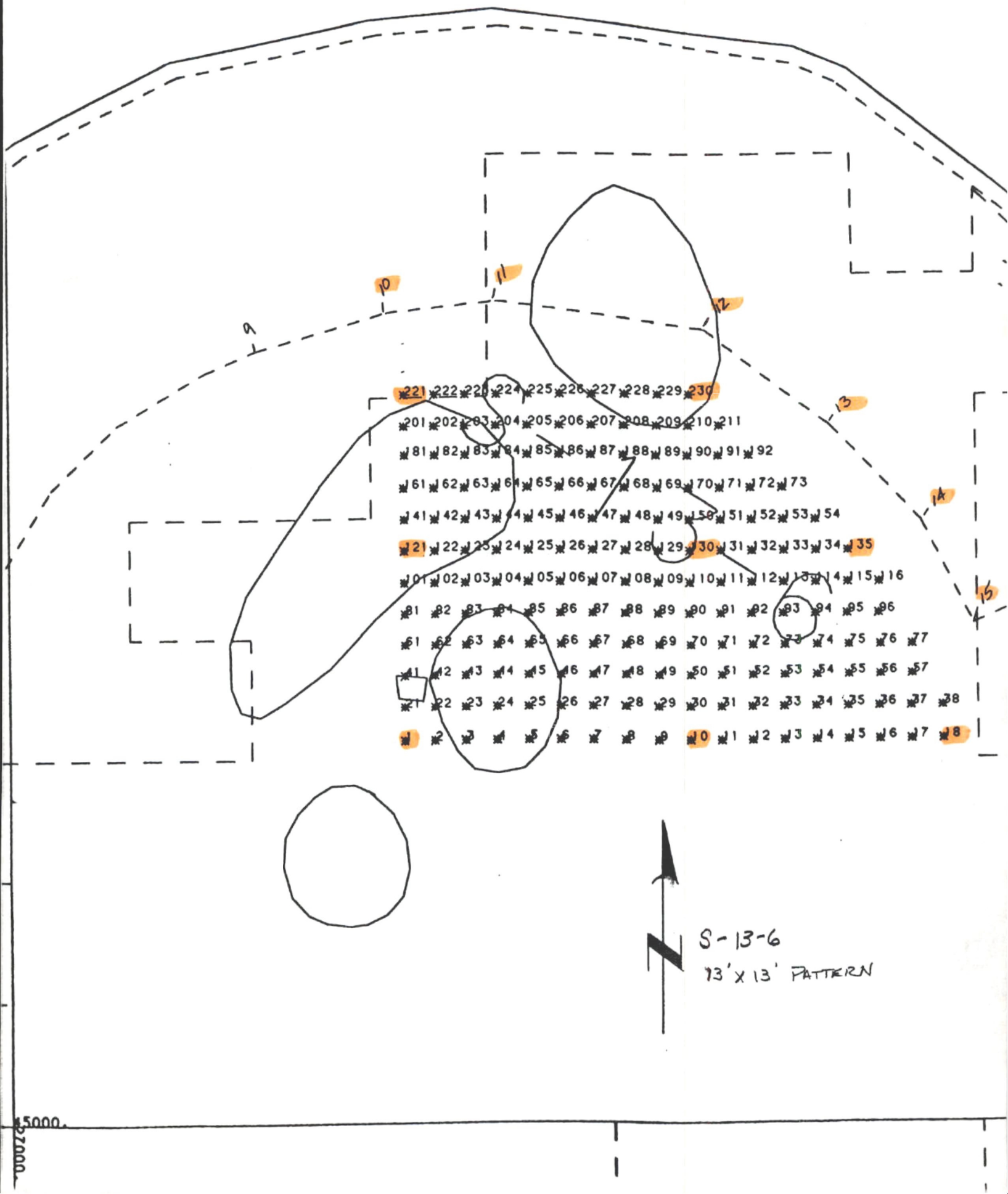

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221 222 223 224 225 226 227 228 229 230
201 202 203 204 205 206 207 208 209 210 211
181 182 183 184 185 186 187 188 189 190 191 192
161 162 163 164 165 166 167 168 169 170 171 172 173
141 142 143 144 145 146 147 148 149 150 151 152 153 154
121 122 123 124 125 126 127 128 129 130 131 132 133 134 135
101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116
81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96
61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77
41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57
21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
N
S-13-6
13' X 13' PATTERN
45000.
27000.

BROHM MINING CORPORATION
BLAST HOLE ORE TYPE

PATTERN S-13-6

DATE 01-11-90

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF	MIX	OXIDE
1		X		41		X		81		X		121			X
2			X	42		X		82			X	122			X
3			X	43	X			83			X	123			X
4			X	44		X		84		X		124		X	
5			X	45			X	85			X	125	X		
6			X	46			X	86			X	126		X	
7			X	47			X	87			X	127			X
8			X	48			X	88			X	128			X
9			X	49			X	89			X	129			X
10			X	50			X	90		X		130			X
11			X	51			X	91			X	131			X
12			X	52			X	92			X	132		X	
13		X		53		X		93			X	133		X	
14		X		54			X	94			X	134	X		
15			X	55			X	95		X		135			X
16			X	56			X	96			X	136		X	
17			X	57			X	97			X				
18			X	58			X					500			X
												501			X
												502			X
21		X		61		X		101			X				
22	X			62		X		102			X	550			X
23			X	63			X	103			X	551			X
24		X		64			X	104			X	552			X
25			X	65			X	105		X		553			X
26			X	66			X	106			X	554			
27			X	67			X	107			X	555			
28			X	68			X	108			X				
29			X	69			X	109			X				
30			X	70		X		110			X				
31			X	71			X	111		X					
32			X	72			X	112			X				
33			X	73			X	113			X				
34			X	74			X	114	X						
35			X	75			X	115		X					
36			X	76			X	116		X					
37			X	77			X	117			X				
38			X	78			X								

85° → 80°

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern # 5-13-6

Submittal Date 1/10/90 1:45 (mt)

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 1/11/90

NAME:

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	91	.024	.024	25.	Standard ✓	.0146	.015
2.	92	.021	.019	26.	126	.023	.019
3.	93	.067	.048	27.	127-1	.129	.053
4.	94	.018	.012	28.	127-2	.149	.049
5.	1/Pulp6		.028	29.	131	.019	.013
6.	101	.027	.022	30.	132	.023	.019
7.	102	.062	.046	31.	133	.040	.038
8.	Standard ✓	.0146	.015	32.	Standard ✓	.0146	.014
9.	103	.108	.047	33.			
10.	104	.184	.100	34.			
11.	105	.049	.052	35.			
12.	106	.425	.214	36.			
13.	107	.231	.062	37.			
14.	111	.029	.028	38.			
15.	112	.055	.032	39.			
16.				40.			
17.				41.			
18.	113	.086	.067	42.	Standard ✓		
19.	114	.006	.002	43.			
20.	121	.097	.056	44.			
21.	122	.091	.072	45.			
22.	123	.060	.037	46.			
23.	124	.088	.053	47.			
24.	125	.045	.027	48.			

LLD

85°C →

2

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
5-13-6

Submittal Date
1-09-90 1:10 pm

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 1/10/90

NAME: VD, KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	15	.013	.010	25.	Standard ✓		.014
2.	16	.018	.016	26.	117-1	.018	.015
3.	17	.020	.019	27.	117-2	.023	.012
4.	18	.016	.013	28.	134	.017	.008
5.	35	.045	.026	29.	✓pulp		.028
6.	36	.032	.027	30.	135	.043	.050
7.	37	.037	.037	31.	136	.087	.067
8.	Standard ✓		.015	32.	500	.023	.024
9.	38	.031	.027	33.			
10.	55	.113	.064	34.			
11.	56	.057	.052	35.	501	.044	.037
12.	57	.022	.019	36.	502	.039	.083 ✓
13.	58	.015	.014	37.	550	.021	.020
14.	75	.077	.072	38.	551	.021	.019
15.	76	.137	.127	39.	552	.089	.027 Rerun
16.				40.	553	.081	.036
17.				41.	Std ✓		.015
18.	77	.091	.036	42.	Standard ✓		.015
19.	78	.015	.013	43.			
20.	95	.015	.008	44.			
21.	96	.033	.020	45.			
22.	97	.030	.030	46.			
23.	115	.022	.012	47.			
24.	116	.042	.034	48.			

VD
GZL

78 → 70°C

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern
S-13-6

Submittal Date
1-11-90 9:30 am
*9:45 am

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 1/12/90
NAME: VD, KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	1	.073	.043	25.	Standard ✓		.015
2.	2	.019	.014	26.	48	.088	.077
3.	✓pulp		.031	27.	49	.058	.052
4.	3	.043	.040	28.	50	.036	.032
5.	4	.073	.061	29.	68	.024	.015
6.	5-1	.262	.095	30.	69	.079	.053
7.	5-2		.100	31.	70	.016	.009
8.	Standard ✓		.015	32.	88	.016	.015
9.	21	.090	.074	33.			
10.	22	.061	.050	34.			
11.	23	.043	.030	35.	89	.029	.031
12.	24	.041	.027	36.	90	.121	.026
13.	41	.256	.155	37.	108	.030	.025
14.	42	.142	.086	38.	109	.014	.010
15.	43	.038	.024	39.	110	.036	.031
16.				40.	128	.016	.024
17.				41.	129	.012	.014
18.	44	.061	.047	42.	Standard ✓		.015
*19.	8	.021	.016	43.	130	.014	.040
20.	9	.035	.032	44.			
21.	10	.031	.023	45.			
22.	28	.021	.019	46.			
23.	29	.051	.047	47.			
24.	30	.041	.024	48.			

LLD
G.L.

792 → 15'C

BROHM MINING CORPORATION
Gilt Edge Project

Pit-Bench-Pattern #
S-13-6

Submittal Date
1-10-90 1:45p

BLAST HOLE

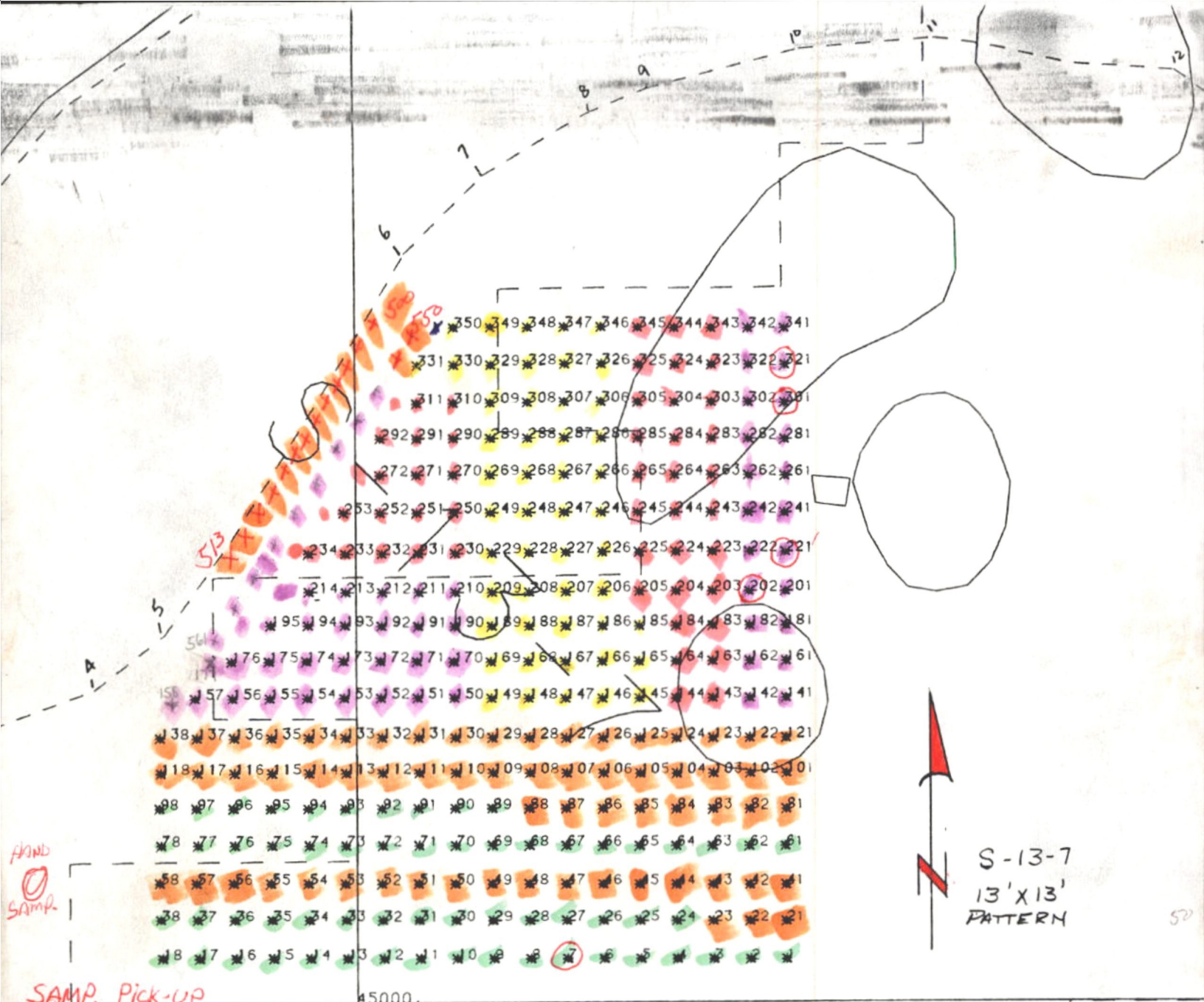
Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 1/11/90

NAME: KW, UD

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	6	.034	.006	25.	Standard ✓		.014
2.	7	.020 ~~.016~~	.018	26.	61	.107	.009
3.	11	.026	.022	27.	62	.498	.057
4.	12	.039	.037	28.	63	.156	.096
5.	13	.033	.013	29.	64	.126	.103
6.	14	.030	.028	30.	65	.043	.038
7.	25	.069	.048	31.	66	.052	.042
8.	Standard ✓		.015	32.	67	.039	.033
9.	26	.023	.013	33.			
10.	27-1	.050	.033	34.			
11.	27-2	.058	.029	35.	71	.016	.014
12.	31	.055	.031	36.	72	.047	.041
13.	32	.119	.041	37.	73	.023	.019
14.	33	.030	.023	38.	74	.773	.196
15.	34	.059	.050	39.	Pulp		.028
16.				40.	81	.292	.170
17.				41.	82	.184	.089
18.	45	.050	.029	42.	Standard ✓		.015
19.	46	.042	.045	43.	83	.081	.034
20.	47	.156	.132	44.	84	.159	.045
21.	51	.021	.020	45.	85	.400	.283
22.	52	.044	.030	46.	86	.152	.110
23.	53	.020	.015	47.	87	.038	.036
24.	54	.091	.018	48.	Std ✓		.014

LD



1-12-90	61
1-15-90	81
1-16-90	62
1-17-90	51
1-18-90	50
	306

BENCH NO	SHOT NO	BLASTHOLE NO	ORE TYPE	FIRE AU	AA AU	AA/FIRE	AA/.88
S13	7	1	3	0.010	0.010	100.00%	0.010
S13	7	2	3		0.009		0.010
S13	7	3	2	0.039	0.034	87.18%	0.039
S13	7	4	3		0.010		0.011
S13	7	5	3	0.042	0.039	92.86%	0.042
S13	7	6	3		0.029		0.034
S13	7	7	3		0.004		0.004
S13	7	8	3		0.010		0.011
S13	7	9	3	0.034	0.017	50.00%	0.034
S13	7	10	3		0.060		0.077
S13	7	11	3	0.044	0.039	88.64%	0.044
S13	7	12	3	0.024	0.022	91.67%	0.024
S13	7	13	3		0.076		0.101
S13	7	14	3		0.033		0.039
S13	7	15	3		0.009		0.010
S13	7	16	3		0.009		0.010
S13	7	17	3		0.045		0.053
S13	7	18	3		0.036		0.042
S13	7	21	2	0.007	0.007	100.00%	0.007
S13	7	22	3		0.005		0.005
S13	7	23	3		0.006		0.007
S13	7	24	3		0.017		0.019
S13	7	25	3	0.024	0.022	91.67%	0.024
S13	7	26	3	0.028	0.028	100.00%	0.028
S13	7	27	3		0.009		0.010
S13	7	28	3		0.014		0.015
S13	7	29	3		0.018		0.020
S13	7	30	3		0.035		0.041
S13	7	31	3	0.023	0.018	78.26%	0.023
S13	7	32	3		0.077		0.102
S13	7	33	3		0.027		0.032
S13	7	34	3		0.025		0.028
S13	7	35	3		0.015		0.016
S13	7	36	3	0.028	0.025	89.29%	0.028
S13	7	37	3		0.015		0.016
S13	7	38	3	0.057	0.052	91.23%	0.057
S13	7	41	3		0.006		0.007
S13	7	42	3		0.007		0.008
S13	7	43	3		0.028		0.033
S13	7	44	3		0.031		0.036
S13	7	45	3	0.024	0.021	87.50%	0.024
S13	7	46	3	0.043	0.047	109.30%	0.043
S13	7	47	3		0.014		0.015
S13	7	48	3	0.026	0.027	103.85%	0.026
S13	7	49	3		0.074		0.095
S13	7	50	3		0.069		0.089
S13	7	51	3		0.032		0.037
S13	7	52	3	0.026	0.023	88.46%	0.026
S13	7	53	3		0.027		0.032
S13	7	54	3		0.068		0.087
S13	7	55	3		0.030		0.035
S13	7	56	3	0.013	0.010	76.92%	0.013
S13	7	57	3		0.048		0.056
S13	7	58	3		0.011		0.012
S13	7	61	2	0.011	0.010	90.91%	0.011
S13	7	62	3		0.001		0.001
S13	7	63	3		0.004		0.004
S13	7	64	3		0.008		0.009
S13	7	65	3		0.035		0.041

S-13-7 ✓O.K. 3-12-90

S13	7	66	3		0.045		0.053
S13	7	67	3		0.038		0.044
S13	7	68	3	0.029	0.030	103.45%	0.029
S13	7	69	3		0.044		0.051
S13	7	70	3		0.097		0.128
S13	7	71	3		0.064		0.082
S13	7	72	3		0.084		0.111
S13	7	73	3		0.087		0.115
S13	7	74	3		0.063		0.081
S13	7	75	3	0.023	0.022	95.65%	0.023
S13	7	76	3		0.011		0.012
S13	7	77	3	0.083	0.090	108.43%	0.083
S13	7	78	3	0.023	0.019	82.61%	0.023
S13	7	81	3	0.050	0.043	86.00%	0.050
S13	7	82	3		0.009		0.010
S13	7	83	3	0.034	0.035	102.94%	0.034
S13	7	84	3		0.012		0.013
S13	7	85	3		0.038		0.044
S13	7	86	3		0.043		0.050
S13	7	87	3		0.073		0.094
S13	7	88	3		0.033		0.039
S13	7	89	3		0.052		0.067
S13	7	90	3		0.056		0.072
S13	7	91	3		0.072		0.092
S13	7	92	3		0.083		0.110
S13	7	93	3	0.024	0.027	112.50%	0.024
S13	7	94	3		0.065		0.083
S13	7	95	3		0.135		0.179
S13	7	96	3		0.063		0.081
S13	7	97	3	0.016	0.013	81.25%	0.016
S13	7	98	3	0.027	0.028	103.70%	0.027
S13	7	101	3		0.047		0.055
S13	7	102	3	0.020	0.018	90.00%	0.020
S13	7	103	3		0.018		0.020
S13	7	104	3	0.027	0.028	103.70%	0.027
S13	7	105	3		0.012		0.013
S13	7	106	3		0.035		0.041
S13	7	107	3		0.035		0.041
S13	7	108	3		0.041		0.048
S13	7	109	3		0.080		0.106
S13	7	110	3	0.018	0.019	105.56%	0.018
S13	7	111	3		0.067		0.086
S13	7	112	3		0.045		0.053
S13	7	113	3		0.038		0.044
S13	7	114	3	0.023	0.022	95.65%	0.023
S13	7	115	3		0.070		0.090
S13	7	116	2	0.017	0.016	94.12%	0.017
S13	7	117	3		0.059		0.076
S13	7	118	3		0.037		0.043
S13	7	121	3		0.027		0.032
S13	7	122	3		0.019		0.022
S13	7	123	3		0.036		0.042
S13	7	124	3	0.018	0.017	94.44%	0.018
S13	7	125	3		0.011		0.012
S13	7	126	3		0.049		0.063
S13	7	127	3		0.046		0.054

OK 12-20-90

S-13-7
183-(2)=(3)
184-(2)=(3)
196-(2)-(3)
351-(3)-2

			3	0.095	0.094	98.95%	0.095
			3	0.038	0.037	97.37%	0.038
			3		0.032		0.037
			3		0.094		0.124
			3		0.021		0.024
			3		0.022		0.025
			3	0.020	0.020	100.00%	0.020
			3		0.014		0.015
			3		0.099		0.131
			2	0.020	0.021	105.00%	0.020
			2	0.030	0.028	93.33%	0.030
			3	0.018	0.019	105.56%	0.018
			3		0.015		0.016
			3	0.301	0.250	83.06%	0.301
S13	7	144	3		0.026		0.030
S13	7	145	3		0.014		0.015
S13	7	146	3		0.008		0.009
S13	7	147	3		0.035		0.041
S13	7	148	3	0.050	0.054	108.00%	0.050
S13	7	149	3		0.036		0.042
S13	7	150	3		0.016		0.018
S13	7	151	3		0.027		0.032
S13	7	152	3		0.035		0.041
S13	7	153	3		0.018		0.020
S13	7	154	3		0.029		0.034
S13	7	155	3	0.035	0.034	97.14%	0.035
S13	7	156	2	0.014	0.016	114.29%	0.014
S13	7	157	2	0.015	0.014	93.33%	0.015
S13	7	158	2	0.017	0.016	94.12%	0.017
S13	7	161	3		0.076		0.101
S13	7	162	3	0.249	0.179	71.89%	0.249
S13	7	163	3		0.041		0.048
S13	7	164	3		0.031		0.036
S13	7	165	3		0.034		0.040
S13	7	166	3	0.012	0.012	100.00%	0.012
S13	7	167	3		0.025		0.028
S13	7	168	3		0.061		0.078
S13	7	169	3		0.037		0.043
S13	7	170	3		0.020		0.023
S13	7	171	3		0.048		0.056
S13	7	172	3		0.010		0.011
S13	7	173	3	0.020	0.018	90.00%	0.020
S13	7	174	3		0.025		0.028
S13	7	175	3		0.012		0.013
S13	7	176	3		0.009		0.010
S13	7	177	2	0.021	0.016	76.19%	0.021
S13	7	181	3		0.080		0.106
S13	7	182	3		0.125		0.165
S13	7	183	2 3	0.067	0.062	92.54%	0.067
S13	7	184	2 3	0.035	0.037	105.71%	0.035
S13	7	185	3	0.024	0.022	91.67%	0.024
S13	7	186	3		0.012		0.013
S13	7	187	3		0.067		0.086
S13	7	188	3	0.020	0.020	100.00%	0.020
S13	7	189	3	0.136	0.075	55.15%	0.136
S13	7	190	3		0.010		0.011

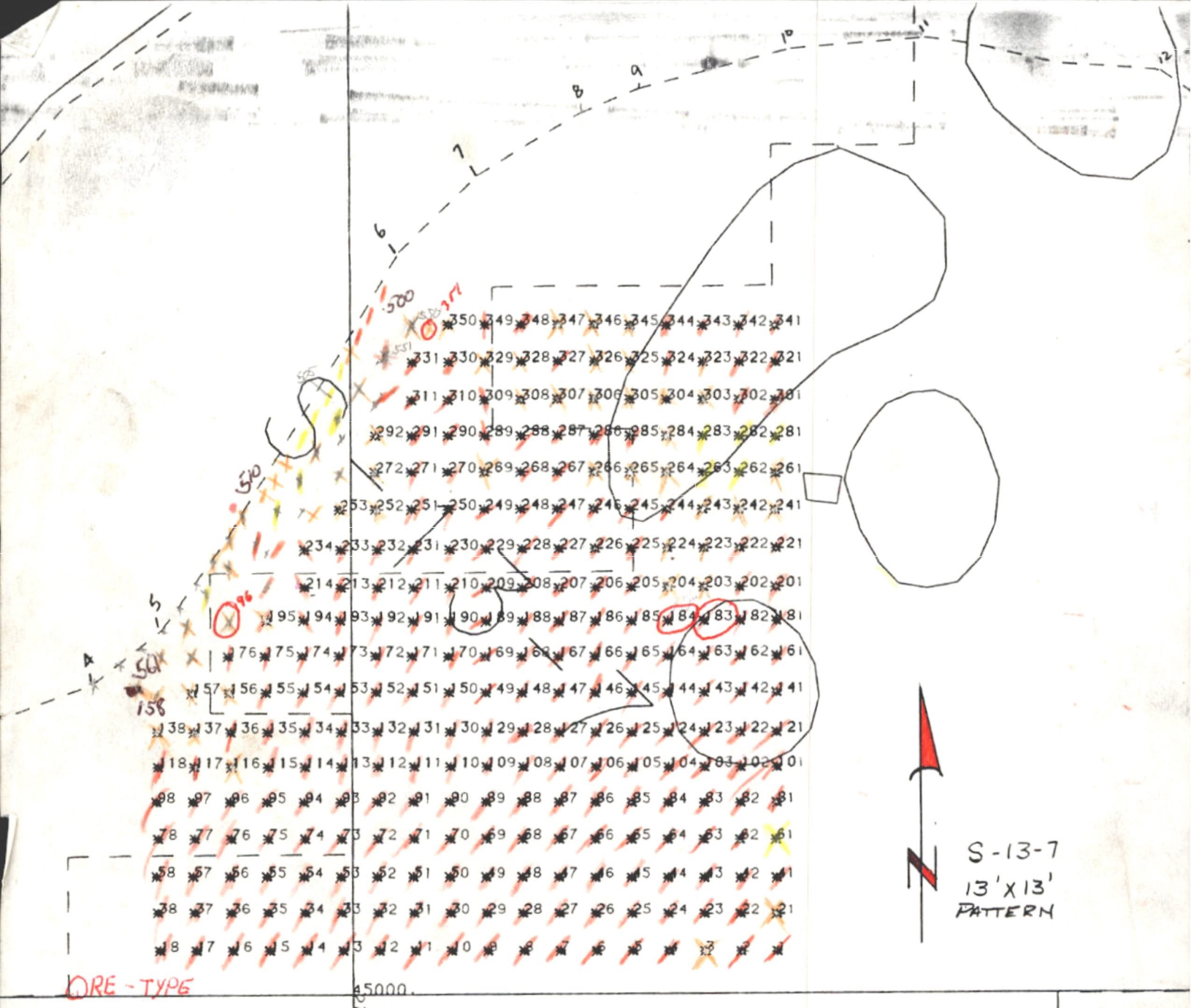
OK 12-20-90

S13	7	128	3	0.095	0.094	98.95%	0.095
S13	7	129	3	0.038	0.037	97.37%	0.038
S13	7	130	3		0.032		0.037
S13	7	131	3		0.094		0.124
S13	7	132	3		0.021		0.024
S13	7	133	3		0.022		0.025
S13	7	134	3	0.020	0.020	100.00%	0.020
S13	7	135	3		0.014		0.015
S13	7	136	3		0.099		0.131
S13	7	137	2	0.020	0.021	105.00%	0.020
S13	7	138	2	0.030	0.028	93.33%	0.030
S13	7	141	3	0.018	0.019	105.56%	0.018
S13	7	142	3		0.015		0.016
S13	7	143	3	0.301	0.250	83.06%	0.301
S13	7	144	3		0.026		0.030
S13	7	145	3		0.014		0.015
S13	7	146	3		0.008		0.009
S13	7	147	3		0.035		0.041
S13	7	148	3	0.050	0.054	108.00%	0.050
S13	7	149	3		0.036		0.042
S13	7	150	3		0.016		0.018
S13	7	151	3		0.027		0.032
S13	7	152	3		0.035		0.041
S13	7	153	3		0.018		0.020
S13	7	154	3		0.029		0.034
S13	7	155	3	0.035	0.034	97.14%	0.035
S13	7	156	2	0.014	0.016	114.29%	0.014
S13	7	157	2	0.015	0.014	93.33%	0.015
S13	7	158	2	0.017	0.016	94.12%	0.017
S13	7	161	3		0.076		0.101
S13	7	162	3	0.249	0.179	71.89%	0.249
S13	7	163	3		0.041		0.048
S13	7	164	3		0.031		0.036
S13	7	165	3		0.034		0.040
S13	7	166	3	0.012	0.012	100.00%	0.012
S13	7	167	3		0.025		0.028
S13	7	168	3		0.061		0.078
S13	7	169	3		0.037		0.043
S13	7	170	3		0.020		0.023
S13	7	171	3		0.048		0.056
S13	7	172	3		0.010		0.011
S13	7	173	3	0.020	0.018	90.00%	0.020
S13	7	174	3		0.025		0.028
S13	7	175	3		0.012		0.013
S13	7	176	3		0.009		0.010
S13	7	177	2	0.021	0.016	76.19%	0.021
S13	7	181	3		0.080		0.106
S13	7	182	3		0.125		0.165
S13	7	183	2 3	0.067	0.062	92.54%	0.067
S13	7	184	2 3	0.035	0.037	105.71%	0.035
S13	7	185	3	0.024	0.022	91.67%	0.024
S13	7	186	3		0.012		0.013
S13	7	187	3		0.067		0.086
S13	7	188	3	0.020	0.020	100.00%	0.020
S13	7	189	3	0.136	0.075	55.15%	0.136
S13	7	190	3		0.010		0.011

S13	7	191	3		0.007		0.008
S13	7	192	3	0.021	0.020	95.24%	0.021
S13	7	193	3		0.036		0.042
S13	7	194	3		0.005		0.005
S13	7	195	3	0.009	0.006	66.67%	0.009
S13	7	196	3		0.002		0.002
S13	7	201	3		0.055		0.071
S13	7	202	3		0.046		0.054
S13	7	203	2	0.189	0.143	75.66%	0.189
S13	7	204	2	0.016	0.014	87.50%	0.016
S13	7	205	3	0.060	0.020	33.33%	0.060
S13	7	206	3		0.075		0.096
S13	7	207	3		0.044		0.051
S13	7	208	3		0.048		0.056
S13	7	209	3	0.010	0.009	90.00%	0.010
S13	7	210	3		0.006		0.007
S13	7	211	3		0.008		0.009
S13	7	212	3		0.012		0.013
S13	7	213	3		0.009		0.010
S13	7	214	3		0.010		0.011
S13	7	215	3		0.002		0.002
S13	7	221	3		0.067		0.086
S13	7	222	3	0.113	0.090	79.65%	0.113
S13	7	223	2	0.058	0.046	79.31%	0.058
S13	7	224	2	0.009	0.011	122.22%	0.009
S13	7	225	3		0.017		0.019
S13	7	226	3	0.024	0.022	91.67%	0.024
S13	7	227	3		0.038		0.044
S13	7	228	3		0.008		0.009
S13	7	229	3		0.006		0.007
S13	7	230	3		0.007		0.008
S13	7	231	3		0.012		0.013
S13	7	232	3		0.005		0.005
S13	7	233	3	0.005	0.003	60.00%	0.005
S13	7	234	3		0.008		0.009
S13	7	235	3		0.001		0.001
S13	7	241	2	0.184	0.097	52.72%	0.184
S13	7	242	2	0.144	0.120	83.33%	0.144
S13	7	243	2	0.052	0.046	88.46%	0.052
S13	7	244	3		0.017		0.019
S13	7	245	3		0.016		0.018
S13	7	246	3		0.014		0.015
S13	7	247	3		0.006		0.007
S13	7	248	3		0.005		0.005
S13	7	249	3		0.012		0.013
S13	7	250	3		0.004		0.004
S13	7	251	3		0.002		0.002
S13	7	252	2	0.004	0.001	25.00%	0.004
S13	7	253	2		0.001		0.001
S13	7	254	2		0.002		0.002
S13	7	261	2	0.227	0.034	14.98%	0.227
S13	7	262	1	0.124	0.076	61.29%	0.124
S13	7	263	1	0.023	0.012	52.17%	0.023
S13	7	264	2	0.014	0.010	71.43%	0.014
S13	7	265	2	0.010	0.009	90.00%	0.010
S13	7	266	2	0.021	0.020	95.24%	0.021

S13	7	267	3		0.010		0.011
S13	7	268	3		0.007		0.008
S13	7	269	2	0.004	0.003	75.00%	0.004
S13	7	270	3		0.002		0.002
S13	7	271	3		0.005		0.005
S13	7	272	2	0.005	0.002	40.00%	0.005
S13	7	273	2		0.001		0.001
S13	7	281	1	0.296	0.103	34.80%	0.296
S13	7	282	1	0.140	0.091	65.00%	0.140
S13	7	283	1	0.022	0.015	68.18%	0.022
S13	7	284	2	0.006	0.007	116.67%	0.006
S13	7	285	3		0.005		0.005
S13	7	286	3		0.011		0.012
S13	7	287	3		0.007		0.008
S13	7	288	3		0.005		0.005
S13	7	289	3		0.012		0.013
S13	7	290	3		0.003		0.003
S13	7	291	3		0.007		0.008
S13	7	292	2	0.005	0.006	120.00%	0.005
S13	7	301	3	0.253	0.195	77.08%	0.253
S13	7	302	3		0.057		0.073
S13	7	303	2	0.026	0.019	73.08%	0.026
S13	7	304	2	0.019	0.013	68.42%	0.019
S13	7	305	2	0.018	0.015	83.33%	0.018
S13	7	306	2	0.013	0.009	69.23%	0.013
S13	7	307	2		0.006		0.007
S13	7	308	2	0.006	0.003	50.00%	0.006
S13	7	309	3		0.011		0.012
S13	7	310	3		0.010		0.011
S13	7	311	3		0.010		0.011
S13	7	312	3		0.010		0.011
S13	7	321	3		0.093		0.123
S13	7	322	3	0.038	0.037	97.37%	0.038
S13	7	323	2	0.024	0.024	100.00%	0.024
S13	7	324	3	0.023	0.020	86.96%	0.023
S13	7	325	2	0.037	0.007	18.92%	0.037
S13	7	326	2	0.040	0.015	37.50%	0.040
S13	7	327	3		0.012		0.013
S13	7	328	2	0.013	0.006	46.15%	0.013
S13	7	329	2		0.002		0.002
S13	7	330	3	0.006	0.004	66.67%	0.006
S13	7	331	3	0.055	0.048	87.27%	0.055
S13	7	341	3		0.032		0.037
S13	7	342	3		0.027		0.032
S13	7	343	3		0.013		0.014
S13	7	344	3		0.017		0.019
S13	7	345	2	0.020	0.010	50.00%	0.020
S13	7	346	2	0.010	0.005	50.00%	0.010
S13	7	347	2		0.003		0.003
S13	7	348	3		0.005		0.005
S13	7	349	3		0.004		0.004
S13	7	350	2	0.004	0.002	50.00%	0.004
S13	7	351	3 2		0.004		0.005
S13	7	500	3		0.004		0.004
S13	7	501	3		0.007		0.008
S13	7	502	3		0.012		0.013

S13	7	503	2		0.005		0.005
S13	7	504	1		0.002		0.002
S13	7	505	1	0.004	0.001	25.00%	0.004
S13	7	506	1		0.000		0.000
S13	7	507	1	0.003	0.001	33.33%	0.003
S13	7	508	2		0.002		0.002
S13	7	509	2	0.004	0.002	50.00%	0.004
S13	7	510	2		0.000		0.000
S13	7	511	2		0.005		0.005
S13	7	512	2		0.002		0.002
S13	7	513	2		0.002		0.002
S13	7	550	2	0.005	0.005	100.00%	0.005
S13	7	551	3		0.004		0.004
S13	7	552	2	0.014	0.012	85.71%	0.014
S13	7	553	1		0.008		0.009
S13	7	554	2	0.003	0.002	66.67%	0.003
S13	7	555	1		0.001		0.001
S13	7	556	1	0.004	0.001	25.00%	0.004
S13	7	557	3		0.000		0.000
S13	7	558	2		0.002		0.002
S13	7	559	1	0.003	0.000	0.00%	0.003
S13	7	560	2		0.001		0.001
S13	7	561	2	0.005	0.006	120.00%	0.005
		MEAN		0.043	0.029	80.59%	0.037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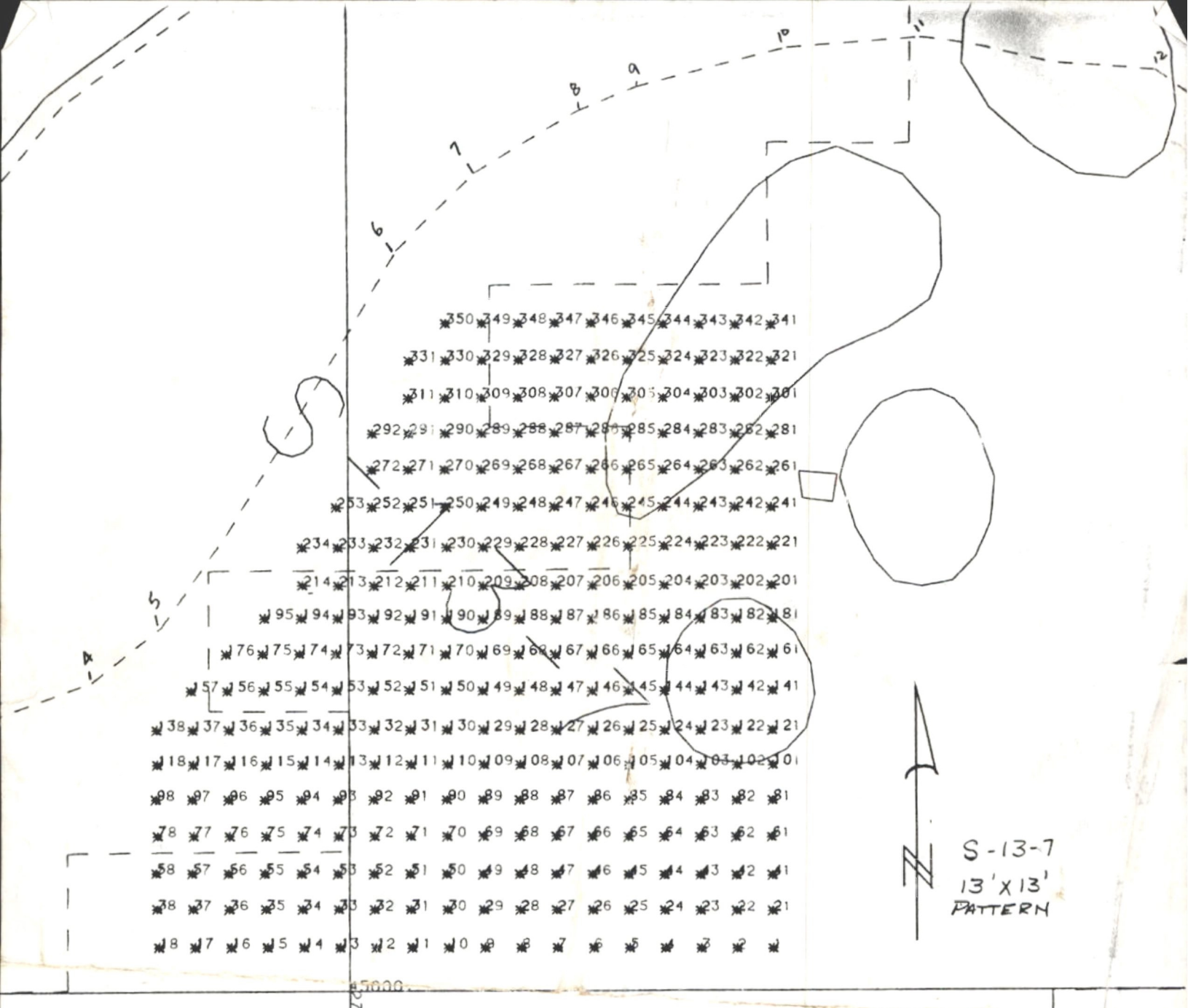
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