BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
S-14-1

Submittal Date
3-20-90 1:45 pm

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 3-21-90

NAME: VD, KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	28	.007	.006	25.	Standard ✓	.0146	.015
2.	29		.003	26.	112		.004
3.	✓prep		.027	27.	113	.057	.043
4.	91	.034	.032	28.	114		.014
5.	92-1	.025	.026	29.	115	.033	.029
6.	92-2		.025	30.	116		.008
7.	93		.016	31.	117		.009
8.	Standard ✓	.0146	.015	32.	118	.023	.020
9.	94		.005	33.			
10.	95		.006	34.			
11.	96		.033	35.	119		.009
12.	97	.047	.047	36.	121		.007
13.	101		.016	37.	122		.020
14.	102	.009	.010	38.	123		.016
15.	103		.013	39.	124	.022	.019
16.				40.	125	.033	.030
17.				41.	131		.006
18.	104		.009	42.	Standard ✓	.0146	.015
19.	105		.006	43.	132		.012
20.	106		.011	44.	133		.017
21.	107		.013	45.	134	.038	.037
22.	108		.013	46.	135		.032
23.	109		.009	47.	136		.025
24.	111		.007	48.	Standard ✓	.0146	.015

LLD
BM
GZL

(70° H2O Bath)

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern # 5-14-1

Submittal Date 3/16/90 10:30A

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 3/19/90

NAME: [illegible]

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	1	.010	.009	25.	Standard ✓		.015
2.	2		.009	26.	23-2		.003
3.	3	.020	.018	27.	24		.002
4.	4		.004	28.	25		.006
5.	5		.004	29.	26		.002
6.	6		.006	30.	27		.002
7.	7		.003	31.	51		.005
8.	Standard ✓		.015	32.	52		.007
9.	8		.002	33.			
10.	9		.003	34.			
11.	11		.009	35.	53		.005
12.	12	.007	.005	36.	54		.007
13.	13		.006	37.	55		.010
14.	14		.006	38.	56	.023	.021
15.	15		.006	39.	57		.010
16.				40.	58		.007
17.				41.	59		.006
18.	16		.002	42.	Standard ✓		.015
19.	17		.002	43.	61		.005
20.	18		.002	44.	✓ Rubbed		.026
21.	19		.001	45.	62		.005
22.	21		.003	46.	63		.002
23.	22		.004	47.	64		.007
24.	23-1	.009	.003	48.		Std ✓	.015

c.j.c.

ALD

S-14-2

OK 6-12-90 Bill

OK 12-20-90

BENCH NO	SHOT NO	BLAST HOLE NO	ORE TYPE	FIRE AU	AA AU	AA/FIRE	AA/RAT.
S14	2	1	3	0.014	0.014	100.00%	0.014
S14	2	2	3	0.073	0.053	72.60%	0.073
S14	2	3	3	0.022	0.024	109.09%	0.022
S14	2	4	2	0.016	0.013	81.25%	0.016
S14	2	5	3		0.016		0.018
S14	2	6	3		0.006		0.007
S14	2	7	3		0.015		0.016
S14	2	8	3		0.015		0.016
S14	2	9	3		0.011		0.012
S14	2	11	3	0.017	0.018	105.88%	0.017
S14	2	12	3	0.073	0.062	84.93%	0.073
S14	2	13	3	0.014	0.015	107.14%	0.014
S14	2	14	2	0.015	0.014	93.33%	0.015
S14	2	15	3	0.164	0.113	68.90%	0.164
S14	2	16	3		0.052		0.067
S14	2	17	3	0.013	0.013	100.00%	0.013
S14	2	18	3	0.023	0.021	91.30%	0.023
S14	2	19	3		0.010		0.011
S14	2	21	3		0.012		0.013
S14	2	22	3	0.020	0.018	90.00%	0.020
S14	2	23	3		0.017		0.019
S14	2	24	3	0.154	0.035	22.73%	0.154
S14	2	25	3	0.043	0.038	88.37%	0.043
S14	2	26	2	0.022	0.019	86.36%	0.022
S14	2	27	3		0.023		0.026
S14	2	28	3	0.021	0.022	104.76%	0.021
S14	2	29	3		0.029		0.034
S14	2	31	3	0.023	0.024	104.35%	0.023
S14	2	32	3		0.042		0.049
S14	2	33	3		0.046		0.054
S14	2	34	3	0.116	0.115	99.14%	0.116
S14	2	35	3	0.046	0.044	95.65%	0.046
S14	2	36	3	0.017	0.018	105.88%	0.017
S14	2	37	3		0.011		0.012
S14	2	38	3	0.061	0.061	100.00%	0.061
S14	2	39	3	0.013	0.014	107.69%	0.013
S14	2	41	3		0.035		0.041
S14	2	42	3	0.092	0.084	91.30%	0.092
S14	2	43	3	0.077	0.052	67.53%	0.077
S14	2	44	3	0.013	0.011	84.62%	0.013
S14	2	45	3		0.014		0.015
S14	2	46	3	0.020	0.021	105.00%	0.020
S14	2	47	3	0.020	0.020	100.00%	0.020
S14	2	48	3	0.089	0.040	44.94%	0.089
S14	2	49	3	0.013	0.007	53.85%	0.013
S14	2	51	3	0.034	0.023	67.65%	0.034
S14	2	52	3	0.040	0.046	115.00%	0.040
S14	2	53	3	0.018	0.017	94.44%	0.018
S14	2	54	3	0.021	0.021	100.00%	0.021
S14	2	55	3	0.018	0.019	105.56%	0.018
S14	2	56	3		0.014		0.015
S14	2	57	3	0.019	0.020	105.26%	0.019

S14	2	58	3		0.018		0.020
S14	2	59	3		0.004		0.004
S14	2	61	3		0.012		0.013
S14	2	62	3		0.017		0.019
S14	2	63	3		0.018		0.020
S14	2	64	3	0.028	0.027	96.43%	0.028
S14	2	65	3	0.123	0.106	86.18%	0.123
S14	2	66	3	0.014	0.013	92.86%	0.014
S14	2	67	3	0.026	0.027	103.85%	0.026
S14	2	68	3		0.008		0.009
S14	2	69	3		0.002		0.002
S14	2	71	3	0.033	0.023	69.70%	0.033
S14	2	72	3	0.057	0.056	98.25%	0.057
S14	2	73	3	0.047	0.049	104.26%	0.047
S14	2	74	3	0.040	0.040	100.00%	0.040
S14	2	75	3	0.014	0.013	92.86%	0.014
S14	2	76	3	0.024	0.022	91.67%	0.024
S14	2	77	3	0.061	0.055	90.16%	0.061
S14	2	78	3	0.008	0.007	87.50%	0.008
S14	2	79	3		0.011		0.012
S14	2	81	3		0.015		0.016
S14	2	82	3	0.226	0.223	98.67%	0.226
S14	2	83	3	0.040	0.043	107.50%	0.040
S14	2	84	3	0.014	0.016	114.29%	0.014
S14	2	85	3		0.036		0.042
S14	2	86	3		0.043		0.050
S14	2	87	3		0.036		0.042
S14	2	88	3	0.011	0.009	81.82%	0.011
S14	2	89	3		0.009		0.010
S14	2	91	3	0.023	0.021	91.30%	0.024
S14	2	92	3		0.115		0.152
S14	2	93	3	0.127	0.110	86.61%	0.127
S14	2	94	3	0.018	0.018	100.00%	0.018
S14	2	95	3		0.017		0.019
S14	2	96	3	0.070	0.069	98.57%	0.070
S14	2	97	3	0.009	0.009	100.00%	0.009
S14	2	98	3		0.004		0.004
S14	2	99	3		0.011		0.012
S14	2	101	3	0.025	0.027	108.00%	0.025
S14	2	102	3	0.200	0.195	97.50%	0.200
S14	2	103	3		0.064		0.082
S14	2	104	3		0.041		0.048
S14	2	105	3	0.022	0.023	104.55%	0.022
S14	2	106	3		0.029		0.034
S14	2	107	3	0.008	0.008	100.00%	0.008
S14	2	108	3		0.006		0.007
S14	2	109	3		0.006		0.007
S14	2	111	3	0.072	0.072	100.00%	0.072
S14	2	112	3	0.026	0.024	92.31%	0.026
S14	2	113	3		0.025		0.028
S14	2	114	3	0.095	0.067	70.53%	0.095
S14	2	115	3	0.014	0.017	121.43%	0.014
S14	2	116	3	0.046	0.043	93.48%	0.046
S14	2	117	3	0.011	0.011	100.00%	0.011
S14	2	118	3		0.007		0.008
S14	2	119	3		0.011		0.012

S14	2	121	3	0.057	0.059	103.51%	0.057
S14	2	122	3	0.030	0.029	96.67%	0.030
S14	2	123	3	0.034	0.037	108.82%	0.034
S14	2	124	3	0.074	0.068	91.89%	0.074
S14	2	125	3		0.027		0.032
S14	2	126	3	0.008	0.007	87.50%	0.008
S14	2	127	3	0.026	0.022	84.62%	0.026
S14	2	128	3		0.016		0.018
S14	2	129	3		0.006		0.007
S14	2	131	3	0.106	0.072	67.92%	0.106
S14	2	132	3		0.040		0.047
S14	2	133	3	0.051	0.024	47.06%	0.051
S14	2	134	3		0.047		0.055
S14	2	135	3		0.036		0.042
S14	2	136	3	0.022	0.015	68.18%	0.022
S14	2	137	3	0.018	0.019	105.56%	0.018
S14	2	138	3		0.005		0.005
S14	2	139	3		0.008		0.009
S14	2	141	3	0.053	0.038	71.70%	0.053
S14	2	142	3		0.074		0.095
S14	2	143	3		0.030		0.035
S14	2	144	3	0.117	0.121	103.42%	0.117
S14	2	145	3	0.173	0.145	83.82%	0.173
S14	2	146	3	0.020	0.021	105.00%	0.020
S14	2	147	3	0.014	0.014	100.00%	0.014
S14	2	148	3		0.004		0.004
S14	2	149	3	0.025	0.026	104.00%	0.025
S14	2	151	3	0.225	0.144	64.00%	0.225
S14	2	152	2	0.299	0.027	9.03%	0.299
S14	2	153	3	0.083	0.073	87.95%	0.083
S14	2	154	3		0.047		0.055
S14	2	155	3		0.038		0.044
S14	2	156	3	0.018	0.017	94.44%	0.018
S14	2	157	3		0.011		0.012
S14	2	158	3	0.022	0.021	95.45%	0.022
S14	2	159	3	0.030	0.021	70.00%	0.030
S14	2	161	3	0.735	0.493	67.07%	0.735
S14	2	162	3	0.612	0.284	46.41%	0.612
S14	2	163	2	0.630	0.132	20.95%	0.630
S14	2	164	2	0.473	0.081	17.12%	0.473
S14	2	165	3	0.121	0.070	57.85%	0.121
S14	2	166	3		0.050		0.064
S14	2	167	3	0.011	0.013	118.18%	0.011
S14	2	168	3	0.059	0.050	84.75%	0.059
S14	2	169	3	0.021	0.021	100.00%	0.021
S14	2	171	3		0.053		0.068
S14	2	172	3	0.341	0.237	69.50%	0.341
S14	2	173	3	0.410	0.266	64.88%	0.410
S14	2	174	2	0.433	0.196	45.27%	0.433
S14	2	175	3	0.169	0.135	79.88%	0.169
S14	2	176	3	0.080	0.070	87.50%	0.080
S14	2	177	3		0.138		0.183
S14	2	178	2	0.035	0.028	80.00%	0.035
S14	2	179	3		0.044		0.051
S14	2	181	2	0.246	0.202	82.11%	0.246
S14	2	182	2	0.260	0.096	36.92%	0.260

S14	2	183	3	0.164	0.151	92.07%	0.164
S14	2	184	3	0.145	0.110	75.86%	0.145
S14	2	185	3	0.138	0.115	83.33%	0.138
S14	2	186	3		0.030		0.035
S14	2	187	3	0.096	0.094	97.92%	0.096
S14	2	188	3		0.034		0.040
S14	2	189	3	0.027	0.021	77.78%	0.027
S14	2	191	3	0.180	0.131	72.78%	0.180
S14	2	192	3		0.047		0.055
S14	2	193	3		0.038		0.044
S14	2	194	3		0.033		0.039
S14	2	195	3	0.024	0.022	91.67%	0.024
S14	2	196	2	0.071	0.055	77.46%	0.071
S14	2	197	3		0.035		0.041
S14	2	198	3	0.068	0.066	97.06%	0.068
S14	2	199	3		0.045		0.053
S14	2	201	3		0.045		0.053
S14	2	202	3		0.038		0.044
S14	2	203	3		0.048		0.056
S14	2	204	2	0.025	0.019	76.00%	0.025
S14	2	205	2	0.095	0.051	53.68%	0.095
S14	2	206	3	0.204	0.087	42.65%	0.204
S14	2	207	3		0.034		0.040
S14	2	208	3		0.043		0.050
S14	2	209	3	0.028	0.020	71.43%	0.028
S14	2	211	3		0.030		0.035
S14	2	212	3	0.115	0.096	83.48%	0.115
S14	2	213	3		0.039		0.046
S14	2	214	2	0.035	0.032	91.43%	0.035
S14	2	215	1	0.096	0.057	59.38%	0.096
S14	2	216	3		0.067		0.086
S14	2	217	3	0.026	0.022	84.62%	0.026
S14	2	218	2	0.017	0.009	52.94%	0.017
S14	2	219	1		0.004		0.004
S14	2	221	3	0.030	0.025	83.33%	0.030
S14	2	222	3		0.028		0.033
S14	2	223	1	0.072	0.040	55.56%	0.072
S14	2	224	1	0.028	0.017	60.71%	0.028
S14	2	225	2	0.027	0.021	77.78%	0.027
S14	2	226	3		0.031		0.036
S14	2	227	3		0.031		0.036
S14	2	228	3		0.040		0.047
S14	2	229	3	0.009	0.008	88.89%	0.009
S14	2	231	3		0.015		0.016
S14	2	232	3	0.046	0.026	56.52%	0.046
S14	2	233	3	0.013	0.014	107.69%	0.013
S14	2	234	3		0.039		0.046
S14	2	235	3		0.032		0.037
S14	2	236	3	0.036	0.023	63.89%	0.036
S14	2	237	3	0.014	0.012	85.71%	0.014
S14	2	238	3	0.020	0.024	120.00%	0.020
S14	2	239	3		0.014		0.015
S14	2	241	2		0.008		0.009
S14	2	242	3	0.028	0.029	103.57%	0.028
S14	2	243	3	0.010	0.009	90.00%	0.010
S14	2	244	3		0.016		0.018

S14	2	245	3		0.032		0.037
S14	2	246	3	0.054	0.054	100.00%	0.054
S14	2	247	3	0.025	0.020	80.00%	0.025
S14	2	248	3	0.022	0.016	72.73%	0.022
S14	2	249	3	0.033	0.026	78.79%	0.033
S14	2	251	3		0.031		0.036
S14	2	252	3		0.033		0.039
S14	2	253	2	0.015	0.014	93.33%	0.015
S14	2	254	3	0.116	0.050	43.10%	0.116
S14	2	255	3	0.015	0.011	73.33%	0.015
S14	2	256	2		0.006		0.007
S14	2	257	2		0.010		0.011
S14	2	258	3	0.022	0.020	90.91%	0.022
S14	2	259	3		0.026		0.030
S14	2	261	3	0.072	0.025	34.72%	0.072
S14	2	262	3	0.021	0.020	95.24%	0.021
S14	2	263	3		0.046		0.054
S14	2	264	3	0.013	0.010	76.92%	0.013
S14	2	265	2	0.070	0.063	90.00%	0.070
S14	2	266	3	0.021	0.019	90.48%	0.021
S14	2	267	2	0.025	0.024	96.00%	0.025
S14	2	501	2		0.012		0.013
S14	2	502	3		0.008		0.009
S14	2	503	3		0.009		0.010
S14	2	504	3	0.019	0.020	105.26%	0.019
S14	2	505	3		0.029		0.034
S14	2	506	3		0.032		0.037
S14	2	507	2	0.028	0.026	92.86%	0.028
S14	2	508	2	0.010	0.006	60.00%	0.010
S14	2	509	3		0.027		0.032
S14	2	510	2	0.022	0.017	77.27%	0.022
S14	2	511	3		0.035		0.041
S14	2	512	3	0.081	0.082	101.23%	0.081
		MEAN		0.076	0.042	84.78%	0.059

S-14-2 ✓ O.K. 4-16-90

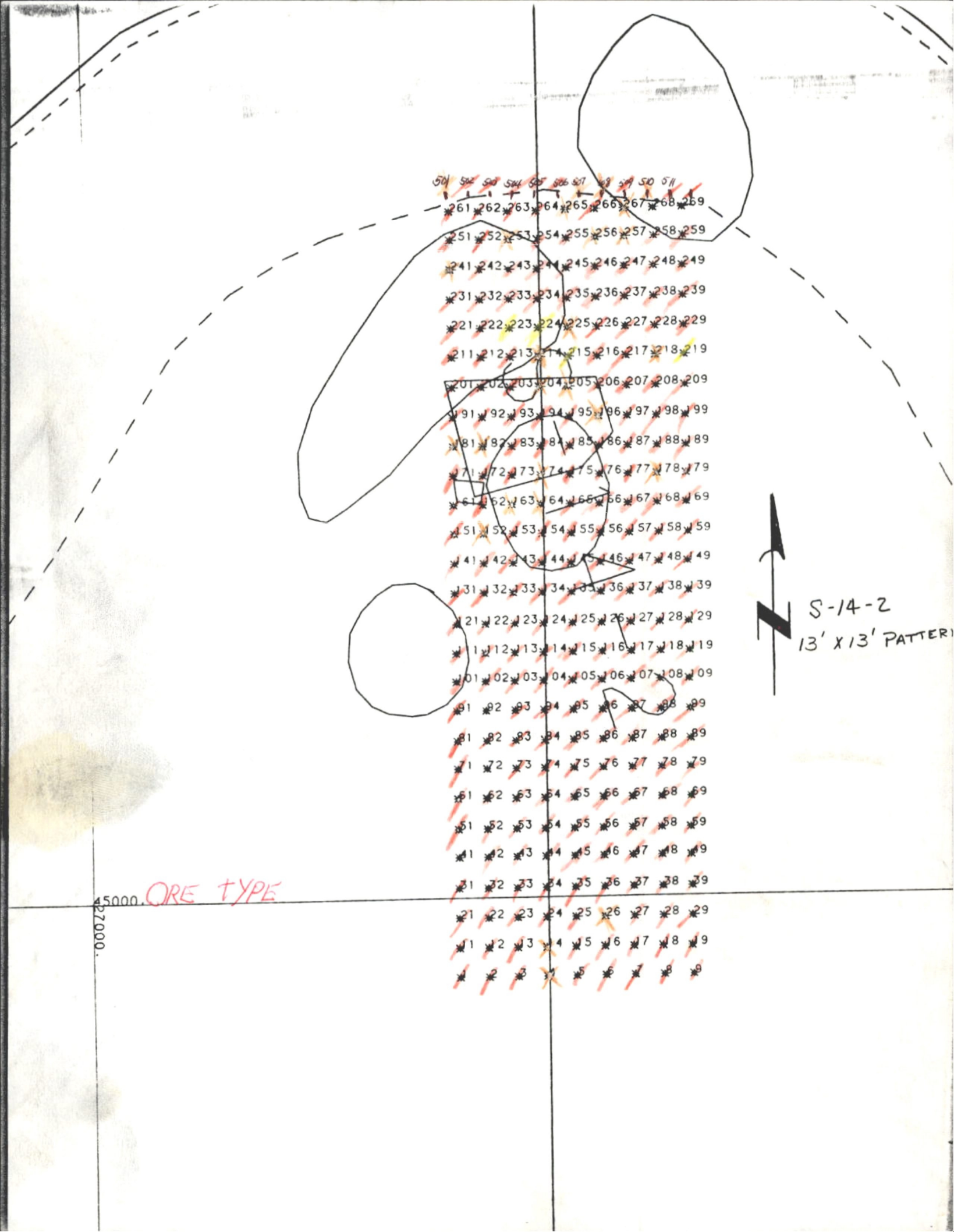
BENCH NO	SHOT NO	BLAST HOLE NO	ORE TYPE	FIRE AU	AA AU	AA/FIRE	AA/RAT.
S14	2	1	3	0.014	0.014	100.00%	0.014
S14	2	2	3	0.073	0.053	72.60%	0.073
S14	2	3	3	0.022	0.024	109.09%	0.022
S14	2	4	2	0.016	0.013	81.25%	0.016
S14	2	5	3		0.016		0.018
S14	2	6	3		0.006		0.007
S14	2	7	3		0.015		0.016
S14	2	8	3		0.015		0.016
S14	2	9	3		0.011		0.012
S14	2	11	3	0.017	0.018	105.88%	0.017
S14	2	12	3	0.073	0.062	84.93%	0.073
S14	2	13	3	0.014	0.015	107.14%	0.014
S14	2	14	2	0.015	0.014	93.33%	0.015
S14	2	15	3	0.164	0.113	68.90%	0.164
S14	2	16	3		0.052		0.067
S14	2	17	3	0.013	0.013	100.00%	0.013
S14	2	18	3	0.023	0.021	91.30%	0.023
S14	2	19	3		0.010		0.011
S14	2	21	3		0.012		0.013
S14	2	22	3	0.020	0.018	90.00%	0.020
S14	2	23	3		0.017		0.019
S14	2	24	3	0.154	0.035	22.73%	0.154
S14	2	25	3	0.043	0.038	88.37%	0.043
S14	2	26	2	0.022	0.019	86.36%	0.022
S14	2	27	3		0.023		0.026
S14	2	28	3	0.021	0.022	104.76%	0.021
S14	2	29	3		0.029		0.034
S14	2	31	3	0.023	0.024	104.35%	0.023
S14	2	32	3		0.042		0.049
S14	2	33	3		0.046		0.054
S14	2	34	3	0.116	0.115	99.14%	0.116
S14	2	35	3	0.046	0.044	95.65%	0.046
S14	2	36	3	0.017	0.018	105.88%	0.017
S14	2	37	3		0.011		0.012
S14	2	38	3	0.061	0.061	100.00%	0.061
S14	2	39	3	0.013	0.014	107.69%	0.013
S14	2	41	3		0.035		0.041
S14	2	42	3	0.092	0.084	91.30%	0.092
S14	2	43	3	0.077	0.052	67.53%	0.077
S14	2	44	3	0.013	0.011	84.62%	0.013
S14	2	45	3		0.014		0.015
S14	2	46	3	0.020	0.021	105.00%	0.020
S14	2	47	3	0.020	0.020	100.00%	0.020
S14	2	48	3	0.089	0.040	44.94%	0.089
S14	2	49	3	0.013	0.007	53.85%	0.013
S14	2	51	3	0.034	0.023	67.65%	0.034
S14	2	52	3	0.040	0.046	115.00%	0.040
S14	2	53	3	0.018	0.017	94.44%	0.018
S14	2	54	3	0.021	0.021	100.00%	0.021
S14	2	55	3	0.018	0.019	105.56%	0.018
S14	2	56	3		0.014		0.015
S14	2	57	3	0.019	0.020	105.26%	0.019
S14	2	58	3		0.018		0.020

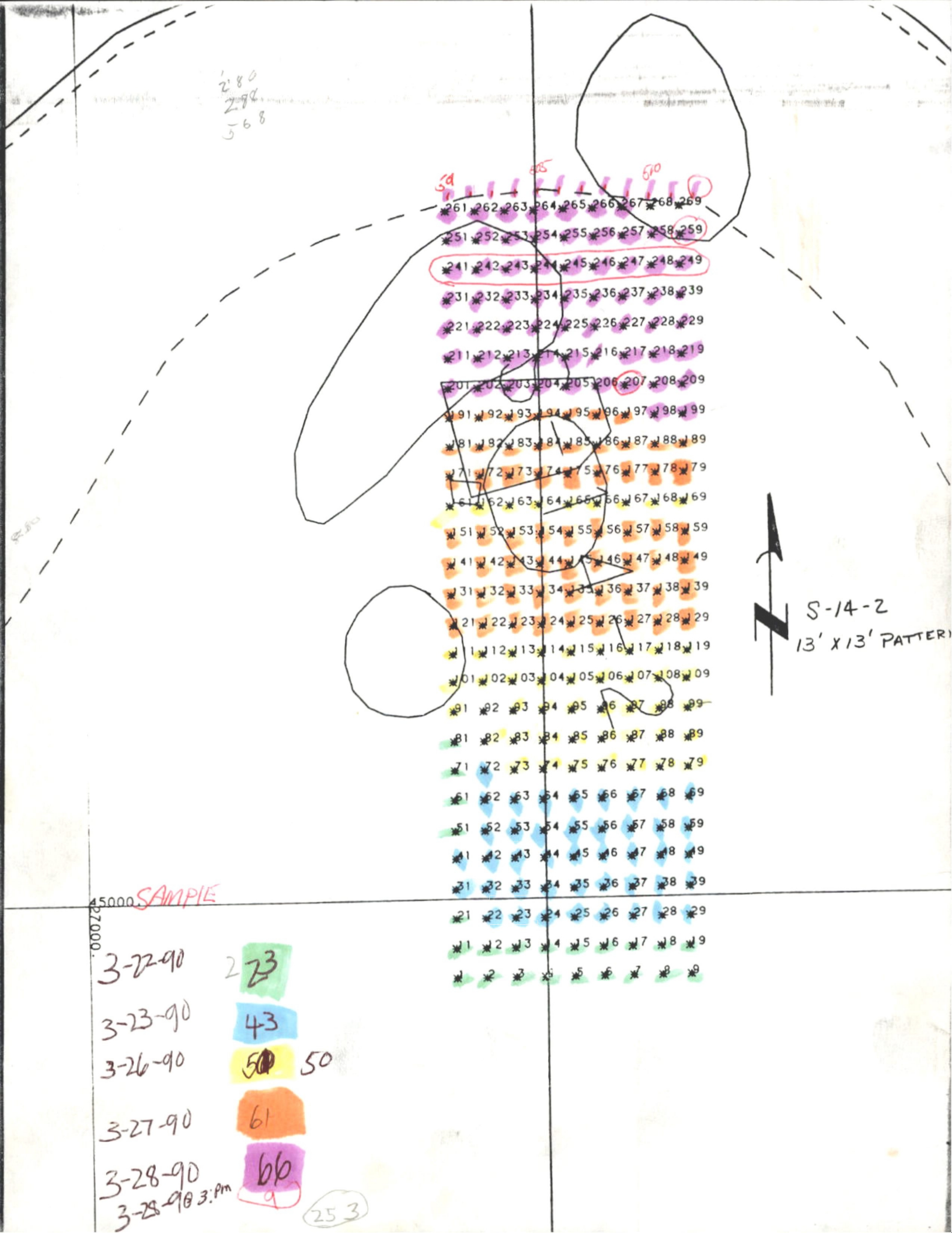
S14	2	59	3		0.004		0.004
S14	2	61	3		0.012		0.013
S14	2	62	3		0.017		0.019
S14	2	63	3		0.018		0.020
S14	2	64	3	0.028	0.027	96.43%	0.028
S14	2	65	3	0.123	0.106	86.18%	0.123
S14	2	66	3	0.014	0.013	92.86%	0.014
S14	2	67	3	0.026	0.027	103.85%	0.026
S14	2	68	3		0.008		0.009
S14	2	69	3		0.002		0.002
S14	2	71	3	0.033	0.023	69.70%	0.033
S14	2	72	3	0.057	0.056	98.25%	0.057
S14	2	73	3	0.047	0.049	104.26%	0.047
S14	2	74	3	0.040	0.040	100.00%	0.040
S14	2	75	3	0.014	0.013	92.86%	0.014
S14	2	76	3	0.024	0.022	91.67%	0.024
S14	2	77	3	0.061	0.055	90.16%	0.061
S14	2	78	3	0.008	0.007	87.50%	0.008
S14	2	79	3		0.011		0.012
S14	2	81	3		0.015		0.016
S14	2	82	3	0.226	0.223	98.67%	0.226
S14	2	83	3	0.040	0.043	107.50%	0.040
S14	2	84	3	0.014	0.016	114.29%	0.014
S14	2	85	3		0.036		0.042
S14	2	86	3		0.043		0.050
S14	2	87	3		0.036		0.042
S14	2	88	3	0.011	0.009	81.82%	0.011
S14	2	89	3		0.009		0.010
S14	2	91	3	0.023	0.021	91.30%	0.024
S14	2	92	3		0.115		0.152
S14	2	93	3	0.127	0.110	86.61%	0.127
S14	2	94	3	0.018	0.018	100.00%	0.018
S14	2	95	3		0.017		0.019
S14	2	96	3	0.070	0.069	98.57%	0.070
S14	2	97	3	0.009	0.009	100.00%	0.009
S14	2	98	3		0.004		0.004
S14	2	99	3		0.011		0.012
S14	2	101	3	0.025	0.027	108.00%	0.025
S14	2	102	3	0.200	0.195	97.50%	0.200
S14	2	103	3		0.064		0.082
S14	2	104	3		0.041		0.048
S14	2	105	3	0.022	0.023	104.55%	0.022
S14	2	106	3		0.029		0.034
S14	2	107	3	0.008	0.008	100.00%	0.008
S14	2	108	3		0.006		0.007
S14	2	109	3		0.006		0.007
S14	2	111	3	0.072	0.072	100.00%	0.072
S14	2	112	3	0.026	0.024	92.31%	0.026
S14	2	113	3		0.025		0.028
S14	2	114	3	0.095	0.067	70.53%	0.095
S14	2	115	3	0.014	0.017	121.43%	0.014
S14	2	116	3	0.046	0.043	93.48%	0.046
S14	2	117	3	0.011	0.011	100.00%	0.011
S14	2	118	3		0.007		0.008
S14	2	119	3		0.011		0.012
S14	2	121	3	0.057	0.059	103.51%	0.057

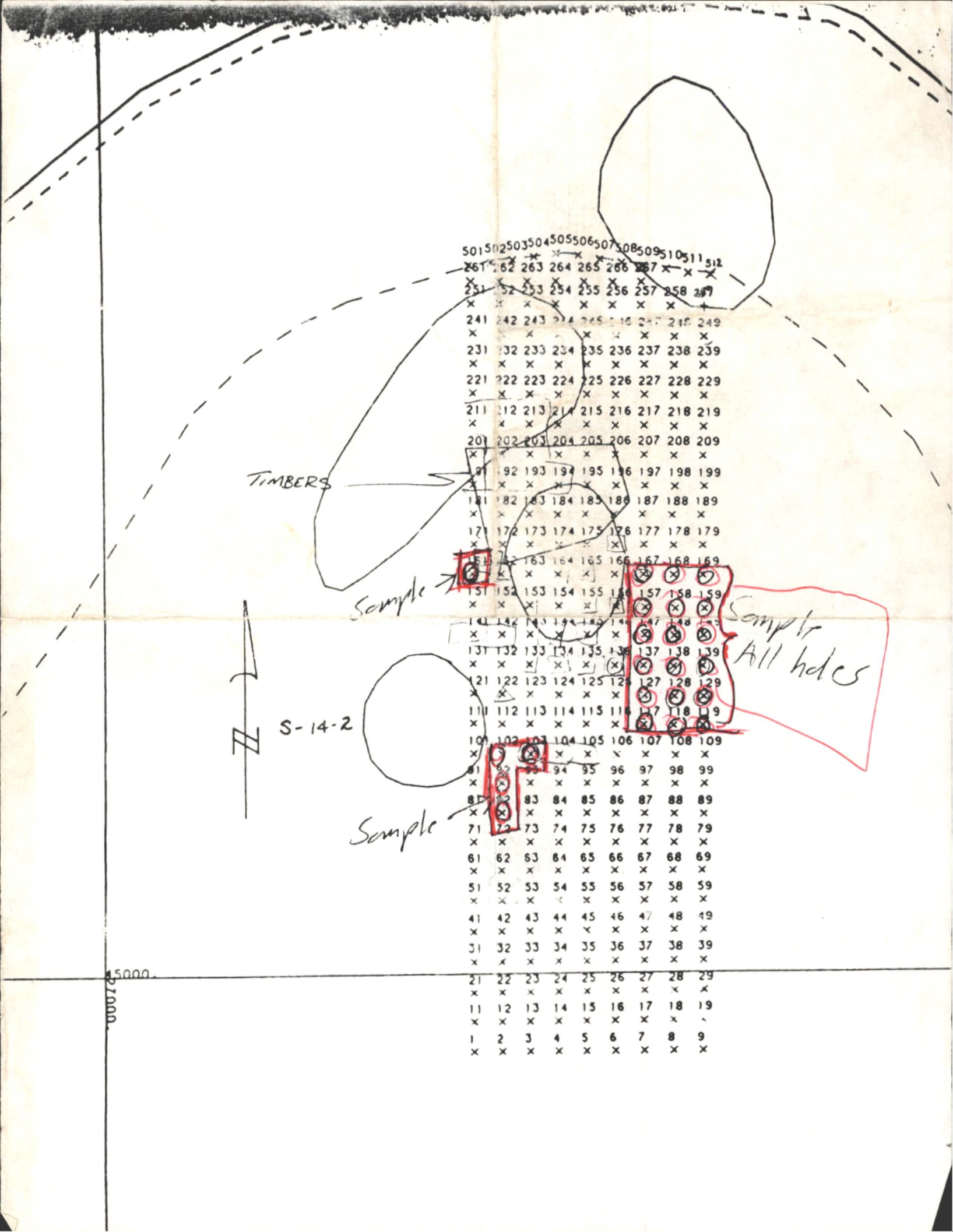
S14	2	122	3	0.030	0.029	96.67%	0.030
S14	2	123	3	0.034	0.037	108.82%	0.034
S14	2	124	3	0.074	0.068	91.89%	0.074
S14	2	125	3		0.027		0.032
S14	2	126	3	0.008	0.007	87.50%	0.008
S14	2	127	3	0.026	0.022	84.62%	0.026
S14	2	128	3		0.016		0.018
S14	2	129	3		0.006		0.007
S14	2	131	3	0.106	0.072	67.92%	0.106
S14	2	132	3		0.040		0.047
S14	2	133	3	0.051	0.024	47.06%	0.051
S14	2	134	3		0.047		0.055
S14	2	135	3		0.036		0.042
S14	2	136	3	0.022	0.015	68.18%	0.022
S14	2	137	3	0.018	0.019	105.56%	0.018
S14	2	138	3		0.005		0.005
S14	2	139	3		0.008		0.009
S14	2	141	3	0.053	0.038	71.70%	0.053
S14	2	142	3		0.074		0.095
S14	2	143	3		0.030		0.035
S14	2	144	3	0.117	0.121	103.42%	0.117
S14	2	145	3	0.173	0.145	83.82%	0.173
S14	2	146	3	0.020	0.021	105.00%	0.020
S14	2	147	3	0.014	0.014	100.00%	0.014
S14	2	148	3		0.004		0.004
S14	2	149	3	0.025	0.026	104.00%	0.025
S14	2	151	3	0.225	0.144	64.00%	0.225
S14	2	152	2	0.299	0.027	9.03%	0.299
S14	2	153	3	0.083	0.073	87.95%	0.083
S14	2	154	3		0.047		0.055
S14	2	155	3		0.038		0.044
S14	2	156	3	0.018	0.017	94.44%	0.018
S14	2	157	3		0.011		0.012
S14	2	158	3	0.022	0.021	95.45%	0.022
S14	2	159	3	0.030	0.021	70.00%	0.030
S14	2	161	3	0.735	0.493	67.07%	0.735
S14	2	162	3	0.612	0.284	46.41%	0.612
S14	2	163	2	0.630	0.132	20.95%	0.630
S14	2	164	2	0.473	0.081	17.12%	0.473
S14	2	165	3	0.121	0.070	57.85%	0.121
S14	2	166	3		0.050		0.064
S14	2	167	3	0.011	0.013	118.18%	0.011
S14	2	168	3	0.059	0.050	84.75%	0.059
S14	2	169	3	0.021	0.021	100.00%	0.021
S14	2	171	3		0.053		0.068
S14	2	172	3	0.341	0.237	69.50%	0.341
S14	2	173	3	0.410	0.266	64.88%	0.410
S14	2	174	2	0.433	0.196	45.27%	0.433
S14	2	175	3	0.169	0.135	79.88%	0.169
S14	2	176	3	0.080	0.070	87.50%	0.080
S14	2	177	3		0.138		0.183
S14	2	178	2	0.035	0.028	80.00%	0.035
S14	2	179	3		0.044		0.051
S14	2	181	2	0.246	0.202	82.11%	0.246
S14	2	182	2	0.260	0.096	36.92%	0.260
S14	2	183	3	0.164	0.151	92.07%	0.164

S14	2	184	3	0.145	0.110	75.86%	0.145
S14	2	185	3	0.138	0.115	83.33%	0.138
S14	2	186	3		0.030		0.035
S14	2	187	3	0.096	0.094	97.92%	0.096
S14	2	188	3		0.034		0.040
S14	2	189	3	0.027	0.021	77.78%	0.027
S14	2	191	3	0.180	0.131	72.78%	0.180
S14	2	192	3		0.047		0.055
S14	2	193	3		0.038		0.044
S14	2	194	3		0.033		0.039
S14	2	195	3	0.024	0.022	91.67%	0.024
S14	2	196	2	0.071	0.055	77.46%	0.071
S14	2	197	3		0.035		0.041
S14	2	198	3	0.068	0.066	97.06%	0.068
S14	2	199	3		0.045		0.053
S14	2	201	3		0.045		0.053
S14	2	202	3		0.038		0.044
S14	2	203	3		0.048		0.056
S14	2	204	2	0.025	0.019	76.00%	0.025
S14	2	205	2	0.095	0.051	53.68%	0.095
S14	2	206	3	0.204	0.087	42.65%	0.204
S14	2	207	3		0.034		0.040
S14	2	208	3		0.043		0.050
S14	2	209	3	0.028	0.020	71.43%	0.028
S14	2	211	3		0.030		0.035
S14	2	212	3	0.115	0.096	83.48%	0.115
S14	2	213	3		0.039		0.046
S14	2	214	2	0.035	0.032	91.43%	0.035
S14	2	215	1	0.096	0.057	59.38%	0.096
S14	2	216	3		0.067		0.086
S14	2	217	3	0.026	0.022	84.62%	0.026
S14	2	218	2	0.017	0.009	52.94%	0.017
S14	2	219	1		0.004		0.004
S14	2	221	3	0.030	0.025	83.33%	0.030
S14	2	222	3		0.028		0.033
S14	2	223	1	0.072	0.040	55.56%	0.072
S14	2	224	1	0.028	0.017	60.71%	0.028
S14	2	225	2	0.027	0.021	77.78%	0.027
S14	2	226	3		0.031		0.036
S14	2	227	3		0.031		0.036
S14	2	228	3		0.040		0.047
S14	2	229	3	0.009	0.008	88.89%	0.009
S14	2	231	3		0.015		0.016
S14	2	232	3	0.046	0.026	56.52%	0.046
S14	2	233	3	0.013	0.014	107.69%	0.013
S14	2	234	3		0.039		0.046
S14	2	235	3		0.032		0.037
S14	2	236	3	0.036	0.023	63.89%	0.036
S14	2	237	3	0.014	0.012	85.71%	0.014
S14	2	238	3	0.020	0.024	120.00%	0.020
S14	2	239	3		0.014		0.015
S14	2	241	2		0.008		0.009
S14	2	242	3	0.028	0.029	103.57%	0.028
S14	2	243	3	0.010	0.009	90.00%	0.010
S14	2	244	3		0.016		0.018
S14	2	245	3		0.032		0.037

S14	2	246	3	0.054	0.054	¦	100.00%	0.054
S14	2	247	3	0.025	0.020	¦	80.00%	0.025
S14	2	248	3	0.022	0.016	¦	72.73%	0.022
S14	2	249	3	0.033	0.026	¦	78.79%	0.033
S14	2	251	3		0.031	¦		0.036
S14	2	252	3		0.033	¦		0.039
S14	2	253	2	0.015	0.014	¦	93.33%	0.015
S14	2	254	3	0.116	0.050	¦	43.10%	0.116
S14	2	255	3	0.015	0.011	¦	73.33%	0.015
S14	2	256	2		0.006	¦		0.007
S14	2	257	2		0.010	¦		0.011
S14	2	258	3	0.022	0.020	¦	90.91%	0.022
S14	2	259	3		0.026	¦		0.030
S14	2	261	3	0.072	0.025	¦	34.72%	0.072
S14	2	262	3	0.021	0.020	¦	95.24%	0.021
S14	2	263	3		0.046	¦		0.054
S14	2	264	3	0.013	0.010	¦	76.92%	0.013
S14	2	265	2	0.070	0.063	¦	90.00%	0.070
S14	2	266	3	0.021	0.019	¦	90.48%	0.021
S14	2	267	2	0.025	0.024	¦	96.00%	0.025
S14	2	501	2		0.012	¦		0.013
S14	2	502	3		0.008	¦		0.009
S14	2	503	3		0.009	¦		0.010
S14	2	504	3	0.019	0.020	¦	105.26%	0.019
S14	2	505	3		0.029	¦		0.034
S14	2	506	3		0.032	¦		0.037
S14	2	507	2	0.028	0.026	¦	92.86%	0.028
S14	2	508	2	0.010	0.006	¦	60.00%	0.010
S14	2	509	3		0.027	¦		0.032
S14	2	510	2	0.022	0.017	¦	77.27%	0.022
S14	2	511	3		0.035	¦		0.041
S14	2	512	3	0.081	0.082	¦	101.23%	0.081
			MEAN	0.076	0.042	¦	84.78%	0.059


S-14-2
13' X 13' PATTERN
ORE TYPE
45000.
27000.


S-14-2
13' X 13' PATTERN
45000.
SAMPLE
27000.
3-22-90
3-23-90
3-26-90
3-27-90
3-28-90
3-28-90 @ 3:PM
50
61
66
253


TIMBERS
Sample
Sample
Sample
All holes
S-14-2
N
5000.
7000.

BROHM MINING CORPORATION
BLAST HOLE ORE TYPE

PATTERN S-142 DATE

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF	MIX	OXIDE
1			X	41			X	81			X	121			X
2			X	42			X	82			X	122			X
3			X	43			X	83			X	123			X
4		X		44			X	84			X	124			X
5			X	45			X	85			X	125			X
6			X	46			X	86			X	126			X
7			X	47			X	87			X	127			X
8			X	48			X	88			X	128			X
9			X	49			X	89			X	129			X
11			X	51			X	91			X	131			X
12			X	52			X	92				132			X
13			X	53			X	93			X	133			X
14		X		54			X	94			X	134			X
15			X	55			X	95			X	135			X
16			X	56			X	96			X	136			X
17			X	57			X	97			X	137			X
18			X	58			X	98			X	138			X
19			X	59			X	99			X	139			X
21			X	61			X	101			X	141			X
22			X	62			X	102			X	142			X
23			X	63			X	103			X	143			X
24			X	64			X	104			X	144			X
25			X	65			X	105			X	145			X
26		X		66			X	106			X	146			X
27			X	67			X	107			X	147			X
28			X	68			X	108			X	148			X
29			X	69			X	109			X	149			X
31			X	71			X	111			X	151			X
32			X	72				112			X	152		X	
33			X	73			X	113			X	153			X
34			X	74			X	114			X	154			X
35			X	75			X	115			X	155			X
36			X	76			X	116			X	156			X
37				77			X	117			X	157			X
38				78			X	118			X	158			X
39				79			X	119			X	159			X

BROHM MINING CORPORATION
BLAST HOLE ORE TYPE

PATTERN S-142 DATE

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF	MIX	OXIDE
161			X	201			X	241		X					
162			X	202			X	242			X	510		X	
163		X		203			X	243			X	511			X
164		X		204		X		244			X	512			X
165			X	205		X		245			X				
166			X	206			X	246			X				
167			X	207			X	247			X				
168			X	208			X	248			X				
169			X	209			X	249			X				
171			X	211			X	251			X				
172			X	212			X	252			X				
173			X	213			X	253		X					
174		X		214		X		254			X				
175			X	215	X			255			X				
176			X	216			X	256		X					
177			X	217			X	257		X					
178		X		218		X		258			X				
179			X	219	X			259			X				
181		X		221			X	261			X				
182		X		222			X	262			X				
183			X	223	X			263			X				
184			X	224	X			264			X				
185			X	225		X		265		X					
186			X	226			X	266			X				
187			X	227			X	267		X					
188			X	228			X	268							
189			X	229			X	269							
191			X	231			X								
192			X	232			X	501		X					
193			X	233			X	502			X				
194			X	234			X	503			X				
195			X	235			X	504			X				
196		X		236			X	505			X				
197			X	237			X	506			X				
198			X	238			X	507		X					
199			X	239			X	508		X					
								509			X				

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
5-14-2 HAND SAMPLE DUPLICATES

Submittal Date
4-2-90 12:44pm.

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 4-3-90

NAME: VO

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.				25.	Standard ✓		.015
2.				26.	148		.009
3.				27.	149		.031
4.				28.	157		.009
5.				29.	158		.024
6.	✓pulp		.027	30.	159		.025
7.	82		.360	31.	161		.530
8.	Standard ✓		.015	32.	167		.013
9.	92		.115	33.			
10.	102		.169	34.			
11.	103		.057	35.	168		.076
12.	117		.010	36.	169		.018
13.	118		.007	37.			
14.	119		.011	38.			
15.	127		.013	39.			
16.				40.			
17.				41.			
18.	128		.017	42.	Standard ✓		
19.	129		.008	43.			
20.	137		.014	44.			
21.	138		.005	45.			
22.	139		.011	46.			
23.	147-1		.012	47.			
24.	147-2		.016	48.			

GSL

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
S-14-2

Submittal Date
3/22/90 12:00p

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 3/23/90

NAME: [illegible]

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	√6		.026	25.	Standard √		.015
2.	1	.014	.014	26.	51	.034	.023
3.	2	.073	.053	27.	61		.012
4.	3	.022	.024	28.	71	.033	.023
5.	4	.016	.013	29.	81		.015
6.	5		.016	30.		StdV	.016
7.	6		.006	31.			
8.	Standard √		.016	32.			
9.	7		.015	33.	[redacted]		
10.	8		.015	34.			
11.	9-1		.011	35.			
12.	9-2		.011	36.			
13.	11	.017	.018	37.			
14.	12	.073	.062	38.			
15.	13	.014	.015	39.			
16.	[redacted]			40.			
17.				41.			
18.	14	.015	.014	42.	Standard √		
19.	15	.164	.113	43.			
20.	16		.052	44.			
21.	17	.013	.013	45.			
22.	18	.023	.021	46.			
23.	19		.010	47.			
24.	21		.012	48.			

6-12-90

GJK. BM