BROHM MINING CORPORATION
Gilt Edge Project

1

Pit-Bench-Pattern #
5-14-9

Submittal Date
5-15-90 1:00p

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 5/16/90

NAME: KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	16		.026	25.	Standard ✓		.015
2.	61	.014	.014	26.	81	.018	.016
3.	62		.035	27.	91		.010
4.	63		.015	28.	92		.011
5.	64		.028	29.	93-1		.007
6.	65		.010	30.	93-2		.008
7.	66		.011	31.	94		.006
8.	Standard ✓		.014	32.	95		.014
9.	67		.005	33.			
10.	68		.010	34.			
11.	69		.004	35.	96		.021
12.	70		.003	36.	97		.007
13.	71	.003	.002	37.	98		.014
14.	72		.006	38.	99		.049
15.	73		.010	39.	100	.002	.003
16.				40.	101		.007
17.				41.	102		.005
18.	173		.025	42.	Standard ✓		.014
19.	174	.019	.021	43.	103		.007
20.	175		.015	44.	104		.010
21.	176		.013	45.	105		.016
22.	78		.035	46.	106		.008
23.	79		.020	47.	107		.019
24.	80		.046	48.		Std✓	.015

Schaps Flocculant *

LD
VBM 6-13-90

BROWN MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
5-14-9

Submittal Date
5-16-90 1:00pm

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 5/17/90
NAME: LW, LD

* 5-14-9
5-15-90
1:00pm
Hand Samples
74-77

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
* 1.	74	.004	.005	25.	Standard ✓		.015
2.	75		.013	26.	191		.008
3.	76		.011	27.	192	.012	.012
* 4.	77		.027	28.	193		.018
5.	112		.073	29.	194		.013
6.	~~prep~~		.030	30.	195		.014
7.	113		.018	31.	196		.009
8.	Standard ✓		.014	32.	197		.015
9.	114-1		.009	33.	[redacted]		
10.	114-2		.009	34.	[redacted]		
11.	115		.004	35.	198		.020
12.	116		.013	36.	199		.017
13.	181		.020	37.	200		.018
14.	182	.016	.015	38.	201		.027
15.	183		.011	39.	202	.014	.014
16.	[redacted]			40.	203		.024
17.	[redacted]			41.	204		.033
18.	184		.007	42.	Standard ✓		.015
19.	185		.013	43.	205		.029
20.	186		.011	44.	206		.031
21.	187		.175	45.		Std ✓	.014
22.	188		.018	46.			
23.	189		.017	47.			
24.	190		.014	48.			

5 drg flocc

5 drgs flocculent *

LLD
✓ BM 6-13-90

BROWN MINING CONSULTANTS
Gilt Edge Project

Pit-Bench-Pattern #
5-14-9

Submittal Date
5-14-90 1:30pm (CONT.)

BLAST HOLE

Hot NaCN Shake and FIRE DETERMINATIONS

DATE: 5-15-90

NAME: VD, KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	86		.010	25.	Standard ✓		.015
2.	136		.015	26.	384-1		.011 (.010)
3.	137		.017	27.	384-2		.009
4.	138		.050	28.	501		.005
5.	139		.024	29.	✓pulp		.026
6.	140		.040	30.	502		.004
7.	141	.031	.032	31.	503		.004
8.	Standard ✓		.015	32.	504	.022	.013
9.	142		.026	33.	[redacted]		
10.	143		.030	34.			
11.	144		.010	35.	505		.013
12.	145		.009	36.	506		.016
13.	146		.011	37.	507		.014
14.	234		.015	38.	508		.012
15.	235		.069	39.	509		.023
16.	[redacted]			40.	510	.065	.065
17.				41.	511	.220	.183
18.	264		.060	42.	Standard ✓		.015
19.	265		.009	43.	512	.051	.036
20.	294	.056	.052	44.	513	.018	.020
21.	295		.011	45.	514	.024	.020
22.	324		.043	46.	515	.043	.039
23.	325		.025	47.	516	.019	.016
24.	354		.028	48.	517	.037	.028
					518	.039	.035
					Standard		.015

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LLD
BM 6-15-90

BROWN MINING CORPORATION
Gilt Edge Project

2

Pit-Bench-Pattern #
S-14-9

Submittal Date
5/15/90 1:00p Cont.

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 5/16/90

NAME: LW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	108	.022	.023	25.	Standard ✓		.015
2.	109		.033	26.	153		.020
3.	110		.078	27.	154		.017
4.	111		.048	28.	155		.010
5.	121		.022	29.	156		.043
6.	122		.009	30.	157		.058
7.	123		.016	31.	158		.023
8.	Standard ✓		.014	32.	159		.013
9.	124		.013	33.			
10.	125		.016	34.			
11.	126		.046	35.	160		.011
12.	127	.025	.026	36.	161		.015
13.	128		.013	37.	16		.028
14.	129		.004	38.	162	.011	.011
15.	130		.004	39.	163		.007
16.				40.	164		.005
17.				41.	165		.007
18.	131		.004	42.	Standard ✓		.015
19.	132		.004	43.	166		.016
20.	133		.029	44.	167		.016
21.	134		.010	45.	168		.019
22.	135		.014	46.	169-1		.018
23.	151		.025	47.	169-2		.019
24.	152	.043	.044	48.	170		.032
					171	.062	.055
					172		.054
					Std ✓		.015

LLD
6-13-90

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern # 5-14-9

Submittal Date 5-10-90 1:00pm

BLAST HOLE

Hot NaCN Shake and FIRE DETERMINATIONS

DATE: 5/11/90

NAME: KW, LD

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.				25.	Standard ✓		.016
2.				26.	271		.014
3.				27.	272		.013
4.				28.	301		.019
5.				29.		✓Std	.016
6.				30.			
7.				31.			
8.	Standard ✓			32.			
9.				33.			
10.	211	.009	.009	34.			
11.	212		.018	35.			
12.	213		.009	36.			
13.	214		.006	37.			
14.	215		.007	38.			
15.	216		.024	39.			
16.				40.			
17.				41.			
18.	241		.009	42.	Standard ✓		
19.	242		.030	43.			
20.	243		.019	44.			
21.	244-1	.017	.014	45.			
22.	244-2		.015	46.			
23.	245		.013	47.			
24.	246		.020	48.			

LLD
BM 6-13-90

BROWN MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
5-14-9

Submittal Date
5/11/90 1:30p (Crd.)

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 5/14/90

NAME: KW

* 5 drops Flocculant

		SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
	1.	262		.011	25.	Standard ✓		
*	2.	263		.010	26.			
*	3.	292		.008	27.			
	4.	293		.011	28.			
	5.	322		.012	29.			
*	6.	323-1	.033	.029	30.			
*	7.	323-2		.025	31.			
	8.	Standard ✓		.013	32.			
	9.		Std ✓	.014	33.			
	10.				34.			
	11.				35.			
	12.				36.			
	13.				37.			
	14.				38.			
	15.				39.			
	16.				40.			
	17.				41.			
	18.				42.	Standard ✓		
	19.				43.			
	20.				44.			
	21.				45.			
	22.				46.			
	23.				47.			
	24.				48.			

LLD
EIN 6-13-90

S-14-10

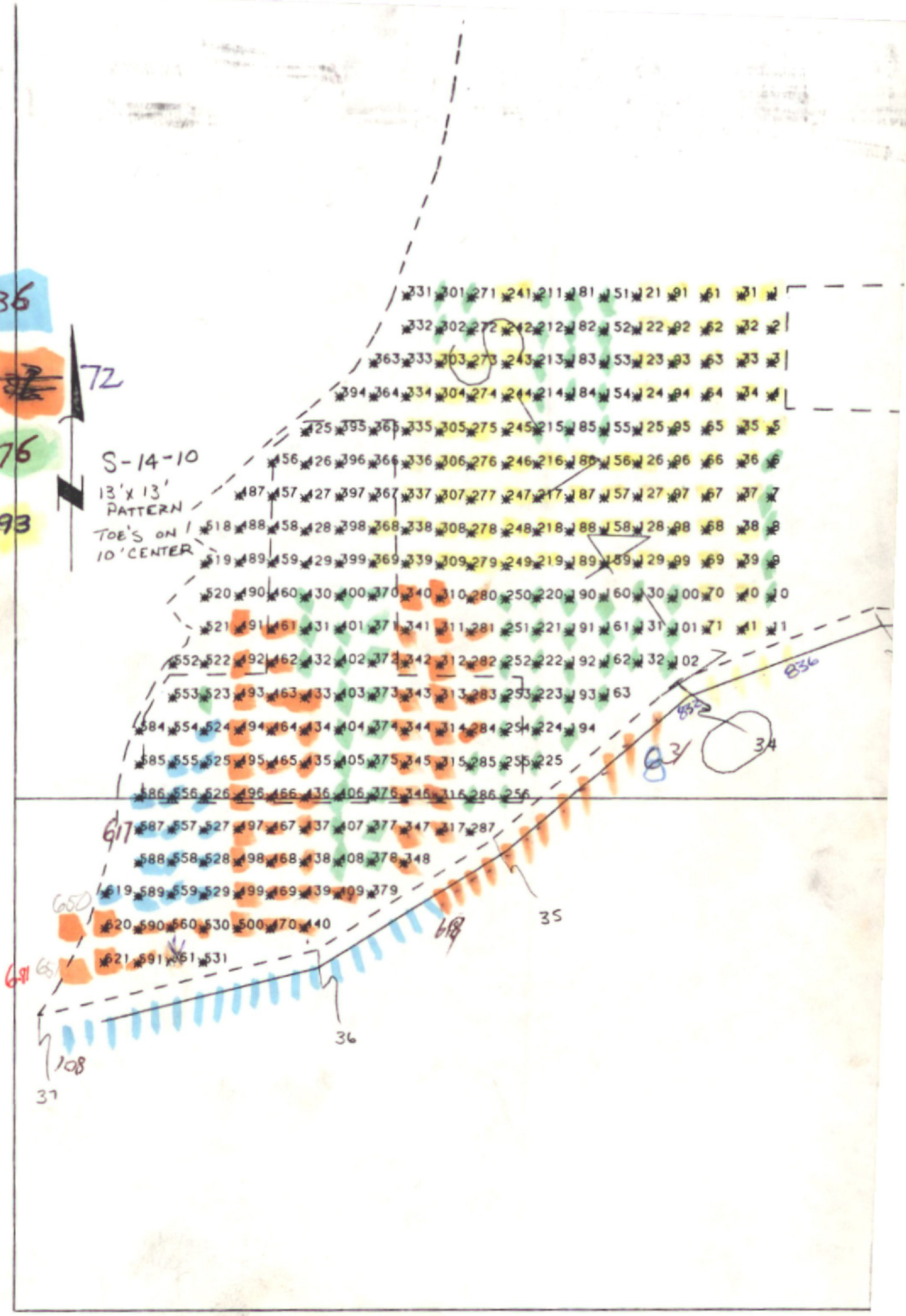
SAMPLES

5-17-90 36

5-18-90 ~~82~~ 72

5-21-90 76

5-22-90 93



BENCH NO	SHOT NO	BLAST HOLE NO	ORE TYPE	FIRE AU	AA AU	AA/FIRE	AA/RAT.
S14	10	1	3	0.013	0.013	100.00%	0.013
S14	10	2	3		0.010		0.011
S14	10	3	3		0.060		0.077
S14	10	4	3		0.042		0.049
S14	10	5	3		0.045		0.053
S14	10	6	3	0.029	0.029	100.00%	0.029
S14	10	7	3		0.056		0.072
S14	10	8	3		0.016		0.018
S14	10	9	3		0.017		0.019
S14	10	10	3		0.006		0.007
S14	10	31	3		0.106		0.140
S14	10	32	3		0.013		0.014
S14	10	33	3		0.041		0.048
S14	10	34	3		0.029		0.034
S14	10	35	3		0.046		0.054
S14	10	36	3	0.063	0.062	98.41%	0.063
S14	10	37	3		0.012		0.013
S14	10	38	3		0.017		0.019
S14	10	39	3		0.002		0.002
S14	10	40	3		0.005		0.005
S14	10	41	3		0.004		0.004
S14	10	61	3		0.014		0.015
S14	10	62	3		0.013		0.014
S14	10	63	3		0.046		0.054
S14	10	64	3		0.029		0.034
S14	10	65	3	0.064	0.061	95.31%	0.064
S14	10	66	3		0.052		0.067
S14	10	67	3		0.023		0.026
S14	10	68	3		0.012		0.013
S14	10	69	3		0.004		0.004
S14	10	70	3		0.005		0.005
S14	10	71	3		0.008		0.009
S14	10	91	3		0.081		0.107
S14	10	92	3		0.028		0.033
S14	10	93	3		0.068		0.087
S14	10	94	3	0.035	0.033	94.29%	0.035
S14	10	95	3		0.034		0.040
S14	10	96	3		0.043		0.050
S14	10	97	3		0.029		0.034
S14	10	98	3		0.010		0.011
S14	10	99	3		0.011		0.012
S14	10	100	3		0.001		0.001
S14	10	101	3		0.002		0.002
S14	10	102	3		0.017		0.019
S14	10	121	3		0.035		0.041
S14	10	122	3		0.049		0.063
S14	10	123	3		0.043		0.050
S14	10	124	3	0.080	0.082	102.50%	0.080
S14	10	125	3		0.166		0.220
S14	10	126	3		0.037		0.043
S14	10	127	3		0.023		0.026
S14	10	128	3		0.029		0.034
S14	10	129	3		0.007		0.008
S14	10	130	3		0.002		0.002
S14	10	131	3		0.002		0.002
S14	10	132	3	0.007	0.006	85.71%	0.007
S14	10	151	3		0.027		0.032
S14	10	152	3		0.028		0.033
S14	10	153	3		0.034		0.040

OK 6-13-90

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S14	10	154	3		0.015		0.016
S14	10	155	3		0.121		0.160
S14	10	156	3		0.114		0.151
S14	10	157	3		0.013		0.014
S14	10	158	3		0.012		0.013
S14	10	159	3		0.004		0.004
S14	10	160	3		0.002		0.002
S14	10	161	3		0.003		0.003
S14	10	162	3		0.001		0.001
S14	10	163	3		0.002		0.002
S14	10	181	3	0.035	0.033	94.29%	0.035
S14	10	182	3		0.032		0.037
S14	10	183	3		0.046		0.054
S14	10	184	3		0.042		0.049
S14	10	185	3		0.048		0.056
S14	10	186	3		0.192		0.254
S14	10	187	3	0.022	0.023	104.55%	0.022
S14	10	188	3		0.011		0.012
S14	10	189	3		0.006		0.007
S14	10	190	3		0.003		0.003
S14	10	191	3		0.013		0.014
S14	10	192	3		0.006		0.007
S14	10	193	3		0.002		0.002
S14	10	194	3		0.005		0.005
S14	10	211	3	0.026	0.024	92.31%	0.026
S14	10	212	3		0.015		0.016
S14	10	213	3		0.026		0.030
S14	10	214	3		0.020		0.023
S14	10	215	3		0.023		0.026
S14	10	216	3		0.171		0.226
S14	10	217	3		0.016		0.018
S14	10	218	3		0.064		0.082
S14	10	219	3		0.005		0.005
S14	10	220	3		0.004		0.004
S14	10	221	3		0.003		0.003
S14	10	222	3		0.009		0.010
S14	10	223	3		0.008		0.009
S14	10	224	3		0.019		0.022
S14	10	225	3	0.009	0.007	77.78%	0.009
S14	10	241	3		0.008		0.009
S14	10	242	3		0.016		0.018
S14	10	243	3		0.015		0.016
S14	10	244	3	0.017	0.016	94.12%	0.017
S14	10	245	3		0.014		0.015
S14	10	246	3	0.019	0.018	94.74%	0.019
S14	10	247	3		0.011		0.012
S14	10	248	3		0.026		0.030
S14	10	249	3		0.016		0.018
S14	10	250	3		0.007		0.008
S14	10	251	3		0.005		0.005
S14	10	252	3		0.006		0.007
S14	10	253	3		0.009		0.010
S14	10	254	3		0.010		0.011
S14	10	255	3		0.012		0.013
S14	10	256	3		0.008		0.009
S14	10	271	3		0.021		0.024

S14	10	272	3		0.013		0.014
S14	10	273	3		0.019		0.022
S14	10	274	3		0.027		0.032
S14	10	275	3		0.048		0.056
S14	10	276	3		0.024		0.027
S14	10	277	3		0.036		0.042
S14	10	278	3		0.029		0.034
S14	10	279	3	0.020	0.021	105.00%	0.020
S14	10	280	3	0.011	0.009	81.82%	0.011
S14	10	281	3		0.009		0.010
S14	10	282	3		0.006		0.007
S14	10	283	3		0.011		0.012
S14	10	284	3		0.010		0.011
S14	10	285	3	0.009	0.010	111.11%	0.009
S14	10	286	3		0.009		0.010
S14	10	301	3		0.021		0.024
S14	10	302	3		0.019		0.022
S14	10	303	3		0.014		0.015
S14	10	304	3		0.009		0.010
S14	10	305	3		0.050		0.064
S14	10	306	3		0.016		0.018
S14	10	307	3		0.017		0.019
S14	10	308	3		0.043		0.050
S14	10	309	3		0.026		0.030
S14	10	310	3		0.021		0.024
S14	10	311	3		0.011		0.012
S14	10	312	3		0.017		0.019
S14	10	313	3		0.017		0.019
S14	10	314	3		0.026		0.030
S14	10	315	3	0.021	0.019	90.48%	0.021
S14	10	316	3		0.009		0.010
S14	10	317	3		0.042		0.049
S14	10	334	3		0.025		0.028
S14	10	335	3		0.008		0.009
S14	10	336	3	0.020	0.018	90.00%	0.020
S14	10	337	3		0.018		0.020
S14	10	338	3		0.028		0.033
S14	10	339	3		0.016		0.018
S14	10	340	3		0.027		0.032
S14	10	341	3		0.016		0.018
S14	10	342	3		0.022		0.025
S14	10	343	3		0.050		0.064
S14	10	344	3		0.035		0.041
S14	10	345	3		0.023		0.026
S14	10	346	3		0.018		0.020
S14	10	347	3	0.085	0.076	89.41%	0.085
S14	10	348	3		0.025		0.028
S14	10	368	3		0.016		0.018
S14	10	369	3		0.019		0.022
S14	10	370	3		0.068		0.087
S14	10	371	3		0.023		0.026
S14	10	372	3		0.017		0.019
S14	10	373	3		0.019		0.022
S14	10	374	3		0.018		0.020
S14	10	375	3		0.017		0.019
S14	10	376	3	0.031	0.032	103.23%	0.031

S14	10	377	3		0.089		0.118
S14	10	378	3		0.053		0.068
S14	10	400	3		0.023		0.026
S14	10	401	3		0.080		0.106
S14	10	402	3		0.010		0.011
S14	10	403	3		0.015		0.016
S14	10	404	3		0.011		0.012
S14	10	405	3		0.021		0.024
S14	10	406	3		0.047		0.055
S14	10	407	3	0.015	0.013	86.67%	0.015
S14	10	408	3		0.015		0.016
S14	10	409	3		0.012		0.013
S14	10	430	3		0.032		0.037
S14	10	431	3		0.037		0.043
S14	10	432	3		0.017		0.019
S14	10	433	3		0.016		0.018
S14	10	434	3		0.016		0.018
S14	10	435	3		0.017		0.019
S14	10	436	3		0.128		0.169
S14	10	437	3		0.011		0.012
S14	10	438	3		0.041		0.048
S14	10	439	3		0.034		0.040
S14	10	440	3	0.052	0.053	101.92%	0.052
S14	10	461	3		0.016		0.018
S14	10	462	3		0.018		0.020
S14	10	463	3		0.044		0.051
S14	10	464	3		0.024		0.027
S14	10	465	3		0.012		0.013
S14	10	466	3		0.161		0.213
S14	10	467	3		0.015		0.016
S14	10	468	3		0.005		0.005
S14	10	469	3		0.036		0.042
S14	10	470	3	0.010	0.007	70.00%	0.010
S14	10	491	3		0.034		0.040
S14	10	492	3		0.029		0.034
S14	10	493	3		0.042		0.049
S14	10	494	3		0.016		0.018
S14	10	495	3		0.022		0.025
S14	10	496	3		0.029		0.034
S14	10	497	3		0.009		0.010
S14	10	498	3		0.198	176 .179 RERUN	0.262
S14	10	499	3		0.012		0.013
S14	10	500	3	0.007	0.006	85.71%	0.007
S14	10	523	3		0.048		0.056
S14	10	524	3	0.046	0.040	86.96%	0.046
S14	10	525	3		0.129		0.171
S14	10	526	3		0.085		0.112
S14	10	527	3		0.025		0.028
S14	10	528	3		0.027		0.032
S14	10	529	3		0.031		0.036
S14	10	530	3		0.002		0.002
S14	10	555	3		0.108		0.143
S14	10	556	3		0.265		0.351
S14	10	557	3		0.095		0.126
S14	10	558	3		0.011		0.012
S14	10	559	3	0.006	0.005	83.33%	0.006

S14	10	560	3		0.001		0.001
S14	10	561	3		0.003		0.003
S14	10	586	3		0.080		0.106
S14	10	587	3		0.147		0.194
S14	10	588	3		0.015		0.016
S14	10	589	3		0.004		0.004
S14	10	590	3		0.011		0.012
S14	10	591	3		0.001		0.001
S14	10	617	3		0.217		0.287
S14	10	619	3		0.005		0.005
S14	10	620	3		0.006		0.007
S14	10	621	3		0.002		0.002
S14	10	650	3		0.003		0.003
S14	10	651	3		0.002		0.002
S14	10	681	3	0.011	0.006	54.55%	0.011
S14	10	801	3		0.005		0.005
S14	10	802	3		0.016		0.018
S14	10	803	3		0.001		0.001
S14	10	804	3	0.000	0.001	100.00%	0.000
S14	10	805	3		0.001		0.001
S14	10	806	3		0.001		0.001
S14	10	807	3		0.001		0.001
S14	10	808	3		0.018		0.020
S14	10	809	3		0.001		0.001
S14	10	810	3		0.003		0.003
S14	10	811	3		0.002		0.002
S14	10	812	3		0.002		0.002
S14	10	813	3		0.005		0.005
S14	10	814	3	0.051	0.047	92.16%	0.051
S14	10	815	3		0.031		0.036
S14	10	816	3		0.010		0.011
S14	10	817	3		0.018		0.020
S14	10	818	3		0.026		0.030
S14	10	819	3		0.048		0.056
S14	10	820	3	0.060	0.055	91.67%	0.060
S14	10	821	3		0.006		0.007
S14	10	822	3		0.010		0.011
S14	10	823	3		0.005		0.005
S14	10	824	3		0.006		0.007
S14	10	825	3		0.006		0.007
S14	10	826	3		0.030		0.035
S14	10	827	3		0.002		0.002
S14	10	828	1	0.003	0.002	66.67%	0.003
S14	10	829	3		0.005		0.005
S14	10	830	3	0.004	0.003	75.00%	0.004
S14	10	831	3		0.006		0.007
S14	10	832	3		0.003		0.003
S14	10	833	3		0.008		0.009
S14	10	834	3		0.011		0.012
S14	10	835	3		0.014		0.015
S14	10	836	3		0.006		0.007
		MEAN		0.028	0.028	90.61%	0.034

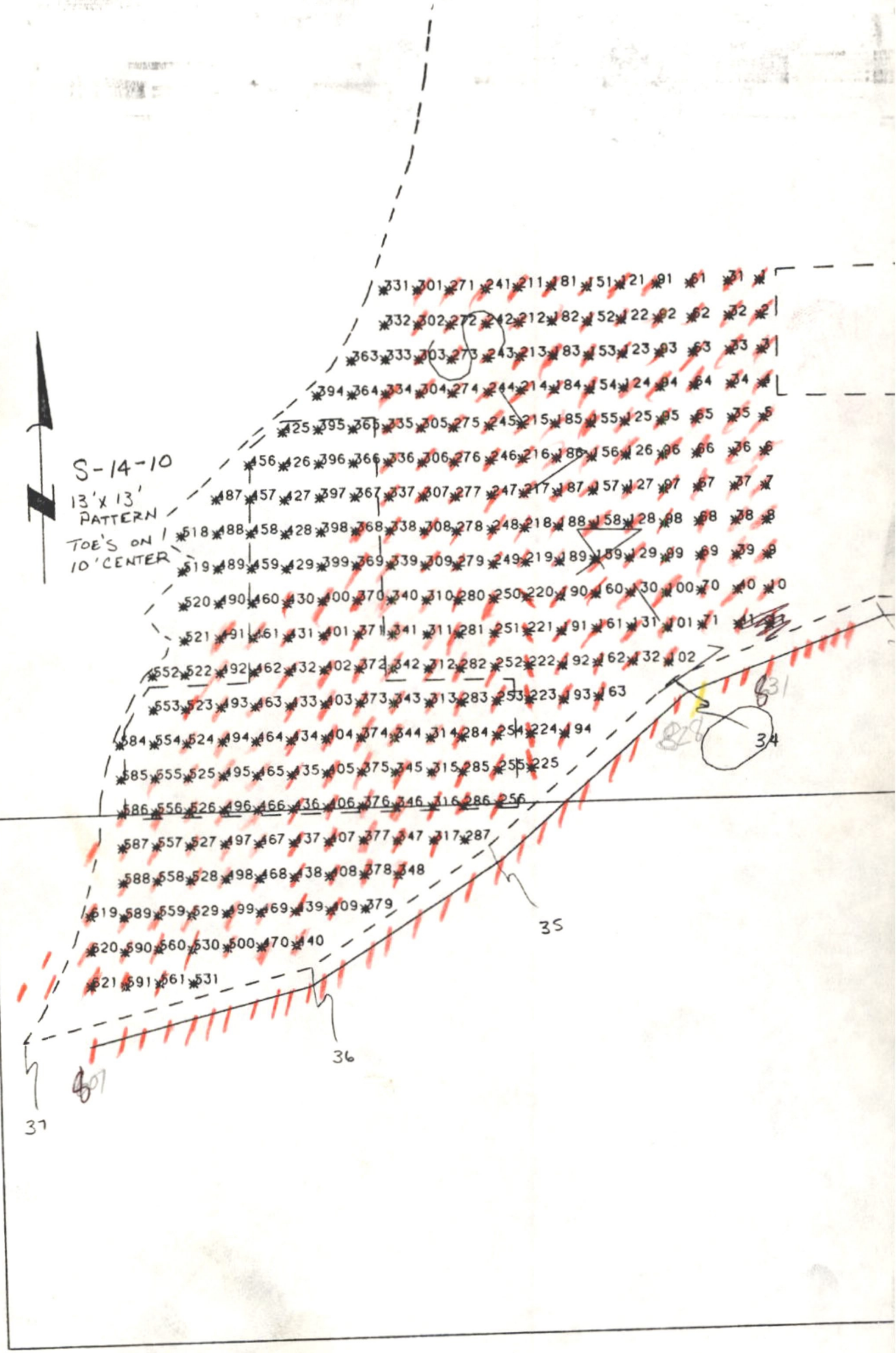
S-14-10

S14	10	1	3	0.013	0.013	100.00%
S14	10	2	3		0.010	ERR
S14	10	3	3		0.060	ERR
S14	10	4	3		0.042	ERR
S14	10	5	3		0.045	ERR
S14	10	6	3	0.029	0.029	100.00%
S14	10	7	3		0.056	ERR
S14	10	8	3		0.016	ERR
S14	10	9	3		0.017	ERR
S14	10	10	3		0.006	ERR
S14	10	31	3		0.106	ERR
S14	10	32	3		0.013	ERR
S14	10	33	3		0.041	ERR
S14	10	34	3		0.029	ERR
S14	10	35	3		0.046	ERR
S14	10	36	3	0.063	0.062	98.41%
S14	10	37	3		0.012	ERR
S14	10	38	3		0.017	ERR
S14	10	39	3		0.002	ERR
S14	10	40	3		0.005	ERR
S14	10	41	3		0.004	ERR
S14	10	61	3		0.014	ERR
S14	10	62	3		0.013	ERR
S14	10	63	3		0.046	ERR
S14	10	64	3		0.029	ERR
S14	10	65	3	0.064	0.061	95.31%
S14	10	66	3		0.052	ERR
S14	10	67	3		0.023	ERR
S14	10	68	3		0.012	ERR
S14	10	69	3		0.004	ERR
S14	10	70	3		0.005	ERR
S14	10	71	3		0.008	ERR
S14	10	91	3		0.081	ERR
S14	10	92	3		0.028	ERR
S14	10	93	3		0.068	ERR
S14	10	94	3	0.035	0.033	94.29%
S14	10	95	3		0.034	ERR
S14	10	96	3		0.043	ERR
S14	10	97	3		0.029	ERR
S14	10	98	3		0.010	ERR
S14	10	99	3		0.011	ERR
S14	10	100	3		0.001	ERR
S14	10	101	3		0.002	ERR
S14	10	102	3		0.017	ERR
S14	10	121	3		0.035	ERR
S14	10	122	3		0.049	ERR
S14	10	123	3		0.043	ERR
S14	10	124	3	0.080	0.082	102.50%
S14	10	125	3		0.166	ERR
S14	10	126	3		0.037	ERR
S14	10	127	3		0.023	ERR
S14	10	128	3		0.029	ERR
S14	10	129	3		0.007	ERR
S14	10	130	3		0.002	ERR
S14	10	131	3		0.002	ERR
S14	10	132	3	0.007	0.006	85.71%

S14	10	151	3		0.027	ERR
S14	10	152	3		0.028	ERR
S14	10	153	3		0.034	ERR
S14	10	154	3		0.015	ERR
S14	10	155	3		0.121	ERR
S14	10	156	3		0.114	ERR
S14	10	157	3		0.013	ERR
S14	10	158	3		0.012	ERR
S14	10	159	3		0.004	ERR
S14	10	160	3		0.002	ERR
S14	10	161	3		0.003	ERR
S14	10	162	3		0.001	ERR
S14	10	163	3		0.002	ERR
S14	10	181	3	0.035	0.033	94.29%
S14	10	182	3		0.032	ERR
S14	10	183	3		0.046	ERR
S14	10	184	3		0.042	ERR
S14	10	185	3		0.048	ERR
S14	10	186	3		0.192	ERR
S14	10	187	3	0.022	0.023	104.55%
S14	10	188	3		0.011	ERR
S14	10	189	3		0.006	ERR
S14	10	190	3		0.003	ERR
S14	10	191	3		0.006 .13	ERR
S14	10	192	3		0.002 .006	ERR
S14	10	193	3		0.002 OK	ERR
S14	10	194	3		0.005	ERR
S14	10	211	3	0.026	0.024	92.31%
S14	10	212	3		0.015	ERR
S14	10	213	3		0.026	ERR
S14	10	214	3		0.020	ERR
S14	10	215	3		0.023	ERR
S14	10	216	3		0.171	ERR
S14	10	217	3		0.016	ERR
S14	10	218	3		0.064	ERR
S14	10	219	3		0.005	ERR
S14	10	220	3		0.004	ERR
S14	10	221	3		0.003	ERR
S14	10	222	3		0.009	ERR
S14	10	223	3		0.008	ERR
S14	10	224	3		0.019	ERR
S14	10	225	3	0.009	0.007	77.78%
S14	10	241	3		0.008	ERR
S14	10	242	3		0.016	ERR
S14	10	243	3		0.015	ERR
S14	10	244	3	0.017	0.016	94.12%
S14	10	245	3		0.014	ERR
S14	10	246	3	0.019	0.018	94.74%
S14	10	247	3		0.011	ERR
S14	10	248	3		0.026	ERR
S14	10	249	3		0.016	ERR
S14	10	250	3		0.007	ERR
S14	10	251	3		0.005	ERR
S14	10	252	3		0.006	ERR
S14	10	253	3		0.009	ERR
S14	10	254	3		0.010	ERR

S14	10	255	3		0.012	ERR
S14	10	256	3		0.008	ERR
S14	10	271	3		0.021	ERR
S14	10	272	3		0.013	ERR
S14	10	273	3		0.019	ERR
S14	10	274	3		0.027	ERR
S14	10	275	3		0.048	ERR
S14	10	276	3		0.024	ERR
S14	10	277	3		0.036	ERR
S14	10	278	3		0.029	ERR
S14	10	279	3	0.020	0.021	105.00%
S14	10	280	3	0.011	0.009	81.82%
S14	10	281	3		0.009	ERR
S14	10	282	3		0.006	ERR
S14	10	283	3		0.011	ERR
S14	10	284	3		0.010	ERR
S14	10	285	3	0.009	0.010	111.11%
S14	10	286	3		0.009	ERR
S14	10	301	3		0.021	ERR
S14	10	302	3		0.019	ERR
S14	10	303	3		0.014	ERR
S14	10	304	3		0.009	ERR
S14	10	305	3		0.050	ERR
S14	10	306	3		0.016	ERR
S14	10	307	3		0.017	ERR
S14	10	308	3		0.043	ERR
S14	10	309	3		0.026	ERR
S14	10	310	3		0.021	ERR
S14	10	311	3		0.011	ERR
S14	10	312	3		0.017	ERR
S14	10	313	3		0.017	ERR
S14	10	314	3		0.026	ERR
S14	10	315	3	0.021	0.019	90.48%
S14	10	316	3		0.009	ERR
S14	10	317	3		0.042	ERR
S14	10	334	3		0.025	ERR
S14	10	335	3		0.008	ERR
S14	10	336	3	0.020	0.018	90.00%
S14	10	337	3		0.018	ERR
S14	10	338	3		0.028	ERR
S14	10	339	3		0.016	ERR
S14	10	340	3		0.027	ERR
S14	10	341	3		0.016	ERR
S14	10	342	3		0.022	ERR
S14	10	343	3		0.050	ERR
S14	10	344	3		0.035	ERR
S14	10	345	3		0.023	ERR
S14	10	346	3		0.018	ERR
S14	10	347	3	0.085	0.076	89.41%
S14	10	348	3		0.025	ERR
S14	10	368	3		0.016	ERR
S14	10	369	3		0.019	ERR
S14	10	370	3		0.068	ERR
S14	10	371	3		0.023	ERR
S14	10	372	3		0.017	ERR
S14	10	373	3		0.019	ERR

S14	10	374	3		0.018	ERR
S14	10	375	3		0.017	ERR
S14	10	376	3	0.031	0.032	103.23%
S14	10	377	3		0.089	ERR
S14	10	378	3		0.053	ERR
S14	10	400	3		0.023	ERR
S14	10	401	3		0.080	ERR
S14	10	402	3		0.010	ERR
S14	10	403	3		0.015	ERR
S14	10	404	3		0.011	ERR
S14	10	405	3		0.021	ERR
S14	10	406	3		0.047	ERR
S14	10	407	3	0.015	0.013	86.67%
S14	10	408	3		0.015	ERR
S14	10	409	3		0.012	ERR
S14	10	430	3		0.032	ERR
S14	10	431	3		0.037	ERR
S14	10	432	3		0.017	ERR
S14	10	433	3		0.016	ERR
S14	10	434	3		0.016	ERR
S14	10	435	3		0.017	ERR
S14	10	436	3		0.128	ERR
S14	10	437	3		0.011	ERR
S14	10	438	3		0.041	ERR
S14	10	439	3		0.034	ERR
S14	10	440	3	0.052	0.053	101.92%
S14	10	461	3		0.016	ERR
S14	10	462	3		0.018	ERR
S14	10	463	3		0.044	ERR
S14	10	464	3		0.024	ERR
S14	10	465	3		0.012	ERR
S14	10	466	3		0.161	ERR
S14	10	467	3		0.015	ERR
S14	10	468	3		0.005	ERR
S14	10	469	3		0.036	ERR
S14	10	470	3	0.010	0.007	70.00%
S14	10	491	3		0.034	ERR
S14	10	492	3		0.029	ERR
S14	10	493	3		0.042	ERR
S14	10	494	3		0.016	ERR
S14	10	495	3		0.022	ERR
S14	10	496	3		0.029	ERR
S14	10	497	3		0.009	ERR
S14	10	498	3		0.198	ERR
S14	10	499	3		0.012	ERR
S14	10	500	3	0.007	0.006	85.71%
S14	10	523	3		0.048	ERR
S14	10	524	3	0.046	0.040	86.96%
S14	10	525	3		0.129	ERR
S14	10	526	3		0.085	ERR
S14	10	527	3		0.025	ERR
S14	10	528	3		0.027	ERR
S14	10	529	3		0.031	ERR
S14	10	530	3		0.002	ERR
S14	10	555	3		0.108	ERR
S14	10	556	3		0.265	ERR

S14	10	557	3		0.095	ERR
S14	10	558	3		0.011	ERR
S14	10	559	3	0.006	0.005	83.33%
S14	10	560	3		0.001	ERR
S14	10	561	3		0.003	ERR
S14	10	586	3		0.080	ERR
S14	10	587	3		0.147	ERR
S14	10	588	3		0.015	ERR
S14	10	589	3		0.004	ERR
S14	10	590	3		0.011	ERR
S14	10	591	3		0.001	ERR
S14	10	617	3		0.217	ERR
S14	10	619	3		0.005	ERR
S14	10	620	3		0.006	ERR
S14	10	621	3		0.002	ERR
S14	10	650	3		0.003	ERR
S14	10	651	3		0.002	ERR
S14	10	681	3	0.011	0.006	54.55%
S14	10	801	3		0.005	ERR
S14	10	802	3		0.016	ERR
S14	10	803	3		0.001	ERR
S14	10	804	3	0.000	0.001	ERR
S14	10	805	3		0.001	ERR
S14	10	806	3		0.001	ERR
S14	10	807	3		0.001	ERR
S14	10	808	3		0.018	ERR
S14	10	809	3		0.001	ERR
S14	10	810	3		0.003	ERR
S14	10	811	3		0.002	ERR
S14	10	812	3		0.002	ERR
S14	10	813	3		0.005	ERR
S14	10	814	3	0.051	0.047	92.16%
S14	10	815	3		0.031	ERR
S14	10	816	3		0.010	ERR
S14	10	817	3		0.018	ERR
S14	10	818	3		0.026	ERR
S14	10	819	3		0.048	ERR
S14	10	820	3	0.060	0.055	91.67%
S14	10	821	3		0.006	ERR
S14	10	822	3		0.010	ERR
S14	10	823	3		0.005	ERR
S14	10	824	3		0.006	ERR
S14	10	825	3		0.006	ERR
S14	10	826	3		0.030	ERR
S14	10	827	3		0.002	ERR
S14	10	828	1	0.003	0.002	66.67%
S14	10	829	3		0.005	ERR
S14	10	830	3	0.004	0.003	75.00%
S14	10	831	3		0.006	ERR
S14	10	832	3		0.003	ERR
S14	10	833	3		0.008	ERR
S14	10	834	3		0.011	ERR
S14	10	835	3		0.014	ERR
S14	10	836	3		0.006	ERR

ORE TYPE