B	7.40	5.8	0.8	1.440	0.127	0.593	3.03	0.610	4.39	19.5	2.85	15.5
9	24	1200	228.0	1	B	7.50	7.0	1.8	1.450	0.151	0.596	2.29	0.419	5.40	20.0	3.95	17.0

946510537

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	24	1302	229.0	1	B	7.40	8.0	1.6	1.400	0.137	0.473	NA	NA	5.40	19.2	2.95	17.5
9	24	1400	230.0	1	B	7.40	7.8	2.8	1.410	0.142	0.525	2.67	0.804	6.07	19.5	3.65	18.0
9	24	1503	231.0	1	B	7.40	5.3	1.2	1.490	0.165	0.559	NA	NA	6.74	19.5	3.50	17.5
9	24	1602	232.0	1	B	7.50	6.5	1.2	1.390	0.156	0.548	2.59	0.603	6.07	19.5	4.00	18.0
9	24	1700	233.0	1	B	7.50	9.5	2.2	1.330	0.151	0.512	NA	NA	5.40	19.5	4.25	19.0
9	24	1800	234.0	1	B	7.50	5.8	2.8	1.320	0.156	0.527	2.10	0.428	4.72	19.5	4.50	19.0
9	24	1902	235.0	1	B	7.50	5.2	3.2	1.300	0.146	0.504	NA	NA	4.72	19.0	4.45	19.0
9	24	2030	236.5	1	B	7.50	7.0	4.0	1.480	0.160	0.567	2.97	0.851	8.09	19.0	4.00	19.5
9	24	2200	238.0	1	B	7.50	6.7	3.1	1.260	0.151	0.510	NA	NA	8.43	19.0	4.25	19.5
9	24	2329	239.5	1	B	7.60	8.0	5.6	1.420	0.160	0.659	NA	NA	2.24	19.0	3.50	16.5
9	25	57	240.9	1	B	7.40	7.0	2.2	0.468	0.080	0.283	NA	NA	4.09	19.0	3.30	18.5
9	25	230	242.5	1	B	7.50	8.0	2.2	1.350	0.156	0.737	NA	NA	4.72	19.1	3.30	16.8
9	25	328	243.5	1	B	7.60	7.0	1.2	1.480	0.165	0.586	2.82	0.652	4.72	19.7	3.95	18.5
9	25	428	244.5	1	B	7.50	10.0	1.6	1.400	0.156	0.598	NA	NA	7.42	19.0	4.10	19.1
9	25	532	245.5	1	B	7.50	8.0	1.6	0.600	0.075	0.299	NA	NA	2.33	18.4	4.25	19.8
9	25	630	246.5	1	B	7.60	8.0	2.4	0.565	0.085	0.414	NA	NA	2.33	18.3	4.25	20.0
9	25	729	247.5	1	B	7.50	7.0	1.6	0.585	0.089	0.326	1.43	0.345	2.14	18.0	3.50	20.2
9	25	827	248.4	1	B	7.50	7.0	1.8	0.917	0.123	0.418	NA	NA	4.86	18.3	4.30	19.7
9	25	931	249.5	1	B	7.60	8.0	5.2	0.906	0.094	0.326	1.89	0.430	1.56	18.9	4.25	19.4
9	25	1029	250.5	1	B	7.60	7.0	1.8	0.754	0.085	0.341	NA	NA	6.42	19.0	3.90	18.6
		AVERAGE READING				7.36	6.1	1.6	1.256	0.119	0.468	2.30	0.495	6.66	21.4	2.10	17.6

94510538

STORM #2

JACKSON

STREET

9-15/9-25-81

1/3 DEPTH

946510539

JACKSON STREET-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1210	12.2	2	A	7.30	4.4	1.2	1.670	0.137	0.818	3.39	0.590	6.74	23.7	1.10	12.5
9	15	1502	15.0	2	A	7.30	6.1	1.8	1.490	0.146	1.310	NA	NA	14.80	23.0	0.70	6.3
9	15	1810	18.2	2	A	7.30	6.6	2.0	1.360	0.156	1.560	2.43	0.444	12.10	23.0	0.60	3.3
9	15	2100	21.0	2	A	7.20	5.0	2.8	1.980	0.094	0.559	NA	NA	16.20	23.5	1.20	14.0
9	16	5	24.1	2	A	7.30	5.2	1.8	1.710	0.137	0.771	3.53	0.539	11.81	23.9	0.90	13.0
9	16	255	26.9	2	A	7.20	4.3	1.8	1.290	0.146	1.280	NA	NA	13.17	23.0	0.50	6.9
9	16	555	29.9	2	A	7.20	5.5	1.8	1.340	0.165	1.700	NA	NA	NA	22.5	0.60	3.0
9	16	905	33.1	2	A	7.10	4.5	2.2	1.720	0.137	0.791	NA	NA	5.64	22.9	1.00	11.2
9	16	1200	36.0	2	A	7.30	5.4	2.6	1.530	0.127	0.796	2.74	0.579	10.79	23.0	0.70	11.0
9	16	1450	38.8	2	A	7.20	7.2	2.8	1.370	0.137	1.290	NA	NA	15.51	22.5	1.00	5.8
9	16	1755	41.9	2	A	7.30	6.6	2.6	1.270	0.175	1.880	2.23	0.380	16.18	22.0	0.90	1.8
9	16	2100	45.0	2	A	7.30	8.6	2.2	1.590	0.146	0.994	NA	NA	12.14	22.3	0.80	8.0
9	17	0	48.0	2	A	7.10	3.7	1.4	1.730	0.146	1.050	2.31	0.519	7.39	22.3	0.40	12.2
9	17	555	53.9	2	A	7.30	4.8	1.2	0.891	0.184	2.010	NA	NA	16.18	22.0	0.80	1.5
9	17	900	57.0	2	A	7.10	5.3	1.9	1.690	0.151	1.060	2.99	0.775	18.88	22.0	0.70	7.0
9	17	1200	60.0	2	A	7.30	2.7	2.8	0.892	0.070	0.529	0.49	0.190	3.60	22.8	0.70	15.5
9	17	1447	62.8	2	A	7.30	2.9	1.6	1.250	0.089	0.777	NA	NA	12.14	22.0	0.40	7.3
9	17	1755	65.9	2	A	7.30	3.3	2.2	1.070	0.170	1.910	2.13	0.416	14.84	21.5	0.80	2.3
9	17	2050	68.8	2	A	7.20	3.1	2.6	0.615	0.080	0.960	NA	NA	14.84	21.5	0.80	4.0
9	18	0	72.0	2	A	7.40	2.9	1.4	1.550	0.156	1.020	2.50	0.463	10.79	22.0	0.70	14.0
9	18	255	74.9	2	A	7.20	3.1	1.0	1.490	0.165	1.360	NA	NA	9.44	22.0	0.50	7.0
9	18	550	77.8	2	A	7.30	4.0	1.4	0.823	0.142	1.730	1.82	0.390	9.44	21.2	0.40	2.2
9	18	850	80.8	2	A	7.20	3.8	1.2	1.280	0.170	1.750	NA	NA	6.74	21.0	0.60	3.6
9	18	1200	84.0	2	A	7.20	3.7	1.4	1.450	0.113	0.560	2.42	0.514	13.49	22.5	0.60	15.0
9	18	1505	87.1	2	A	7.20	3.3	1.6	1.400	0.151	1.240	NA	NA	12.81	22.3	1.40	8.5
9	18	1800	90.0	2	A	7.20	4.0	1.4	1.160	0.146	1.550	1.83	0.400	22.93	21.5	1.40	3.5

946510540

JACKSON STREET-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH.	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	2105	93.1	2	A	7.20	3.7	2.9	1.100	0.146	1.770	NA	NA	13.49	21.0	0.80	3.0
9	19	140	97.7	2	A	7.20	2.7	1.6	0.827	0.113	1.140	1.44	0.221	8.09	21.8	0.80	11.5
9	19	505	101.1	2	A	7.20	3.6	1.0	1.150	0.146	1.560	NA	NA	14.84	21.0	0.60	6.0
9	19	825	104.4	2	A	7.10	4.0	1.8	0.625	0.127	1.670	1.10	0.247	12.14	20.4	0.75	3.5
9	19	1035	106.6	2	A	7.20	3.4	2.0	0.823	0.051	0.524	NA	NA	11.47	21.3	1.35	8.1
9	19	1200	108.0	2	A	7.20	3.0	3.0	1.530	0.151	0.842	2.43	0.460	6.03	21.9	1.90	13.5
9	19	1505	111.1	2	A	7.20	2.8	1.6	1.630	0.146	0.717	NA	NA	6.74	21.4	1.70	11.9
9	19	1800	114.0	2	A	7.20	3.6	0.4	1.560	0.142	1.390	1.81	0.399	8.77	20.6	1.05	6.1
9	19	2105	117.1	2	A	7.20	4.2	0.8	1.320	0.142	1.760	NA	NA	10.12	19.7	0.95	2.9
9	20	0	120.0	2	A	7.30	3.0	0.4	1.390	0.137	1.250	1.88	0.407	2.53	19.6	1.20	8.3
9	20	315	123.3	2	A	7.20	2.5	0.4	0.948	0.146	1.010	NA	NA	2.14	20.3	1.20	9.0
9	20	600	126.0	2	A	7.20	3.4	0.4	1.220	0.156	1.450	2.38	0.418	7.42	20.7	0.70	6.0
9	20	905	129.1	2	A	7.20	5.0	0.4	0.620	0.123	1.560	NA	NA	10.79	19.8	1.00	2.8
9	20	1200	132.0	2	A	7.30	4.1	1.4	1.360	0.137	1.190	2.21	0.435	3.11	20.6	2.00	8.9
9	20	1505	135.1	2	A	7.30	3.6	1.6	1.570	0.156	0.964	NA	NA	2.33	21.4	1.95	14.6
9	20	1800	138.0	2	A	7.30	3.7	3.0	1.280	0.137	1.250	0.93	0.224	2.14	20.9	1.50	8.1
9	20	2105	141.1	2	A	7.30	5.0	1.8	1.000	0.156	1.790	NA	NA	1.56	19.8	1.65	3.7
9	20	2345	143.8	2	A	7.30	3.9	3.4	1.160	0.137	1.390	1.95	0.424	6.03	20.0	2.20	6.0
9	21	255	146.9	2	A	7.30	3.0	1.0	1.440	0.118	0.664	NA	NA	1.56	21.0	1.70	14.3
9	21	600	150.0	2	A	7.30	3.3	1.6	0.465	0.061	0.590	1.16	0.209	3.50	20.3	0.75	15.0
9	21	850	152.8	2	A	7.20	4.3	1.2	0.717	0.108	1.180	NA	NA	3.89	19.8	1.00	5.3
9	21	1200	156.0	2	A	7.20	3.0	0.8	1.570	0.146	1.130	NA	NA	6.07	20.0	2.10	6.7
9	21	1505	159.1	2	A	7.30	4.2	3.6	1.530	0.142	0.654	NA	NA	7.42	20.9	2.10	17.2
9	21	1800	162.0	2	A	7.20	2.5	0.4	1.470	0.142	1.040	NA	0.466	6.74	20.8	2.00	12.5
9	21	2105	165.1	2	A	7.20	3.0	0.6	1.510	0.146	1.200	NA	NA	8.09	20.2	1.65	9.0
9	21	2345	167.8	2	A	7.20	4.3	1.8	0.636	0.108	1.000	0.78	0.225	12.14	20.0	1.80	6.8

946510541

JACKSON STREET-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	22	255	170.9	2	A	7.30	3.7	1.0	0.994	0.094	0.986	NA	NA	6.07	20.8	1.75	11.3
9	22	605	174.1	2	A	7.30	3.0	1.2	1.300	0.145	1.060	2.06	0.377	8.77	20.3	1.20	10.0
9	22	855	176.9	2	A	7.30	3.9	2.4	0.792	0.074	0.709	NA	NA	8.77	20.0	1.25	8.5
9	22	1200	180.0	2	A	7.20	4.8	1.2	0.902	0.131	1.170	1.68	0.262	6.74	20.0	1.60	8.2
9	22	1505	183.1	2	A	7.30	4.8	1.2	1.530	0.145	0.995	NA	NA	4.05	21.1	2.90	12.0
9	22	1805	186.1	2	A	7.30	4.6	1.4	1.590	0.140	0.940	2.33	0.408	5.06	21.1	2.75	12.3
9	22	2100	189.0	2	A	7.30	5.0	0.8	1.500	0.154	1.260	NA	NA	3.50	20.2	1.70	9.7
9	22	2345	191.8	2	A	7.30	5.5	0.4	1.130	0.135	1.260	3.51	0.677	4.05	19.8	1.80	6.3
9	23	250	194.8	2	A	7.30	5.0	0.6	0.585	0.097	0.973	NA	NA	2.70	20.0	1.80	9.5
9	23	550	197.8	2	A	7.30	5.0	0.4	1.220	0.135	0.995	NA	NA	2.02	19.8	2.00	11.0
9	23	850	200.8	2	A	7.40	4.7	0.4	0.843	0.126	1.130	NA	NA	2.02	19.5	1.55	8.3
9	23	1200	204.0	2	A	7.20	6.5	0.6	1.350	0.168	1.720	2.09	0.328	3.50	19.2	2.25	5.1
9	23	1505	207.1	2	A	7.30	5.2	1.2	1.370	0.159	1.340	NA	NA	5.64	19.8	3.60	7.9
9	23	1805	210.1	2	A	7.40	5.0	0.6	1.420	0.145	0.915	2.92	0.559	3.50	20.0	3.50	14.1
9	23	2100	213.0	2	A	7.40	5.3	0.6	1.540	0.107	0.827	NA	NA	1.75	19.9	2.50	10.2
9	23	2345	215.8	2	A	7.30	7.0	0.4	0.978	0.154	1.560	1.43	0.301	4.72	18.5	2.20	5.8
9	24	250	218.8	2	A	7.30	7.0	0.4	0.841	0.112	1.170	NA	NA	8.77	18.3	2.10	6.0
9	24	555	221.9	2	A	7.40	6.0	0.8	0.868	0.064	0.379	2.03	0.520	4.72	19.3	2.65	17.8
9	24	845	224.8	2	A	7.30	6.0	0.9	1.350	0.150	1.030	NA	NA	4.05	19.0	2.00	13.5
9	24	1200	228.0	2	A	7.30	8.0	1.0	1.140	0.173	1.670	2.07	0.408	8.77	18.5	2.10	7.8
9	24	1505	231.1	2	A	7.30	8.0	1.0	1.440	0.173	1.720	NA	NA	12.14	18.5	1.75	6.6
9	24	1805	234.1	2	A	7.40	8.0	1.0	1.400	0.150	0.806	3.20	0.766	4.72	19.5	1.60	19.1
9	24	2100	237.0	2	A	7.30	7.0	1.1	1.590	0.154	1.040	NA	NA	4.05	18.8	3.30	15.1
9	25	1	240.0	2	A	7.50	8.0	1.4	1.100	0.116	1.060	2.23	0.455	5.40	17.0	3.00	8.0
9	25	300	243.0	2	A	7.40	7.0	1.0	1.010	0.173	1.710	NA	NA	2.33	17.5	2.25	7.0
9	25	600	246.0	2	A	7.40	7.0	1.2	1.310	0.131	0.691	2.06	0.700	2.14	18.5	3.25	16.0

946510542

JACKSON STREET-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	25	900	249.0	2	A	7.50	7.0	1.8	0.953	0.065	0.397	NA	NA	2.33	18.5	3.30	16.0
		AVERAGE READING				7.27	4.7	1.4	1.242	0.135	1.158	2.12	0.435	7.95	20.8	1.50	8.9

946510543

STØRM #2

JACKSØN STREET

9-15/9-25-81

2/3 DEPTH

946510544

JACKSON STREET-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	15	1215	12.3	2	B	7.20	5.4	2.2	1.560	0.137	0.717	2.19	0.527	16.20	23.8	1.20	13.0
9	15	1510	15.2	2	B	7.20	6.5	2.0	1.440	0.146	1.310	NA	NA	19.60	23.0	0.60	5.8
9	15	1805	18.1	2	B	7.20	8.0	2.0	0.730	0.142	1.580	1.23	0.301	18.81	23.0	0.40	3.5
9	15	2105	21.1	2	B	7.30	6.2	2.4	1.270	0.085	0.443	NA	NA	7.42	23.8	1.20	14.5
9	16	0	24.0	2	B	7.20	6.7	2.4	1.650	0.146	0.598	2.82	0.648	13.17	23.9	0.80	13.2
9	16	250	26.8	2	B	7.20	4.7	2.0	1.630	0.146	1.070	NA	NA	7.52	22.9	0.40	6.8
9	16	550	29.8	2	B	7.20	5.9	2.2	1.360	0.170	1.700	NA	NA	11.29	22.5	0.40	3.2
9	16	900	33.0	2	B	7.20	6.7	1.8	1.730	0.146	0.748	NA	NA	9.41	22.9	0.80	12.0
9	16	1205	36.1	2	B	7.30	5.4	2.0	1.460	0.113	0.463	2.20	0.532	11.46	23.0	0.40	14.5
9	16	1455	38.9	2	B	7.30	5.9	2.4	1.500	0.156	1.320	NA	NA	12.14	22.5	1.00	5.5
9	16	1800	42.0	2	B	7.30	8.4	2.4	1.310	0.165	1.820	2.21	0.467	26.33	22.0	0.40	3.5
9	16	2105	45.1	2	B	7.30	9.5	2.0	1.050	0.099	0.684	NA	NA	15.50	22.5	0.50	10.5
9	17	0	48.0	2	B	7.20	3.2	0.4	1.540	0.142	0.577	2.53	0.551	8.77	23.0	0.40	16.9
9	17	555	53.9	2	B	7.30	5.4	1.2	1.230	0.189	1.940	NA	NA	9.44	22.0	0.80	1.5
9	17	900	57.0	2	B	7.10	5.3	1.3	1.600	0.156	1.090	2.83	0.686	13.49	22.0	0.50	7.5
9	17	1205	60.1	2	B	7.10	2.3	1.8	0.970	0.051	0.292	1.19	0.396	10.12	23.0	0.40	17.0
9	17	1453	62.9	2	B	7.20	2.3	2.0	NA	0.097	0.744	NA	NA	3.89	22.0	0.40	7.5
9	17	1800	66.0	2	B	7.30	3.0	1.6	1.000	0.156	1.820	1.52	0.336	18.81	21.5	0.70	2.5
9	17	2055	68.9	2	B	7.20	3.1	2.3	1.370	0.165	1.680	NA	NA	18.21	21.5	0.80	4.0
9	18	10	72.2	2	B	7.20	2.8	0.4	1.720	0.156	0.864	2.55	0.492	10.79	22.8	0.60	15.2
9	18	255	74.9	2	B	7.30	3.1	1.0	0.754	0.070	0.860	NA	NA	10.79	22.0	0.40	7.0
9	18	550	77.8	2	B	7.30	4.4	1.0	0.963	0.151	1.850	1.41	0.323	12.81	21.2	0.40	2.2
9	18	850	80.8	2	B	7.20	4.0	0.6	1.550	0.156	1.530	NA	NA	4.72	21.0	0.60	3.9
9	18	1205	84.1	2	B	7.20	3.9	1.2	1.310	0.108	0.572	2.04	0.438	10.79	22.5	0.50	17.3
9	18	1510	87.2	2	B	7.20	3.7	1.2	1.360	0.099	0.591	NA	NA	10.79	22.0	1.10	10.0
9	18	1805	90.1	2	B	7.20	4.0	1.2	2.010	0.113	0.607	2.92	0.540	12.14	21.5	1.10	4.5

946510545

JACKSON STREET-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	2110	93.2	2	B	7.40	3.8	0.4	1.520	0.151	1.250	NA	NA	15.51	21.0	0.70	3.5
9	19	140	97.7	2	B	7.20	3.1	1.8	1.100	0.061	0.298	2.09	0.396	9.44	22.5	0.60	16.4
9	19	505	101.1	2	B	7.20	3.4	2.4	1.430	0.146	1.360	NA	NA	12.14	21.0	0.60	6.0
9	19	835	104.6	2	B	7.10	3.6	1.0	0.734	0.094	1.280	1.18	0.275	8.09	20.8	0.55	4.4
9	19	1045	106.8	2	B	7.20	3.3	0.7	0.940	0.142	1.120	NA	NA	11.47	21.4	1.05	8.3
9	19	1205	108.1	2	B	7.20	3.4	0.4	2.060	0.137	0.690	2.36	0.466	1.17	21.9	1.60	13.8
9	19	1510	111.2	2	B	7.20	3.0	0.6	1.620	0.137	0.656	NA	NA	5.25	21.7	1.20	13.1
9	19	1805	114.1	2	B	7.20	3.2	0.6	1.390	0.146	1.290	2.33	0.542	8.09	20.7	1.00	6.2
9	19	2110	117.2	2	B	7.20	3.7	0.9	0.965	0.066	0.838	NA	NA	8.77	20.9	0.50	9.9
9	20	0	120.0	2	B	7.20	3.5	0.4	1.060	0.070	0.614	2.41	1.000	4.86	20.8	1.20	9.8
9	20	310	123.2	2	B	7.20	3.0	0.4	0.782	0.047	0.255	NA	NA	3.70	20.8	1.10	17.9
9	20	605	126.1	2	B	7.20	3.2	0.4	1.420	0.137	1.310	1.90	0.465	4.47	20.0	0.60	6.0
9	20	900	129.0	2	B	7.20	4.5	0.4	1.470	0.132	1.070	NA	NA	3.70	19.9	0.70	3.0
9	20	1205	132.1	2	B	7.20	6.0	2.0	1.500	0.137	1.110	2.35	0.499	3.89	20.6	1.90	9.0
9	20	1510	135.2	2	B	7.30	3.6	1.8	1.370	0.108	0.738	NA	NA	6.61	21.6	1.60	16.2
9	20	1805	138.1	2	B	7.20	3.6	1.4	1.450	0.137	1.210	2.03	0.457	2.33	20.9	1.45	8.2
9	20	2110	141.2	2	B	7.30	4.4	1.6	1.450	0.137	1.150	NA	NA	6.74	19.8	1.50	4.0
9	20	2350	143.8	2	B	7.20	4.3	1.2	1.470	0.137	1.140	2.20	0.450	5.84	20.0	2.00	8.0
9	21	300	147.0	2	B	7.30	3.2	0.6	1.490	0.137	1.040	NA	NA	2.92	21.0	1.60	16.3
9	21	605	150.1	2	B	7.30	3.8	1.0	1.280	0.118	1.100	1.71	0.377	4.09	20.3	0.75	15.5
9	21	855	152.9	2	B	7.30	3.6	1.6	1.500	0.165	1.240	NA	NA	6.42	21.3	1.00	15.0
9	21	1205	156.1	2	B	7.20	3.6	0.8	2.050	0.142	1.090	2.49	0.510	4.72	19.9	1.80	8.1
9	21	1510	159.2	2	B	7.30	3.9	1.0	1.750	0.146	0.696	NA	NA	4.72	20.8	1.80	18.1
9	21	1805	162.1	2	B	7.20	2.8	0.8	0.742	0.108	0.641	1.07	0.262	6.07	20.8	1.90	12.9
9	21	2110	165.2	2	B	7.20	3.0	0.4	1.450	0.156	0.391	NA	NA	5.40	20.1	1.50	8.5
9	21	2350	167.8	2	B	7.30	3.9	2.0	0.893	0.118	1.180	1.27	0.269	8.77	20.5	1.60	12.5

946510546

JACKSON STREET-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	22	300	171.0	2	B	7.30	4.2	1.6	0.818	0.126	0.736	NA	NA	7.42	20.8	1.75	12.3
9	22	610	174.2	2	B	7.30	3.5	1.6	0.615	0.116	0.678	0.70	0.169	4.05	20.3	1.20	11.3
9	22	900	177.0	2	B	7.30	5.5	1.3	1.690	0.145	1.140	NA	NA	6.74	20.8	1.25	14.5
9	22	1205	180.1	2	B	7.30	5.3	1.2	1.380	0.125	0.771	2.93	0.536	3.11	20.1	1.40	10.6
9	22	1510	183.2	2	B	7.30	4.8	0.8	1.540	0.140	0.990	NA	NA	5.40	21.0	1.65	12.9
9	22	1810	186.2	2	B	7.30	4.7	1.2	1.640	0.140	0.831	3.68	0.717	3.37	21.0	2.45	15.0
9	22	2105	189.1	2	B	7.30	4.7	1.2	1.350	0.116	0.847	NA	NA	5.40	20.2	1.60	10.1
9	22	2350	191.8	2	B	7.30	6.0	NA	1.110	0.078	0.406	1.81	0.473	5.40	20.5	1.50	11.5
9	23	255	194.9	2	B	7.30	5.3	1.6	1.410	NA	NA	NA	NA	5.40	20.0	1.75	11.0
9	23	600	198.0	2	B	7.30	4.4	1.2	1.350	NA	NA	NA	NA	2.70	20.0	1.80	12.5
9	23	855	200.9	2	B	7.40	4.7	0.4	1.040	0.121	0.939	NA	NA	2.70	19.8	1.40	9.8
9	23	1205	204.1	2	B	7.30	6.0	0.4	1.530	0.145	0.826	2.45	0.476	1.17	19.2	1.90	11.4
9	23	1510	207.2	2	B	7.30	5.0	0.4	1.570	0.159	0.861	NA	NA	4.09	19.8	3.40	8.5
9	23	1810	210.2	2	B	7.40	4.8	0.8	1.330	0.145	0.670	2.78	0.566	10.12	20.3	3.00	17.1
9	23	2105	213.1	2	B	7.40	4.8	0.6	1.440	0.150	1.040	NA	NA	12.14	19.9	2.45	10.7
9	23	2350	215.8	2	B	7.30	7.0	2.4	0.809	0.060	0.293	2.43	0.542	5.40	18.8	2.00	6.5
9	24	255	218.9	2	B	7.30	6.0	2.4	0.876	0.116	1.160	NA	NA	8.77	18.3	1.90	6.8
9	24	600	222.0	2	B	7.30	7.0	1.0	0.724	0.069	0.390	1.71	0.374	7.42	20.0	2.45	19.3
9	24	850	224.8	2	B	7.40	6.0	0.6	1.170	0.112	0.652	NA	NA	6.07	19.3	1.80	13.8
9	24	1205	228.1	2	B	7.20	7.0	1.4	1.350	0.168	1.550	2.19	0.430	11.47	18.5	2.00	7.8
9	24	1510	231.2	2	B	7.30	7.0	1.6	1.470	0.154	1.150	NA	NA	6.74	18.6	1.60	7.2
9	24	1810	234.2	2	B	7.40	6.0	1.6	1.430	0.154	0.717	2.44	0.513	4.72	19.6	1.50	19.4
9	24	2105	237.1	2	B	7.50	6.0	1.1	1.490	0.154	0.976	NA	NA	8.09	19.5	3.20	19.0
9	25	5	240.1	2	B	7.40	7.0	2.0	1.080	0.078	0.571	2.06	0.453	3.50	17.5	2.75	9.5
9	25	305	243.1	2	B	7.40	7.0	2.4	1.120	0.093	0.604	NA	NA	5.40	17.3	2.00	7.3
9	25	605	246.1	2	B	7.40	8.0	2.6	1.390	0.107	0.519	2.78	1.100	9.44	17.3	3.50	18.0

3465105547

JACKSON STREET-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	25	905	249.1	2	B	7.60	6.0	2.0	1.440	0.154	0.688	NA	NA	3.70	18.5	2.75	16.3
		AVERAGE READING				7.27	4.8	1.3	1.322	0.127	0.938	2.13	0.488	8.22	20.9	1.32	10.4

946510548

STØRM #2

BELLEVILLE TURNPIKE

9-15/9-25-81

1/3 DEPTH

946510549

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1350	13.8	3	A	7.30	18.0	2.8	1.100	0.168	2.120	3.09	0.577	26.30	23.0	2.20	0.8
9	15	1655	16.9	3	A	7.40	16.0	3.0	1.080	0.208	2.610	NA	NA	32.00	23.0	2.50	NA
9	15	1945	19.9	3	A	7.30	18.0	2.8	0.931	0.168	2.190	2.23	0.323	20.70	22.8	1.00	3.5
9	15	2245	22.8	3	A	7.20	7.5	2.8	0.937	0.092	1.220	NA	NA	20.70	22.8	1.00	3.5
9	16	55	24.9	3	A	7.20	7.6	2.4	1.210	0.168	2.130	2.42	0.400	9.41	22.5	0.70	1.0
9	16	340	27.7	3	A	7.30	10.2	3.4	1.280	0.208	2.510	NA	NA	20.69	22.5	1.50	NA
9	16	635	30.6	3	A	7.30	7.9	3.2	0.882	0.188	2.560	1.64	0.386	9.41	22.5	2.30	NA
9	16	945	33.8	3	A	7.20	11.0	3.2	1.730	0.148	1.790	NA	NA	26.33	22.0	1.00	1.5
9	16	1340	37.7	3	A	7.30	21.0	3.6	1.070	0.188	2.400	1.83	0.334	30.10	22.0	2.60	NA
9	16	1700	41.0	3	A	7.40	24.0	3.6	0.525	0.132	2.290	NA	NA	18.81	22.0	3.20	NA
9	16	1930	43.5	3	A	7.40	21.0	5.0	0.590	0.132	2.250	NA	NA	18.81	22.0	2.80	NA
9	16	2220	46.3	3	A	7.40	21.0	3.1	1.010	0.168	2.230	NA	NA	35.74	21.8	0.80	1.0
9	17	45	48.8	3	A	7.20	5.4	0.4	1.050	0.168	2.260	1.93	0.307	13.48	21.5	1.30	0.4
9	17	350	51.8	3	A	7.30	6.4	1.0	2.470	0.112	2.270	NA	NA	13.49	22.0	2.20	NA
9	17	640	54.7	3	A	7.20	5.6	0.4	0.393	0.092	2.000	0.82	0.292	18.81	21.0	1.80	NA
9	17	945	57.8	3	A	7.20	9.2	1.0	0.707	0.148	2.230	NA	NA	35.74	21.5	1.40	0.1
9	17	1345	61.8	3	A	7.30	3.2	2.0	0.560	0.132	2.150	1.35	0.274	10.79	21.5	1.20	0.2
9	17	1642	64.7	3	A	7.30	4.0	2.6	0.569	0.096	1.940	NA	NA	22.57	21.0	1.40	NA
9	17	1950	67.8	3	A	7.20	5.3	4.0	0.838	0.096	1.920	1.25	0.323	18.81	21.5	0.80	0.2
9	17	2252	70.9	3	A	7.20	4.0	3.5	0.475	0.132	2.000	NA	NA	26.33	21.5	0.80	0.2
9	18	50	72.8	3	A	7.40	4.5	1.8	0.682	0.112	2.030	2.00	0.313	12.81	21.0	0.70	0.5
9	18	330	75.5	3	A	7.30	8.6	2.4	1.410	0.092	1.930	NA	NA	26.33	20.5	1.00	NA
9	18	630	78.5	3	A	7.30	20.0	3.2	0.448	0.132	2.150	NA	NA	18.81	20.0	4.00	NA
9	18	925	81.4	3	A	7.20	24.0	3.1	0.478	0.096	1.850	NA	NA	22.57	20.0	1.80	NA
9	18	1235	84.6	3	A	7.20	6.0	1.8	0.672	0.132	1.990	1.30	0.294	16.93	21.0	1.00	1.3
9	18	1545	87.8	3	A	7.20	15.0	1.6	0.476	0.096	1.830	NA	NA	20.69	20.5	1.50	NA

946510550

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	1830	90.5	3	A	7.30	25.0	3.0	0.532	0.132	2.200	1.49	0.405	16.93	20.3	3.50	NA
9	18	2120	93.3	3	A	7.20	23.0	3.2	0.270	0.112	2.090	NA	NA	20.69	20.0	3.10	NA
9	19	0	96.0	3	A	7.30	6.6	2.2	0.670	0.130	1.950	1.75	0.371	13.17	20.5	4.50	1.0
9	19	315	99.3	3	A	7.20	8.0	2.4	0.417	0.112	2.010	NA	NA	16.93	19.4	1.40	NA
9	19	625	102.4	3	A	7.20	23.0	2.6	0.508	0.132	2.290	1.59	0.380	15.05	19.2	3.60	NA
9	19	900	105.0	3	A	7.20	20.0	2.9	0.598	0.168	2.640	NA	NA	18.81	19.2	3.60	NA
9	19	1215	108.3	3	A	7.20	17.0	0.8	1.510	0.132	3.640	3.27	0.438	11.46	20.3	1.10	2.0
9	19	1520	111.3	3	A	7.20	10.0	1.0	0.739	0.132	1.970	NA	NA	13.17	20.0	1.30	0.9
9	19	1815	114.3	3	A	7.20	21.0	1.6	0.626	0.168	2.520	2.04	0.639	43.26	19.0	3.15	NA
9	19	2115	117.3	3	A	7.20	18.0	1.8	0.634	0.168	2.220	NA	NA	18.81	18.7	3.55	NA
9	20	35	120.6	3	A	7.20	20.0	0.4	0.790	0.132	2.060	NA	NA	14.84	19.2	1.50	0.3
9	20	340	123.7	3	A	7.20	5.7	0.4	0.731	0.168	2.720	NA	NA	14.84	19.2	1.40	0.8
9	20	625	126.4	3	A	7.30	30.0	1.2	0.789	0.168	2.340	1.93	0.505	31.98	18.8	2.80	NA
9	20	930	129.5	3	A	7.30	20.0	0.4	0.780	0.168	2.340	NA	NA	16.93	18.5	3.80	NA
9	20	1220	132.3	3	A	7.30	28.0	2.4	0.902	0.152	2.210	2.67	0.691	10.79	19.0	2.05	0.1
9	20	1525	135.4	3	A	7.30	11.0	1.6	0.802	0.132	2.070	NA	NA	6.07	19.4	1.70	1.0
9	20	1815	138.3	3	A	7.30	18.0	1.6	0.851	0.168	2.350	1.58	0.370	9.44	19.1	2.75	NA
9	20	2120	141.3	3	A	7.40	21.0	2.4	0.840	0.168	2.340	NA	NA	10.12	18.9	3.80	NA
9	21	30	144.5	3	A	7.20	13.0	1.6	0.910	0.168	2.290	2.12	0.418	9.44	19.0	2.30	0.8
9	21	330	147.5	3	A	7.20	6.4	0.8	1.130	0.148	2.010	NA	NA	6.07	19.3	1.50	2.8
9	21	635	150.6	3	A	7.20	18.0	1.8	0.496	0.168	2.530	0.99	0.392	9.44	18.5	2.65	0.2
9	21	920	153.3	3	A	7.30	21.0	1.6	0.685	0.188	2.640	NA	NA	10.12	18.5	3.40	NA
9	21	1215	156.3	3	A	7.20	17.0	2.4	0.937	0.188	2.530	1.50	0.319	13.17	18.6	2.50	0.2
9	21	1520	159.3	3	A	7.20	6.2	0.6	1.260	0.132	1.690	NA	NA	11.29	19.7	1.30	4.6
9	21	1820	162.3	3	A	7.20	8.1	2.0	0.826	0.152	2.050	2.08	0.341	16.93	19.1	2.40	1.0
9	21	2125	165.4	3	A	7.20	16.0	1.6	0.940	0.168	2.400	NA	NA	13.17	18.9	2.60	0.2

94510551

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	22	15	168.3	3	A	7.20	17.0	5.0	0.748	0.188	2.640	1.39	0.498	16.93	19.0	2.75	0.2
9	22	325	171.4	3	A	7.20	7.4	2.4	0.672	0.112	1.360	NA	NA	9.41	19.5	1.40	3.8
9	22	640	174.7	3	A	7.20	12.0	2.6	0.754	0.168	2.130	1.79	0.401	18.81	19.0	2.20	1.0
9	22	920	177.3	3	A	7.30	18.0	4.1	0.896	0.188	2.700	NA	NA	24.45	19.0	2.60	0.1
9	22	1220	180.3	3	A	7.40	20.0	4.0	0.918	0.208	2.850	1.73	0.560	5.64	18.9	3.15	0.1
9	22	1525	183.4	3	A	7.30	7.4	2.4	1.180	0.168	2.020	NA	NA	13.49	19.8	1.55	4.2
9	22	1825	186.4	3	A	7.30	6.8	0.8	1.020	0.168	2.190	1.86	0.528	10.12	19.8	1.95	2.9
9	22	2120	189.3	3	A	7.40	9.5	1.4	0.969	0.188	2.610	NA	NA	13.17	19.1	2.40	0.8
9	23	15	192.3	3	A	7.50	14.0	2.8	0.550	0.188	2.770	0.92	0.402	12.81	19.0	3.00	0.3
9	23	320	195.3	3	A	7.30	12.0	1.8	0.982	0.132	1.980	NA	NA	3.50	19.0	2.00	2.5
9	23	620	198.3	3	A	7.30	11.0	1.6	1.140	0.148	2.060	2.13	0.395	2.72	19.0	1.80	2.6
9	23	915	201.3	3	A	7.40	12.0	2.0	0.915	0.168	2.390	NA	NA	7.42	18.8	2.70	0.5
9	23	1220	204.3	3	A	7.40	17.0	3.0	0.968	0.224	3.080	2.08	0.540	37.62	18.2	3.70	0.1
9	23	1525	207.4	3	A	7.40	15.0	2.0	0.988	0.188	2.430	NA	NA	26.33	19.1	2.50	2.1
9	23	1825	210.4	3	A	7.30	12.0	1.2	1.180	0.168	1.980	2.33	0.497	20.69	19.1	2.20	3.2
9	23	2120	213.3	3	A	7.40	14.0	1.4	1.450	0.168	2.320	NA	NA	24.45	18.7	2.90	1.1
9	24	18	216.3	3	A	7.40	17.0	3.0	0.899	0.208	2.920	1.76	0.453	16.93	17.8	3.65	NA
9	24	330	219.5	3	A	7.40	14.0	1.4	1.050	0.168	2.410	NA	NA	20.69	18.3	2.90	1.8
9	24	635	222.6	3	A	7.30	9.0	0.8	0.607	0.092	1.160	1.23	0.318	15.05	18.5	2.10	5.8
9	24	915	225.3	3	A	7.40	15.0	0.8	1.040	0.167	1.760	NA	NA	18.81	18.8	2.75	1.8
9	24	1215	228.3	3	A	7.50	20.0	2.6	0.928	0.244	3.040	1.99	0.638	30.10	17.2	3.80	NA
9	24	1525	231.4	3	A	7.40	20.0	3.0	0.868	0.208	2.810	NA	NA	22.57	17.3	4.05	0.1
9	24	1825	234.4	3	A	7.40	13.0	2.2	1.160	0.168	2.060	2.72	0.645	11.29	18.0	2.40	4.9
9	24	2120	237.3	3	A	7.40	13.0	1.4	1.180	0.188	2.510	NA	NA	16.93	17.6	2.90	2.7
9	25	15	240.3	3	A	7.40	17.0	5.0	1.260	0.168	2.220	1.73	0.337	7.52	17.0	3.75	1.0
9	25	320	243.3	3	A	7.50	15.0	6.2	0.758	0.208	2.780	NA	NA	11.29	16.5	3.75	0.5

94651052

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	25	625	246.4	3	A	7.40	13.0	3.0	0.767	0.132	1.620	1.44	0.392	8.77	17.0	2.50	6.0
9	25	920	249.3	3	A	7.40	9.0	3.0	0.532	0.092	1.210	NA	NA	3.89	17.3	2.90	3.8
		AVERAGE READING				7.29	13.9	2.3	0.877	0.155	2.237	1.84	0.424	17.14	19.7	2.32	1.0

946510553

STØRM #2

BELLEVILLE TURNPIKE

9-15/9-25-81

2/3 DEPTH

946510554

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1355	13.9	3	B	7.30	19.0	3.4	1.100	0.168	2.200	2.19	0.621	20.70	23.0	1.30	0.8
9	15	1700	17.0	3	B	7.40	18.0	3.2	1.020	0.208	2.750	NA	NA	20.70	23.0	2.60	0.0
9	15	1950	19.8	3	B	7.30	17.0	3.2	1.350	0.168	2.130	1.74	0.414	18.80	23.0	0.60	3.5
9	15	2250	22.8	3	B	7.20	10.0	2.8	0.877	0.132	1.420	NA	NA	11.30	23.0	0.60	3.5
9	16	50	24.8	3	B	7.20	7.5	1.8	0.494	0.148	1.690	2.26	0.437	15.05	22.5	0.70	1.0
9	16	335	27.6	3	B	7.30	11.0	3.2	1.370	0.208	2.740	NA	NA	20.69	22.5	1.50	0.0
9	16	630	30.5	3	B	7.30	9.5	3.2	0.885	0.150	2.340	1.92	0.636	7.52	22.5	2.30	0.0
9	16	940	33.7	3	B	7.30	12.0	2.8	1.040	0.148	2.020	NA	NA	7.53	22.0	1.00	1.8
9	16	1345	37.8	3	B	7.30	24.0	3.0	0.576	0.188	2.310	2.05	0.552	28.22	22.0	2.60	0.0
9	16	1705	41.1	3	B	7.30	21.0	3.0	0.597	0.132	2.320	NA	NA	15.05	22.0	3.20	0.0
9	16	1935	43.6	3	B	7.40	28.0	3.4	0.892	0.132	2.210	1.15	0.333	20.69	22.0	2.70	0.0
9	16	2225	46.4	3	B	7.30	22.0	1.6	1.170	0.168	2.110	NA	NA	20.69	21.8	0.80	0.8
9	17	45	48.8	3	B	7.20	5.4	1.0	0.820	0.168	2.050	1.62	0.257	22.57	21.5	1.20	0.5
9	17	350	51.8	3	B	7.30	6.3	1.4	0.514	0.112	2.230	NA	NA	26.33	22.0	2.20	0.0
9	17	640	54.7	3	B	7.20	6.4	1.4	0.417	0.096	1.870	1.58	0.458	24.45	21.0	1.80	0.0
9	17	945	57.8	3	B	7.20	9.8	4.1	0.999	0.132	2.130	NA	NA	31.98	21.5	1.40	0.1
9	17	1350	61.8	3	B	7.20	2.8	2.2	0.533	0.148	2.110	1.95	0.510	13.17	21.5	1.20	0.2
9	17	1649	64.8	3	B	7.20	4.2	4.4	0.323	0.096	1.900	NA	NA	20.69	21.0	1.60	0.0
9	17	1956	67.9	3	B	7.20	5.5	4.2	0.430	0.096	1.860	NA	NA	8.77	20.3	3.00	0.0
9	17	2258	71.0	3	B	7.20	4.0	4.0	0.542	0.132	1.980	NA	NA	24.45	21.5	0.80	0.2
9	18	55	72.8	3	B	7.50	4.3	1.2	0.705	0.208	2.060	1.98	0.426	NA	21.0	0.60	0.7
9	18	330	75.5	3	B	7.20	9.5	2.8	1.990	0.096	1.760	NA	NA	20.69	20.5	1.00	0.0
9	18	630	78.5	3	B	7.30	13.0	3.6	NA	NA	NA	NA	NA	11.29	20.0	4.00	0.0
9	18	925	81.4	3	B	7.20	16.0	4.0	0.461	0.112	1.880	NA	NA	20.69	20.0	1.90	0.0
9	18	1240	84.7	3	B	7.10	5.1	0.8	0.535	0.112	1.870	1.09	0.240	13.17	21.0	0.80	1.5
9	18	1550	87.8	3	B	7.20	17.0	2.0	0.424	0.112	1.850	NA	NA	20.69	20.5	1.50	0.0

946510555

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	1835	90.6	3	B	7.30	24.0	2.8	0.511	0.132	2.150	1.80	0.657	16.93	20.3	3.40	0.0
9	18	2125	93.4	3	B	7.20	20.0	2.7	0.292	0.168	2.330	NA	NA	15.05	20.0	3.10	0.0
9	19	0	96.0	3	B	7.30	16.0	3.8	0.746	0.112	1.860	2.25	0.467	16.93	20.2	4.50	1.0
9	19	315	99.3	3	B	7.10	12.0	2.0	0.540	0.096	1.830	NA	NA	15.05	19.8	1.40	0.0
9	19	630	102.5	3	B	7.20	30.0	3.2	0.520	0.152	2.330	1.72	0.559	15.05	19.4	3.55	0.0
9	19	910	105.2	3	B	7.20	18.0	2.9	0.605	0.168	2.540	NA	NA	15.05	19.4	3.50	0.0
9	19	1220	108.3	3	B	7.10	17.0	2.6	0.934	0.112	1.690	3.10	0.692	13.49	20.4	1.10	2.1
9	19	1525	111.4	3	B	7.20	9.0	1.2	0.996	0.112	1.710	NA	NA	9.44	20.0	1.30	0.9
9	19	1820	114.3	3	B	7.30	23.0	1.2	0.614	0.168	2.370	1.88	0.384	12.14	19.0	3.10	0.0
9	19	2120	117.3	3	B	7.20	21.0	1.7	0.727	NA	NA	NA	NA	26.33	18.9	3.05	0.0
9	20	29	120.5	3	B	7.20	18.0	1.6	0.563	0.132	1.990	NA	NA	20.69	19.0	1.70	0.5
9	20	335	123.6	3	B	7.20	9.3	0.4	1.050	0.132	2.010	NA	NA	8.09	19.2	1.30	0.3
9	20	630	126.5	3	B	7.30	32.0	0.6	0.832	0.168	2.380	NA	NA	35.74	18.5	2.80	0.0
9	20	915	129.3	3	B	7.30	24.0	0.6	0.553	0.208	2.420	NA	NA	16.93	18.5	3.70	0.0
9	20	1225	132.4	3	B	7.20	29.0	3.4	1.010	0.152	2.350	2.34	0.544	5.40	18.9	2.05	0.1
9	20	1530	135.5	3	B	7.20	10.0	1.8	0.725	0.132	1.850	NA	NA	6.07	19.5	1.40	1.6
9	20	1820	138.3	3	B	7.20	20.0	2.4	0.744	0.168	2.420	1.37	0.476	8.09	19.1	2.70	0.0
9	20	2125	141.4	3	B	7.30	20.0	2.6	0.713	0.188	2.550	NA	NA	6.07	18.9	3.75	0.0
9	21	35	144.6	3	B	7.20	12.0	2.4	0.905	0.168	2.230	2.14	0.468	12.81	18.8	2.30	0.8
9	21	335	147.6	3	B	7.30	6.0	1.8	0.899	0.168	2.170	NA	NA	10.12	19.3	1.50	3.0
9	21	640	150.7	3	B	7.30	20.0	2.6	0.963	0.152	2.060	2.34	0.435	7.42	18.5	2.60	0.2
9	21	925	153.4	3	B	7.30	20.0	2.6	0.774	0.168	2.420	NA	NA	13.49	18.5	3.40	0.0
9	21	1220	156.3	3	B	7.20	18.0	1.6	0.996	0.168	2.360	2.23	0.415	13.17	18.6	2.50	0.2
9	21	1525	159.4	3	B	7.20	6.8	0.8	1.140	0.148	1.830	NA	NA	11.29	19.6	1.25	4.8
9	21	1825	162.4	3	B	7.20	7.8	2.0	0.880	0.168	2.150	1.56	0.359	15.05	19.1	2.30	1.1
9	21	2130	165.5	3	B	7.20	15.0	2.4	0.889	0.168	2.260	NA	NA	16.93	19.0	2.50	0.4

946510556

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	22	20	168.3	3	B	7.30	22.0	5.0	0.774	0.168	2.530	NA	NA	22.57	19.0	2.75	0.2
9	22	330	171.5	3	B	7.20	10.0	2.4	0.585	0.096	1.340	NA	NA	15.05	19.5	1.40	4.0
9	22	645	174.8	3	B	7.20	12.0	2.6	0.881	0.132	1.790	1.89	0.458	18.81	19.0	2.10	1.5
9	22	925	177.4	3	B	7.30	17.0	3.7	0.896	0.188	2.530	NA	NA	22.57	19.0	2.20	0.3
9	22	1225	180.4	3	B	7.60	14.0	4.8	0.897	0.208	2.760	1.63	0.685	13.17	18.8	3.05	0.1
9	22	1530	183.5	3	B	7.30	8.0	2.0	1.330	0.168	1.870	NA	NA	5.40	19.8	1.50	4.4
9	22	1830	186.5	3	B	7.40	6.3	1.8	1.200	0.168	2.030	2.71	0.547	2.70	19.8	1.55	4.0
9	22	2125	189.4	3	B	7.40	7.8	2.3	1.030	0.168	2.210	NA	NA	9.41	19.2	2.35	1.8
9	23	20	192.3	3	B	7.40	12.0	3.0	0.840	0.188	2.650	2.30	0.613	6.74	19.3	2.75	0.8
9	23	325	195.4	3	B	7.30	12.0	1.4	1.260	0.132	1.980	NA	NA	6.07	19.3	1.90	2.5
9	23	625	198.4	3	B	7.30	9.0	1.2	1.200	0.148	2.060	2.23	0.615	11.47	19.3	1.70	2.8
9	23	920	201.3	3	B	7.50	11.0	1.7	1.060	0.168	2.390	NA	NA	15.51	18.8	2.60	0.8
9	23	1225	204.4	3	B	7.40	18.0	2.8	0.943	0.244	3.070	1.74	0.681	26.33	18.3	3.60	0.0
9	23	1530	207.5	3	B	7.30	15.0	1.4	1.080	0.168	2.350	NA	NA	28.22	19.2	2.45	2.1
9	23	1830	210.5	3	B	7.30	11.0	1.0	1.180	0.168	2.080	2.42	0.472	15.05	19.3	1.90	4.9
9	23	2125	213.4	3	B	7.40	14.0	1.3	1.250	0.198	2.550	NA	NA	26.33	18.9	2.60	2.0
9	24	23	216.4	3	B	7.40	18.0	11.4	0.845	0.224	3.080	2.61	0.773	15.05	18.0	3.50	0.1
9	24	335	219.6	3	B	7.30	15.0	2.0	2.220	0.188	2.400	NA	NA	18.81	18.3	2.85	2.0
9	24	640	222.7	3	B	7.40	12.0	0.6	0.658	0.112	1.300	1.58	0.334	9.41	18.8	1.80	6.1
9	24	920	225.3	3	B	7.30	13.0	1.3	0.967	0.176	1.750	NA	NA	16.93	18.8	2.75	2.0
9	24	1220	228.3	3	B	7.40	19.0	3.2	0.908	0.230	2.370	NA	NA	18.81	17.4	3.60	0.0
9	24	1530	231.5	3	B	7.40	19.0	3.6	0.921	0.208	2.630	NA	NA	26.33	17.3	3.95	0.1
9	24	1830	234.5	3	B	7.30	13.0	1.4	1.320	0.188	2.160	2.08	0.592	15.05	18.0	2.25	5.0
9	24	2125	237.4	3	B	7.40	14.0	1.1	1.310	0.188	2.210	NA	NA	20.69	17.9	2.40	4.8
9	25	20	240.3	3	B	7.40	20.0	4.8	0.638	0.208	2.750	1.72	0.540	18.81	17.0	3.80	1.0
9	25	325	243.4	3	B	7.40	17.0	8.4	0.932	0.188	2.640	NA	NA	18.81	16.8	3.75	0.5

946510557

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	25	630	246.5	3	B	7.30	13.0	4.0	0.974	0.132	1.610	2.04	0.430	10.12	17.3	2.60	6.5
9	25	925	249.4	3	B	7.40	12.0	3.2	0.882	0.168	1.990	NA	NA	5.40	17.3	3.00	3.8
		AVERAGE READING				7.28	14.4	2.6	0.876	0.158	2.168	1.98	0.502	16.05	19.8	2.27	1.2

946510558

STØRM #2

UNIØN

AVENUE

9-15/9-25-81

1/2 DEPTH

946510559

UNION AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB (NTU)	BOD (PPM)	NH3 (PPM)	NO2 (PPM)	NO3 (PPM)	TKN (PPM)	TP (PPM)	CHLOR (PPB)	TEMP (°C)	D.O. (PPM)	SAL (PPT)
9	15	1430	14.5	5	C	7.50	9.1	4.6	0.719	0.168	2.530	1.13	0.379	15.05	23.5	4.20	0.0
9	15	1730	17.5	5	C	7.40	8.3	4.8	0.359	0.076	2.410	0.00	0.000	11.29	24.0	5.80	0.0
9	15	2020	20.3	5	C	7.40	16.0	4.4	0.502	0.136	2.630	0.84	0.409	16.93	23.5	3.20	0.0
9	16	120	25.3	5	C	7.30	6.4	3.8	0.572	0.136	2.640	0.00	0.000	9.41	23.2	0.80	0.1
9	16	400	28.0	5	C	7.30	7.5	3.4	0.394	0.096	2.480	1.24	0.493	16.93	23.2	2.20	0.0
9	16	700	31.0	5	C	7.30	5.5	3.6	0.428	0.096	2.400	0.00	0.000	13.17	22.5	1.60	0.0
9	16	1005	34.1	5	C	7.30	7.6	3.7	0.471	0.096	2.320	1.45	0.464	11.29	22.2	2.80	0.0
9	16	1410	38.2	5	C	7.20	9.0	3.0	0.237	0.096	2.130	0.00	0.000	8.77	21.8	2.60	0.0
9	16	1725	41.4	5	C	7.40	15.0	4.6	0.328	0.096	2.040	1.17	0.414	6.74	20.0	7.40	0.0
9	16	2010	44.2	5	C	7.40	15.0	4.4	0.361	0.076	2.070	0.00	0.000	8.09	20.0	5.10	0.0
9	16	2300	47.0	5	C	7.30	18.0	4.3	0.327	0.056	1.950	1.64	0.568	7.76	20.8	2.10	0.0
9	17	115	49.3	5	C	7.50	5.3	2.2	0.423	0.076	1.960	0.00	0.000	24.45	20.0	4.10	0.0
9	17	420	52.3	5	C	7.30	4.5	3.0	0.313	0.096	2.290	1.06	0.515	24.45	20.5	6.00	0.0
9	17	710	55.2	5	C	7.30	4.2	2.6	0.366	0.136	2.520	0.00	0.000	16.93	20.0	5.10	0.0
9	17	1020	58.3	5	C	7.30	7.1	2.4	0.397	0.096	2.060	0.91	0.438	16.93	20.0	4.90	0.0
9	17	1410	62.2	5	C	7.50	3.7	4.2	0.443	0.096	2.230	0.00	0.000	11.46	20.3	4.90	0.0
9	17	1708	65.1	5	C	7.40	3.1	4.0	0.241	0.172	2.680	0.95	0.402	10.79	19.8	5.50	0.0
9	17	2011	68.2	5	C	7.30	2.6	4.6	0.534	0.172	3.060	0.00	0.000	14.16	19.5	4.70	0.0
9	17	2310	71.2	5	C	7.30	4.7	4.6	0.408	0.156	2.440	1.32	0.566	15.51	20.0	4.60	0.0
9	18	110	73.2	5	C	7.40	5.6	3.0	0.457	0.156	2.510	0.00	0.000	14.16	20.0	4.10	0.0
9	18	350	75.8	5	C	7.40	3.5	3.2	0.647	0.172	2.760	1.64	0.664	14.84	19.5	4.50	0.0
9	18	650	78.8	5	C	7.40	4.2	5.2	0.702	0.156	2.300	1.96	0.707	11.46	19.3	6.00	0.0
9	18	945	81.9	5	C	7.40	16.0	3.7	0.677	0.172	2.380	0.00	0.000	14.84	19.5	5.50	0.0
9	18	1305	85.1	5	C	7.30	6.6	3.0	0.430	0.288	2.630	0.76	0.531	13.17	19.5	4.60	0.0
9	18	1610	88.2	5	C	7.30	8.3	2.4	0.773	0.172	2.310	0.00	0.000	16.93	20.0	5.30	0.0
9	18	1845	90.8	5	C	7.40	6.8	2.6	0.502	0.172	2.470	4.76	0.547	18.81	19.5	6.30	0.0

946510560

UNION AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	18	2140	93.7	5	C	7.40	8.2	3.1	0.845	0.136	2.370	0.00	0.000	16.93	19.3	5.90	0.0
9	19	30	96.5	5	C	7.20	6.5	2.8	0.591	0.172	2.370	1.38	0.613	5.64	19.0	4.00	0.0
9	19	345	99.8	5	C	7.30	7.0	2.8	0.839	0.172	2.390	0.00	0.000	15.05	19.0	5.00	0.0
9	19	700	103.0	5	C	7.40	8.6	3.4	0.671	0.210	2.460	0.00	0.000	18.81	19.2	6.70	0.0
9	19	930	105.5	5	C	7.40	9.0	4.0	0.596	0.116	2.490	0.00	0.000	18.81	19.3	6.10	0.0
9	19	1240	108.7	5	C	7.30	9.4	2.2	0.897	0.172	2.390	2.09	0.693	14.16	19.3	4.85	0.0
9	19	1545	111.8	5	C	7.30	7.5	2.0	1.120	0.172	3.330	0.00	0.000	15.51	19.1	4.65	0.0
9	19	1835	114.6	5	C	7.40	8.7	2.2	0.659	0.172	2.720	1.34	0.652	13.49	18.9	5.40	0.0
9	19	2135	117.6	5	C	7.40	7.3	2.2	0.722	0.192	2.800	0.00	0.000	10.12	18.4	5.20	0.0
9	20	50	120.8	5	C	7.40	9.3	1.0	0.733	0.172	2.580	1.32	0.596	20.69	18.8	4.60	0.0
9	20	355	123.9	5	C	7.40	9.0	0.6	0.722	0.172	2.730	0.00	0.000	8.09	19.0	4.80	0.0
9	20	645	126.8	5	C	7.40	8.3	1.2	0.730	0.212	3.100	1.36	0.558	24.45	19.0	4.60	0.0
9	20	935	129.6	5	C	7.50	9.7	1.2	0.984	0.252	3.090	0.00	0.000	14.84	18.5	5.40	0.0
9	20	1245	132.8	5	C	7.40	14.0	2.4	0.741	0.212	3.030	1.90	0.735	15.51	18.9	4.45	0.0
9	20	1550	135.8	5	C	7.40	11.0	2.2	0.756	0.212	2.940	0.00	0.000	4.28	18.9	4.20	0.0
9	20	1835	138.6	5	C	7.50	10.0	2.6	0.901	0.232	3.110	0.00	0.000	4.09	18.9	5.20	0.0
9	20	2140	141.7	5	C	7.50	8.6	1.6	0.972	0.212	3.180	0.00	0.000	5.64	18.1	5.25	0.0
9	21	55	144.9	5	C	7.40	9.2	2.8	0.893	0.232	3.030	1.61	0.635	16.19	18.3	4.60	0.0
9	21	400	148.0	5	C	7.40	8.4	2.8	0.846	0.252	3.200	0.00	0.000	12.14	18.5	4.50	0.0
9	21	655	150.9	5	C	7.40	7.5	2.6	0.872	0.232	3.030	1.58	0.565	12.81	17.8	4.80	0.0
9	21	950	153.8	5	C	7.40	6.8	3.0	0.696	0.232	3.050	0.00	0.000	16.19	18.3	5.50	0.0
9	21	1235	156.6	5	C	7.40	10.0	2.4	1.030	0.200	3.440	3.37	0.594	18.81	18.0	4.70	0.0
9	21	1540	159.7	5	C	7.40	10.0	3.2	0.862	0.156	4.200	0.00	0.000	16.93	18.9	4.25	0.1
9	21	1840	162.7	5	C	7.40	10.0	2.6	0.895	0.232	3.160	2.80	0.635	11.29	18.1	4.95	0.0
9	21	2145	165.8	5	C	7.40	8.2	3.8	0.892	0.200	3.330	0.00	0.000	13.17	18.3	5.70	0.0
9	22	45	168.8	5	C	7.40	8.3	4.2	0.809	0.192	3.190	2.32	0.546	16.93	18.5	5.25	0.0

946510561

UNION AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	22	350	171.8	5	C	7.40	9.0	5.2	0.881	0.232	3.110	0.00	0.000	15.05	18.3	4.30	0.0
9	22	715	175.3	5	C	7.40	7.9	5.0	0.891	0.192	3.180	1.81	0.578	13.17	18.5	5.30	0.0
9	22	945	177.8	5	C	7.50	8.7	5.5	0.749	0.232	3.130	0.00	0.000	20.69	18.3	5.50	0.0
9	22	1240	180.7	5	C	7.70	6.3	9.0	0.728	0.176	3.380	1.29	0.500	16.93	18.4	5.85	0.0
9	22	1545	183.8	5	C	7.60	6.8	5.2	0.889	0.192	3.200	0.00	0.000	11.29	19.0	4.60	0.0
9	22	1845	186.8	5	C	7.50	6.8	5.4	0.870	0.192	3.110	1.39	0.499	11.29	18.9	4.80	0.0
9	22	2135	189.6	5	C	7.60	6.5	4.2	0.704	0.200	3.150	0.00	0.000	18.81	18.9	5.60	0.0
9	23	40	192.7	5	C	7.70	12.0	7.2	0.453	0.168	3.030	1.50	0.602	24.95	19.3	5.75	0.0
9	23	335	195.6	5	C	7.60	8.0	3.0	0.751	0.000	0.000	0.00	0.000	5.40	18.8	5.30	0.0
9	23	640	198.7	5	C	7.60	8.0	2.8	0.724	0.224	3.110	0.00	0.000	6.74	18.5	5.10	0.0
9	23	935	201.6	5	C	7.50	8.0	3.9	0.408	0.000	0.000	0.00	0.000	8.77	18.8	5.30	0.0
9	23	1240	204.7	5	C	7.60	7.5	7.8	0.344	0.156	3.070	1.69	0.509	5.64	19.1	6.80	0.0
9	23	1545	207.8	5	C	7.60	14.0	3.6	0.511	0.176	3.040	0.00	0.000	22.57	18.9	5.65	0.0
9	23	1845	210.8	5	C	7.60	13.0	2.8	0.591	0.156	2.970	2.17	0.666	15.05	18.8	5.55	0.0
9	23	2135	213.6	5	C	7.50	10.0	3.5	0.364	0.156	2.950	0.00	0.000	41.38	18.9	5.80	0.0
9	24	40	216.7	5	C	7.40	8.0	2.8	0.377	0.156	3.220	1.21	0.487	22.57	18.0	4.15	0.0
9	24	400	220.0	5	C	7.50	9.0	3.0	0.389	0.136	2.980	0.00	0.000	22.57	18.5	5.75	0.0
9	24	700	223.0	5	C	7.50	7.6	2.2	0.472	0.156	2.940	1.41	0.413	35.74	18.0	5.50	0.0
9	24	940	225.7	5	C	7.40	8.5	3.0	0.438	0.156	3.070	0.00	0.000	24.45	17.8	4.90	0.0
9	24	1230	228.5	5	C	7.40	9.5	7.0	0.439	0.156	3.090	1.31	0.599	24.45	16.9	5.40	0.0
9	24	1545	231.8	5	C	7.50	12.0	3.6	0.443	0.156	3.030	0.00	0.000	30.10	17.0	5.50	0.0
9	24	1850	234.8	5	C	7.50	12.0	3.4	0.466	0.156	3.090	1.38	0.490	26.33	17.7	5.10	0.0
9	24	2140	237.7	5	C	7.50	9.0	2.6	0.478	0.136	3.140	0.00	0.000	30.10	17.3	4.70	0.0
9	25	40	240.7	5	C	7.60	9.2	4.2	0.399	0.156	3.180	1.32	0.409	18.88	16.5	6.00	0.0
9	25	345	243.8	5	C	7.60	9.5	5.0	0.420	0.156	3.110	0.00	0.000	13.49	16.0	5.50	0.0
9	25	650	246.8	5	C	7.50	9.2	5.4	0.456	0.156	3.000	2.02	0.432	0.20	17.1	4.60	0.0

94510562

UNION AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	25	945	249.8	5	C	7.50	9.5	4.6	0.453	0.156	3.010	0.00	0.000	39.50	16.0	4.60	0.0
		AVERAGE READING				7.43	8.6	3.6	0.612	0.166	2.807	1.63	0.543	15.84	19.2	4.90	0.0

946510563

STØRM #2

SECØND

RIVER

9-15/9-18-81

1/2 DEPTH

946510564

SECOND RIVER-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	15	1255	12.9	4	C	7.20	18.0	11.4	0.676	0.063	1.870	2.27	1.640	5.40	22.0	7.90	0.0
9	15	1545	15.8	4	C	7.50	13.0	13.6	0.606	0.077	1.850	NA	NA	3.37	21.5	9.20	0.0
9	15	1845	18.8	4	C	7.20	6.5	10.2	0.178	0.072	1.810	2.64	0.653	2.33	20.5	7.10	0.0
9	15	2145	21.8	4	C	7.50	4.3	7.6	0.038	0.043	1.800	NA	NA	2.14	20.5	7.10	0.0
9	16	30	24.5	4	C	7.40	9.0	7.8	0.091	0.039	1.640	1.19	0.426	2.02	17.5	7.40	0.0
9	16	320	27.3	4	C	7.40	7.2	7.6	0.071	0.034	1.440	NA	NA	1.56	19.8	7.20	0.0
9	16	620	30.3	4	C	7.30	20.0	8.0	0.114	0.010	0.650	0.58	0.350	7.52	17.5	8.10	0.0
9	16	935	33.6	4	C	7.20	9.3	7.6	0.105	0.005	0.490	NA	NA	1.35	17.0	8.40	0.0
9	16	1235	36.6	4	C	7.40	12.0	3.8	0.073	0.005	0.560	0.46	0.370	5.64	17.8	10.20	0.0
9	16	1535	39.6	4	C	7.70	8.0	4.8	0.002	0.005	0.860	NA	NA	2.14	18.5	10.00	0.0
9	16	1830	42.5	4	C	7.80	6.0	3.6	0.038	0.005	1.080	2.36	0.355	3.11	18.3	8.80	0.0
9	16	2135	45.6	4	C	7.80	9.0	4.8	0.033	0.019	1.420	NA	NA	3.89	17.5	9.70	0.0
9	17	30	48.5	4	C	7.80	4.6	14.2	0.020	0.005	1.480	1.01	0.284	NA	17.8	8.60	0.0
9	17	335	51.6	4	C	7.90	3.7	3.2	0.016	0.005	1.550	NA	NA	0.97	18.0	8.40	0.0
9	17	625	54.4	4	C	7.90	2.7	2.4	0.013	0.005	1.750	0.39	0.254	1.36	17.5	8.80	0.0
9	17	935	57.6	4	C	8.20	2.8	2.0	0.022	0.005	1.880	NA	NA	2.72	18.0	10.00	0.0
9	17	1235	60.6	4	C	8.50	1.4	3.8	0.065	0.014	2.030	1.58	0.256	1.36	18.8	8.70	0.0
9	17	1530	63.5	4	C	8.20	1.7	15.4	0.002	0.039	1.640	NA	NA	1.17	19.0	9.30	0.0
9	17	1825	66.4	4	C	8.10	1.4	4.4	0.010	0.014	1.970	0.25	0.252	2.14	19.8	8.20	0.0
9	17	2126	69.4	4	C	8.00	2.3	4.4	0.002	0.010	1.950	NA	NA	1.56	18.5	7.80	0.0
9	18	25	72.4	4	C	8.10	1.7	7.4	0.022	0.010	2.090	0.87	0.290	0.78	18.9	7.70	0.0
9	18	320	75.3	4	C	7.70	2.7	12.8	0.147	0.043	1.870	NA	NA	0.78	21.0	6.70	0.0
9	18	610	78.2	4	C	7.70	2.6	3.6	0.032	0.005	1.720	0.48	0.244	NA	18.5	8.20	0.0
9	18	915	81.3	4	C	7.90	2.6	5.0	0.023	0.014	1.810	NA	NA	2.72	18.5	9.10	0.0
		AVERAGE READING				7.72	6.4	7.1	0.100	0.023	1.550	1.17	0.448	2.55	18.9	8.44	0.0

94651056S

STØRM #2

SADDLE RIVER

9-15/9-18-81

1/2 DEPTH

946510566

SADDLE RIVER-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1319	13.3	7	C	7.60	5.0	7.2	2.170	0.484	4.800	5.02	1.200	6.07	22.0	5.40	0.0
9	15	1615	16.3	7	C	7.50	6.0	9.4	1.840	0.356	3.640	NA	NA	6.07	22.0	4.60	0.0
9	15	1912	19.2	7	C	7.50	6.0	9.4	1.430	0.300	3.140	2.72	1.050	8.77	21.0	4.40	0.0
9	15	2206	22.1	7	C	7.40	6.5	9.2	0.973	0.224	2.580	NA	NA	6.07	21.0	3.60	0.0
9	16	40	24.7	7	C	7.30	4.8	6.8	0.684	0.244	3.020	2.97	0.822	11.29	22.0	4.50	0.0
9	16	345	27.8	7	C	7.50	6.3	6.6	0.820	0.356	4.240	NA	NA	5.64	21.0	3.75	0.0
9	16	650	30.8	7	C	7.50	9.1	6.8	1.480	0.356	3.370	3.25	1.070	9.41	19.0	5.50	0.0
9	16	945	33.8	7	C	7.40	7.1	6.3	0.858	0.152	1.650	NA	NA	31.98	18.0	6.75	0.0
9	16	1315	37.3	7	C	7.40	13.0	5.2	0.731	0.244	1.570	1.86	0.882	12.14	18.0	6.70	0.0
9	16	1640	40.7	7	C	7.40	13.0	5.6	0.873	0.356	2.260	NA	NA	14.16	18.5	6.70	0.0
9	16	1900	43.0	7	C	7.40	11.0	5.4	0.950	0.300	2.130	2.15	1.030	9.44	18.5	6.10	0.0
9	16	2200	46.0	7	C	7.50	11.0	5.8	0.992	0.300	2.100	NA	NA	12.81	18.0	5.80	0.0
9	17	50	48.8	7	C	7.40	4.5	5.2	1.150	0.376	2.340	2.33	0.902	9.41	18.0	5.50	0.0
9	17	350	51.8	7	C	7.40	3.7	5.6	0.824	0.356	2.540	NA	NA	13.17	17.3	6.00	0.0
9	17	710	55.2	7	C	7.40	3.5	4.8	1.290	0.356	2.650	1.99	1.010	12.14	17.0	5.75	0.0
9	17	930	57.5	7	C	7.50	3.5	4.9	1.390	0.376	3.040	NA	NA	8.09	17.0	6.00	0.0
9	17	1305	61.1	7	C	7.50	2.5	4.6	1.180	0.376	3.310	1.83	0.980	10.79	17.5	6.30	0.0
9	17	1610	64.2	7	C	7.60	4.1	4.6	0.806	0.376	3.200	NA	NA	6.74	18.0	6.90	0.0
9	17	1903	67.0	7	C	7.50	3.7	4.6	0.746	0.468	3.360	1.36	0.944	6.74	18.2	6.40	0.0
9	17	2210	70.2	7	C	7.50	4.0	4.4	0.841	0.468	3.470	NA	NA	4.05	18.5	6.00	0.0
9	18	100	73.0	7	C	7.60	3.1	3.6	0.610	0.544	3.940	1.49	1.090	5.84	17.0	6.00	0.0
9	18	435	76.6	7	C	7.60	3.7	4.2	1.000	0.544	4.220	NA	NA	5.06	17.0	5.75	0.0
9	18	735	79.6	7	C	7.60	3.9	4.0	1.370	0.468	4.170	3.00	1.260	10.79	17.0	6.00	0.0
9	18	1010	82.2	7	C	7.60	3.6	4.6	1.600	NA	NA	NA	NA	10.79	17.5	5.75	0.0
		AVERAGE READING				7.48	5.9	5.8	1.109	0.364	3.076	2.50	1.020	9.89	18.7	5.67	0.0

94651056?

STØRM #2

MARKET STREET

9-15/9-18-81

1/2 DEPTH

946510568

MARKET STREET-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1330	13.5	9	C	7.50	5.3	5.0	NA	0.111	2.400	1.33	0.530	15.05	23.0	5.60	0.0
9	15	1625	16.4	9	C	7.50	6.1	5.0	0.117	0.111	2.330	NA	NA	10.79	23.0	5.60	0.0
9	15	1926	19.4	9	C	7.50	6.5	5.0	0.136	0.111	2.320	1.42	0.486	9.41	23.0	5.20	0.0
9	15	2217	22.3	9	C	7.40	6.0	5.0	0.184	0.111	2.550	NA	NA	10.12	23.0	3.60	0.0
9	16	55	24.9	9	C	7.30	4.1	4.2	0.186	0.111	2.500	1.41	0.445	11.29	22.5	7.00	0.0
9	16	400	28.8	9	C	7.40	5.0	5.4	0.236	0.149	2.590	NA	NA	7.52	22.0	6.50	0.0
9	16	705	31.1	9	C	7.20	4.7	4.4	0.273	0.149	2.530	1.38	0.517	6.07	21.5	4.50	0.0
9	16	1000	34.0	9	C	7.20	6.4	3.0	0.343	0.188	2.890	NA	NA	5.64	21.0	4.00	0.0
9	16	1325	37.4	9	C	7.30	8.0	4.8	0.448	0.224	2.640	1.61	0.525	14.84	21.0	4.10	0.0
9	16	1655	40.9	9	C	7.30	9.0	4.8	0.438	0.224	2.630	NA	NA	10.12	20.0	4.80	0.0
9	16	1910	43.2	9	C	7.20	10.0	6.8	0.757	0.014	0.820	2.58	0.694	12.14	20.0	3.90	0.0
9	16	2215	46.3	9	C	7.30	10.0	6.9	0.874	0.264	2.670	NA	NA	16.18	20.5	4.00	0.0
9	17	100	49.0	9	C	7.30	4.0	5.2	0.916	0.264	2.460	2.48	0.662	10.79	20.5	5.75	0.0
9	17	400	52.0	9	C	7.40	4.7	5.0	0.908	0.066	2.550	NA	NA	18.88	19.0	6.00	0.0
9	17	720	55.3	9	C	7.40	4.6	5.2	0.894	0.224	2.260	1.68	0.465	12.81	19.0	6.00	0.0
9	17	945	57.8	9	C	7.40	4.7	4.7	0.977	0.224	2.250	NA	NA	6.07	19.0	6.00	0.0
9	17	1315	61.3	9	C	7.40	3.3	4.2	1.050	0.224	2.340	2.18	0.598	12.14	19.5	5.90	0.0
9	17	1622	64.4	9	C	7.40	4.3	4.2	1.010	0.244	2.480	NA	NA	18.81	20.0	6.30	0.0
9	17	1913	67.2	9	C	7.40	5.6	4.0	0.949	0.224	2.480	NA	NA	8.09	20.0	6.80	0.0
9	17	2220	70.3	9	C	7.40	5.0	4.3	0.822	0.208	2.450	NA	NA	12.14	20.0	6.80	0.0
9	18	110	73.2	9	C	7.50	5.9	NA	0.774	0.188	2.460	2.34	0.645	11.46	20.0	6.50	0.0
9	18	445	76.9	9	C	7.40	6.2	5.6	0.825	0.244	2.780	NA	NA	9.44	19.8	6.00	0.0
9	18	755	79.8	9	C	7.40	5.8	5.2	0.902	0.264	2.750	2.17	0.609	10.79	19.0	6.00	0.0
9	18	1020	82.3	9	C	7.50	6.7	4.5	0.843	0.264	2.780	NA	NA	10.12	19.0	6.00	0.0
		AVERAGE READING				7.37	5.9	4.9	0.646	0.184	2.455	1.87	0.561	11.28	20.6	5.54	0.0

946510569

STØRM #2

LINCØLN

AVENUE

9-15/9-18-81

1/2 DEPTH

946510570

LINCOLN AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
9	15	1236	12.6	10	C	7.30	5.0	5.8	0.441	0.224	2.750	2.20	0.580	5.40	22.5	4.00	0.0
9	15	1535	15.6	10	C	7.40	5.6	5.4	0.451	0.244	2.870	NA	NA	11.29	22.5	5.20	0.0
9	15	1831	18.5	10	C	7.30	6.6	6.4	0.512	0.244	2.790	1.73	0.613	3.37	23.0	5.00	0.0
9	15	2124	21.4	10	C	7.40	7.5	7.3	0.557	0.244	2.700	NA	NA	6.41	22.5	4.70	0.0
9	16	0	24.0	10	C	7.30	5.1	5.4	0.578	0.264	2.690	1.53	0.669	5.64	22.5	5.50	0.0
9	16	305	27.1	10	C	7.50	6.4	4.8	0.525	0.264	2.740	NA	NA	5.64	21.0	4.00	0.0
9	16	610	30.2	10	C	7.40	8.5	4.2	0.635	0.264	2.700	2.28	0.607	3.76	21.0	4.75	0.0
9	16	910	33.2	10	C	7.40	6.7	6.7	0.674	0.224	2.250	NA	NA	7.52	21.0	6.00	0.0
9	16	1240	36.7	10	C	7.30	13.0	8.8	1.120	0.224	2.100	3.91	0.771	12.14	21.0	5.90	0.0
9	16	1605	40.1	10	C	7.50	13.0	7.6	1.020	0.264	2.260	NA	NA	12.81	20.5	7.00	0.0
9	16	1825	42.4	10	C	7.50	11.0	4.2	1.020	0.224	2.110	2.17	0.720	8.76	20.0	6.70	0.0
9	16	2127	45.4	10	C	7.50	13.0	5.1	1.010	0.208	2.020	NA	NA	12.14	20.0	6.40	0.0
9	17	15	48.3	10	C	7.40	4.7	5.8	1.170	0.208	2.110	2.09	0.596	13.17	20.0	6.75	0.0
9	17	310	51.2	10	C	7.40	4.6	6.0	1.200	0.264	2.440	NA	NA	3.76	20.0	7.00	0.0
9	17	615	54.3	10	C	7.50	5.0	5.2	1.230	0.224	2.340	2.47	0.549	5.64	20.0	6.75	0.0
9	17	900	57.0	10	C	7.50	6.0	5.3	1.030	0.224	2.380	NA	NA	3.76	19.8	7.50	0.0
9	17	1230	60.5	10	C	7.50	4.8	5.4	0.770	0.208	2.370	1.58	0.709	2.92	19.8	5.80	0.0
9	17	1530	63.5	10	C	7.50	5.3	5.6	0.901	0.224	2.440	NA	NA	8.09	20.0	7.30	0.0
9	17	1825	66.4	10	C	7.50	5.6	6.2	0.921	0.264	2.730	1.79	0.909	15.51	20.0	7.50	0.0
9	17	2126	69.4	10	C	7.50	5.2	6.6	0.949	0.264	2.800	NA	NA	8.77	20.0	6.20	0.0
9	18	30	72.5	10	C	7.50	5.2	5.6	1.130	0.300	3.020	2.48	0.766	10.12	20.0	6.50	0.0
9	18	335	75.6	10	C	7.50	5.1	5.4	1.480	0.300	2.910	NA	NA	8.77	20.0	6.50	0.0
9	18	630	78.5	10	C	7.50	5.6	6.4	1.770	0.300	2.720	4.22	0.818	7.42	19.0	6.75	0.0
9	18	930	81.5	10	C	7.50	6.2	6.8	1.870	0.300	2.630	NA	NA	6.07	19.0	7.00	0.0
		AVERAGE READING				7.44	6.9	5.9	0.957	0.249	2.536	2.37	0.692	7.87	20.6	6.11	0.0

946510571

STØRM #2

MARKET

ISLAND

9-15/9-18-81

1/2 DEPTH

946510572

MARKET ISLAND-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [•C]	D.O. [PPM]	SAL [PPT]
9	15	1224	12.4	11	C	7.60	5.4	7.0	0.843	0.264	2.780	3.37	0.790	3.37	23.0	7.00	0.0
9	15	1523	15.4	11	C	7.60	6.1	7.8	0.740	0.224	2.440	NA	NA	8.77	23.0	7.80	0.0
9	15	1820	18.3	11	C	7.60	7.0	5.4	0.901	0.264	2.440	2.77	0.773	6.07	23.0	7.60	0.0
9	15	2117	21.3	11	C	7.70	7.4	NA	1.010	0.264	2.500	NA	NA	12.81	22.0	7.40	0.0
9	16	250	26.8	11	C	7.60	6.6	6.2	0.585	0.264	2.620	2.73	0.890	7.52	21.5	7.00	0.0
9	16	600	30.0	11	C	7.70	8.3	6.6	0.995	0.264	2.490	NA	NA	5.64	21.0	8.00	0.0
9	16	855	32.9	11	C	7.60	7.4	7.7	1.380	0.264	2.220	2.20	0.725	16.93	21.0	8.50	0.0
9	16	1223	36.4	11	C	7.70	12.0	5.6	1.010	0.264	2.200	2.27	0.647	9.44	20.5	8.60	0.0
9	16	1550	39.8	11	C	7.60	12.0	3.4	1.240	0.224	1.940	NA	NA	10.79	20.0	9.10	0.0
9	16	1815	42.3	11	C	7.70	12.0	5.0	1.260	0.264	1.880	2.84	0.575	18.21	20.0	9.10	0.0
9	16	2115	45.3	11	C	7.70	12.0	5.0	1.430	0.208	2.090	NA	NA	14.16	20.0	8.90	0.0
9	17	5	48.1	11	C	7.60	5.8	6.2	1.170	0.224	2.120	2.62	0.617	9.41	20.0	8.50	0.0
9	17	300	51.0	11	C	7.60	5.7	6.8	1.000	0.224	2.210	NA	NA	5.40	20.0	8.75	0.0
9	17	605	54.1	11	C	7.60	6.2	5.8	1.090	0.208	2.160	2.27	0.654	4.05	19.8	9.00	0.0
9	17	845	56.8	11	C	7.70	7.3	5.2	1.150	0.188	2.130	NA	NA	12.81	19.8	9.75	0.0
9	17	1220	60.3	11	C	7.60	5.3	6.6	1.070	0.224	2.280	2.73	0.832	2.72	19.8	9.20	0.0
9	17	1515	63.3	11	C	7.60	5.6	6.2	1.100	0.224	2.400	NA	NA	5.84	20.0	9.20	0.0
9	17	1813	66.2	11	C	7.70	5.4	7.2	1.220	0.244	2.520	2.85	0.778	2.92	20.0	9.00	0.0
9	17	2116	69.3	11	C	7.70	5.3	6.3	1.060	0.244	2.550	NA	NA	7.42	20.0	9.10	0.0
9	18	15	72.3	11	C	7.70	6.4	5.8	1.700	0.300	2.710	2.96	0.785	6.74	20.0	8.50	0.0
9	18	325	75.4	11	C	7.70	7.7	6.8	2.100	0.280	2.450	NA	NA	12.14	19.0	8.50	0.0
9	18	615	78.3	11	C	7.70	8.3	6.4	1.880	0.264	2.220	2.65	0.677	5.40	19.0	8.50	0.0
9	18	915	81.3	11	C	7.70	11.0	5.8	1.540	0.264	2.120	NA	NA	5.40	19.0	9.00	0.0
		AVERAGE READING				7.65	7.7	6.1	1.195	0.246	2.325	2.69	0.729	8.43	20.5	8.52	0.0

946510573

STØRM #2

MCBRIDE AVENUE

9-15/9-18-81

1/2 DEPTH

946510574

MC BRIDE AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1216	12.3	12	C	7.40	6.0	5.4	0.809	0.224	2.540	2.74	0.754	10.12	23.5	4.60	0.0
9	15	1515	15.3	12	C	7.30	5.8	4.4	1.040	0.244	2.510	NA	NA	10.79	23.0	4.80	0.0
9	15	1811	18.2	12	C	7.30	7.0	4.0	1.210	0.264	2.430	2.17	0.678	8.77	23.0	4.60	0.0
9	15	2109	21.1	12	C	7.30	7.0	4.4	1.230	0.264	2.730	NA	NA	8.77	22.0	4.10	0.0
9	16	240	26.7	12	C	7.20	8.5	6.0	1.070	0.224	2.430	3.10	0.866	9.41	22.0	5.00	0.0
9	16	545	29.8	12	C	7.40	8.0	5.6	1.440	0.264	2.460	NA	NA	11.29	21.0	4.25	0.0
9	16	845	32.8	12	C	7.40	7.6	6.1	1.430	0.264	2.230	2.30	0.683	9.41	21.0	4.50	0.0
9	16	1218	36.3	12	C	7.30	7.2	4.2	1.420	0.264	2.260	NA	NA	10.12	20.5	5.00	0.0
9	16	1515	39.3	12	C	7.40	8.2	5.2	1.280	0.204	1.800	3.39	0.708	14.16	20.0	5.80	0.0
9	16	1808	42.1	12	C	7.40	8.5	5.0	1.400	0.168	1.810	NA	NA	14.84	20.0	5.30	0.0
9	16	2110	45.2	12	C	7.40	6.4	6.0	1.600	0.168	1.730	NA	NA	20.69	20.5	4.40	0.0
9	17	0	48.0	12	C	7.30	6.2	2.4	1.620	0.224	2.180	2.18	0.666	6.74	20.0	3.75	0.0
9	17	255	50.9	12	C	7.30	7.1	4.2	1.590	0.204	2.210	NA	NA	10.79	20.0	4.25	0.0
9	17	555	53.9	12	C	7.20	6.7	5.2	1.180	0.188	2.130	2.75	0.682	8.77	19.8	4.75	0.0
9	17	840	56.7	12	C	7.30	6.7	4.1	1.190	0.188	2.150	NA	NA	10.79	19.8	4.50	0.0
9	17	1215	60.3	12	C	7.30	5.8	5.8	1.170	0.204	2.380	3.33	0.832	12.14	20.0	4.70	0.0
9	17	1508	63.1	12	C	7.30	6.5	5.4	1.360	0.224	2.540	NA	NA	10.79	20.0	4.70	0.0
9	17	1806	66.1	12	C	7.30	7.5	5.0	1.490	0.244	2.620	4.00	0.972	19.56	20.0	4.30	0.0
9	17	2108	69.1	12	C	7.30	5.5	4.3	1.670	0.264	2.670	NA	NA	2.92	20.0	3.60	0.0
9	18	10	72.2	12	C	7.40	6.1	3.4	NA	NA	NA	NA	NA	12.81	20.0	4.00	0.0
9	18	315	75.3	12	C	7.30	6.9	3.8	2.330	0.264	2.360	3.23	0.745	5.40	19.0	4.25	0.0
9	18	610	78.2	12	C	7.30	8.6	4.4	2.120	0.224	2.800	NA	NA	4.72	19.0	4.25	0.0
9	18	910	81.2	12	C	7.30	9.4	6.6	1.900	0.224	2.060	2.99	0.729	6.74	19.0	4.25	0.0
		AVERAGE READING				7.32	7.1	4.8	1.434	0.227	2.320	2.93	0.756	10.46	20.6	4.51	0.0

946510575

STØRM #2

HILLARY

STREET

9-15/9-18-81

1/2 DEPTH

946510576

HILLERY STREET-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
9	15	1205	12.1	13	C	7.30	6.8	4.4	1.390	0.280	2.630	3.70	1.060	10.12	23.0	5.20	0.0
9	15	1503	15.0	13	C	7.30	7.0	4.2	1.490	0.280	2.610	NA	NA	14.84	22.5	5.60	0.0
9	15	1806	18.1	13	C	7.40	8.0	5.8	1.880	0.320	2.540	3.33	0.830	3.37	22.0	5.40	0.0
9	15	2103	21.0	13	C	7.40	8.0	6.2	1.590	0.280	2.320	NA	NA	4.05	22.0	4.60	0.0
9	16	230	26.5	13	C	7.30	7.2	6.8	1.450	0.280	2.480	2.81	0.731	7.52	21.5	4.50	0.0
9	16	530	29.5	13	C	7.40	6.5	6.6	1.190	0.264	2.280	NA	NA	9.41	21.0	5.00	0.0
9	16	830	32.5	13	C	7.30	6.8	7.7	1.620	0.204	2.170	3.16	0.810	11.29	20.0	6.00	0.0
9	16	1205	36.1	13	C	7.40	8.4	7.8	1.380	0.188	1.930	NA	NA	15.51	20.0	5.40	0.0
9	16	1500	39.0	13	C	7.40	7.9	7.2	2.440	0.188	2.070	2.76	0.763	18.21	20.5	4.20	0.0
9	16	1800	42.0	13	C	7.30	6.8	8.0	1.650	0.204	2.100	NA	NA	18.21	20.5	4.20	0.0
9	16	2058	45.0	13	C	7.30	8.3	6.9	0.648	0.188	2.250	1.70	0.638	16.18	20.0	4.30	0.0
9	16	2345	47.8	13	C	7.20	6.8	6.2	1.280	0.188	2.000	NA	NA	7.42	20.0	5.75	0.0
9	17	245	50.8	13	C	7.30	6.6	5.4	1.040	0.188	2.200	2.79	0.628	9.44	19.5	4.75	0.0
9	17	545	53.8	13	C	7.30	6.4	4.6	1.360	0.224	2.420	NA	NA	11.46	20.0	5.00	0.0
9	17	830	56.5	13	C	7.30	6.7	4.8	1.390	0.224	2.600	2.37	0.791	9.11	19.8	4.75	0.0
9	17	1205	60.1	13	C	7.30	5.6	5.4	1.530	0.264	2.600	NA	NA	14.16	20.0	4.60	0.0
9	17	1500	63.0	13	C	7.30	5.1	4.0	1.750	0.264	2.600	2.87	0.828	6.07	20.0	4.50	0.0
9	17	1800	66.0	13	C	7.30	4.8	4.6	2.320	0.280	2.540	NA	NA	12.14	20.0	4.70	0.0
9	17	2105	69.1	13	C	7.30	5.7	6.1	NA	NA	NA	NA	NA	6.74	19.5	4.20	0.0
9	18	0	72.[illegible]	13	C	7.30	7.6	4.4	2.060	0.150	2.120	NA	NA	6.41	19.0	5.75	0.0
9	18	300	75.[illegible]	13	C	7.30	8.8	4.6	1.700	0.224	2.060	NA	NA	6.74	19.0	5.00	0.0
9	18	550	77.8	13	C	7.30	8.7	5.0	1.840	0.264	2.080	4.09	0.838	9.44	19.0	4.50	0.0
9	18	900	81.0	13	C	7.30	7.9	7.1	1.420	0.244	2.000	NA	NA	11.46	19.0	4.50	0.0
		AVERAGE READING				7.32	7.1	5.8	1.564	0.236	2.300	2.96	0.792	10.40	20.3	4.89	0.0

9465105777

STØRM #2

DUNDEE DAM

UPSTREAM

9-15/9-25-81

1/2 DEPTH

946510578

DUNDEE DAM UPSTREAM-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
9	15	1255	8	C	23.8	5.2
9	15	1550	8	C	23.2	5.3
9	15	1847	8	C	23.0	5.0
9	15	2148	8	C	22.5	5.0
9	16	0015	8	C	22.0	4.5
9	16	0320	8	C	22.5	4.5
9	16	0625	8	C	22.0	3.8
9	16	0930	8	C	21.0	3.8
9	16	1258	8	C	21.0	3.6
9	16	1625	8	C	21.0	3.5
9	16	1845	8	C	20.5	4.5
9	16	2145	8	C	20.0	3.8
9	17	0030	8	C	20.0	2.5
9	17	0325	8	C	20.0	4.3
9	17	0635	8	C	20.0	4.5
9	17	0915	8	C	19.8	5.5
9	17	1246	8	C	19.5	5.4
9	17	1550	8	C	19.5	5.8
9	17	1843	8	C	20.0	5.2
9	17	2145	8	C	19.5	6.0
9	18	0045	8	C	20.0	6.0
9	18	0350	8	C	20.0	6.3
9	18	0715	8	C	19.5	6.0
9	18	0950	8	C	19.0	6.0
9	18	1345	8	C	19.5	5.3
9	18	1645	8	C	19.5	5.3
9	18	1910	8	C	19.5	5.1
9	18	2210	8	C	19.5	5.6
9	19	0110	8	C	19.0	4.8
9	19	0438	8	C	18.7	5.1
9	19	0755	8	C	18.8	5.7
9	19	1005	8	C	19.0	5.6
9	19	1310	8	C	19.0	5.6
9	19	1615	8	C	17.7	5.2
9	19	1905	8	C	18.0	5.2
9	19	2210	8	C	17.8	5.0
9	20	0115	8	C	17.4	4.6
9	20	0430	8	C	17.0	4.8
9	20	0720	8	C	17.0	4.5
9	20	1020	8	C	16.5	4.5
9	20	1310	8	C	18.0	5.1
9	20	1615	8	C	18.0	5.5
9	20	1900	8	C	18.1	5.9
9	20	2210	8	C	17.5	5.4

946510579

DUNDEE DAM UPSTREAM-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #2

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
9	21	0140	8	C	17.5	5.3
9	21	0450	8	C	17.3	5.3
9	21	0735	8	C	17.3	5.3
9	21	1035	8	C	17.3	5.4
9	21	1305	8	C	17.5	6.0
6	21	1615	8	C	17.8	6.9
9	21	1905	8	C	17.8	6.5
9	21	2210	8	C	17.5	6.3
9	22	0110	8	C	18.0	5.0
9	22	0420	8	C	17.5	5.4
9	22	0750	8	C	17.8	5.7
9	22	1025	8	C	17.8	5.6
9	22	1305	8	C	17.9	5.9
9	22	1610	8	C	18.0	5.8
9	22	1915	8	C	18.4	6.1
9	22	2210	8	C	18.7	6.3
9	23	0110	8	C	18.8	8.3
9	23	0425	8	C	18.5	5.8
9	23	0720	8	C	18.3	5.3
9	23	1015	8	C	17.3	4.6
9	23	1305	8	C	17.8	4.7
9	23	1605	8	C	18.0	5.2
9	23	1915	8	C	17.9	5.7
9	23	2205	8	C	17.8	6.0
9	24	0112	8	C	17.8	5.1
9	24	0440	8	C	17.0	5.8
9	24	0735	8	C	16.8	5.6
9	24	1015	8	C	16.5	5.3
9	24	1300	8	C	16.2	5.0
9	24	1610	8	C	16.1	5.1
9	24	1920	8	C	15.7	5.9
9	24	2205	8	C	15.6	6.2
9	25	0110	8	C	15.0	5.8
9	25	0405	8	C	15.0	5.5
9	25	0745	8	C	15.0	6.3
9	25	1010	8	C	15.0	6.0

946510580

STØRM #2

DUNDEE DAM

DØWNSTREAM

9-15/9-25-81

1/2 DEPTH

946510581

STORM #2 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL 6C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
9	15	1307	6	C	23.3	7.4
9	15	1601	6	C	23.0	7.8
9	15	1858	6	C	23.0	7.2
9	15	2155	6	C	22.5	7.0
9	16	0030	6	C	22.0	7.5
9	16	0335	6	C	22.0	7.3
9	16	0636	6	C	21.0	7.8
9	16	0937	6	C	21.0	7.8
9	16	1305	6	C	21.5	8.2
9	16	1630	6	C	21.0	7.4
9	16	1852	6	C	21.0	7.8
9	16	2150	6	C	20.5	7.6
9	17	0040	6	C	20.0	8.0
9	17	0335	6	C	19.8	8.0
9	17	0645	6	C	19.0	8.0
9	17	0925	6	C	20.0	8.5
9	17	1255	6	C	20.0	8.5
9	17	1600	6	C	19.8	8.5
9	17	1851	6	C	19.8	8.2
9	17	2158	6	C	19.5	8.0
9	18	0055	6	C	20.0	8.0
9	18	0400	6	C	19.5	8.3
9	18	0725	6	C	19.0	8.3
9	18	1000	6	C	19.0	8.3
9	18	1325	6	C	19.8	9.2
9	18	1635	6	C	20.0	8.5
9	18	1900	6	C	19.5	8.0
9	18	2155	6	C	19.5	7.5
9	19	0100	6	C	19.0	7.3
9	19	0410	6	C	18.5	7.8
9	19	0730	6	C	18.4	8.1
9	19	0950	6	C	19.1	8.3
9	19	1255	6	C	19.1	8.3
9	19	1600	6	C	18.9	7.3
9	19	1850	6	C	18.2	7.4
9	19	2150	6	C	17.7	7.5
9	20	0105	6	C	17.5	7.2
9	20	0415	6	C	17.2	7.8
9	20	0705	6	C	17.0	7.4
9	20	1000	6	C	17.0	8.0
9	20	1300	6	C	18.8	8.2
9	20	1605	6	C	19.0	7.1
9	20	1850	6	C	18.5	7.6
9	20	2155	6	C	17.9	7.2

946510582

STORM #2 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL AT - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
9	21	0125	6	C	17.5	7.5
9	21	0425	6	C	17.3	7.7
9	21	0730	6	C	17.3	7.9
9	21	1030	6	C	17.5	8.9
9	21	1250	6	C	18.5	8.5
9	21	1555	6	C	19.6	8.5
9	21	1850	6	C	18.1	7.9
9	21	2155	6	C	17.7	7.7
9	22	0100	6	C	18.3	7.1
9	22	0410	6	C	18.0	7.7
9	22	0735	6	C	18.0	8.0
9	22	1005	6	C	18.5	8.9
9	22	1250	6	C	19.2	9.4
9	22	1600	6	C	19.6	8.3
9	22	1905	6	C	19.7	7.3
9	22	2155	6	C	18.9	7.2
9	23	0100	6	C	18.5	7.3
9	23	0400	6	C	18.8	8.1
9	23	0700	6	C	17.5	8.1
9	23	1005	6	C	17.5	8.7
9	23	1255	6	C	18.0	9.0
9	23	1555	6	C	17.9	8.5
9	23	1900	6	C	17.0	7.8
9	23	2150	6	C	16.4	7.8
9	24	0100	6	C	16.0	9.0
9	24	0420	6	C	15.8	8.5
9	24	0718	6	C	15.5	8.3
9	24	1002	6	C	15.8	9.3
9	24	1250	6	C	17.0	9.3
9	24	1600	6	C	16.1	8.8
9	24	1910	6	C	15.8	8.2
9	24	2150	6	C	15.1	8.0
9	25	0100	6	C	15.0	8.5
9	25	0355	6	C	14.8	8.3
9	25	0710	6	C	15.0	8.5
9	25	0959	6	C	16.0	10.0

946510583

Storm Sampling
December 1981

946510584

STØRM #3

KEARNY

PØINT

12-1/12-11-81

1/3 DEPTH

946510585

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POC [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1800	18.0	1	A	7.48	3.2	3.2	1.000	0.019	0.235	NA	0.269	2.53	NA	NA	12.8
12	1	1915	19.2	1	A	7.55	3.7	4.0	1.340	0.051	0.793	1.70	0.675	3.50	NA	NA	12.5
12	1	2006	20.1	1	A	7.61	3.5	3.6	0.779	0.021	0.380	0.95	0.347	2.14	NA	NA	15.0
12	1	2105	21.1	1	A	7.63	3.6	3.6	1.380	0.103	0.751	NA	NA	2.53	NA	NA	15.5
12	1	2235	22.6	1	A	7.61	3.7	5.4	0.923	0.042	0.315	2.51	0.739	2.72	NA	NA	16.3
12	1	2355	23.9	1	A	7.61	3.8	4.6	0.778	0.042	0.315	NA	NA	2.72	NA	NA	16.3
12	2	120	25.3	1	A	7.59	3.7	3.8	1.450	0.041	0.390	1.83	0.567	3.70	NA	NA	13.5
12	2	227	26.4	1	A	7.57	3.6	3.4	1.190	0.074	0.770	NA	NA	2.33	NA	NA	12.3
12	2	355	27.9	1	A	7.57	5.8	4.4	0.921	0.037	0.331	NA	NA	3.11	NA	NA	10.0
12	2	507	29.1	1	A	7.57	4.7	3.8	1.120	0.055	0.503	NA	NA	3.70	NA	NA	9.4
12	2	610	30.2	1	A	7.61	7.1	5.8	1.420	0.079	0.921	1.62	0.335	6.03	NA	NA	7.0
12	2	700	31.0	1	A	7.60	10.5	7.4	1.120	0.046	0.523	NA	NA	6.10	NA	NA	11.5
12	2	905	33.1	1	A	NA	NA	NA	NA	NA	NA	NA	NA	NA	7.3	7.25	15.0
12	2	1004	34.1	1	A	7.60	2.0	4.2	1.370	0.099	0.693	2.39	0.409	2.33	NA	NA	11.4
12	2	1105	35.1	1	A	7.50	2.2	5.8	1.390	0.047	0.414	NA	NA	2.14	7.4	6.10	15.9
12	2	1203	36.0	1	A	7.60	2.3	4.6	1.240	0.103	0.730	1.79	0.421	1.75	7.3	6.10	14.5
12	2	1304	37.1	1	A	7.60	2.4	3.4	1.360	0.106	0.809	NA	NA	2.14	NA	NA	NA
12	2	1405	38.1	1	A	7.50	2.7	4.4	1.450	0.113	0.917	2.28	0.510	3.89	7.1	6.90	10.6
12	2	1503	39.0	1	A	7.50	2.3	2.8	1.410	0.108	0.746	NA	NA	2.33	6.8	7.68	6.8
12	2	1605	40.1	1	A	7.50	3.1	2.8	1.220	0.056	0.653	NA	0.275	8.17	6.4	7.50	5.0
12	2	1703	41.0	1	A	7.50	2.7	3.2	1.210	0.108	0.992	2.53	0.455	2.72	6.2	7.50	5.1
12	2	1802	42.0	1	A	7.50	3.3	2.6	1.420	0.108	1.160	2.45	0.579	2.72	6.3	6.75	4.9
12	2	1902	43.0	1	A	7.50	4.0	3.2	1.460	0.101	1.370	NA	NA	2.33	6.2	7.35	4.3
12	2	2020	44.3	1	A	7.50	3.3	2.4	0.752	0.028	0.371	0.95	0.365	3.11	NA	NA	14.0
12	2	2118	45.3	1	A	7.50	2.2	2.6	1.220	0.052	0.450	NA	NA	8.17	NA	NA	16.0
12	2	2219	46.3	1	A	7.50	3.4	3.6	1.430	0.066	0.560	3.03	0.641	2.53	NA	NA	16.5

9465510586

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
12	2	2325	47.4	1	A	7.50	2.8	4.6	1.250	0.094	0.625	3.47	0.646	4.67	7.4	7.10	15.7
12	3	29	48.5	1	A	7.50	2.7	5.4	0.729	0.017	0.130	NA	NA	2.72	7.3	5.30	16.5
12	3	135	49.6	1	A	7.60	7.8	7.4	1.330	0.089	0.662	2.42	0.411	8.77	7.2	5.80	16.3
12	3	240	50.7	1	A	7.60	3.5	6.2	1.250	0.099	0.714	1.48	0.427	3.50	7.3	6.90	15.7
12	3	352	51.9	1	A	7.50	3.0	4.6	1.420	0.042	0.450	1.53	0.338	5.06	7.1	7.00	10.0
12	3	502	53.0	1	A	7.50	4.5	6.2	0.880	0.037	0.496	1.15	0.487	5.45	7.2	6.50	14.5
12	3	558	54.0	1	A	7.50	5.4	8.0	1.100	0.056	0.550	NA	NA	1.56	6.9	6.60	15.3
12	3	700	55.0	1	A	7.50	6.0	8.2	1.290	0.113	0.957	3.43	0.712	4.28	7.0	6.50	14.5
12	3	804	56.1	1	A	7.40	7.5	4.6	1.510	0.113	1.040	2.73	0.645	3.99	7.1	6.30	7.0
12	3	1003	58.0	1	A	7.40	5.0	3.0	1.520	0.103	0.896	2.78	0.585	3.89	7.2	6.62	12.1
12	3	1101	59.0	1	A	7.40	3.3	2.8	1.390	0.108	0.829	NA	NA	3.89	7.2	6.40	14.8
12	3	1204	60.1	1	A	7.40	4.0	2.8	1.400	0.118	0.840	2.32	0.462	3.70	7.5	6.60	15.8
12	3	1301	61.0	1	A	7.40	3.5	2.7	1.250	0.103	0.751	NA	NA	3.31	7.4	7.30	15.7
12	3	1405	62.1	1	A	7.40	5.1	4.2	0.846	0.056	0.405	1.71	0.395	4.08	7.5	6.75	16.1
12	3	1503	63.0	1	A	7.50	4.0	2.8	0.818	0.061	0.389	NA	NA	2.14	6.9	6.95	8.5
12	3	1605	64.1	1	A	7.50	4.5	2.6	1.240	0.094	0.708	2.26	0.474	3.31	7.0	7.20	7.2
12	3	1704	65.1	1	A	7.40	5.7	3.0	1.400	0.089	0.941	NA	NA	2.14	6.3	7.70	7.3
12	3	1806	66.1	1	A	7.40	5.4	4.4	1.420	0.061	0.586	NA	0.368	3.89	6.5	7.25	7.3
12	3	1902	67.0	1	A	7.40	5.8	3.6	1.450	0.094	1.030	2.53	0.558	3.89	6.3	7.10	6.3
12	3	2010	68.2	1	A	7.40	6.6	4.0	0.850	0.019	0.297	1.07	0.331	5.76	7.0	6.20	13.0
12	3	2108	69.1	1	A	7.40	19.0	11.0	1.200	0.103	0.875	NA	NA	11.46	7.2	6.60	14.5
12	3	2206	70.1	1	A	7.40	4.5	4.4	1.040	0.052	0.450	2.16	0.475	5.45	7.5	6.40	15.0
12	3	2304	71.1	1	A	7.40	5.7	3.0	1.590	0.108	0.756	NA	NA	6.07	7.5	6.80	15.3
12	4	5	72.1	1	A	7.40	4.2	2.4	1.050	0.033	0.324	1.65	0.419	3.31	7.2	6.80	15.2
12	4	107	73.1	1	A	7.40	4.6	2.8	0.925	0.019	0.276	NA	NA	3.70	7.0	6.60	13.3
12	4	225	74.4	1	A	7.40	5.4	3.8	1.200	0.037	0.372	3.65	0.731	4.86	7.2	6.20	12.5

9465105 87

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	4	322	75.4	1	A	7.50	9.3	14.0	1.130	0.056	0.653	NA	NA	3.11	7.0	7.80	10.3
12	4	415	76.3	1	A	7.40	5.1	3.4	1.140	0.047	0.548	2.38	0.551	2.53	7.0	6.60	13.0
12	4	510	77.2	1	A	7.40	4.3	2.6	0.932	0.070	0.567	2.06	0.382	5.06	7.0	7.40	10.5
12	4	609	78.1	1	A	7.40	6.2	3.4	0.855	0.036	0.392	NA	NA	5.06	7.0	7.40	12.0
12	4	700	79.0	1	A	7.40	5.7	2.6	1.030	0.037	0.403	NA	NA	4.08	6.5	7.00	9.5
12	4	802	80.0	1	A	7.40	6.0	3.8	1.450	0.083	0.814	2.75	0.561	2.53	6.3	8.05	7.0
12	4	905	81.1	1	A	7.40	7.2	4.0	1.410	0.072	0.755	NA	NA	2.72	6.3	7.75	9.8
12	4	1006	82.1	1	A	7.40	5.8	5.2	1.420	0.065	0.609	1.92	0.413	2.33	6.7	7.15	12.2
12	4	1104	83.1	1	A	7.40	4.4	3.8	1.450	0.065	0.599	NA	NA	1.75	7.0	7.05	12.5
12	4	1203	84.0	1	A	7.40	4.0	2.6	1.410	0.090	0.754	2.06	0.430	1.75	7.1	6.70	12.8
12	4	1302	85.0	1	A	7.40	5.8	6.0	1.220	0.067	0.602	NA	NA	1.36	7.3	6.50	14.4
12	4	1409	86.1	1	A	7.40	5.3	5.0	1.050	0.055	0.535	1.72	0.324	2.53	7.4	5.70	15.5
12	4	1502	87.0	1	A	7.50	4.1	4.4	0.887	0.041	0.485	NA	NA	1.56	7.3	6.80	13.0
12	4	1604	88.1	1	A	7.40	4.3	3.0	1.420	0.093	1.010	3.19	0.610	1.95	7.1	7.10	13.7
12	4	1702	89.0	1	A	7.40	5.7	4.6	1.510	0.095	1.060	NA	NA	1.75	6.7	8.00	7.2
12	4	1804	90.1	1	A	7.40	5.0	3.2	1.540	0.096	1.090	1.85	0.442	2.53	6.5	8.55	6.5
12	4	1900	91.0	1	A	7.40	4.8	3.6	1.510	0.093	0.937	NA	NA	2.33	6.3	7.10	6.3
12	4	2015	92.3	1	A	7.40	4.4	2.6	1.420	0.099	0.911	2.35	0.428	1.95	7.0	6.20	11.9
12	4	2110	93.2	1	A	7.40	7.0	3.4	1.480	0.081	1.180	NA	NA	2.72	6.5	7.60	10.0
12	4	2210	94.2	1	A	7.40	5.0	3.0	1.460	0.099	0.921	2.95	0.585	3.11	6.9	7.00	14.5
12	4	2308	95.1	1	A	7.40	4.3	2.8	1.510	0.104	0.878	NA	NA	3.11	7.0	7.80	15.6
12	5	8	96.1	1	A	7.50	5.4	2.6	1.040	0.031	0.290	1.58	0.285	2.53	6.8	7.40	15.3
12	5	112	97.2	1	A	7.50	4.5	2.6	1.360	0.099	0.843	NA	NA	2.53	6.7	7.30	15.3
12	5	209	98.1	1	A	7.50	4.0	2.4	1.260	0.044	0.369	1.07	0.279	1.75	6.4	6.40	16.3
15	5	320	99.3	1	A	7.50	4.3	3.0	1.290	0.095	0.805	NA	NA	2.14	7.0	8.40	16.0
12	5	415	100.3	1	A	7.40	5.2	3.0	1.490	0.099	0.961	2.15	0.414	2.33	6.9	8.20	14.0

946510588

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	5	510	101.2	1	A	7.50	3.8	2.8	1.460	0.099	0.850	NA	NA	3.31	6.9	8.40	15.0
12	5	608	102.1	1	A	7.50	4.5	3.2	1.520	0.099	0.899	2.07	0.428	3.50	7.0	8.60	15.1
12	5	705	103.1	1	A	7.50	5.0	2.8	1.420	0.099	0.878	NA	NA	2.43	6.9	7.20	15.1
12	5	805	104.1	1	A	7.30	6.4	1.8	1.600	0.090	1.200	2.53	0.505	4.08	7.0	7.80	10.0
12	5	906	105.1	1	A	7.40	4.7	2.2	1.570	0.099	1.000	NA	NA	3.30	7.0	7.90	8.0
12	5	1003	106.0	1	A	7.40	4.3	2.0	1.440	0.081	0.864	1.45	0.313	1.95	7.0	6.20	12.0
12	5	1104	107.1	1	A	7.40	5.1	2.2	1.580	0.127	0.993	NA	NA	2.14	7.1	7.00	7.1
12	5	1205	108.1	1	A	7.40	4.0	1.8	1.450	0.095	0.868	2.47	0.454	2.53	7.1	6.80	14.0
12	5	1333	109.5	1	A	7.50	4.5	1.4	1.300	0.090	0.843	NA	NA	1.95	7.2	6.00	15.2
12	5	1504	111.1	1	A	7.50	5.7	1.8	1.240	0.090	0.774	2.23	0.449	1.56	7.1	6.10	15.8
12	5	1633	112.5	1	A	7.50	3.8	2.0	1.270	0.090	0.783	NA	NA	1.95	7.2	6.80	12.5
12	5	1802	114.0	1	A	7.40	7.0	2.2	0.944	0.026	0.518	0.97	0.254	4.08	6.8	7.50	7.2
12	5	1900	115.0	1	A	7.40	6.8	2.2	1.100	0.040	0.684	NA	NA	3.89	6.9	7.30	8.6
12	5	2030	116.5	1	A	7.40	3.3	1.6	0.833	0.026	0.388	1.00	0.177	2.92	6.8	7.20	14.0
12	5	2200	118.0	1	A	7.40	4.3	1.8	1.260	0.076	0.776	NA	NA	3.78	6.7	7.50	13.8
12	5	2332	119.5	1	A	7.40	4.0	2.0	1.830	0.108	0.912	2.40	0.406	3.30	6.0	8.00	13.0
12	6	105	121.1	1	A	7.50	4.1	2.0	1.330	0.081	0.744	NA	NA	3.89	6.3	7.60	14.6
12	6	229	122.5	1	A	7.50	5.5	2.8	1.040	0.063	0.589	1.83	0.409	1.95	6.3	7.60	15.1
12	6	400	124.0	1	A	7.50	4.0	2.2	1.260	0.090	0.787	NA	NA	2.72	6.0	7.60	14.5
12	6	530	125.5	1	A	7.50	3.7	1.8	1.070	0.063	0.574	1.24	0.305	3.11	6.4	7.80	15.6
12	6	658	127.0	1	A	7.50	3.7	2.0	0.634	0.026	0.257	NA	NA	2.43	5.3	9.00	9.3
12	6	805	128.1	1	A	7.50	7.5	2.6	1.290	0.037	1.140	2.89	0.570	5.64	5.5	9.00	8.7
12	6	933	129.5	1	A	7.50	11.0	3.6	1.210	0.065	1.080	NA	NA	5.40	5.6	8.15	7.0
12	6	1106	131.1	1	A	7.40	11.0	3.2	1.190	0.060	1.180	2.15	0.476	8.09	5.5	7.60	6.9
12	6	1235	132.6	1	A	7.40	7.3	3.0	1.480	0.079	1.070	NA	NA	6.74	6.0	9.30	10.0
12	6	1405	134.1	1	A	7.50	5.4	3.0	1.620	0.093	0.917	3.07	0.616	8.77	6.2	8.05	13.0

946510589

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	6	1536	135.6	1	A	7.50	5.1	2.4	1.420	0.083	0.803	NA	NA	5.40	6.1	7.60	14.0
12	6	1701	137.9	1	A	7.50	5.3	2.6	1.500	0.083	0.917	3.99	0.730	8.09	6.0	8.45	12.8
12	6	1833	138.5	1	A	7.50	8.5	2.4	0.933	0.023	0.397	NA	NA	7.42	5.5	8.80	11.0
12	6	2030	140.5	1	A	7.50	8.4	2.8	1.330	0.074	0.986	1.99	0.471	6.07	5.4	9.00	11.0
12	6	2202	142.0	1	A	7.40	12.0	2.8	1.290	0.069	1.150	NA	NA	5.40	5.0	9.00	9.0
12	6	2329	143.5	1	A	7.30	11.0	3.4	1.320	0.074	0.897	2.35	0.468	5.40	5.0	8.80	8.5
12	7	100	145.0	1	A	7.40	6.8	3.0	1.760	0.088	0.777	NA	NA	8.77	5.7	8.30	13.5
12	7	232	146.5	1	A	7.60	7.6	3.0	1.360	0.083	0.750	2.10	0.405	8.77	5.5	9.20	15.1
12	7	405	148.1	1	A	7.60	4.7	2.6	1.420	0.088	0.798	NA	NA	3.37	5.0	8.00	15.1
12	7	533	149.5	1	A	7.60	5.3	2.4	0.691	0.009	0.306	0.70	0.207	4.05	4.9	8.60	15.0
12	7	655	150.9	1	A	7.50	5.5	2.4	1.440	0.088	0.830	NA	NA	5.40	5.3	9.60	14.0
12	7	850	152.8	1	A	7.50	7.5	3.0	1.630	0.083	0.927	2.44	0.416	3.50	5.0	9.80	12.2
12	7	955	153.9	1	A	7.40	9.4	3.4	1.540	0.079	1.000	NA	NA	3.11	5.0	8.80	11.0
12	7	1050	154.8	1	A	7.40	11.0	2.2	1.160	0.051	0.740	2.06	0.354	5.64	5.0	8.60	9.8
12	7	1150	155.8	1	A	7.40	10.0	2.4	1.320	0.060	0.815	NA	NA	3.50	5.0	8.70	10.5
12	7	1305	157.1	1	A	7.50	6.0	2.0	1.650	0.088	0.904	2.29	0.362	4.47	5.5	8.40	12.9
12	7	1355	157.9	1	A	7.50	8.8	2.4	1.720	0.093	0.878	NA	NA	4.47	5.5	9.20	13.5
12	7	1500	159.0	1	A	7.60	10.0	3.2	1.350	0.037	0.415	NA	0.269	2.92	5.2	8.70	14.5
12	7	1600	160.0	1	A	7.60	7.4	4.4	0.881	0.018	0.244	1.75	0.352	2.92	5.5	8.75	14.5
12	7	1658	161.9	1	A	7.60	7.1	3.4	1.120	0.060	0.551	1.94	0.337	2.53	5.4	8.20	15.5
12	7	1800	162.0	1	A	7.60	6.9	2.0	1.430	0.088	0.551	NA	NA	2.14	5.4	7.15	14.2
12	7	1855	162.9	1	A	7.60	5.0	2.4	1.500	0.074	0.791	1.55	0.341	2.33	5.3	7.00	15.5
12	7	2005	164.1	1	A	7.50	6.5	1.8	1.580	0.088	0.872	NA	NA	2.92	5.2	8.00	13.4
12	7	2100	165.0	1	A	7.50	7.7	2.2	1.580	0.027	0.425	1.64	0.320	3.50	5.2	8.80	12.0
12	7	2202	166.0	1	A	7.40	8.5	1.6	1.510	0.074	0.897	NA	NA	3.31	5.1	9.40	11.0
12	7	2300	167.0	1	A	7.50	8.0	1.8	1.530	0.083	0.947	2.64	0.516	2.53	5.0	8.60	10.8

946510590

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	8	5	168.1	1	A	7.40	9.3	1.8	1.490	0.074	0.966	NA	NA	3.31	5.1	8.80	11.5
12	8	104	169.1	1	A	7.50	7.6	2.0	1.610	0.065	0.641	1.75	0.447	2.92	5.1	9.00	14.0
12	8	200	170.0	1	A	7.50	8.7	2.2	1.710	0.093	0.846	NA	NA	2.72	5.4	9.20	20.0
12	8	303	171.0	1	A	7.60	11.0	2.4	1.380	0.083	0.761	2.31	0.642	2.33	5.5	8.00	15.0
12	8	405	172.1	1	A	7.60	6.9	1.8	1.280	0.079	0.860	NA	NA	1.75	5.4	7.80	15.3
12	8	509	173.1	1	A	7.60	5.3	2.4	0.764	0.032	0.367	0.96	0.281	1.56	5.3	7.50	15.7
12	8	600	174.0	1	A	7.60	5.8	2.4	1.250	0.079	0.712	NA	NA	1.75	5.3	7.70	15.9
12	8	655	174.9	1	A	7.50	8.1	3.2	1.080	0.037	0.373	1.70	0.405	2.72	5.5	7.80	15.6
12	8	807	176.1	1	A	7.50	6.4	1.4	1.640	0.092	0.918	2.69	0.496	3.70	5.5	7.80	14.5
12	8	905	177.1	1	A	7.40	12.0	4.2	1.760	0.096	1.000	NA	NA	4.67	5.5	7.00	13.0
12	8	1006	178.1	1	A	7.40	12.0	3.4	1.720	0.087	1.000	NA	0.341	6.74	5.5	7.40	12.5
12	8	1108	179.1	1	A	7.40	11.0	2.6	1.710	0.153	1.160	NA	NA	4.08	5.3	7.70	11.5
12	8	1203	180.0	1	A	7.30	15.0	5.0	1.520	0.077	1.120	2.82	0.822	4.86	5.3	7.60	10.3
12	8	1300	181.0	1	A	7.40	12.0	3.0	1.550	0.082	1.130	NA	NA	4.30	5.3	7.70	10.3
12	8	1406	182.1	1	A	7.40	9.5	3.0	1.640	0.087	1.000	1.67	0.431	2.92	5.5	7.70	13.0
12	8	1505	183.1	1	A	7.40	10.5	2.0	1.380	0.087	0.870	NA	NA	3.70	5.5	7.90	14.5
12	8	1608	184.1	1	A	7.50	10.0	2.8	1.280	0.082	0.813	2.58	0.509	2.92	5.8	8.70	15.5
12	8	1701	185.0	1	A	7.50	9.3	3.0	1.380	0.087	0.842	NA	NA	2.92	5.5	7.40	15.3
12	8	1805	186.1	1	A	7.50	7.8	2.4	1.060	0.058	0.600	1.26	0.353	0.19	5.5	7.90	15.3
12	8	1900	187.0	1	A	7.50	7.0	2.5	1.460	0.092	0.891	NA	NA	3.70	5.8	7.80	15.0
12	8	2005	188.1	1	A	7.50	8.1	2.8	1.570	0.092	0.958	2.00	0.442	3.31	5.5	7.80	13.9
12	8	2100	189.0	1	A	7.40	11.0	2.8	1.230	0.025	0.509	NA	NA	3.11	5.2	8.30	12.2
12	8	2202	190.0	1	A	7.40	14.0	2.4	1.500	0.087	1.080	1.64	0.356	4.67	5.1	8.40	11.1
12	8	2300	191.0	1	A	7.40	13.0	3.0	1.480	0.082	1.110	NA	NA	3.99	5.3	8.60	12.0
12	9	3	192.0	1	A	7.40	14.0	2.8	1.280	0.044	0.847	1.60	0.306	0.58	5.0	8.00	12.0
12	9	106	193.1	1	A	7.40	15.0	3.4	1.190	0.025	0.504	NA	NA	5.06	4.9	7.90	8.2

946510591

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB (NTU)	BOD (PPM)	NH3 (PPM)	NO2 (PPM)	NO3 (PPM)	TKN (PPM)	TP (PPM)	CHLOR (PPB)	TEMP (*C)	D.O. (PPM)	SAL (PPT)
12	9	201	194.0	1	A	7.40	12.0	4.0	0.964	0.021	0.339	1.15	0.250	3.89	5.3	8.00	13.0
12	9	300	195.0	1	A	7.50	14.0	3.6	1.600	0.096	0.934	NA	NA	5.06	5.6	8.20	13.9
12	9	403	196.0	1	A	7.50	12.0	4.2	1.430	0.087	0.886	2.49	0.496	2.72	5.6	8.50	15.1
12	9	531	197.5	1	A	7.60	17.0	5.4	1.200	0.077	0.830	NA	NA	3.89	5.3	8.00	15.8
12	9	700	199.0	1	A	7.60	8.5	3.2	1.320	0.082	0.871	1.93	0.208	NA	5.3	8.40	15.0
12	9	835	200.6	1	A	7.50	6.8	2.6	1.470	0.087	0.923	2.51	0.450	2.72	5.5	7.90	15.5
12	9	1002	202.0	1	A	7.50	9.5	3.4	1.020	0.016	0.283	NA	NA	3.30	5.5	7.60	13.5
12	9	1134	203.6	1	A	7.50	15.0	2.9	1.510	0.087	1.180	2.23	0.454	3.50	5.0	7.50	11.3
12	9	1309	205.1	1	A	7.40	15.0	3.2	1.390	0.073	1.270	NA	NA	3.30	5.5	7.50	11.3
12	9	1435	206.6	1	A	7.40	14.0	3.0	0.896	0.030	0.561	1.75	0.635	3.50	4.5	7.60	8.3
12	9	1605	208.1	1	A	7.50	18.0	4.4	1.710	0.092	0.998	NA	NA	4.28	5.3	7.80	13.3
12	9	1732	209.5	1	A	7.60	11.0	3.0	1.220	0.030	0.420	1.42	0.303	2.53	5.3	8.40	16.0
12	9	1900	211.0	1	A	7.60	12.0	3.0	1.180	0.049	0.565	NA	NA	1.56	5.3	7.50	16.3
12	9	2030	212.5	1	A	7.50	7.5	2.4	1.070	0.049	0.548	1.77	0.330	5.40	5.0	7.40	14.0
12	9	2204	214.1	1	A	7.50	12.0	3.2	1.510	0.092	1.130	NA	NA	5.40	5.0	7.80	13.0
12	9	2332	215.5	1	A	7.50	16.0	3.8	1.180	0.040	0.582	2.01	0.516	3.11	4.9	7.00	11.3
12	10	102	217.0	1	A	7.40	15.0	3.2	1.220	0.063	1.120	NA	NA	3.31	4.1	7.90	8.9
12	10	231	218.5	1	A	7.50	12.0	3.4	1.330	0.063	0.811	2.17	0.605	2.72	5.0	8.20	13.3
12	10	400	220.0	1	A	7.60	15.0	3.4	1.410	0.087	0.859	NA	NA	2.33	5.0	8.40	15.0
12	10	529	221.5	1	A	7.60	11.0	2.4	1.170	0.077	0.796	NA	0.215	1.17	5.0	8.30	16.1
12	10	700	223.0	1	A	7.60	7.8	2.4	1.110	0.073	0.745	NA	NA	1.46	4.7	8.20	16.7
12	10	835	224.6	1	A	7.60	8.0	3.0	1.310	0.082	0.901	NA	0.177	1.16	4.8	8.00	15.8
12	10	1003	226.0	1	A	7.60	9.5	2.4	0.853	0.035	0.392	NA	NA	3.11	4.8	7.80	15.0
12	10	1135	227.6	1	A	7.60	14.0	3.2	1.520	0.082	0.978	1.82	0.398	3.50	4.8	8.10	12.8
12	10	1305	229.1	1	A	7.50	16.0	3.0	1.440	0.082	1.130	NA	NA	4.08	4.8	7.90	11.0
12	10	1432	230.5	1	A	7.60	17.0	3.0	0.934	0.030	0.615	1.44	0.430	4.28	4.3	7.60	8.8

946510592

KEARNY POINT-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	10	1600	232.0	1	A	7.60	14.0	2.6	1.540	0.092	1.010	NA	NA	2.92	5.0	8.20	13.0
12	10	1736	233.6	1	A	7.70	22.0	3.0	1.380	0.082	0.857	2.53	0.668	3.11	5.0	8.30	15.0
12	10	1845	234.8	1	A	7.70	21.0	2.8	0.877	0.044	0.526	NA	NA	3.31	5.0	8.50	16.9
12	10	2025	236.4	1	A	7.70	13.0	2.2	1.030	0.076	0.779	1.97	0.387	1.36	4.5	7.80	15.8
12	10	2200	238.0	1	A	7.60	13.0	2.2	1.120	0.087	0.889	NA	NA	2.92	4.3	8.80	15.1
12	10	2330	239.5	1	A	7.60	17.0	2.8	1.270	0.068	0.815	1.92	0.326	2.92	4.2	8.30	12.8
12	11	101	241.0	1	A	7.60	18.0	3.0	1.260	0.063	0.909	3.19	0.499	4.08	4.0	8.40	11.0
12	11	203	242.0	1	A	7.50	17.0	2.8	0.741	0.016	0.465	NA	0.140	9.44	3.8	8.40	9.0
12	11	302	243.0	1	A	7.50	18.0	4.6	0.882	0.025	0.416	NA	NA	7.42	3.8	7.40	9.9
12	11	400	244.0	1	A	7.70	16.0	3.0	1.670	0.082	0.829	NA	0.198	2.92	4.2	8.40	14.0
12	11	458	245.0	1	A	7.70	17.0	2.6	1.140	0.021	0.318	1.94	0.528	2.72	4.3	8.40	15.1
12	11	600	246.2	1	A	7.70	17.0	2.8	1.230	0.077	0.753	NA	0.131	2.14	4.5	8.80	16.2
12	11	655	246.9	1	A	7.70	24.0	4.0	1.160	0.077	0.732	NA	NA	3.31	4.2	8.60	17.5
12	11	810	248.2	1	A	7.60	5.6	2.0	0.813	0.076	0.725	NA	NA	2.14	4.5	7.70	16.8
12	11	935	249.1	1	A	7.60	6.2	2.2	0.949	0.028	0.340	1.23	0.248	2.72	4.3	7.90	16.0
12	11	1007	250.1	1	A	7.60	6.3	1.8	0.921	0.076	0.814	NA	NA	2.53	4.5	7.60	15.5
12	11	1108	251.1	1	A	7.60	8.3	2.4	1.170	0.081	0.919	NA	NA	1.95	4.5	7.60	15.0
12	11	1235	252.6	1	A	7.50	14.0	3.2	1.460	0.062	0.782	NA	NA	3.31	4.3	7.90	13.3
12	11	1336	253.6	1	A	7.50	13.0	2.6	1.570	0.076	1.090	2.87	0.669	2.92	4.3	8.00	11.5
12	11	1435	254.6	1	A	7.50	14.0	2.8	1.130	0.076	1.230	NA	NA	3.31	4.0	8.20	9.5
12	11	1535	255.5	1	A	7.50	11.0	2.8	1.220	0.028	0.477	1.96	0.690	1.56	4.0	7.60	8.8
12	11	1638	256.6	1	A	7.50	10.0	2.6	1.120	0.081	1.100	NA	NA	2.53	4.3	7.80	11.5
12	11	1730	257.5	1	A	7.60	14.0	2.8	1.210	0.043	0.478	1.69	0.343	3.11	4.5	7.70	14.5
12	11	1830	258.5	1	A	7.60	18.0	3.0	0.890	0.043	0.420	NA	NA	3.21	4.8	7.90	16.0
		AVERAGE READING				7.49	8.0	3.3	1.283	0.070	0.745	2.07	0.434	3.54	5.9	7.69	12.7

946510593

STØRM #3

KEARNY

PØINT

12-1/12-11-81

2/3 DEPTH

946510594

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1805	18.1	1	B	7.57	3.4	3.6	1.270	0.097	0.855	NA	0.177	2.72	NA	NA	15.6
12	1	1916	19.3	1	B	7.52	2.3	3.2	1.250	0.049	0.367	NA	NA	1.95	NA	NA	16.0
12	1	2011	20.2	1	B	7.54	2.2	3.2	1.270	0.088	0.700	NA	0.141	2.92	NA	NA	16.2
12	1	2110	21.2	1	B	7.53	3.1	3.0	0.737	0.014	0.128	0.78	0.176	3.11	NA	NA	16.0
12	1	2241	22.7	1	B	7.52	2.6	5.2	1.090	0.088	0.707	1.45	0.188	2.92	NA	NA	16.5
12	1	2400	24.2	1	B	7.54	2.1	3.8	0.808	0.023	0.200	NA	NA	2.14	NA	NA	16.8
12	2	126	25.4	1	B	7.52	2.4	4.2	0.855	0.023	0.213	0.97	0.268	2.72	NA	NA	15.2
12	2	232	26.5	1	B	7.49	2.6	3.6	1.390	0.113	1.020	NA	NA	2.14	NA	NA	13.3
12	2	401	28.2	1	B	7.46	4.8	6.0	0.907	0.023	0.450	1.00	0.244	3.11	NA	NA	15.5
12	2	511	29.2	1	B	7.51	2.8	3.8	0.939	0.028	0.406	NA	NA	2.53	NA	NA	16.2
12	2	615	30.3	1	B	7.51	3.2	4.2	1.060	0.056	0.405	1.48	0.349	2.72	NA	NA	15.0
12	2	705	31.1	1	B	7.57	3.3	3.7	1.110	0.070	0.443	NA	NA	2.72	NA	NA	16.3
12	2	900	33.0	1	B	7.50	2.4	4.6	1.390	0.103	0.648	2.38	0.408	3.50	6.4	7.50	16.8
12	2	958	34.	1	B	7.50	1.9	3.6	1.350	0.107	0.803	NA	NA	2.53	NA	NA	16.2
12	2	1059	35.0	1	B	7.50	3.4	4.6	1.280	0.102	0.766	NA	NA	4.05	7.5	6.50	16.2
12	2	1158	36.0	1	B	7.50	3.0	8.4	1.170	0.075	0.531	2.97	1.080	7.42	7.9	5.71	14.8
12	2	1257	36.9	1	B	7.50	2.5	4.8	1.180	0.094	0.657	2.35	0.575	3.50	NA	NA	NA
12	2	1400	38.2	1	B	7.50	2.9	5.5	1.190	0.085	0.645	NA	NA	4.72	7.3	7.60	16.4
12	2	1457	38.9	1	B	7.50	2.1	4.0	1.330	0.075	0.510	1.85	0.395	4.08	7.4	7.20	15.5
12	2	1600	40.0	1	B	7.50	2.1	4.0	1.390	0.111	0.810	NA	NA	2.92	6.9	7.40	11.8
12	2	1658	41.	1	B	7.50	2.3	4.4	1.290	0.094	0.657	1.40	0.265	3.70	7.3	6.30	14.0
12	2	1757	41.9	1	B	7.50	2.1	2.8	1.350	0.103	0.761	NA	NA	2.72	7.3	5.60	15.8
12	2	1856	42.9	1	B	7.50	5.0	5.4	1.450	0.066	1.180	2.80	0.631	3.11	7.2	6.49	13.8
12	2	2026	44.4	1	B	7.50	2.8	4.4	1.440	0.121	1.050	NA	NA	3.70	NA	NA	16.0
12	2	2123	45.4	1	B	7.50	2.3	2.8	1.220	0.136	1.010	3.05	0.514	4.28	NA	NA	16.5
12	2	2224	46.4	1	B	7.50	2.0	3.4	1.060	0.112	0.844	NA	NA	4.47	NA	NA	17.3

94510595

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	2	2329	47.5	1	B	7.50	2.8	4.0	0.824	0.055	0.407	1.31	0.338	3.11	7.2	7.10	17.2
12	3	34	48.6	1	B	7.60	2.0	2.6	0.927	0.083	0.629	NA	NA	2.72	7.3	6.20	17.3
12	3	139	49.6	1	B	7.50	3.2	5.8	1.070	0.107	0.783	2.14	0.382	3.11	7.3	6.10	17.3
12	3	245	50.8	1	B	7.50	2.1	2.6	0.832	0.036	0.260	NA	NA	2.72	7.5	7.00	17.0
12	3	356	51.9	1	B	7.50	3.1	2.9	0.874	0.055	0.383	NA	NA	4.05	7.3	5.90	16.0
12	3	506	53.1	1	B	7.50	2.8	2.4	1.160	0.056	0.508	NA	NA	4.05	7.2	5.85	16.0
12	3	603	54.1	1	B	7.50	3.4	2.8	0.731	0.023	0.283	2.03	0.382	2.70	7.2	6.20	16.0
12	3	705	55.1	1	B	7.50	3.2	3.0	1.040	0.045	0.332	1.81	0.352	4.39	7.2	6.00	16.3
12	3	758	56.0	1	B	7.40	7.6	5.6	1.220	0.083	0.610	NA	NA	NA	7.3	6.65	16.1
12	3	859	57.0	1	B	7.40	5.6	7.0	1.350	0.112	0.810	2.94	0.572	3.11	7.3	7.80	16.8
12	3	957	57.9	1	B	7.40	5.2	4.2	1.430	0.116	0.954	3.46	0.657	2.92	7.3	6.90	16.3
12	3	1056	58.9	1	B	7.40	4.7	5.0	1.560	0.121	1.100	NA	NA	4.28	7.4	7.30	17.8
12	3	1158	60.0	1	B	7.50	3.1	3.8	1.170	0.102	0.760	2.20	0.440	3.31	7.8	6.90	16.1
12	3	1255	60.9	1	B	7.40	4.6	3.6	1.480	0.112	1.250	NA	NA	4.08	7.8	7.25	17.2
12	3	1400	62.1	1	B	7.50	4.6	4.4	0.919	0.036	0.244	1.09	0.294	2.14	7.8	6.80	17.0
12	3	1457	62.9	1	B	7.50	4.2	3.4	1.130	0.061	0.472	NA	NA	2.92	7.4	6.60	17.0
12	3	1559	64.1	1	B	7.50	3.7	2.6	1.070	0.074	0.635	1.78	0.367	3.31	7.0	7.10	14.8
12	3	1657	64.9	1	B	7.40	9.4	3.0	0.953	0.045	0.368	NA	NA	NA	7.0	7.35	11.9
12	3	1800	66.0	1	B	7.50	3.8	2.6	1.290	0.112	0.859	NA	NA	2.53	7.1	6.00	16.0
12	3	1855	66.9	1	B	7.40	6.0	5.4	1.280	0.102	0.795	1.70	0.323	3.33	6.6	6.20	14.8
12	3	2014	68.2	1	B	7.40	5.2	5.6	0.854	0.055	0.445	3.25	0.478	7.42	7.2	6.00	15.0
12	3	2113	69.2	1	B	7.40	11.0	3.2	1.570	0.097	0.778	2.20	0.411	2.53	7.2	6.00	15.8
12	3	2211	70.2	1	B	7.40	11.0	6.4	1.280	0.121	0.899	NA	NA	5.45	7.5	6.30	15.3
12	3	2309	71.1	1	B	7.40	7.4	3.4	0.926	0.064	0.436	1.42	0.338	3.31	7.5	6.20	16.5
12	4	10	72.2	1	B	7.40	5.9	3.9	1.130	0.093	0.675	NA	NA	2.72	7.3	6.40	16.9
12	4	112	73.2	1	B	7.40	5.4	3.6	1.250	0.036	0.409	1.25	0.235	2.92	7.3	6.20	16.2

946510596

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	4	230	74.5	1	B	7.40	5.3	4.2	1.230	0.078	0.771	1.31	0.282	3.70	7.3	5.80	16.0
12	4	327	75.4	1	B	7.40	5.2	3.6	1.080	0.074	0.724	NA	NA	5.40	7.5	6.30	15.0
12	4	419	76.2	1	B	7.40	4.8	2.6	0.915	0.017	0.231	1.25	0.382	3.89	7.0	6.30	14.5
12	4	515	77.3	1	B	7.40	4.2	2.2	1.240	0.069	0.671	NA	NA	3.70	7.3	6.40	15.0
12	4	614	78.2	1	B	7.40	12.0	3.6	0.872	0.012	0.188	1.01	0.203	4.08	7.2	6.80	14.8
12	4	705	79.1	1	B	7.40	14.0	3.2	1.110	0.078	0.743	2.58	0.499	3.41	7.0	6.70	14.0
12	4	757	79.9	1	B	7.30	4.8	3.6	1.580	0.063	0.627	NA	0.187	2.14	7.0	7.12	14.6
12	4	859	81.0	1	B	7.40	7.7	5.2	1.320	0.072	0.685	NA	NA	2.33	7.1	7.28	15.0
12	4	1000	82.0	1	B	7.40	4.0	3.6	1.660	0.090	0.763	2.32	0.457	2.53	7.3	7.55	15.8
12	4	1058	83.0	1	B	7.50	4.0	3.4	1.060	0.085	0.727	NA	NA	1.75	7.3	6.85	16.4
12	4	1156	83.9	1	B	7.50	4.8	3.4	1.200	0.085	0.713	2.09	0.422	1.75	7.3	6.80	16.4
12	4	1255	84.9	1	B	7.50	4.7	3.8	1.200	0.061	0.618	1.81	0.235	1.36	7.3	6.62	16.0
12	4	1404	86.1	1	B	7.40	5.8	4.0	1.150	0.032	0.458	NA	0.158	3.11	7.5	6.20	17.0
12	4	1455	86.9	1	B	7.50	7.6	5.6	1.260	0.094	0.800	NA	NA	2.92	7.4	6.70	16.5
12	4	1558	88.0	1	B	7.50	3.5	4.0	1.390	0.090	0.714	4.14	0.623	1.75	7.3	6.90	15.8
12	4	1658	89.0	1	B	7.40	6.0	4.0	1.420	0.065	1.020	NA	NA	2.33	7.1	6.80	14.4
12	4	1758	90.0	1	B	7.40	4.0	3.4	1.470	0.094	0.916	1.99	0.405	2.53	6.8	7.60	14.3
12	4	1856	90.9	1	B	7.50	5.0	5.0	1.330	0.063	0.497	NA	NA	2.33	6.6	6.20	14.8
12	4	2018	92.3	1	B	7.40	4.0	3.2	1.580	0.099	0.802	2.34	0.416	2.14	7.3	5.80	15.1
12	4	2115	93.3	1	B	7.40	8.0	3.8	1.590	0.099	0.871	NA	NA	1.95	6.5	6.20	13.0
12	4	2213	94.2	1	B	7.40	5.7	1.6	1.530	0.099	0.873	2.72	0.551	1.75	6.9	5.80	15.5
12	4	2311	95.2	1	B	7.50	4.8	2.2	1.640	0.108	0.846	NA	NA	1.75	7.0	6.40	16.0
12	5	14	96.2	1	B	7.40	6.5	2.2	1.360	0.090	0.737	2.55	0.475	1.36	7.0	6.20	16.7
12	5	115	97.3	1	B	7.50	4.5	1.8	1.290	0.081	0.702	NA	NA	1.75	6.9	6.20	16.9
12	5	213	98.2	1	B	7.50	4.2	1.6	1.110	0.072	0.591	1.62	0.310	0.97	6.9	5.80	17.1
12	5	323	99.4	1	B	7.50	4.3	2.2	0.878	0.035	0.247	NA	NA	1.36	7.0	7.60	16.6

946510597

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	5	423	100.3	1	B	7.50	7.8	4.2	1.320	0.086	0.704	2.18	0.521	1.75	7.0	7.60	16.3
12	5	515	101.3	1	B	7.40	4.0	2.0	0.953	0.031	0.277	NA	NA	1.56	6.9	7.40	16.1
12	5	611	102.2	1	B	7.40	4.5	2.6	1.520	0.099	0.786	2.64	0.470	2.72	6.9	7.40	16.6
12	5	708	103.1	1	B	7.50	6.2	2.6	1.400	0.090	0.746	NA	NA	1.56	7.0	7.00	16.2
12	5	800	104.0	1	B	7.40	6.0	2.6	1.150	0.063	0.517	1.69	0.367	2.53	7.2	7.50	15.1
12	5	859	105.0	1	B	7.40	4.2	5.8	1.610	0.099	0.852	NA	NA	2.33	7.2	6.60	15.2
12	5	957	105.9	1	B	7.40	4.0	1.8	1.610	0.090	0.856	1.70	0.369	2.72	7.2	6.60	15.2
12	5	1058	107.0	1	B	7.50	4.3	2.6	1.330	0.081	0.707	NA	NA	1.36	7.3	7.50	17.1
12	5	1200	108.0	1	B	7.40	12.0	2.0	1.310	0.090	0.736	2.20	0.615	4.47	7.2	7.30	16.2
12	5	1327	109.4	1	B	7.50	4.3	2.2	1.350	0.083	0.806	NA	NA	3.11	7.1	6.60	15.2
12	5	1456	111.0	1	B	7.50	6.2	1.6	1.310	0.083	0.823	2.58	0.495	3.11	7.2	7.00	16.1
12	5	1627	112.4	1	B	7.50	11.0	2.2	1.310	0.083	0.823	2.17	0.778	1.36	7.2	7.40	16.0
12	5	1756	113.9	1	B	7.40	8.5	4.4	1.480	0.083	0.885	NA	NA	2.92	7.2	6.80	13.9
12	5	1855	114.9	1	B	7.40	3.8	1.6	1.380	0.083	0.827	1.75	0.264	2.33	7.2	6.50	14.2
12	5	2040	116.7	1	B	7.50	3.3	1.8	1.450	0.088	0.824	1.76	0.628	2.72	7.0	5.60	16.0
12	5	2204	118.1	1	B	7.40	4.0	1.8	0.936	0.008	0.293	NA	NA	2.72	7.0	6.20	15.8
12	5	2334	119.6	1	B	7.40	23.0	3.6	1.520	0.088	0.852	2.07	0.427	1.95	6.7	7.40	15.4
12	6	139	121.1	1	B	7.50	5.5	1.6	1.570	0.017	0.875	NA	NA	2.92	6.6	6.70	15.6
12	6	233	122.5	1	B	7.50	5.0	1.6	1.460	0.086	0.713	1.80	0.413	2.72	6.5	6.60	15.9
12	6	436	124.1	1	B	7.50	7.4	2.2	1.040	0.044	0.375	NA	NA	3.50	6.5	7.00	15.9
12	6	534	125.6	1	B	7.50	4.0	1.2	0.671	0.031	0.262	0.99	0.271	2.33	6.5	7.20	16.0
12	6	714	127.1	1	B	7.50	3.7	1.2	0.792	0.017	0.239	NA	NA	2.24	6.5	7.00	15.1
12	6	800	128.0	1	B	7.50	8.3	2.0	1.330	0.085	0.802	3.21	0.634	7.42	6.8	7.90	15.5
12	6	927	129.4	1	B	7.40	7.8	5.2	0.954	0.089	1.050	NA	NA	4.72	6.2	6.52	15.0
12	6	1100	131.0	1	B	7.20	4.5	5.2	1.370	0.089	1.060	3.13	0.790	8.09	6.4	6.60	12.8
12	6	1230	132.5	1	B	7.40	6.5	4.0	1.560	0.085	0.814	NA	NA	8.09	6.6	9.50	14.3

946510598

KEARNY POINT-LEVEL 0-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	6	1358	134.[illegible]	1	B	7.50	5.8	3.4	1.320	0.089	0.831	3.44	0.946	6.74	6.7	8.05	14.9
12	6	1530	135.5	1	B	7.50	6.4	3.6	0.951	0.061	0.563	NA	NA	5.40	6.4	7.65	15.4
12	6	1655	136.[illegible]	1	B	7.50	6.6	3.4	1.120	0.094	0.887	3.36	0.772	5.40	6.3	7.45	15.4
12	6	1827	138.4	1	B	7.50	6.7	2.6	0.749	0.028	0.416	NA	NA	4.72	6.0	8.40	12.4
12	6	2035	140.6	1	B	7.50	6.4	3.0	1.280	0.075	0.906	1.51	0.383	4.72	5.9	7.60	14.0
12	6	2215	142.1	1	B	7.40	12.0	3.4	1.000	0.037	0.776	NA	NA	6.74	5.1	8.80	9.2
12	6	2333	143.5	1	B	7.30	8.0	3.4	0.902	0.023	0.274	1.50	0.445	4.72	5.0	8.70	9.0
12	7	104	145.1	1	B	7.50	7.2	3.0	1.230	0.056	0.553	NA	NA	8.77	6.0	7.80	14.7
12	7	235	146.6	1	B	7.60	12.0	3.0	1.340	0.089	0.886	2.29	0.484	4.05	5.7	8.80	15.5
12	7	407	148.1	1	B	7.60	5.9	3.0	1.320	0.089	0.867	NA	NA	8.77	5.3	7.80	15.8
12	7	535	149.6	1	B	7.60	5.1	2.8	0.610	0.019	0.304	0.61	0.298	3.37	5.3	8.60	15.0
12	7	7[illegible]	151.[illegible]	1	B	7.60	7.7	3.2	1.490	0.094	0.926	NA	NA	4.05	5.4	9.60	14.5
12	7	855	152.9	1	B	7.40	16.0	5.4	1.580	0.075	0.899	1.95	0.412	5.25	5.2	9.80	12.2
12	7	958	154.[illegible]	1	B	7.40	7.9	3.4	1.540	0.099	0.981	NA	NA	2.72	5.5	8.10	13.0
12	7	1155	154.[illegible]	1	B	7.40	15.0	3.6	1.100	0.052	0.757	1.54	0.425	4.08	5.5	7.20	12.5
12	7	1155	155.9	1	B	7.40	8.2	2.4	1.330	0.094	0.916	NA	NA	3.89	5.5	8.40	13.0
12	7	1319	157.2	1	B	7.50	7.3	2.2	1.500	0.089	0.921	2.66	0.505	3.50	5.5	8.00	14.0
12	7	1439	158.[illegible]	1	B	7.50	15.0	3.6	1.580	0.099	0.921	NA	NA	5.25	5.5	9.00	14.0
12	7	1555	159.1	1	B	7.60	8.5	2.6	1.330	0.085	0.842	2.13	0.486	2.53	5.5	8.80	15.0
12	7	1655	160.1	1	B	7.60	8.4	3.0	1.230	0.080	0.786	NA	NA	2.53	5.7	9.45	15.5
12	7	1705	161.1	1	B	7.60	12.0	3.6	1.080	0.070	0.661	1.97	0.497	2.53	5.5	7.80	16.0
12	7	1806	162.1	1	B	7.60	7.3	3.0	1.290	0.089	0.842	NA	NA	2.14	5.5	7.00	15.5
12	7	1914	163.[illegible]	1	B	7.60	5.1	3.0	1.360	0.089	0.864	2.02	0.368	1.75	5.5	7.75	14.9
12	7	2019	164.2	1	B	7.50	12.0	3.2	1.550	0.094	0.899	NA	NA	3.50	5.3	7.80	14.0
12	7	2104	165.1	1	B	7.50	7.6	3.2	1.560	0.075	0.787	1.62	0.396	2.72	5.2	8.60	12.6
12	7	2205	166.1	1	B	7.40	8.4	2.2	1.470	0.080	0.920	NA	NA	3.70	5.1	8.80	11.3

946510599

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #5

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [STU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
12	7	2304	167.1	1	B	7.40	9.5	3.2	1.420	0.080	1.150	2.58	0.642	3.31	5.2	7.60	13.0
12	8	7	168.1	1	B	7.60	10.0	3.2	1.440	0.089	0.876	NA	NA	3.89	5.3	7.60	14.0
12	8	107	169.1	1	B	7.50	13.0	3.4	1.410	0.085	0.896	2.54	0.602	3.11	5.4	8.70	14.9
12	8	205	170.1	1	B	7.60	7.7	4.4	0.914	0.037	0.378	NA	NA	1.75	5.4	8.80	19.9
12	8	307	171.1	1	B	7.60	18.0	4.8	1.350	0.094	0.824	2.10	1.520	3.50	5.5	7.70	15.5
12	8	408	172.1	1	B	7.50	15.0	6.0	1.240	0.047	0.468	1.36	0.382	1.95	5.4	7.80	16.0
12	8	504	173.1	1	B	7.60	21.0	3.6	1.210	0.085	0.782	2.88	0.615	2.14	5.3	7.60	16.0
12	8	608	174.1	1	B	7.60	21.0	4.0	1.220	0.085	0.787	2.30	0.411	3.70	5.3	6.40	16.0
12	8	706	175.1	1	B	7.60	6.5	3.6	1.200	0.085	0.779	1.82	0.399	1.56	5.5	7.80	15.9
12	8	802	176.0	1	B	7.60	11.0	3.8	1.370	0.083	0.874	NA	0.246	3.31	5.5	8.30	15.5
12	8	900	177.0	1	B	7.50	8.8	4.0	1.430	0.088	0.922	4.02	0.704	3.11	5.8	8.20	14.8
12	8	1001	178.0	1	B	7.40	13.0	3.6	1.740	0.088	1.050	NA	0.370	5.45	5.5	7.50	13.3
12	8	1103	179.0	1	B	7.50	16.0	4.2	1.540	0.088	0.962	NA	NA	3.70	5.5	7.50	13.0
12	8	1157	179.9	1	B	7.40	20.0	5.6	1.570	0.088	1.010	NA	0.245	3.89	5.5	7.30	14.3
12	8	1255	180.9	1	B	7.50	18.0	4.2	1.310	0.078	0.942	NA	NA	5.06	5.5	7.70	13.5
12	8	1401	182.0	1	B	7.50	11.0	2.8	1.500	0.088	0.972	2.54	0.474	3.50	5.8	8.10	15.0
12	8	1500	183.0	1	B	7.50	28.0	3.6	1.540	0.088	1.010	2.92	0.704	6.74	5.9	8.10	15.0
12	8	1603	184.1	1	B	7.60	26.0	3.8	1.270	0.065	0.735	NA	0.168	5.40	5.8	8.70	16.0
12	8	1656	184.9	1	B	7.60	9.5	2.4	1.080	0.072	0.647	2.03	0.382	3.11	5.8	7.90	16.3
12	8	1800	186.0	1	B	7.60	20.0	3.4	0.778	0.031	0.270	0.78	0.316	3.70	5.5	7.20	16.3
12	8	1855	186.9	1	B	7.60	11.0	2.6	0.648	0.017	0.132	NA	NA	2.43	5.8	7.00	16.5
12	8	2010	188.2	1	B	7.50	11.0	2.9	1.560	0.095	0.871	NA	0.218	2.92	5.5	7.80	15.0
12	8	2103	189.	1	B	7.50	12.0	2.6	1.550	0.090	0.960	2.86	0.587	3.70	5.3	8.20	12.8
12	8	2200	190.1	1	B	7.50	17.0	3.2	1.520	0.090	1.020	2.18	0.485	4.28	5.3	8.00	12.0
12	8	2304	191.1	1	B	7.60	18.0	3.0	1.290	0.086	0.784	NA	NA	3.31	5.6	7.60	14.8
12	9	6	192.1	1	B	7.60	14.0	4.2	1.260	0.014	0.700	1.84	0.604	0.78	5.3	8.00	14.0

946510600

KEARNY POINT-LEVEL 6-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	9	138	193.1	1	B	7.60	13.0	4.4	1.030	0.023	0.536	NA	NA	4.08	5.2	7.60	10.5
12	9	204	194.1	1	B	7.40	17.0	3.8	1.480	0.088	1.080	NA	0.250	3.70	5.7	7.80	14.0
12	9	3 5	195.1	1	B	7.50	13.0	3.8	1.650	0.092	1.060	NA	NA	6.07	5.9	8.00	14.6
12	9	436	196.1	1	B	7.50	15.0	5.0	1.310	0.078	0.962	NA	0.172	7.42	5.8	8.20	15.6
12	9	535	197.6	1	B	7.50	41.0	3.2	1.170	0.074	0.883	NA	NA	5.40	5.7	7.80	16.1
12	9	702	199.0	1	B	7.60	17.0	2.6	1.190	0.074	0.899	1.97	0.273	1.75	5.6	7.90	15.9
12	9	830	200.5	1	B	7.60	10.0	2.4	1.210	0.083	0.967	NA	0.132	2.14	5.5	7.90	16.5
12	9	957	201.9	1	B	7.50	15.0	4.6	1.200	0.055	0.749	NA	NA	2.72	5.5	7.60	14.5
12	9	1129	203.5	1	B	7.50	14.0	3.4	1.180	0.046	0.830	1.59	0.415	3.50	5.5	7.50	13.8
12	9	1304	205.1	1	B	7.50	12.0	3.0	1.470	0.088	1.230	NA	NA	2.14	5.5	7.50	13.8
12	9	1430	206.5	1	B	7.50	12.0	2.6	1.260	0.074	0.966	2.33	0.558	3.11	5.5	8.10	15.3
12	9	16..	208..	1	B	7.50	26.0	3.4	1.640	0.078	1.010	NA	NA	2.33	5.5	8.00	14.5
12	9	1727	209.4	1	B	7.60	13.0	2.8	1.170	0.069	0.883	2.32	0.529	2.14	5.5	8.50	16.3
12	9	1855	210.9	1	B	7.60	14.0	2.6	0.986	0.060	0.739	NA	NA	2.33	5.3	8.30	16.5
12	9	2035	212.6	1	B	7.60	7.9	2.0	1.000	0.046	0.610	1.17	0.292	1.56	5.1	7.30	14.9
12	9	2207	214.1	1	B	7.50	9.7	2.4	1.360	0.046	0.924	NA	NA	2.92	5.0	7.60	13.2
12	9	2335	215.6	1	B	7.50	15.0	4.1	1.120	0.069	0.971	2.24	0.661	2.92	5.0	6.70	11.9
12	10	105	217.1	1	B	7.60	21.0	5.0	1.280	0.078	0.911	NA	NA	3.70	5.0	7.10	12.3
12	10	234	218.6	1	B	7.50	14.0	3.6	1.360	0.065	0.914	1.81	0.520	2.53	5.1	7.80	14.0
12	10	4 4	220.1	1	B	7.60	34.0	5.2	0.650	0.014	0.583	NA	NA	6.07	5.2	8.10	15.4
12	10	534	221.6	1	B	7.60	15.0	3.0	1.130	0.069	0.877	NA	0.177	2.14	5.0	8.00	16.6
12	10	705	223.	1	B	7.60	12.0	2.8	1.090	0.069	0.827	NA	NA	1.36	5.0	8.20	16.7
12	10	839	224.9	1	B	7.70	13.0	2.6	1.180	0.069	0.818	1.65	0.295	1.36	5.3	8.20	16.8
12	10	959	226.	1	B	7.7	12.0	3.0	1.240	0.074	0.936	NA	NA	2.33	5.0	8.00	15.8
12	10	1130	227.5	1	B	7.60	17.0	3.0	1.480	0.097	1.220	3.44	0.792	2.72	4.8	8.40	13.0
12	10	1300	229.0	1	B	7.60	19.0	4.0	1.410	0.065	0.985	NA	NA	3.70	5.0	7.60	11.5

946510601

KEARNY POINT-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
12	10	1427	230.4	1	B	7.60	32.0	5.6	1.260	0.069	1.120	2.56	0.789	5.40	4.8	7.70	12.3
12	10	1555	231.9	1	B	7.60	20.0	3.8	1.510	0.078	1.040	NA	NA	6.07	5.0	8.10	15.0
12	10	1731	233.5	1	B	7.60	38.0	2.4	1.550	0.078	0.962	2.51	0.794	6.07	5.0	8.20	15.0
12	10	1840	234.7	1	B	7.70	32.0	3.5	0.636	0.023	0.376	NA	NA	4.72	5.0	8.50	16.0
12	10	2030	236.5	1	B	7.70	50.0	5.8	0.890	0.032	0.457	0.95	0.348	7.42	4.8	7.60	16.3
12	10	2233	238.7	1	B	7.60	15.0	3.0	1.330	0.078	1.000	NA	NA	3.11	4.7	8.60	15.3
12	10	2332	239.5	1	B	7.60	19.0	3.2	1.550	0.083	1.200	NA	0.246	3.11	4.3	8.20	12.9
12	11	104	241.1	1	B	7.60	20.0	3.6	1.430	0.078	1.180	NA	NA	2.72	4.0	8.20	11.4
12	11	205	242.1	1	B	7.60	17.0	2.8	0.924	0.032	0.548	1.62	0.539	2.53	4.0	7.20	10.2
12	11	305	243.1	1	B	7.60	33.0	4.2	1.210	0.074	1.020	NA	NA	7.42	4.3	7.40	13.2
12	11	403	244.1	1	B	7.60	20.0	2.8	1.510	0.083	1.100	NA	0.213	2.53	4.5	8.00	14.8
12	11	501	245.0	1	B	7.60	43.0	4.6	1.360	0.078	0.992	NA	NA	5.40	4.5	8.30	15.4
12	11	603	246.0	1	B	7.70	32.0	2.4	1.000	0.055	0.745	1.00	0.402	6.74	4.6	8.40	16.4
12	11	700	247.0	1	B	7.70	26.0	3.2	1.130	0.065	0.827	NA	NA	3.92	4.6	8.40	17.9
12	11	805	248.1	1	B	7.70	7.5	2.0	1.090	0.072	0.689	1.23	0.253	1.36	4.5	8.10	17.0
12	11	900	249.0	1	B	7.70	5.4	1.8	0.903	0.072	0.686	NA	NA	1.56	4.8	7.30	17.3
12	11	1002	250.0	1	B	7.60	6.8	2.0	0.989	0.072	0.744	1.39	0.294	1.56	4.5	7.80	16.3
12	11	1103	251.0	1	B	7.60	8.8	2.4	1.470	0.076	0.821	NA	NA	1.56	4.5	7.70	15.3
12	11	1230	252.5	1	B	7.60	15.0	3.0	1.490	0.081	0.969	2.51	0.536	2.33	4.5	8.10	13.5
12	11	1330	253.5	1	B	7.50	17.0	4.8	1.540	0.081	1.080	NA	NA	3.89	4.3	8.00	12.0
12	11	1430	254.5	1	B	7.50	16.0	3.2	1.330	0.081	1.070	3.03	0.821	3.50	4.5	7.40	10.5
12	11	1525	255.4	1	B	7.50	22.0	3.8	1.280	0.076	0.873	NA	NA	6.74	4.5	7.70	11.0
12	11	1633	256.5	1	B	7.60	11.0	2.6	1.370	0.081	0.867	NA	0.267	2.72	4.5	8.00	16.0
12	11	1725	257.4	1	B	7.60	21.0	3.4	1.600	0.086	0.901	NA	NA	6.07	4.5	7.70	15.3
12	11	1825	258.4	1	B	7.60	23.0	3.2	1.130	0.072	0.743	2.09	0.745	2.82	4.8	8.00	16.0

946510602

AVERAGE READING	7.51	13.2	3.5	1.247	0.073	0.750	2.07	0.443	3.43	6.1	7.40	15.0

946510603

STØRM #3

JACKSØN STREET

12-1/12-11-81

1/3 DEPTH

946510604

JACKSON ST-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1800	18.0	2	A	7.55	4.0	4.2	1.160	0.066	1.120	2.67	0.683	3.89	5.5	6.40	6.5
12	1	2100	21.0	2	A	7.44	3.6	3.4	0.699	0.043	0.705	NA	NA	3.31	6.0	7.00	12.3
12	2	0	24.0	2	A	7.46	3.8	4.0	0.824	0.024	0.399	1.16	0.433	4.05	6.0	6.70	10.0
12	2	300	27.0	2	A	7.50	7.4	8.2	1.290	0.085	1.380	NA	NA	5.40	5.5	8.00	5.3
12	2	600	30.0	2	A	7.57	8.6	7.8	1.310	0.057	1.390	2.93	1.090	4.72	5.5	8.20	2.0
12	2	835	32.6	2	A	7.50	5.4	4.0	1.350	0.085	1.980	3.02	0.807	4.05	5.0	8.80	1.5
12	2	1130	35.5	2	A	7.40	4.5	4.0	1.330	0.103	1.370	NA	NA	4.72	5.5	8.30	4.5
12	2	1430	38.5	2	A	7.50	5.9	4.4	1.390	0.089	2.130	3.86	1.120	4.05	5.0	9.30	2.0
12	2	1730	41.5	2	A	7.60	6.6	7.2	1.610	0.066	2.150	NA	NA	2.70	5.0	10.10	0.2
12	2	2030	44.5	2	A	7.50	7.0	5.8	1.570	0.062	1.940	2.80	0.680	0.39	5.0	9.80	0.8
12	2	2333	47.5	2	A	7.50	4.2	4.0	1.010	0.052	0.878	NA	NA	2.70	5.8	6.50	10.5
12	3	245	50.8	2	A	7.50	6.0	5.6	1.120	0.038	0.872	1.47	0.486	2.33	5.3	8.70	2.5
12	3	540	53.7	2	A	7.50	7.2	5.6	1.440	0.066	1.560	NA	NA	5.06	5.3	9.60	1.8
12	3	830	56.5	2	A	7.50	8.7	6.0	1.470	0.062	1.710	2.82	0.622	3.11	5.1	8.70	0.4
12	3	1130	59.5	2	A	7.30	6.3	4.0	1.340	0.096	1.390	NA	NA	2.53	5.7	8.00	8.2
12	3	1430	62.5	2	A	7.30	6.8	4.0	1.410	0.047	0.973	1.47	0.362	3.70	5.8	8.40	5.0
12	3	1730	65.5	2	A	7.30	9.0	6.8	1.150	0.062	1.450	NA	NA	4.28	5.5	8.90	2.1
12	3	2030	68.5	2	A	7.40	13.0	7.4	1.330	0.057	1.440	3.08	0.663	8.09	5.5	8.00	1.3
12	3	2325	71.4	2	A	7.30	8.6	5.6	1.420	0.072	1.380	NA	NA	3.89	5.5	8.10	3.0
12	4	230	74.5	2	A	7.40	8.3	3.6	1.280	0.086	1.150	2.56	0.579	2.72	5.5	8.90	4.5
12	4	530	77.5	2	A	7.50	13.0	5.4	1.340	0.057	1.440	NA	NA	3.31	5.5	6.20	2.3
12	4	825	80.4	2	A	7.20	16.0	5.4	1.050	0.037	1.310	1.96	0.337	7.42	5.2	9.60	0.8
12	4	1125	83.4	2	A	7.30	8.3	4.6	1.130	0.042	1.080	NA	NA	3.31	5.6	9.20	4.2
12	4	1430	86.5	2	A	7.30	7.9	4.4	1.210	0.076	1.300	3.08	0.612	4.67	5.8	7.60	10.0
12	4	1715	89.3	2	A	7.40	12.0	5.4	1.420	0.057	1.530	NA	NA	4.47	5.5	9.10	3.0
12	4	2035	92.6	2	A	7.50	13.0	5.0	1.680	0.052	1.860	3.84	0.754	8.77	5.0	10.60	1.2

946510605

JACKSON ST-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	4	2330	95.5	2	A	7.40	10.0	4.8	1.570	0.052	1.720	NA	NA	4.08	5.1	10.20	2.6
12	5	240	98.7	2	A	7.40	6.3	3.2	1.180	0.086	1.020	1.91	0.409	4.28	6.1	7.80	10.9
12	5	535	101.6	2	A	7.50	11.0	3.6	1.120	0.042	1.100	NA	NA	4.67	5.2	9.70	3.6
12	5	835	104.6	2	A	7.40	17.0	4.0	1.330	0.042	1.600	2.73	0.547	5.84	5.0	9.00	1.3
12	5	1130	107.5	2	A	7.50	14.0	3.6	1.450	0.047	1.500	NA	NA	9.44	5.0	9.20	2.0
12	5	1425	110.4	2	A	7.50	12.0	3.6	1.150	0.037	0.983	2.17	0.419	6.03	5.3	8.60	4.7
12	5	1725	113.4	2	A	7.50	13.0	3.2	1.260	0.062	1.460	NA	NA	4.86	4.7	8.80	4.7
12	5	2030	116.5	2	A	7.50	16.0	3.8	0.927	0.037	1.260	2.57	0.496	5.39	5.0	9.30	3.0
12	5	2330	119.5	2	A	7.50	15.0	3.2	1.100	0.057	1.400	NA	NA	5.64	5.0	10.20	3.3
12	6	230	122.5	2	A	7.50	7.8	2.2	0.580	0.027	0.652	1.22	0.244	2.53	6.4	8.10	14.9
12	6	530	125.5	2	A	7.50	13.0	2.0	0.557	0.017	0.660	NA	NA	5.06	5.1	9.40	6.7
12	6	815	128.3	2	A	7.40	15.0	3.2	0.732	0.037	0.677	1.10	0.226	9.44	5.0	11.25	1.5
12	6	1115	131.3	2	A	7.40	18.0	3.4	0.809	0.062	1.270	NA	NA	7.42	5.0	8.60	2.0
12	6	1415	134.3	2	A	7.40	14.0	2.9	0.840	0.012	1.310	1.97	0.420	3.50	5.0	9.00	6.0
12	6	1700	137.0	2	A	7.40	14.0	3.0	0.560	0.022	0.460	NA	NA	7.42	5.0	9.00	6.0
12	6	2030	140.5	2	A	7.40	19.0	3.0	0.839	0.032	0.919	1.65	0.444	6.74	4.4	10.30	3.6
12	6	2325	143.4	2	A	7.40	22.0	3.8	0.819	0.062	1.350	NA	NA	7.42	4.0	9.30	1.2
12	7	235	146.6	2	A	7.30	16.0	2.8	1.100	0.052	1.230	1.71	0.358	3.89	4.4	9.30	8.2
12	7	530	149.5	2	A	7.40	12.0	2.8	0.825	0.062	0.666	1.83	0.354	4.67	4.9	8.70	10.2
12	7	750	151.8	2	A	7.40	13.0	3.0	1.060	0.042	1.230	2.25	0.429	2.53	4.5	9.00	6.0
12	7	1050	154.8	2	A	7.40	17.0	4.1	0.869	0.072	1.450	NA	NA	4.86	4.0	9.00	3.0
12	7	1450	158.8	2	A	7.30	15.0	3.6	1.220	0.049	1.210	2.13	0.472	4.28	5.0	8.00	5.0
12	7	1635	160.6	2	A	7.40	8.2	3.3	1.140	0.062	0.968	NA	NA	3.50	5.0	9.00	12.0
12	7	2030	164.5	2	A	7.40	14.0	3.6	0.995	0.042	1.329	2.47	0.633	4.67	4.8	9.10	7.0
12	7	2340	167.7	2	A	7.40	18.0	4.4	0.892	0.052	1.510	NA	NA	7.42	4.0	9.50	2.2
12	8	230	170.5	2	A	7.40	13.0	3.4	0.852	0.091	0.892	2.46	0.708	3.70	4.9	8.70	8.8

94651060

JACKSON ST-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	8	535	173.6	2	A	7.40	11.0	3.6	1.360	0.066	1.020	NA	NA	3.50	5.3	7.80	13.9
12	8	805	176.1	2	A	7.40	11.0	3.4	1.170	0.057	0.993	2.31	0.620	3.50	5.0	9.50	8.3
12	8	1105	179.1	2	A	7.40	20.0	4.6	0.674	0.024	0.837	NA	NA	6.74	4.0	8.25	4.8
12	8	1405	182.1	2	A	7.40	15.0	4.7	0.971	0.024	0.769	2.50	0.545	6.07	5.0	9.25	6.0
12	8	1740	185.7	2	A	7.40	14.0	3.4	1.220	0.080	1.100	NA	NA	5.40	5.0	8.00	10.0
12	8	2030	188.5	2	A	7.40	16.0	3.4	1.160	0.061	1.410	2.97	0.646	5.40	4.6	9.10	6.6
12	8	2335	191.6	2	A	7.40	21.0	3.4	0.924	0.038	0.726	NA	NA	6.74	4.0	9.80	2.8
12	9	235	194.6	2	A	7.40	17.0	3.6	1.030	0.056	1.490	NA	2.300	3.37	3.9	9.70	2.9
12	9	535	197.6	2	A	7.50	15.0	2.8	1.510	0.089	1.050	NA	NA	4.72	5.1	8.00	13.5
12	9	805	200.1	2	A	7.50	19.0	3.0	1.270	0.057	0.993	2.68	0.825	4.72	5.0	9.00	10.0
12	9	1110	203.2	2	A	7.50	26.0	3.8	1.060	0.052	1.500	NA	NA	8.09	4.0	11.00	4.0
12	9	1405	206.1	2	A	7.50	23.0	2.2	0.854	0.033	1.490	2.33	0.609	6.07	3.0	9.00	1.5
12	9	1640	208.7	2	A	7.40	37.0	4.6	1.230	0.066	1.280	NA	NA	8.09	4.0	9.00	6.0
12	9	2030	212.5	2	A	7.50	17.0	2.6	1.240	0.066	1.160	3.55	0.982	5.40	4.0	8.70	9.2
12	9	2335	215.6	2	A	7.50	32.0	4.0	1.010	0.047	1.590	NA	NA	7.42	2.9	9.80	2.9
12	10	235	218.6	2	A	7.50	22.0	5.0	0.970	0.038	1.420	2.69	0.799	6.74	2.2	10.10	1.6
12	10	530	221.5	2	A	7.50	14.0	3.8	1.020	0.038	0.593	NA	NA	12.81	3.3	8.20	10.7
12	10	805	224.1	2	A	7.60	15.0	2.6	1.220	0.052	0.706	2.39	0.555	2.92	4.8	9.25	12.0
12	10	1105	227.1	2	A	7.50	27.0	3.4	0.918	0.038	0.898	2.45	0.607	4.86	4.0	9.00	6.0
12	10	1405	230.1	2	A	7.50	32.0	5.0	0.936	0.038	1.350	3.42	1.520	7.42	3.0	9.00	2.0
12	10	1640	232.7	2	A	7.50	22.0	3.8	1.020	0.043	1.290	NA	NA	5.40	3.0	9.00	4.0
12	10	2035	236.6	2	A	7.50	17.0	2.8	1.300	0.075	1.220	2.29	0.534	3.70	2.9	8.80	10.9
12	10	2325	239.4	2	A	7.50	32.0	4.4	1.170	0.061	1.510	NA	NA	9.44	2.6	9.20	5.4
12	11	230	242.5	2	A	7.50	38.0	5.8	1.060	0.047	1.870	2.63	0.663	11.46	1.9	10.00	1.2
12	11	530	245.5	2	A	7.50	22.0	4.0	1.050	0.043	0.987	NA	NA	6.74	2.7	9.30	8.5
12	11	820	248.3	2	A	7.60	12.0	2.8	1.360	0.085	0.975	2.48	0.600	2.72	4.8	10.50	15.0

9465106O7

JACKSON ST-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	11	1120	251.3	2	A	7.50	16.0	3.2	1.030	0.047	0.945	NA	NA	2.14	4.0	8.75	8.8
12	11	1405	254.1	2	A	7.50	16.0	3.8	1.110	0.038	1.360	2.73	0.977	5.40	2.0	9.00	4.0
12	11	1635	256.6	2	A	7.50	24.0	3.4	1.090	0.047	1.700	NA	NA	5.40	3.0	9.00	2.0
		AVERAGE READING				7.44	14.5	4.1	1.124	0.054	1.234	2.44	0.655	5.18	4.7	8.91	5.4

946510608

STØRM #3

JACKSØN STREET

12-1/12-11-81

2/3 DEPTH

946510609

JACKSON ST-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1805	18.1	2	B	7.35	3.2	3.8	1.120	0.088	1.270	2.36	0.534	3.37	6.0	6.20	11.3
12	1	2105	21.1	2	B	7.41	2.7	3.6	1.110	0.051	0.638	NA	NA	4.72	6.0	6.80	13.5
12	2	5	24.1	2	B	7.45	2.9	3.6	0.966	0.042	0.541	1.43	0.343	4.72	6.3	4.40	16.0
12	2	305	27.1	2	B	7.50	7.4	8.6	1.420	0.097	1.590	NA	NA	4.72	5.5	6.00	5.5
12	2	605	30.1	2	B	7.58	8.7	7.4	1.130	0.065	1.560	2.40	0.661	4.72	5.5	5.70	2.0
12	2	840	32.7	2	B	7.50	5.4	5.0	1.230	0.074	1.640	2.32	0.649	3.37	5.0	8.60	1.8
12	2	1135	35.6	2	B	7.40	2.7	3.6	0.985	0.065	0.787	NA	NA	3.31	5.5	7.80	9.4
12	2	1435	38.6	2	B	7.50	5.2	4.2	1.320	0.106	1.770	3.95	0.901	4.28	5.0	8.80	2.0
12	2	1735	41.6	2	B	7.40	4.1	5.4	1.190	0.046	0.806	NA	NA	4.08	5.0	10.00	0.2
12	2	2035	44.6	2	B	7.50	6.2	5.6	1.550	0.074	1.940	3.17	0.798	2.53	5.5	6.20	4.8
12	2	2335	47.6	2	B	7.50	3.1	4.0	1.000	0.051	0.685	NA	NA	0.78	6.3	5.50	16.3
12	3	250	50.8	2	B	7.50	4.0	3.6	0.717	0.010	0.201	1.15	0.332	1.95	5.3	8.70	3.0
12	3	545	53.8	2	B	7.50	6.6	4.8	1.370	0.033	0.835	NA	NA	2.92	5.3	7.80	7.0
12	3	835	56.6	2	B	7.30	7.6	4.0	1.410	0.065	1.480	2.37	0.552	2.33	5.1	8.50	3.1
12	3	1135	59.6	2	B	7.40	8.3	NA	1.390	0.088	0.922	NA	NA	4.08	6.0	6.70	12.5
12	3	1435	62.6	2	B	7.40	5.4	2.8	1.160	0.097	1.170	3.21	0.616	4.67	5.8	8.00	5.7
12	3	1735	65.6	2	B	7.30	7.9	3.6	1.180	0.060	1.020	NA	NA	3.11	5.5	8.10	2.1
12	3	2035	68.6	2	B	7.40	8.4	4.0	1.390	0.051	0.820	2.27	0.445	6.03	6.5	6.00	15.0
12	3	2330	71.5	2	B	7.40	22.0	5.0	1.090	0.037	0.695	NA	NA	12.14	5.8	7.00	7.0
12	4	235	74.6	2	B	7.40	7.1	3.4	1.330	0.090	1.080	2.02	0.426	3.50	5.5	8.90	5.5
12	4	535	77.6	2	B	7.40	14.0	4.6	0.917	0.047	0.846	NA	NA	5.93	5.5	8.80	3.3
12	4	830	80.5	2	B	7.30	5.8	3.8	1.110	0.027	0.699	1.57	0.353	2.92	5.7	8.60	9.2
12	4	1130	83.5	2	B	7.40	7.3	4.0	0.767	0.076	0.388	NA	NA	3.89	5.8	8.00	5.0
12	4	1435	86.6	2	B	7.40	4.5	3.6	1.120	0.032	0.791	1.75	0.393	2.72	6.0	6.20	15.0
12	4	1720	89.3	2	B	7.40	6.0	3.8	1.040	0.022	0.472	NA	NA	4.08	5.5	9.10	3.0
12	4	2040	92.7	2	B	7.50	10.0	4.2	1.060	0.091	0.434	1.42	0.344	7.42	5.0	10.20	1.2

946510610

JACKSON ST-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	4	2335	95.6	2	B	7.40	17.0	4.0	1.210	0.096	0.944	NA	NA	6.07	5.1	10.00	3.5
12	5	245	98.8	2	B	7.40	6.2	5.4	1.050	0.022	1.080	1.43	0.294	2.14	6.8	6.20	15.1
12	5	540	101.7	2	B	7.40	6.8	3.6	0.695	0.091	0.303	NA	NA	3.70	5.2	9.50	4.9
12	5	830	104.5	2	B	7.50	6.1	2.4	1.210	0.066	1.030	2.72	0.401	1.95	5.0	9.00	1.3
12	5	1125	107.4	2	B	7.50	12.0	2.8	1.540	0.032	1.480	NA	NA	4.08	5.0	8.80	2.1
12	5	1430	110.5	2	B	7.50	6.0	2.2	0.794	0.022	0.640	1.01	0.229	2.53	6.7	5.40	15.3
12	5	1730	113.5	2	B	7.50	5.3	2.6	0.555	0.076	0.170	NA	NA	2.33	4.7	8.90	4.7
12	5	2035	116.6	2	B	7.50	8.6	2.8	1.280	0.086	0.994	2.74	0.453	3.11	5.0	8.60	3.0
12	5	2335	119.6	2	B	7.50	9.7	2.8	1.200	0.072	1.070	NA	NA	3.11	5.1	9.70	4.8
12	6	235	122.6	2	B	7.50	5.7	2.8	1.190	0.027	0.784	1.93	0.382	2.33	6.8	6.50	16.2
12	6	535	125.6	2	B	7.50	5.5	2.2	0.386	0.091	0.385	NA	NA	2.82	5.1	8.80	8.4
12	6	826	128.4	2	B	7.50	13.0	3.2	0.953	0.037	0.936	2.86	0.569	4.47	5.0	11.50	1.0
12	6	1120	131.3	2	B	7.50	15.0	3.2	0.635	0.047	1.380	NA	NA	4.86	5.0	7.40	6.0
12	6	1420	134.3	2	B	7.40	11.0	3.2	1.150	0.012	0.888	1.71	0.345	4.47	5.5	9.00	6.5
12	6	1705	137.1	2	B	7.40	9.5	2.8	0.290	0.047	0.144	NA	NA	3.89	5.0	8.75	8.0
12	6	2035	140.6	2	B	7.50	18.0	3.4	0.699	0.037	1.140	2.18	0.502	8.09	4.5	9.00	3.7
12	6	2330	143.5	2	B	7.40	23.0	4.0	0.816	0.027	1.390	NA	NA	8.09	4.2	8.10	2.4
12	7	240	146.7	2	B	7.40	26.0	4.2	0.690	0.052	0.459	2.33	0.725	9.44	4.7	9.20	8.6
12	7	535	149.6	2	B	7.40	13.0	3.0	0.861	0.032	0.709	NA	NA	5.40	5.0	8.50	10.9
12	7	745	151.8	2	B	7.60	11.0	2.4	0.958	0.047	0.553	1.14	0.391	2.33	4.0	10.00	7.0
12	7	1045	154.8	2	B	7.40	15.0	2.4	0.927	0.057	0.627	NA	NA	5.45	4.0	9.25	4.0
12	7	1445	158.8	2	B	7.40	18.0	3.1	1.070	0.047	0.953	1.94	0.500	5.84	5.0	8.25	5.5
12	7	1630	160.5	2	B	7.50	8.6	2.4	0.733	0.062	0.566	NA	NA	3.89	6.0	9.00	14.0
12	7	2035	164.6	2	B	7.70	14.0	2.6	1.110	0.042	1.040	2.51	0.551	3.50	4.8	8.70	6.9
12	7	2345	167.8	2	B	7.50	18.0	2.8	0.867	0.042	1.560	NA	NA	7.42	4.1	9.20	2.5
12	8	235	170.6	2	B	7.60	24.0	3.8	1.020	0.057	0.893	3.26	1.110	6.74	4.9	8.60	8.9

94651061

JACKSON ST-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	8	540	173.7	2	B	7.60	22.0	2.8	1.570	0.027	0.375	NA	NA	4.72	5.4	7.20	14.0
12	8	800	176.0	2	B	7.50	11.0	2.2	1.430	0.079	0.991	1.14	0.431	5.40	5.0	10.25	10.0
12	8	1100	179.0	2	B	7.40	18.0	2.6	1.060	0.046	1.370	NA	NA	7.42	4.0	8.50	5.0
12	8	1400	182.0	2	B	7.40	26.0	3.6	1.310	0.056	1.010	2.64	0.745	9.44	4.0	9.00	6.0
12	8	1735	185.6	2	B	7.50	15.0	2.2	1.390	0.079	1.000	NA	NA	5.40	5.8	8.25	14.0
12	8	2035	188.6	2	B	7.40	16.0	1.6	1.280	0.023	0.508	2.00	0.633	5.40	4.4	8.60	6.8
12	8	2340	191.7	2	B	7.40	20.0	3.0	1.010	0.046	1.510	NA	NA	8.09	4.0	9.30	3.0
12	9	240	194.7	2	B	7.50	24.0	2.6	0.961	0.056	1.040	3.44	1.260	8.09	4.0	9.30	3.0
12	9	540	197.7	2	B	7.50	21.0	2.2	1.430	0.083	0.967	NA	NA	7.42	5.3	7.60	14.0
12	9	800	200.0	2	B	7.50	16.0	6.2	0.869	0.028	0.571	1.94	0.639	3.89	5.0	10.00	10.0
12	9	1105	203.1	2	B	7.50	26.0	4.0	1.060	0.051	1.400	NA	NA	8.09	4.0	11.00	4.0
12	9	1400	206.0	2	B	7.50	25.0	5.0	0.916	0.037	1.630	3.89	1.230	7.42	3.0	9.00	2.0
12	9	1635	208.6	2	B	7.40	48.0	5.6	1.280	0.037	0.820	NA	NA	10.12	4.0	8.00	6.0
12	9	2035	212.6	2	B	7.50	16.0	2.8	1.320	0.079	0.981	1.45	0.393	5.40	4.0	8.70	9.9
12	9	2340	215.7	2	B	7.50	34.0	4.6	1.060	0.051	1.480	NA	NA	7.42	3.0	9.30	2.9
12	10	240	218.7	2	B	7.50	37.0	5.2	0.798	0.028	0.857	4.36	1.860	9.44	2.2	10.00	1.8
12	10	535	221.6	2	B	7.60	18.0	5.8	0.986	0.074	0.915	NA	NA	3.71	3.7	7.50	11.6
12	10	800	224.0	2	B	7.60	13.0	3.4	1.270	0.046	0.607	2.03	0.559	3.70	4.8	11.00	12.0
12	10	1100	227.0	2	B	7.50	24.0	4.8	1.020	0.033	0.745	NA	NA	8.09	4.0	9.00	7.0
12	10	1400	230.0	2	B	7.50	29.0	4.8	1.000	0.042	1.590	3.71	1.420	10.79	3.0	10.00	2.0
12	10	1635	232.6	2	B	7.50	23.0	3.8	1.040	0.051	1.430	NA	NA	8.09	3.0	9.00	4.0
12	10	2040	236.7	2	B	7.50	15.0	3.4	1.120	0.060	0.755	2.39	0.607	4.28	3.0	8.50	12.6
12	10	2330	239.5	2	B	7.50	30.0	4.0	1.190	0.060	1.290	NA	NA	14.16	2.6	9.30	5.4
12	11	235	242.6	2	B	7.50	34.0	4.6	1.050	0.046	1.820	2.62	0.767	10.12	2.0	9.10	1.2
12	11	815	248.3	2	B	7.50	13.0	2.8	1.010	0.014	0.239	1.80	0.548	2.72	4.8	11.00	15.0
12	11	1115	251.3	2	B	7.50	16.0	2.8	1.220	0.056	1.060	NA	NA	3.31	4.0	8.75	8.0

94510612

JACKSON ST-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	11	1400	254.5	2	B	7.50	23.0	3.8	1.110	0.051	1.660	4.62	2.300	6.07	2.0	9.25	4.0
12	11	1630	256.5	2	B	7.50	18.0	3.8	1.110	0.046	1.740	NA	NA	5.06	3.0	10.00	2.0
		AVERAGE READING				7.47	14.2	3.7	1.073	0.054	0.969	2.37	0.663	5.24	4.8	8.49	6.9

946510613

STØRM #3

BELLEVILLE TURNPIKE

12-1/12-11-81

1/3 DEPTH

946510614

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1900	19.0	3	A	7.52	4.7	4.2	1.810	0.070	2.190	4.18	0.859	6.07	4.3	7.10	0.5
12	1	2155	21.9	3	A	7.40	6.1	5.3	1.600	0.090	2.170	NA	NA	4.72	5.0	7.80	3.3
12	2	100	25.0	3	A	7.52	5.7	5.0	1.560	0.090	2.350	3.31	0.485	4.72	5.0	9.70	1.0
12	2	350	27.8	3	A	7.58	8.6	5.6	1.580	0.060	2.540	NA	NA	11.46	4.3	10.20	0.0
12	2	635	30.6	3	A	7.54	9.6	6.8	1.690	0.050	2.190	3.69	0.909	5.40	4.3	11.20	0.0
12	2	920	33.3	3	A	7.60	7.4	9.8	2.140	0.040	2.240	5.35	1.190	1.36	5.0	9.70	0.0
12	2	1210	36.2	3	A	7.60	6.6	7.4	1.710	0.057	2.180	NA	NA	1.75	5.0	9.50	0.0
12	2	1510	39.2	3	A	7.50	6.8	7.4	1.670	0.050	1.870	3.29	1.040	5.40	4.9	10.50	0.0
12	2	1815	42.3	3	A	7.40	7.7	11.6	1.720	0.050	1.760	NA	NA	3.37	5.0	10.10	0.0
12	2	2115	45.3	3	A	7.50	8.4	12.4	1.840	0.068	1.660	3.54	0.773	3.89	5.0	9.80	0.0
12	3	20	48.3	3	A	7.50	7.4	8.6	1.710	0.068	1.780	NA	NA	4.08	5.0	10.00	0.0
12	3	325	51.4	3	A	7.50	9.5	11.0	1.530	0.040	1.510	2.61	0.515	3.37	5.3	8.80	0.0
12	3	620	54.3	3	A	7.50	12.0	9.2	1.530	0.053	1.560	NA	NA	12.14	5.3	10.80	0.0
12	3	910	57.2	3	A	7.30	12.0	8.0	1.510	0.040	1.560	2.44	0.402	5.06	5.3	9.60	0.0
12	3	1210	60.2	3	A	7.30	11.0	7.6	1.560	0.040	1.550	NA	NA	4.08	5.3	10.40	0.0
12	3	1505	63.1	3	A	7.30	13.0	7.6	1.490	0.040	1.600	2.91	0.598	6.74	5.5	11.00	0.0
12	3	1810	66.2	3	A	7.40	16.0	8.0	1.680	0.044	1.690	NA	NA	6.07	5.2	11.20	0.0
12	3	2115	69.3	3	A	7.50	14.0	7.8	1.780	0.040	1.810	3.10	0.541	7.42	5.3	9.10	0.0
12	4	10	72.2	3	A	7.40	17.0	7.8	1.610	0.030	1.300	NA	NA	10.79	5.3	9.70	0.0
12	4	310	75.2	3	A	7.50	18.0	8.2	1.780	0.044	1.780	3.88	0.848	10.12	5.0	11.20	0.0
12	4	605	78.1	3	A	7.60	16.0	8.2	2.090	0.053	2.030	NA	NA	18.88	4.8	9.60	0.0
12	4	910	81.2	3	A	7.40	14.0	4.2	1.840	0.040	1.920	3.12	0.648	9.44	5.0	11.80	0.0
12	4	1220	84.3	3	A	7.50	12.0	6.2	2.040	0.040	2.040	NA	NA	7.42	5.0	10.60	0.0
12	4	1520	87.3	3	A	7.50	13.0	7.2	1.930	0.049	2.020	3.33	0.626	5.40	5.0	11.40	0.0
12	4	1800	90.0	3	A	7.40	22.0	6.2	1.300	0.030	1.700	NA	NA	10.12	4.0	10.90	0.0
12	4	2105	93.1	3	A	7.50	18.0	7.0	1.100	0.034	1.660	2.77	0.631	10.79	4.9	11.10	0.0

946510615

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	4	2355	95.9	3	A	7.50	21.0	6.0	1.230	0.039	1.730	NA	NA	13.49	5.0	11.30	0.0
12	5	305	99.1	3	A	7.50	18.0	6.6	1.270	0.039	1.700	2.70	0.499	9.44	5.0	11.20	0.0
12	5	555	101.9	3	A	7.50	18.0	6.6	1.000	0.034	1.650	NA	NA	12.81	4.8	11.30	0.0
12	5	850	104.8	3	A	7.30	19.0	5.8	0.893	0.034	1.600	2.15	0.487	11.46	4.8	11.70	0.0
12	5	1145	107.8	3	A	7.50	20.0	6.0	0.948	0.034	1.640	NA	NA	10.12	4.7	11.50	0.0
12	5	1445	110.8	3	A	7.50	18.0	5.4	0.957	0.034	1.600	2.65	0.420	10.79	4.7	11.10	0.0
12	5	1740	113.7	3	A	7.50	22.0	5.4	0.983	0.034	1.620	NA	NA	7.42	4.9	11.70	0.0
12	5	2055	116.9	3	A	7.50	18.0	5.6	0.915	0.034	1.630	2.19	0.435	6.07	4.8	10.60	0.0
12	6	5	120.1	3	A	7.50	20.0	5.2	0.959	0.034	1.650	NA	NA	15.51	4.6	11.60	0.0
12	6	300	123.0	3	A	7.50	17.0	4.6	1.020	0.034	1.570	2.90	0.483	10.79	4.6	11.40	0.2
12	6	550	125.8	3	A	7.50	18.0	5.4	0.969	0.030	1.660	NA	NA	8.77	4.3	11.60	0.0
12	6	840	128.7	3	A	7.70	28.0	5.8	0.904	0.034	1.770	2.00	0.427	7.42	4.0	12.00	0.0
12	6	1135	131.6	3	A	7.70	30.0	5.4	0.955	0.039	1.800	NA	NA	6.74	4.0	9.50	0.0
12	6	1440	134.7	3	A	7.50	32.0	5.0	0.938	0.039	1.710	3.68	0.661	6.07	4.0	11.00	0.0
12	6	1720	137.3	3	A	7.50	26.0	5.0	0.983	0.039	1.690	NA	NA	6.74	4.3	10.50	1.0
12	6	2045	140.8	3	A	7.60	23.0	4.6	1.030	0.044	1.840	2.30	0.532	12.14	3.5	11.70	0.0
12	6	2345	143.8	3	A	7.60	44.0	5.6	1.060	0.044	1.900	NA	NA	10.12	3.2	11.50	0.0
12	7	250	146.8	3	A	7.50	31.0	7.8	1.010	0.039	1.760	3.57	0.955	12.81	3.7	11.20	0.2
12	7	545	149.8	3	A	7.50	50.0	5.2	0.994	0.044	1.730	NA	NA	3.37	3.5	11.00	0.2
12	7	820	152.3	3	A	7.70	26.0	5.8	1.040	0.044	1.840	2.60	0.768	8.77	3.0	10.50	0.0
12	7	1115	155.3	3	A	7.60	28.0	5.3	1.190	0.039	1.810	NA	NA	5.40	3.0	11.50	0.0
12	7	1510	159.2	3	A	7.50	41.0	6.4	1.290	0.044	1.830	3.19	0.948	8.77	3.0	8.25	0.0
12	7	1700	161.0	3	A	7.40	25.0	4.4	1.120	0.049	1.670	NA	NA	6.74	4.0	11.00	2.0
12	7	2050	164.8	3	A	7.50	32.0	5.4	1.100	0.044	1.840	3.79	1.540	4.72	3.2	10.50	0.0
12	8		168.0	3	A	7.60	21.0	4.2	1.120	0.044	1.920	NA	NA	3.50	3.0	11.30	0.0
12	8	250	170.8	3	A	7.50	43.0	6.2	1.080	0.044	1.790	4.69	1.700	10.12	3.5	10.50	0.2

94510616

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	8	550	173.8	3	A	7.40	21.0	4.4	1.140	0.049	1.630	NA	NA	5.40	3.9	10.10	2.0
12	8	825	176.4	3	A	7.50	25.0	4.2	1.090	0.040	1.690	3.68	0.789	8.09	4.0	9.00	1.0
12	8	1120	179.3	3	A	7.50	28.0	4.6	1.080	0.030	1.850	NA	NA	8.09	3.5	11.00	0.0
12	8	1425	182.4	3	A	7.50	31.0	5.3	1.050	0.030	1.830	4.93	1.670	8.09	4.0	11.25	0.0
12	8	1805	186.1	3	A	7.40	22.0	4.0	1.050	0.030	1.500	NA	NA	7.42	4.0	10.00	2.3
12	8	2100	189.0	3	A	7.50	31.0	4.8	1.040	0.030	1.810	4.36	0.624	6.74	3.3	11.00	0.0
12	9	0	192.0	3	A	7.60	26.0	4.8	1.160	0.040	1.960	NA	NA	4.72	3.0	11.40	0.0
12	9	300	195.0	3	A	7.60	36.0	5.6	1.070	0.020	1.480	3.30	1.550	10.79	2.9	11.50	0.0
12	9	600	198.0	3	A	7.40	32.0	4.8	1.120	0.040	1.540	NA	NA	10.12	3.8	9.50	2.5
12	9	825	200.4	3	A	7.50	28.0	6.6	1.070	0.009	1.510	2.53	0.384	6.07	3.5	11.00	1.0
12	9	1135	203.6	3	A	7.50	32.0	2.6	1.160	0.040	2.000	NA	NA	10.79	2.5	11.25	0.5
12	9	1425	206.4	3	A	7.50	22.0	4.8	1.250	0.040	1.980	2.49	0.816	2.92	3.0	11.00	0.0
12	9	1705	209.1	3	A	7.50	46.0	7.6	1.120	0.040	1.910	NA	NA	12.14	3.0	11.00	0.5
12	9	2055	212.9	3	A	7.50	29.0	5.6	1.120	0.040	1.870	4.48	1.290	1.35	3.6	11.10	0.1
12	10	0	216.0	3	A	7.50	35.0	7.2	1.290	0.040	2.080	NA	NA	8.09	2.3	11.30	0.0
12	10	255	218.9	3	A	7.50	29.0	6.0	1.290	0.040	2.000	2.13	0.416	4.05	2.1	11.40	0.0
12	10	555	221.9	3	A	7.50	48.0	7.4	1.140	0.040	1.810	NA	NA	1.17	2.3	10.10	0.9
12	10	825	224.4	3	A	7.50	26.0	8.6	1.140	0.040	1.810	3.38	0.549	8.09	3.0	10.25	1.0
12	10	1121	227.3	3	A	7.60	44.0	10.2	1.230	0.040	2.020	NA	NA	10.12	2.8	11.00	1.0
12	10	1425	230.4	3	A	7.50	30.0	10.8	1.350	0.040	2.200	3.92	1.030	6.74	3.0	10.50	0.0
12	10	1705	233.1	3	A	7.50	50.0	11.6	1.290	0.040	2.080	NA	NA	9.44	3.0	10.75	1.0
12	10	2055	236.9	3	A	7.50	26.0	8.2	1.160	0.040	1.850	3.36	0.552	4.05	2.0	11.20	0.8
12	10	2345	239.8	3	A	7.50	39.0	11.0	1.310	0.040	2.120	NA	NA	6.07	1.9	10.80	0.0
12	11	250	242.8	3	A	7.50	18.0	8.2	1.330	0.040	2.280	3.17	1.030	4.05	1.9	10.70	0.0
12	11	550	245.8	3	A	7.50	71.0	13.5	1.250	0.030	1.690	NA	NA	16.93	1.8	11.00	0.2
12	11	840	248.7	3	A	7.50	19.0	3.6	1.260	0.040	1.700	3.04	0.550	6.07	3.0	10.00	2.0

946510617

BELLEVILLE TURNPIKE-LEVEL A-1/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
12	11	1135	251.6	3	A	7.50	31.0	6.0	1.330	0.040	2.080	NA	NA	7.42	3.0	10.25	0.0
12	11	1425	254.4	3	A	7.50	28.0	5.0	1.370	0.040	2.320	2.34	0.563	7.42	2.0	10.50	0.0
12	11	1655	256.9	3	A	7.50	26.0	5.2	1.340	0.040	2.320	NA	NA	6.74	2.0	10.50	0.0
		AVERAGE READING				7.50	23.6	6.6	1.301	0.042	1.834	3.24	0.774	7.65	3.9	10.62	0.3

946510618

STØRM #3

BELLEVILLE TURNPIKE

12-1/12-11-81

2/3 DEPTH

946510619

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1905	19.1	3	B	7.45	4.7	4.2	1.810	0.080	2.240	3.87	0.549	4.72	4.5	6.50	1.8
12	1	2200	22.6	3	B	7.40	6.0	6.2	1.570	0.090	1.970	NA	NA	6.07	5.0	8.00	3.5
12	2	105	25.1	3	B	7.48	6.6	4.8	1.580	0.080	2.100	2.95	0.516	4.72	4.5	9.30	1.0
12	2	355	27.9	3	B	7.50	6.3	6.6	1.620	0.070	2.530	NA	NA	6.74	4.3	10.20	0.0
12	2	640	30.7	3	B	7.60	7.8	7.0	1.710	0.060	2.220	3.02	0.530	8.43	4.3	11.20	0.0
12	2	925	33.4	3	B	7.70	7.6	11.6	2.180	0.060	2.260	4.30	0.721	3.11	5.0	9.20	0.0
12	2	1215	36.3	3	B	7.50	6.4	8.2	2.010	0.070	2.350	NA	NA	2.14	5.0	9.30	0.0
12	2	1515	39.3	3	B	7.50	7.0	7.4	1.700	0.050	1.890	2.40	0.435	5.40	4.9	10.50	0.0
12	2	1820	42.3	3	B	7.50	7.6	11.8	1.720	0.050	1.760	NA	NA	6.07	5.0	10.10	0.0
12	2	2120	45.3	3	B	7.50	8.2	11.6	1.750	0.050	1.350	2.34	0.595	3.89	5.0	9.80	0.0
12	3	25	48.4	3	B	7.50	7.3	9.2	1.680	0.050	1.770	NA	NA	4.28	5.0	9.80	0.0
12	3	330	51.5	3	B	7.50	9.3	11.4	1.520	0.040	1.530	3.21	0.885	4.05	5.3	8.80	0.0
12	3	625	54.4	3	B	7.50	11.0	10.2	1.690	0.040	1.560	NA	NA	6.07	5.3	10.60	0.0
12	3	915	57.3	3	B	7.50	15.0	8.2	1.510	0.040	1.570	2.41	0.367	12.14	5.3	9.70	0.0
12	3	1215	60.3	3	B	7.40	13.0	8.4	1.560	0.040	1.560	NA	NA	10.12	5.3	10.40	0.0
12	3	1510	63.2	3	B	7.50	15.0	8.6	1.590	0.053	1.600	2.82	0.665	15.51	5.5	11.10	0.0
12	3	1815	66.3	3	B	7.50	20.0	9.6	1.720	0.040	1.680	NA	NA	18.88	5.2	11.30	0.0
12	3	2120	69.3	3	B	7.60	16.0	7.8	1.780	0.040	1.760	2.68	0.493	8.09	5.3	9.10	0.0
12	4	15	72.3	3	B	7.60	20.0	9.2	1.620	0.040	1.680	NA	NA	7.42	5.3	9.70	0.0
12	4	315	75.3	3	B	7.60	20.0	8.4	1.750	0.049	1.790	3.38	0.557	10.12	5.0	11.20	0.0
12	4	610	78.2	3	B	7.60	18.0	8.6	2.120	0.060	2.260	NA	NA	10.79	4.8	9.60	0.0
12	4	915	81.3	3	B	7.40	15.0	6.6	1.800	0.053	1.900	3.44	0.614	11.46	5.0	11.60	0.0
12	4	1225	84.4	3	B	7.50	13.0	6.6	2.180	0.053	2.000	NA	NA	6.74	5.0	10.60	0.0
12	4	1525	87.4	3	B	7.50	12.0	6.6	2.020	0.053	1.970	3.12	0.675	12.81	5.0	11.30	0.0
12	4	1805	90.1	3	B	7.40	21.0	7.4	1.310	0.039	1.660	NA	NA	11.46	5.0	10.80	0.0
12	4	2110	93.2	3	B	7.50	18.0	6.0	1.080	0.039	1.640	2.59	0.512	11.46	4.9	11.10	0.0

946510620

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	5	0	96.0	3	B	7.50	24.0	7.8	1.220	0.039	1.660	NA	NA	7.42	5.0	11.30	0.0
12	5	310	99.2	3	B	7.50	20.0	6.2	1.320	0.030	1.700	4.60	1.440	6.74	5.0	11.10	0.0
12	5	600	102.0	3	B	7.50	20.0	5.8	1.020	0.020	1.620	NA	NA	12.82	4.8	11.30	0.0
12	5	845	104.8	3	B	7.50	22.0	4.4	0.885	0.034	1.560	2.31	0.537	4.08	4.8	11.70	0.0
12	5	1150	107.8	3	B	7.50	20.0	5.0	0.924	0.034	1.580	NA	NA	5.84	4.8	11.40	0.0
12	5	1450	110.8	3	B	7.50	17.0	5.0	0.965	0.034	1.640	2.41	0.450	6.07	4.8	11.10	0.0
12	5	1745	113.8	3	B	7.50	21.0	5.8	0.884	0.030	1.540	NA	NA	8.77	4.9	11.60	0.0
12	5	2100	117.0	3	B	7.50	18.0	5.2	0.921	0.034	1.610	2.48	0.531	8.77	4.8	10.60	0.0
12	6	10	120.2	3	B	7.50	20.0	5.2	0.941	0.034	1.600	NA	NA	4.72	4.8	11.60	0.0
12	6	305	123.1	3	B	7.50	17.0	4.2	0.966	0.030	1.220	3.06	0.465	8.09	4.7	11.10	0.4
12	6	555	125.9	3	B	7.50	19.0	5.0	0.815	0.034	1.640	NA	NA	7.08	4.2	11.50	0.0
12	6	845	128.8	3	B	7.60	33.0	6.0	0.909	0.039	1.720	2.56	0.645	6.74	4.0	12.00	0.0
12	6	1140	131.7	3	B	7.60	26.0	5.2	0.994	0.044	1.740	NA	NA	6.07	4.0	9.75	0.0
12	6	1445	134.8	3	B	7.60	26.0	5.4	0.946	0.039	1.770	3.35	0.634	9.44	4.0	11.50	0.0
12	6	1725	137.4	3	B	7.50	25.0	4.6	0.954	0.039	1.570	NA	NA	5.40	4.0	10.75	1.0
12	6	2050	140.8	3	B	7.50	21.0	7.6	1.020	0.044	1.770	3.08	1.210	15.51	3.6	11.70	0.0
12	6	2350	143.8	3	B	7.60	47.0	5.4	1.010	0.034	1.760	NA	NA	7.42	3.2	11.40	0.0
12	7	255	146.9	3	B	7.50	48.0	8.6	1.020	0.044	1.720	5.27	2.310	5.64	3.7	11.10	0.1
12	7	555	149.9	3	B	7.50	24.0	5.6	0.979	0.044	1.760	NA	NA	6.75	3.7	10.80	0.8
12	7	815	152.3	3	B	7.50	36.0	5.8	1.080	0.044	1.790	3.19	1.220	6.07	3.0	10.50	0.0
12	7	1110	155.2	3	B	7.50	25.0	5.6	1.040	0.039	1.790	NA	NA	6.74	3.0	11.25	0.0
12	7	1505	159.1	3	B	7.50	35.0	6.4	1.050	0.040	1.740	2.96	1.240	9.44	3.0	8.25	0.0
12	7	1655	160.9	3	B	7.50	24.0	6.8	1.080	0.044	1.630	NA	NA	7.42	4.0	11.00	2.0
12	7	2055	164.9	3	B	7.50	28.0	4.2	1.060	0.040	1.780	2.94	1.110	6.07	3.2	10.40	0.0
12	8	5	168.1	3	B	7.60	18.0	6.8	NA	0.030	1.880	NA	NA	6.07	3.0	11.30	0.0
12	8	255	170.9	3	B	7.40	55.0	4.4	1.070	0.040	1.740	3.68	1.070	9.44	3.4	10.60	0.2

946510621

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	8	600	174.0	3	B	7.60	24.0	3.2	1.080	0.040	1.570	NA	NA	4.47	4.0	9.40	2.9
12	8	820	176.3	3	B	7.50	25.0	3.0	1.110	0.040	1.700	2.63	0.433	5.40	4.0	9.00	1.0
12	8	1115	179.3	3	B	7.50	35.0	4.6	1.080	0.030	1.850	NA	NA	10.79	3.5	11.00	0.0
12	8	1420	182.3	3	B	7.50	31.0	5.4	1.100	0.030	1.840	2.73	0.909	6.74	4.0	11.25	0.0
12	8	1800	186.0	3	B	7.40	35.0	4.0	1.100	0.040	1.650	NA	NA	8.09	4.0	10.00	2.0
12	8	2105	189.1	3	B	7.50	23.0	5.8	1.060	0.030	1.770	2.62	0.500	8.09	3.2	10.90	0.0
12	9	5	192.1	3	B	7.60	22.0	4.2	1.140	0.040	1.960	NA	NA	5.40	3.0	11.40	0.0
12	9	305	195.1	3	B	7.60	43.0	5.8	1.100	0.030	1.910	2.78	0.963	8.77	3.0	11.40	0.0
12	9	605	198.1	3	B	7.40	43.0	5.6	1.200	0.040	1.590	NA	NA	10.12	3.8	9.40	2.7
12	9	820	200.3	3	B	7.50	35.0	5.6	1.060	0.040	1.800	3.94	1.290	9.44	3.0	11.00	1.0
12	9	1130	203.5	3	B	7.60	35.0	6.8	1.160	0.040	1.980	NA	NA	8.77	3.0	11.50	0.5
12	9	1420	206.3	3	B	7.50	24.0	5.8	1.300	0.040	2.040	2.31	0.536	6.07	3.0	11.00	0.0
12	9	1700	209.0	3	B	7.50	53.0	8.8	1.120	0.030	1.770	NA	NA	14.16	3.0	12.00	0.5
12	9	2100	213.0	3	B	7.50	29.0	5.8	1.140	0.040	1.860	2.84	0.608	6.07	3.7	11.00	0.1
12	10	5	216.1	3	B	7.50	33.0	7.0	1.320	0.040	2.020	NA	NA	6.07	2.3	11.20	0.0
12	10	300	219.0	3	B	7.60	27.0	6.4	1.410	0.040	2.080	3.49	1.150	4.05	2.0	11.30	0.0
12	10	600	222.0	3	B	7.50	51.0	8.6	1.230	0.040	1.730	NA	NA	16.86	2.5	10.00	0.0
12	10	820	224.3	3	B	7.50	24.0	8.4	1.310	0.040	1.730	4.15	0.983	9.44	3.0	10.25	2.0
12	10	1116	227.3	3	B	7.50	54.0	11.8	1.370	0.040	1.960	NA	NA	13.49	2.8	11.00	1.0
12	10	1420	230.3	3	B	7.50	25.0	6.4	1.400	0.040	2.220	1.40	0.678	7.42	3.0	10.50	0.0
12	10	1700	233.0	3	B	7.50	42.0	10.9	1.300	0.040	2.200	NA	NA	6.07	3.0	10.75	1.0
12	10	2100	237.0	3	B	7.50	25.0	7.4	1.230	0.040	1.840	3.90	0.900	7.42	2.1	11.00	1.0
12	10	2350	239.8	3	B	7.50	38.0	11.2	1.380	0.040	2.120	NA	NA	9.44	1.9	10.70	0.0
12	11	255	242.9	3	B	7.50	18.0	8.8	1.340	0.040	2.280	3.28	1.000	5.40	1.9	10.60	0.0
12	11	835	248.6	3	B	7.50	21.0	3.6	1.780	0.040	1.680	4.87	1.390	5.40	3.0	11.00	2.0
12	11	1130	251.5	3	B	7.50	32.0	6.0	1.430	0.040	2.040	NA	NA	5.40	3.0	10.00	0.0

94510622

BELLEVILLE TURNPIKE-LEVEL B-2/3 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO_2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
12	11	1420	254.3	3	B	7.50	28.0	5.8	1.410	0.040	2.280	5.26	2.640	6.74	2.0	10.50	0.0
12	11	1650	256.8	3	B	7.50	26.0	4.8	1.380	0.040	1.940	NA	NA	5.40	2.0	10.50	0.0
		AVERAGE READING				7.51	23.8	6.8	1.325	0.043	1.819	3.19	0.853	7.85	4.0	10.59	0.4

946510623

STØRM #3

UNIØN AVENUE

12-1/12-11-81

1/2 DEPTH

946510624

UNION AVENUE-LEVEL C-DEPTH 1/2
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1930	19.5	5	C	7.33	4.8	6.0	2.300	0.101	3.320	0.00	0.000	1.75	4.0	9.80	0.0
12	1	2220	22.3	5	C	7.51	4.6	5.2	2.210	0.068	2.910	4.64	0.959	3.11	4.0	10.00	0.0
12	2	130	25.5	5	C	7.52	7.7	6.6	1.710	0.068	2.060	0.00	0.000	1.95	4.0	11.00	0.0
12	2	420	28.3	5	C	7.54	8.2	9.4	1.730	0.068	1.890	3.39	0.885	3.70	4.5	11.80	0.0
12	2	655	30.9	5	C	7.53	8.1	13.0	1.730	0.063	1.790	3.04	0.550	42.33	4.8	11.70	0.0
12	2	945	33.8	5	C	7.70	8.8	7.6	1.860	0.060	1.850	3.47	0.706	5.40	4.9	9.10	0.0
12	2	1235	36.6	5	C	7.70	11.0	12.6	1.800	0.060	1.730	0.00	0.000	8.09	5.0	10.30	0.0
12	2	1535	39.6	5	C	7.50	13.0	12.6	1.570	0.046	1.500	3.09	0.822	15.51	5.0	10.80	0.0
12	2	1840	42.7	5	C	7.60	14.0	12.0	1.630	0.049	1.580	0.00	0.000	9.44	5.2	10.70	0.0
12	2	2145	45.8	5	C	7.60	15.0	11.3	1.550	0.042	1.610	2.85	0.744	5.40	5.5	10.40	0.0
12	3	50	48.8	5	C	7.60	15.0	10.2	1.580	0.051	1.600	0.00	0.000	9.44	5.3	12.00	0.0
12	3	350	51.6	5	C	7.60	15.0	10.6	1.670	0.042	1.590	2.76	0.503	10.12	5.5	11.40	0.0
12	3	645	54.8	5	C	7.70	15.0	10.2	1.710	0.042	1.780	0.00	0.000	15.18	5.0	11.40	0.0
12	3	930	57.5	5	C	7.60	16.0	7.8	1.810	0.042	1.760	2.76	0.529	10.79	5.0	9.70	0.0
12	3	1235	60.6	5	C	7.60	14.0	7.4	1.900	0.042	1.830	0.00	0.000	6.07	5.0	11.70	0.0
12	3	1530	63.5	5	C	7.60	14.0	7.8	2.180	0.051	2.000	3.79	0.759	10.79	4.9	11.90	0.0
12	3	1835	66.6	5	C	7.70	16.0	9.8	2.070	0.051	1.980	0.00	0.000	6.74	5.0	12.50	0.0
12	3	2145	69.8	5	C	7.60	18.0	7.0	1.770	0.042	1.820	3.33	0.677	13.49	5.0	10.30	0.0
12	4	35	72.6	5	C	7.60	18.0	7.0	1.730	0.042	1.820	0.00	0.000	8.09	5.0	11.00	0.0
12	4	330	75.5	5	C	7.60	23.0	8.6	1.360	0.033	1.660	2.43	0.444	11.46	5.0	11.70	0.0
12	4	630	78.5	5	C	7.60	21.0	7.4	1.420	0.042	1.650	0.00	0.000	9.44	4.8	10.80	0.0
12	4	945	81.8	5	C	7.50	20.0	4.8	1.020	0.035	1.630	2.32	0.505	12.81	4.9	13.40	0.0
12	4	1240	84.7	5	C	7.60	18.0	5.2	1.060	0.035	1.630	0.00	0.000	5.40	4.9	10.20	0.0
12	4	1540	87.7	5	C	7.60	20.0	4.2	0.946	0.030	1.640	2.71	0.685	10.12	4.5	11.70	0.0
12	4	1830	90.5	5	C	7.50	20.0	5.0	0.909	0.030	1.550	0.00	0.000	10.79	5.0	11.60	0.0
12	4	2125	93.4	5	C	7.50	18.0	4.4	0.879	0.030	1.590	2.29	0.590	1.56	4.9	11.40	0.0

94510625

UNION AVENUE-LEVEL C-DEPTH 1/2
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	5	15	96.3	5	C	7.60	17.0	4.6	0.882	0.030	1.580	1.80	0.468	7.42	5.0	11.80	0.0
12	5	325	99.4	5	C	7.50	16.0	5.2	0.869	0.030	1.600	2.43	0.487	3.31	5.0	11.70	0.0
12	5	628	102.3	5	C	7.50	17.0	5.2	0.888	0.030	1.590	0.00	0.000	5.94	4.9	11.80	0.0
12	5	905	105.1	5	C	7.40	18.0	5.2	0.873	0.030	1.440	0.00	0.489	4.47	4.9	11.70	0.0
12	5	1205	108.1	5	C	7.50	17.0	5.4	0.880	0.035	1.640	0.00	0.000	0.97	4.8	11.50	0.0
12	5	1505	111.1	5	C	7.50	17.0	5.6	0.882	0.030	1.600	1.21	0.347	3.30	4.9	11.40	0.0
12	5	1800	114.0	5	C	7.50	18.0	6.0	0.926	0.035	1.730	0.00	0.000	3.30	4.9	11.60	0.0
12	5	2110	117.2	5	C	7.50	17.0	5.8	0.917	0.040	1.750	3.40	0.767	3.70	4.9	11.10	0.0
12	6	35	120.6	5	C	7.60	17.0	7.6	0.955	0.030	1.750	0.00	0.000	2.92	4.8	11.90	0.0
12	6	325	123.3	5	C	7.60	17.0	5.0	0.947	0.030	1.750	1.45	0.407	3.50	4.6	11.80	0.0
12	6	615	126.3	5	C	7.60	18.0	5.8	0.988	0.049	1.800	0.00	0.000	1.56	4.2	11.90	0.0
12	6	910	129..	5	C	7.80	18.0	6.4	1.030	0.044	1.830	2.41	0.488	3.37	4.0	12.25	0.0
12	6	1155	131.9	5	C	7.60	20.0	5.0	0.996	0.030	1.730	0.00	0.000	4.05	4.0	10.25	0.0
12	6	1500	135..	5	C	7.60	25.0	5.0	1.060	0.035	1.820	2.68	0.715	5.40	4.0	11.75	0.0
12	6	1745	137.7	5	C	7.60	18.0	4.2	1.020	0.030	1.820	2.24	0.367	4.05	4.0	12.00	0.0
12	6	2135	141.1	5	C	7.60	16.0	5.0	1.030	0.035	1.880	0.50	0.394	4.72	3.0	12.50	0.0
12	7	5	144.1	5	C	7.60	16.0	5.2	1.050	0.049	1.930	0.00	0.000	5.40	2.8	12.10	0.0
12	7	31	147.0	5	C	7.70	23.0	5.0	1.030	0.040	1.840	2.94	0.702	4.72	2.8	11.90	0.0
12	7	625	150.1	5	C	7.60	17.0	4.2	1.040	0.040	1.860	0.00	0.000	3.71	2.7	12.10	0.0
12	7	850	152.5	5	C	7.70	21.0	4.4	1.290	0.040	1.910	1.81	0.438	2.33	3.0	11.75	0.0
12	7	1125	155.4	5	C	7.60	13.0	4.2	1.250	0.049	1.970	0.00	0.000	2.14	2.5	12.00	0.0
12	7	1525	159.4	5	C	7.60	16.0	4.0	1.310	0.044	1.920	2.22	0.457	2.33	3.0	12.00	0.0
12	7	1715	161.3	5	C	7.70	14.0	4.4	1.100	0.044	1.940	0.00	0.000	3.31	3.0	12.50	0.0
12	7	2115	165..	5	C	7.70	11.0	3.2	1.260	0.049	1.990	2.10	0.420	2.72	2.4	11.30	0.0
12	8	2	168.1	5	C	7.70	16.0	4.0	1.250	0.049	2.080	0.00	0.000	2.14	3.1	12.10	0.0
12	8	31	171.1	5	C	7.60	14.0	5.0	1.260	0.049	1.980	5.75	1.830	2.72	2.4	11.80	0.0

9465 10626

UNION AVENUE-LEVEL C-DEPTH 1/2
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	8	615	174.3	5	C	7.60	12.0	4.2	1.190	0.044	1.950	0.00	0.000	2.72	2.5	11.90	0.0
12	8	840	176.7	5	C	7.60	13.0	8.6	1.270	0.049	1.980	3.04	0.852	1.56	3.0	11.50	0.0
12	8	1132	179.5	5	C	7.60	12.0	9.4	1.280	0.044	2.050	0.00	0.000	3.31	4.0	11.50	0.0
12	8	1440	182.7	5	C	7.60	12.0	4.4	1.290	0.044	1.880	2.25	0.512	2.33	3.5	12.25	0.0
12	8	1820	186.3	5	C	7.70	16.0	8.4	1.250	0.049	2.030	0.00	0.000	2.53	3.0	12.00	0.0
12	8	2120	189.3	5	C	7.50	11.0	4.8	1.370	0.049	2.040	2.78	0.601	1.56	3.4	11.50	0.0
12	9	20	192.3	5	C	7.60	11.0	4.0	1.340	0.035	1.560	0.00	0.000	3.50	3.6	11.30	0.0
12	9	325	195.4	5	C	7.60	14.0	4.3	1.330	0.041	2.060	2.31	0.506	2.33	3.5	11.30	0.0
12	9	620	198.3	5	C	7.60	15.0	3.6	1.280	0.045	2.120	0.00	0.000	2.72	3.0	11.00	0.0
12	9	845	200.8	5	C	7.60	13.0	9.4	1.340	0.054	2.100	2.03	0.422	2.14	3.0	12.00	0.0
12	9	1150	203.8	5	C	7.60	10.0	7.6	1.280	0.045	2.220	0.00	0.000	1.95	3.8	11.50	0.0
12	9	1440	206.7	5	C	7.60	12.0	9.0	1.320	0.045	2.220	2.80	0.551	2.53	3.0	12.00	0.0
12	9	1720	209.3	5	C	7.60	14.0	5.4	1.430	0.050	2.160	0.00	0.000	3.70	2.6	12.00	0.0
12	9	2130	213.5	5	C	7.60	11.0	4.2	1.270	0.045	2.190	2.90	0.679	2.33	3.0	11.30	0.0
12	10	15	216.3	5	C	7.60	9.3	5.0	1.340	0.050	2.270	0.00	0.000	2.53	2.4	11.50	0.0
12	10	315	219.3	5	C	7.60	8.9	4.4	1.350	0.170	3.340	3.31	0.615	2.14	2.0	11.90	0.0
12	10	615	222.3	5	C	7.60	16.0	4.6	1.300	0.045	2.170	0.00	0.000	4.72	2.7	10.90	0.0
12	10	830	224.5	5	C	7.60	13.0	8.4	1.380	0.050	2.220	2.64	0.529	1.75	3.0	11.75	0.0
12	10	1140	227.7	5	C	7.60	11.0	7.4	1.480	0.045	2.190	0.00	0.000	1.95	3.0	11.75	0.0
12	10	1440	230.7	5	C	7.60	11.0	6.8	1.500	0.050	2.550	2.72	0.561	1.17	3.0	12.75	0.0
12	10	1720	233.3	5	C	7.60	17.0	8.0	1.450	0.050	2.590	0.00	0.000	3.31	3.0	12.25	0.0
12	10	2120	237.3	5	C	7.60	13.0	7.6	1.410	0.030	2.530	2.62	0.652	1.56	1.9	12.10	0.0
12	11	9	240.0	5	C	7.80	12.0	8.0	1.570	0.030	2.510	0.00	0.000	1.17	1.2	11.60	0.0
12	11	310	243.2	5	C	7.90	12.0	9.2	1.680	0.130	2.580	2.35	0.556	1.95	1.3	12.30	0.0
12	11	605	246.1	5	C	7.60	26.0	11.0	1.420	0.050	2.560	0.00	0.000	4.26	1.2	11.90	0.0
12	11	900	249.	5	C	7.60	12.0	3.2	1.390	0.032	1.680	2.24	0.834	1.95	2.0	12.00	0.0

946510627

UNION AVENUE-LEVEL C-DEPTH 1/2
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	11	1154	251.9	5	C	7.50	8.4	3.2	1.580	0.030	2.460	2.47	0.482	2.53	2.0	12.25	0.0
12	11	1440	254.7	5	C	7.60	6.8	3.6	1.810	0.050	2.500	2.53	0.482	1.17	2.0	12.25	0.0
12	11	1715	257.3	5	C	7.60	9.7	3.6	1.800	0.050	2.140	0.00	0.000	1.56	2.0	12.00	0.0
		AVERAGE READING				7.60	14.6	6.5	1.355	0.046	1.967	2.67	0.613	5.08	3.7	11.57	0.0

946510628

STØRM #3

SECØND RIVER

12-1/12-4-81

1/2 DEPTH

946510629

SECOND RIVER-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [°C]	D.O. [PPM]	SAL [PPT]
12	1	1840	18.7	4	C	7.22	13.0	16.0	0.245	0.014	0.417	0.36	0.449	12.14	4.5	10.80	0.0
12	1	2140	21.7	4	C	7.17	11.0	13.6	0.290	0.016	0.410	NA	NA	17.53	5.0	12.90	0.0
12	2	40	24.7	4	C	7.10	12.0	9.2	0.212	0.001	0.398	2.41	0.453	7.42	7.3	11.80	0.0
12	2	330	27.5	4	C	7.14	9.3	7.5	0.311	0.005	0.713	NA	NA	6.07	8.5	10.80	0.0
12	2	625	30.4	4	C	7.29	7.9	6.4	0.121	0.012	0.850	0.22	0.270	2.72	9.0	11.00	0.0
12	2	910	33.2	4	C	7.60	8.5	8.9	0.131	0.014	1.210	1.46	0.323	0.97	8.8	11.50	0.0
12	2	1200	36.0	4	C	7.90	5.8	4.0	0.153	0.028	1.620	NA	NA	1.17	9.3	11.50	0.0
12	2	1500	39.0	4	C	8.10	4.7	2.8	0.058	0.026	1.820	0.15	0.251	0.97	9.4	11.30	0.0
12	2	1895	42.1	4	C	7.80	4.8	3.2	0.152	0.042	2.020	NA	NA	0.78	9.0	9.70	0.0
12	2	2100	45.0	4	C	7.80	4.5	4.0	0.197	0.046	2.090	0.71	0.301	0.97	8.5	10.80	0.0
12	3	0	48.0	4	C	7.80	4.3	14.8	0.087	0.051	2.230	NA	NA	1.36	8.8	9.20	0.0
12	3	310	51.2	4	C	7.90	3.1	4.6	0.060	0.042	2.140	0.19	0.186	1.17	8.8	9.70	0.0
12	3	605	54.1	4	C	7.90	2.4	3.0	0.026	0.033	2.160	NA	NA	1.17	8.3	10.60	0.0
12	3	900	57.0	4	C	8.10	3.2	3.0	0.012	0.037	2.150	0.48	0.211	1.56	8.4	11.30	0.0
12	3	1200	60.0	4	C	8.60	3.2	2.6	0.010	0.033	2.070	NA	NA	0.97	10.0	13.80	0.0
12	3	1455	62.9	4	C	8.30	2.4	2.2	0.016	0.033	2.070	0.32	0.216	0.78	9.5	13.10	0.0
12	3	1800	66.0	4	C	8.00	2.8	2.0	0.056	0.028	2.140	NA	NA	1.56	9.2	10.30	0.0
12	3	2100	69.0	4	C	8.00	3.5	2.4	0.157	0.042	2.190	0.18	0.210	0.97	8.0	9.50	0.0
12	3	2355	71.9	4	C	8.00	2.6	2.2	0.080	0.024	2.180	NA	NA	0.58	8.0	9.30	0.0
12	4	255	74.9	4	C	8.00	2.6	1.8	0.010	0.014	2.210	0.24	0.199	0.97	8.0	10.60	0.0
12	4	550	77.8	4	C	8.00	2.4	2.0	0.018	0.024	2.250	NA	NA	1.46	8.0	9.70	0.0
12	4	900	81.0	4	C	8.10	2.0	5.8	0.010	0.035	2.110	0.19	0.137	1.17	8.0	12.00	0.0
12	4	1200	84.0	4	C	8.50	2.8	6.4	0.010	0.035	2.010	1.27	0.221	1.95	8.5	14.00	0.0
12	4	1500	87.0	4	C	8.50	3.0	1.6	0.021	0.040	1.970	2.72	0.405	0.97	9.0	12.20	0.0
12	4	1750	89.8	4	C	8.00	2.8	2.2	0.593	0.063	2.080	0.51	0.143	1.17	9.5	9.40	0.0

946510630

STØRM #3

SADDLE RIVER

12-1/12-4-81

1/2 DEPTH

946510631

SADDLE RIVER-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1920	19.3	7	C	7.70	6.5	14.4	3.860	0.133	2.270	6.29	1.420	6.74	3.9	10.80	0.0
12	1	2230	22.5	7	C	7.50	9.2	15.3	2.140	0.079	1.470	NA	NA	11.46	5.5	10.00	0.0
12	2	220	26.3	7	C	7.40	11.0	13.4	1.460	0.050	0.970	2.94	0.641	22.26	6.7	10.80	0.0
12	2	430	28.5	7	C	7.40	13.0	15.4	1.590	0.042	1.050	NA	NA	37.62	6.4	10.40	0.0
12	2	735	31.6	7	C	7.40	18.0	16.8	0.711	0.022	0.910	3.67	0.982	42.33	6.0	11.20	0.0
12	2	1030	34.5	7	C	7.70	18.0	10.8	0.470	0.019	1.060	2.51	0.634	16.86	6.0	10.50	0.0
12	2	1320	37.3	7	C	7.60	15.0	9.8	0.586	0.018	1.210	NA	NA	17.53	6.0	9.75	0.0
12	2	1630	40.5	7	C	7.60	14.0	9.4	0.901	0.033	1.440	2.60	0.553	16.86	6.8	10.25	0.0
12	2	2125	45.4	7	C	7.70	12.0	8.4	1.230	0.042	1.530	NA	NA	15.51	6.8	9.30	0.0
12	3	20	48.3	7	C	7.60	9.4	8.6	1.340	0.060	1.750	2.54	0.483	13.49	6.6	8.90	0.0
12	3	335	51.6	7	C	7.70	9.2	7.8	1.530	0.065	1.900	NA	NA	13.49	6.2	9.90	0.0
12	3	615	54.3	7	C	7.70	9.0	8.0	1.720	0.069	1.980	3.73	0.622	7.21	6.5	9.50	0.0
12	3	905	57.1	7	C	7.80	11.0	6.5	1.850	0.124	2.020	4.76	0.857	4.86	6.0	10.00	0.0
12	3	1157	59.9	7	C	7.60	8.6	6.2	1.940	0.083	2.030	NA	NA	5.06	6.0	9.50	0.0
12	3	1500	63.0	7	C	7.60	9.8	5.0	1.900	0.092	2.110	3.18	0.648	4.47	7.0	9.25	0.0
12	3	1805	66.1	7	C	7.60	9.6	5.2	1.870	0.068	2.500	NA	NA	4.08	7.0	10.00	0.0
12	3	2140	69.7	7	C	7.60	8.1	6.0	1.940	0.048	2.510	3.27	0.729	3.50	6.9	8.80	0.0
12	4	25	72.4	7	C	7.60	8.1	6.0	1.940	0.087	2.320	NA	NA	2.92	6.2	8.50	0.0
12	4	315	75.3	7	C	7.60	8.0	6.8	2.260	0.068	2.580	3.23	0.658	1.56	5.4	8.60	0.0
12	4	605	78.1	7	C	7.60	7.6	8.0	3.270	NA	NA	NA	NA	3.12	5.2	8.60	0.0
12	4	910	81.2	7	C	7.50	7.6	5.6	3.460	0.130	3.050	4.63	1.070	2.53	5.5	8.75	0.0
12	4	1207	84.1	7	C	7.60	8.0	4.8	3.570	0.150	3.490	5.14	0.837	3.11	6.0	9.00	0.0
12	4	1500	87.0	7	C	7.60	11.0	5.6	3.620	0.130	3.160	5.99	1.120	2.92	6.0	9.25	0.0
12	4	1736	89.6	7	C	7.60	13.0	5.8	3.600	NA	NA	4.84	0.816	2.14	6.0	8.75	0.0
		AVERAGE READING				7.60	10.6	8.7	2.032	0.073	1.969	3.95	0.805	10.90	6.1	9.60	0.0

94651O632

STØRM #3

MARKET STREET

12-1/12-4-81

1/2 DEPTH

946510633

MARKET ST-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1855	18.9	9	C	7.60	3.7	4.6	2.440	0.086	2.730	4.13	0.829	0.78	3.5	11.00	0.0
12	1	2155	21.9	9	C	7.50	4.2	5.2	2.520	0.086	2.650	NA	NA	3.11	3.6	10.60	0.0
12	2	140	25.7	9	C	7.50	9.8	15.2	2.130	0.068	2.270	3.71	0.682	2.14	5.0	10.90	0.0
12	2	400	28.0	9	C	7.50	9.2	15.4	1.930	0.058	1.720	NA	NA	12.81	5.1	11.80	0.0
12	2	655	30.9	9	C	7.40	11.0	13.0	2.220	0.058	1.770	4.05	1.620	16.49	5.2	11.40	0.0
12	2	1045	34.8	9	C	7.60	15.0	13.0	1.700	0.040	1.610	NA	NA	14.84	6.0	11.00	0.0
12	2	1333	37.5	9	C	7.60	16.0	12.8	1.830	0.040	1.440	2.60	0.820	14.84	6.0	9.50	0.0
12	2	1648	40.8	9	C	7.70	15.0	12.2	1.790	0.040	1.540	NA	NA	12.81	6.0	10.50	0.0
12	2	2105	45.1	9	C	7.60	13.0	12.2	1.860	0.040	1.820	2.89	0.503	6.44	5.6	11.10	0.0
12	2	2350	47.8	9	C	7.70	11.0	12.2	2.090	0.040	1.900	NA	NA	12.81	5.0	10.90	0.0
12	3	245	50.8	9	C	7.70	14.0	14.8	2.300	0.040	2.120	4.34	0.791	20.20	4.9	12.20	0.0
12	3	540	53.7	9	C	7.70	13.0	12.3	2.340	0.048	2.030	NA	NA	23.60	4.9	12.00	0.0
12	3	920	57.3	9	C	7.60	18.0	9.6	1.910	0.020	1.840	2.48	0.573	13.49	5.3	11.75	0.0
12	3	1205	60.1	9	C	7.50	27.0	10.6	1.570	0.032	1.600	NA	NA	14.16	6.0	11.75	0.0
12	3	1515	63.3	9	C	7.60	26.0	9.6	1.380	0.020	1.500	2.69	0.500	11.46	5.8	12.00	0.0
12	3	1815	66.3	9	C	7.60	26.0	11.0	1.260	0.020	1.500	NA	NA	12.14	5.8	12.00	0.0
12	3	2110	69.2	9	C	7.50	24.0	8.4	1.130	0.014	1.500	2.15	0.504	10.79	5.5	12.00	0.0
12	3	2355	71.9	9	C	7.50	21.0	8.4	1.060	0.014	1.460	NA	NA	11.46	5.2	12.10	0.0
12	4	250	74.8	9	C	7.50	21.0	8.2	0.946	0.014	1.440	3.25	0.889	8.09	4.9	12.40	0.0
12	4	540	77.7	9	C	7.50	21.0	7.2	0.917	0.014	1.430	NA	NA	6.74	4.8	12.10	0.0
12	4	920	81.3	9	C	7.50	23.0	4.0	0.903	0.033	1.420	2.47	0.501	9.44	5.0	12.00	0.0
12	4	1220	84.3	9	C	7.50	22.0	4.4	0.980	0.036	1.440	2.24	0.461	6.03	6.0	12.25	0.0
12	4	1510	87.2	9	C	7.50	20.0	5.2	0.975	0.027	1.420	2.24	0.441	8.77	6.0	12.00	0.0
12	4	1748	89.6	9	C	7.50	21.0	5.4	0.994	0.031	1.470	2.29	0.414	5.25	5.8	12.25	0.0
		AVERAGE READING				7.56	16.9	9.8	1.632	0.038	1.734	2.97	0.681	10.78	5.3	11.56	0.0

946510634

STØRM #3

LINCØLN AVENUE

12-1/12-4-81

1/2 DEPTH

946510635

LINCOLN AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	POD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1840	18.7	10	C	7.60	11.0	15.2	2.390	0.076	2.380	NA	NA	1.95	4.5	11.80	0.0
12	1	2135	21.6	10	C	7.70	10.0	16.0	2.480	0.094	2.050	5.77	1.120	21.58	4.4	12.20	0.0
12	2	35	24.6	10	C	7.60	11.0	16.0	2.250	0.058	1.560	NA	NA	10.79	4.5	12.40	0.0
12	2	340	27.7	10	C	7.60	10.5	15.8	2.290	0.068	1.790	4.35	1.190	1.75	5.0	13.00	0.0
12	2	635	30.6	10	C	7.60	17.0	16.4	1.770	0.048	1.420	NA	NA	18.21	5.1	13.10	0.0
12	2	945	33.8	10	C	7.80	32.0	14.4	1.880	0.058	1.600	2.60	0.732	16.19	5.3	11.50	0.0
12	2	1235	36.6	10	C	7.60	17.0	14.4	1.790	0.040	1.380	NA	NA	20.90	6.0	10.75	0.0
12	2	1555	39.9	10	C	7.70	16.0	14.4	1.810	0.040	1.540	4.43	1.530	10.89	6.0	11.00	0.0
12	2	2045	44.8	10	C	7.70	15.0	14.4	2.330	0.040	1.940	NA	NA	16.86	5.2	11.90	0.0
12	2	2335	47.6	10	C	7.70	16.0	14.8	2.400	0.048	2.050	3.30	0.889	18.21	4.9	11.60	0.0
12	3	225	50.4	10	C	7.70	17.0	13.6	2.340	0.048	1.990	NA	NA	21.58	4.9	12.80	0.0
12	3	525	53.4	10	C	7.80	24.0	12.1	1.830	0.040	1.720	3.20	0.711	18.17	5.0	12.90	0.0
12	3	825	56.4	10	C	7.50	28.0	11.2	1.590	0.036	1.490	3.50	0.720	12.14	5.0	12.25	0.0
12	3	1120	59.3	10	C	7.60	27.0	10.8	1.470	0.034	1.460	2.81	0.622	13.49	6.0	11.50	0.0
12	3	1420	62.3	10	C	7.60	26.0	10.6	1.350	0.034	1.490	2.37	0.440	16.19	5.8	12.25	0.0
12	3	1725	65.4	10	C	7.60	24.0	10.6	1.240	0.014	1.470	3.14	0.796	6.74	5.8	12.00	0.0
12	3	2055	68.9	10	C	7.50	23.0	10.6	1.120	0.014	1.440	NA	NA	9.44	5.4	12.80	0.0
12	3	2340	71.7	10	C	7.50	24.0	9.4	1.030	0.004	1.420	1.90	0.551	8.09	5.4	12.70	0.0
12	4	235	74.6	10	C	7.50	21.0	8.0	1.030	0.004	1.390	NA	NA	6.07	5.0	13.10	0.0
12	4	525	77.4	10	C	7.50	22.0	8.4	1.030	0.014	1.450	2.31	0.545	5.74	5.0	12.90	0.0
12	4	830	80.5	10	C	7.60	23.0	5.6	1.060	0.014	1.450	NA	NA	5.45	5.8	12.25	0.0
12	4	1125	83.4	10	C	7.50	24.0	6.2	1.080	0.004	1.430	2.13	0.515	7.59	5.3	12.25	0.0
12	4	1420	86.3	10	C	7.50	23.0	5.8	1.020	0.014	1.460	NA	NA	8.09	5.0	13.00	0.0
12	4	1734	89.1	10	C	7.50	24.0	6.6	1.070	0.020	1.500	4.08	0.875	8.43	5.3	13.00	0.0
		AVERAGE READING				7.60	20.2	11.7	1.652	0.036	1.620	3.28	0.803	11.86	5.2	12.29	0.0

946510636

MARKET ISLAND-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1830	18.5	11	C	7.69	5.6	8.8	3.390	0.104	2.200	5.28	1.340	5.84	3.9	12.60	0.0
12	1	2120	21.3	11	C	7.68	5.8	9.2	2.770	0.094	2.270	NA	NA	7.42	3.8	12.80	0.0
12	2	20	24.3	11	C	7.66	8.0	13.2	2.670	0.086	2.230	3.66	0.921	8.09	4.5	13.60	0.0
12	2	325	27.4	11	C	7.61	13.0	15.6	2.030	0.058	1.510	NA	NA	20.90	5.2	13.40	0.0
12	2	620	30.3	11	C	7.61	20.0	14.4	1.880	0.040	1.490	3.39	0.923	17.20	5.4	13.60	0.0
12	2	922	33.4	11	C	7.60	18.0	13.0	1.920	0.048	1.460	NA	NA	20.90	5.3	12.00	0.0
12	2	1223	36.4	11	C	7.60	21.0	13.8	1.780	0.048	1.360	2.82	0.722	18.21	5.8	12.00	0.0
12	2	1540	39.7	11	C	7.80	19.0	14.4	2.030	0.040	1.710	NA	NA	16.19	5.3	10.75	0.0
12	2	2030	44.5	11	C	7.80	24.0	14.8	2.230	0.048	1.450	3.77	1.060	12.81	4.9	12.60	0.0
12	2	2320	47.3	11	C	7.70	16.0	13.6	2.420	0.048	1.970	NA	NA	9.44	4.9	12.00	0.0
12	3	215	50.3	11	C	7.70	17.0	12.4	2.090	0.040	1.850	4.69	1.310	14.84	4.9	11.90	0.0
12	3	510	53.2	11	C	7.80	28.0	11.2	1.580	0.040	1.540	NA	NA	17.53	5.0	13.40	0.0
12	3	810	56.2	11	C	7.60	26.0	10.6	1.530	0.014	1.450	2.81	0.710	16.86	5.0	12.50	0.0
12	3	1107	59.1	11	C	7.60	28.0	10.6	1.440	0.020	1.440	NA	NA	12.81	6.0	12.25	0.0
12	3	1410	62.2	11	C	7.60	25.0	10.6	1.300	0.014	1.460	3.18	0.522	10.12	6.0	12.75	0.0
12	3	1710	65.2	11	C	7.60	23.0	8.8	1.190	0.014	1.420	NA	NA	12.14	6.0	12.75	0.0
12	3	2040	68.7	11	C	7.60	23.0	8.2	1.060	0.004	1.410	3.01	0.792	8.77	5.6	13.40	0.0
12	3	2330	71.5	11	C	7.50	22.0	8.2	1.030	0.004	1.370	NA	NA	8.77	5.3	13.40	0.0
12	4	220	74.3	11	C	7.60	21.0	8.2	1.040	0.014	1.430	3.46	0.728	6.07	5.1	13.70	0.0
12	4	510	77.2	11	C	7.50	22.0	8.2	1.040	0.004	1.340	NA	NA	5.40	5.1	13.50	0.0
12	4	815	80.3	11	C	7.50	22.0	6.0	1.030	0.004	1.370	2.55	5.670	5.25	5.0	12.50	0.0
12	4	1110	83.2	11	C	7.50	20.0	6.2	1.020	0.004	1.400	NA	NA	6.22	5.0	12.75	0.0
12	4	1410	86.2	11	C	7.50	23.0	5.4	1.090	0.004	1.460	1.73	0.395	10.12	5.3	13.00	0.0
12	4	1650	88.8	11	C	7.60	20.0	6.8	1.060	0.014	1.540	NA	NA	9.44	5.0	13.00	0.0
		AVERAGE READING				7.62	19.6	10.5	1.692	0.034	1.589	3.36	1.258	11.72	5.1	12.76	0.0

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STØRM #3

MARKET ISLAND

12-1/12-4-81

1/2 DEPTH

946510637

MC BRIDE AVENUE-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	HOURS (TOTAL)	SITE	DEP	PH	TURB [NTU]	BOD [PPM]	NH3 [PPM]	NO2 [PPM]	NO3 [PPM]	TKN [PPM]	TP [PPM]	CHLOR [PPB]	TEMP [*C]	D.O. [PPM]	SAL [PPT]
12	1	1915	18.3	12	C	7.45	4.8	6.2	3.480	0.114	2.250	NA	NA	3.50	4.0	10.30	0.0
12	1	2110	21.2	12	C	7.41	4.9	6.8	3.130	0.094	2.110	4.12	0.600	2.72	4.1	10.80	0.0
12	2	5	24.1	12	C	7.48	6.2	6.6	2.740	0.086	2.030	NA	NA	7.78	4.9	10.90	0.0
12	2	315	27.3	12	C	7.44	13.0	13.8	1.920	0.058	1.390	2.64	0.971	11.46	5.1	11.20	0.0
12	2	610	30.2	12	C	7.45	16.0	13.2	1.970	0.058	1.530	NA	NA	12.48	5.7	11.30	0.0
12	2	915	33.3	12	C	7.50	15.0	11.8	1.900	0.058	1.490	2.71	0.579	10.12	5.5	11.00	0.0
12	2	1215	36.3	12	C	7.60	19.0	15.0	1.790	0.048	1.370	NA	NA	14.16	6.0	10.00	0.0
12	2	1530	39.5	12	C	7.50	12.0	13.4	2.080	0.048	1.710	NA	0.435	8.77	5.3	9.25	0.0
12	2	2015	44.3	12	C	7.50	14.0	14.0	2.350	0.058	1.980	NA	NA	14.16	4.8	11.10	0.0
12	2	2305	47.1	12	C	7.50	13.0	13.6	2.430	0.048	1.900	3.50	0.531	18.81	5.1	10.30	0.0
12	3	205	50.1	12	C	7.60	17.0	11.6	2.020	0.040	1.730	NA	NA	24.28	5.1	10.30	0.0
12	3	500	53.1	12	C	7.50	22.0	9.6	1.580	0.040	1.500	2.46	0.413	20.24	5.0	11.60	0.0
12	3	800	56.0	12	C	7.40	27.0	9.0	1.530	0.014	1.390	3.84	0.990	14.16	5.0	11.75	0.0
12	3	1102	59.0	12	C	7.40	27.0	9.0	1.360	0.014	1.460	NA	NA	10.12	6.0	11.50	0.0
12	3	1400	62.0	12	C	7.50	20.0	7.0	1.280	0.014	1.460	2.20	0.614	11.46	6.0	12.00	0.0
12	3	1700	65.0	12	C	7.50	21.0	8.8	1.190	0.032	1.390	NA	NA	6.07	6.0	11.50	0.0
12	3	2025	68.4	12	C	7.40	20.0	8.0	1.070	0.014	1.370	1.92	0.427	5.06	5.8	11.20	0.0
12	3	2310	71.2	12	C	7.50	20.0	6.7	1.010	0.014	1.370	NA	NA	6.74	5.6	11.00	0.0
12	4	205	74.1	12	C	7.40	20.0	6.8	1.030	0.014	1.370	2.39	0.515	4.67	5.8	11.10	0.0
12	4	500	77.1	12	C	7.40	21.0	7.0	1.030	0.004	1.350	NA	NA	5.55	5.5	10.90	0.0
12	4	800	80.0	12	C	7.40	20.0	5.2	1.030	0.014	1.350	2.45	0.503	3.89	5.0	12.00	0.0
12	4	1105	83.1	12	C	7.40	22.0	5.2	0.998	0.020	1.380	NA	NA	5.25	5.8	11.50	0.0
12	4	1400	86.0	12	C	7.40	22.0	4.4	1.050	0.014	1.460	2.16	0.479	4.67	5.0	11.50	0.0
12	4	1640	88.7	12	C	7.50	21.0	5.8	1.040	0.020	1.500	NA	NA	7.00	6.0	11.50	0.0
		AVERAGE READING				7.46	17.4	9.1	1.709	0.039	1.577	2.76	0.588	9.71	5.3	11.06	0.0

34510638

STØRM #3

MCBRIDE AVENUE

12-1/12-4-81

1/2 DEPTH

946510639

STØRM #3

DUNDEE DAM

UPSTREAM

12-1/12-11-81

1/2 DEPTH

946510640

DUNDEE DAM UPSTREAM-LEVEL C-1/2 DEPTH
RIVER SAMPLING-STORM #3

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
12	1	1905	8	C	3.8	11.6
12	1	2215	8	C	4.2	10.9
12	2	0205	8	C	5.7	11.1
12	2	0415	8	C	5.1	11.2
12	2	0715	8	C	5.5	11.3
12	2	1005	8	C	6.0	11.0
12	2	1255	8	C	6.0	10.0
12	2	1605	8	C	6.0	10.8
12	2	2115	8	C	5.8	10.9
12	3	0005	8	C	5.2	10.7
12	3	0305	8	C	5.0	12.2
12	3	0555	8	C	4.9	11.5
12	3	0845	8	C	5.0	12.0
12	3	1135	8	C	6.0	11.5
12	3	1428	8	C	5.3	11.8
12	3	1745	8	C	6.0	11.5
12	3	2120	8	C	5.5	12.0
12	4	0010	8	C	5.1	11.8
12	4	0300	8	C	4.8	12.2
12	4	0550	8	C	4.8	12.2
12	4	0850	8	C	5.0	12.3
12	4	1138	8	C	5.5	12.5
12	4	1440	8	C	5.0	12.5
12	4	1721	8	C	5.0	12.3
12	4	2150	8	C	4.8	11.7
12	5	0045	8	C	4.8	12.3
12	5	0350	8	C	4.8	12.3
12	5	0645	8	C	4.5	12.4
12	5	0935	8	C	4.6	12.1
12	5	1235	8	C	4.7	12.3
12	5	1535	8	C	4.8	12.1
12	5	1825	8	C	4.7	12.3
12	5	2140	8	C	4.4	11.3
12	6	0105	8	C	4.1	12.3
12	6	0345	8	C	3.9	12.4
12	6	0645	8	C	3.7	12.3
12	6	0930	8	C	3.0	11.0
12	6	1213	8	C	3.0	13.0
12	6	1523	8	C	3.0	12.5
12	6	1810	8	C	2.8	12.5
12	6	2135	8	C	2.9	12.3
12	7	0030	8	C	2.8	12.4
12	7	0340	8	C	2.3	12.3
12	7	0630	8	C	2.1	11.9

946510641

STORM #3 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
12	7	0900	8	C	2.0	12.0
12	7	1150	8	C	2.0	12.5
12	7	1550	8	C	2.5	12.8
12	7	1735	8	C	2.5	12.5
12	7	2140	8	C	2.9	12.1
12	8	0335	8	C	3.1	12.8
12	8	0645	8	C	3.1	12.8
12	8	0906	8	C	3.0	12.0
12	8	1202	8	C	3.0	12.0
12	8	1510	8	C	3.0	12.5
12	8	1837	8	C	3.0	12.0
12	8	2150	8	C	3.5	11.7
12	9	0105	8	C	3.4	11.3
12	9	0355	8	C	3.2	11.5
12	9	0645	8	C	3.0	11.6
12	9	0910	8	C	2.8	12.8
12	9	1210	8	C	2.5	12.5
12	9	1505	8	C	2.0	12.8
12	9	1734	8	C	2.0	12.8
12	9	2200	8	C	2.1	11.8
12	10	0045	8	C	2.0	11.7
12	10	0350	8	C	1.9	11.9
12	10	0640	8	C	1.8	11.6
12	10	0853	8	C	1.0	13.0
12	10	1200	8	C	1.0	12.8
12	10	1502	8	C	1.0	12.8
12	10	1745	8	C	1.0	12.5
12	10	2200	8	C	1.2	12.1
12	11	0030	8	C	0.8	12.0
12	11	0335	8	C	0.8	12.0
12	11	0645	8	C	0.7	12.1
12	11	0920	8	C	1.0	13.0
12	11	1213	8	C	1.0	12.5
12	11	1505	8	C	1.0	13.0
12	11	1736	8	C	1.0	12.8

946510642

STØRM #3

DUNDEE DAM

DØWNSTREAM

12-1/12-11-81

1/2 DEPTH

946510643

STORM #3 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
12	1	1930	6	C	3.9	12.4
12	1	2240	6	C	4.8	11.7
12	2	0235	6	C	4.9	12.1
12	2	0445	6	C	4.9	12.4
12	2	0750	6	C	5.4	12.4
12	2	1016	6	C	6.0	11.5
12	2	1313	6	C	6.0	10.0
12	2	1620	6	C	6.0	11.0
12	2	2145	6	C	5.8	11.2
12	3	0035	6	C	5.5	11.1
12	3	0350	6	C	5.0	12.5
12	3	0630	6	C	5.0	12.3
12	3	0858	6	C	5.0	11.8
12	3	1145	6	C	6.0	11.8
12	3	1445	6	C	5.3	12.0
12	3	1755	6	C	5.5	12.0
12	3	2200	6	C	5.5	12.4
12	4	0040	6	C	5.0	12.6
12	4	0335	6	C	5.0	12.8
12	4	0625	6	C	4.8	12.8
12	4	0900	6	C	5.0	12.0
12	4	1152	6	C	5.5	12.8
12	4	1445	6	C	5.0	12.8
12	4	1727	6	C	5.0	12.5
12	4	2140	6	C	4.8	12.0
12	5	0030	6	C	4.9	12.7
12	5	0340	6	C	4.8	12.6
12	5	0635	6	C	4.8	12.5
12	5	0920	6	C	4.7	12.7
12	5	1220	6	C	4.8	12.2
12	5	1520	6	C	4.7	12.5
12	5	1815	6	C	4.3	12.7
12	5	2125	6	C	4.3	11.8
12	6	0055	6	C	4.1	12.9
12	6	0335	6	C	3.9	13.1
12	6	0635	6	C	3.4	13.1
12	6	0915	6	C	3.0	13.0
12	6	1210	6	C	3.0	12.3
12	6	1515	6	C	3.0	12.8
12	6	1800	6	C	2.5	13.0
12	6	2120	6	C	2.6	13.3
12	7	0020	6	C	2.1	13.3
12	7	0330	6	C	2.1	13.2
12	7	0620	6	C	2.1	13.2

946510644

STORM #3 - RIVER SAMPLING
DUNDEE DAM DOWNSTREAM - LEVEL C - 1/2 DEPTH

MONTH	DAY	TIME	SITE	DEP	TEMP (*C)	D.O. (PPM)
12	7	0847	6	C	2.0	12.3
12	7	1144	6	C	2.5	12.3
12	7	1540	6	C	3.0	12.5
12	7	1726	6	C	2.8	12.8
12	7	2125	6	C	2.7	12.9
12	8	0035	6	C	2.8	12.8
12	8	0325	6	C	2.8	12.8
12	8	0635	6	C	3.0	12.9
12	8	0852	6	C	3.0	11.8
12	8	1150	6	C	3.3	11.8
12	8	1455	6	C	3.3	11.8
12	8	1831	6	C	3.0	11.0
12	8	2135	6	C	3.2	12.6
12	9	0050	6	C	3.1	12.6
12	9	0345	6	C	3.1	12.6
12	9	0635	6	C	2.7	12.9
12	9	0900	6	C	2.0	13.0
12	9	1205	6	C	2.0	12.8
12	9	1455	6	C	2.0	12.8
12	9	1727	6	C	2.0	12.5
12	9	2145	6	C	2.0	13.3
12	10	0030	6	C	1.8	12.9
12	10	0335	6	C	1.5	13.5
12	10	0630	6	C	1.2	12.7
12	10	0845	6	C	1.0	13.0
12	10	1150	6	C	1.0	12.8
12	10	1450	6	C	1.3	13.0
12	10	1735	6	C	1.0	12.5
12	10	2145	6	C	0.9	13.1
12	11	0015	6	C	0.5	13.1
12	11	0325	6	C	0.2	13.3
12	11	0635	6	C	0.2	13.2
12	11	0910	6	C	0.0	13.0
12	11	1204	6	C	0.8	12.8
12	11	1455	6	C	1.0	12.8
12	11	1724	6	C	1.0	12.5

946510645