S-12-11

1935904 - R8 SEMS

Pit-Bench-Pattern #
S-12-11

Submittal Date
12/19/90 3:30p

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 12/21/90

NAME: KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	2	.009	.010	25.	Standard ✓		.014
2.	3		.016	26.	505	.019	.012
3.	4		.018	27.	506		.007
4.	5	.043	.041	28.	507		.008
5.	6		.024	29.	508		.017
6.	7		.027	30.	509		.029
7.	8		.003	31.	510		.043
8.	Standard ✓		.015	32.	511		.027
9.	9	.004	.003	33.	[redacted]		
10.	10		.002	34.	[redacted]		
11.	11	.014	.014	35.	512		
12.	12	.016	.020	36.	513		.007
13.	13		.011	37.	514	.008	.00[illegible]
14.	14		.003	38.	515		.004
15.	15		.001	39.	516		.004
16.	[redacted]			40.	517	.036	.019
17.	[redacted]			41.	518		.009
18.	16-1	.012	.003	42.	Standard ✓		.015
19.	16-2		.003	43.	519		.00[illegible]
20.	17		.003	44.	520		.013
21.	18		.002	45.	521		.00[illegible]
22.	502		.012	46.	522		.003
23.	503		.017	47.	523		.003
24.	504		.011	48.	524		.003
					525		.004
					526	.009	.003
					527		nil

✓ 7.03

LD

Pit-Bench-Pattern #
S-12-11

Submittal Date
12-19-90 9:15 am

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 12-20-90

NAME: VD

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	21	.019	.008	25.	Standard ✓		.015
2.	22		.013	26.	43		.016
3.	23		.043	27.	44		.024
4.	24		.021	28.	45		.021
5.	25-1	.024	.020 .019	29.	46		.028
6.	25-2		.017	30.	47		.017
7.	26		.012	31.	48	.017	.021
8.	Standard ✓		.015	32.	49		.007
9.	27		.036	33.			
10.	28	.014	.010	34.			
11.	29		.003	35.	50	.012	.008
12.	30	.009	.005	36.	51		.046
13.	31		.020	37.	52		.050
14.	32		.017	38.	53	.082	.089
15.	33		.021	39.	54	.015	.012
16.				40.	55		.005
17.				41.	56		.012
18.	34		.009	42.	Standard ✓		.015
19.	35		.001	43.	57		.002
20.	36		.005	44.	✓ prep		.033
21.	37		.002	45.	58		.011
22.	38		.002	46.			
23.	41		.010	47.			
24.	42	.025	.027	48.			

LD

Pit-Bench-Pattern #
S-12-11
Submittal Date
12/18/00 9:22A

BLAST HOLE

Hot NaCN Shake and FIRE DETERMINATIONS

DATE: 12/19/00
NAME: KW, LLD

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	✓7		.031	25.	Standard ✓		.015
2.	62	.032	.037	26.	86	.024	.021
3.	63		.014	27.	87-1	.014	.015
4.	64		.017	28.	87-2		.016
5.	65		.013	29.	88		.026
6.	66		.019	30.	89		.011
7.	67		.018	31.	90	.040	.043
8.	Standard ✓		.015	32.	91		.019
9.	68		.018	33.			
10.	69	.036	.034	34.			
11.	70		.027	35.	92		.027
12.	71		.044	36.	93	.023	.020
13.	72		.092	37.	94		.007
14.	73	.162	.057	38.	95	.008	.012
15.	74		.033	39.	96		.009
16.				40.	97		.004
17.				41.	98		.004
18.	75		.025	42.	Standard ✓		.015
19.	76		.005	43.	103		.011
20.	77		.003	44.	104		.016
21.	78		.008	45.	105	.039	.040
22.	83	.023	.020	46.	106		.018
23.	84		.024	47.	107	.018	.021
24.	85		.013	48.		Std ✓	.015

LLD

Pit-Bench-Pattern #
S-12-11

Submittal Date
12/18/90 9:22A Cont

BLAST HOLE

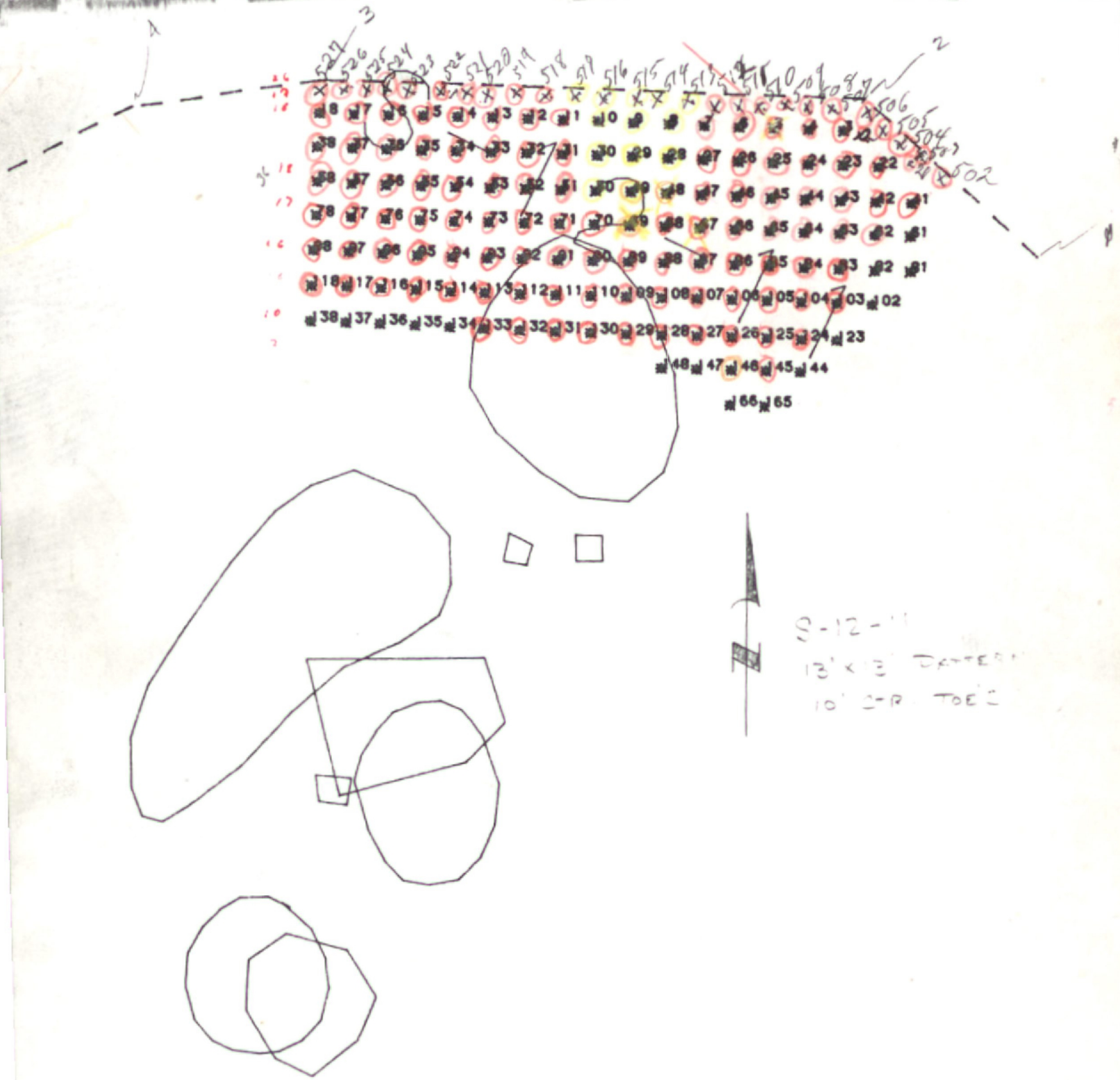
Hot NaCN Shake
and
FIRE DETERMINATIONS

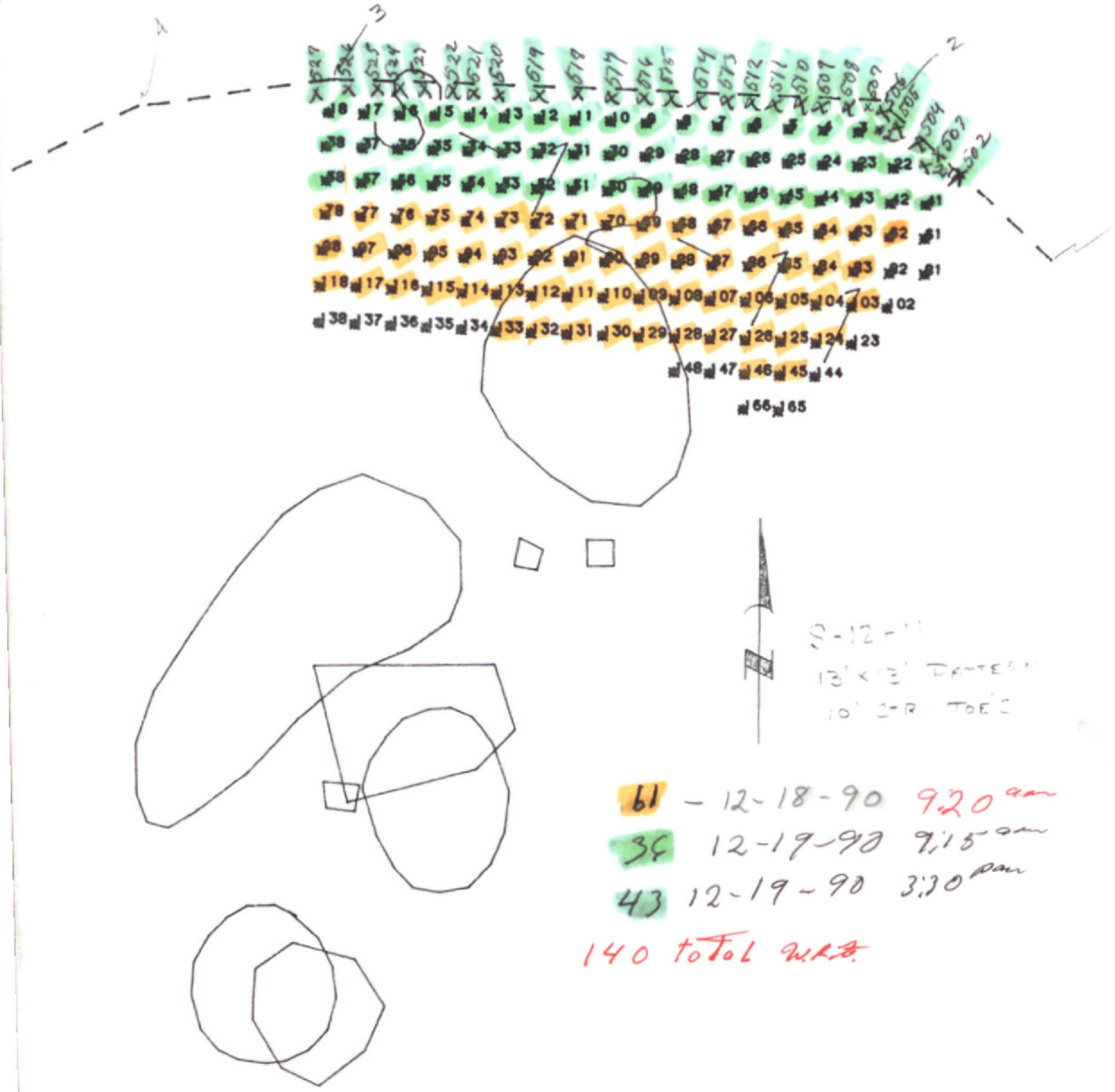
DATE: 12/19/90

NAME: KW, VD

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	108	.074	.076	25.	Standard ✓		.015
2.	109	.019	.021	26.	133		.019
3.	110	.009	.007	27.	145		.021
4.	111		.018	28.	146	.029	.015
5.	112		.024	29.			
6.	113		.047	30.			
7.	114		.006	31.			
8.	Standard ✓		.015	32.			
9.	115		.005	33.	[redacted]		
10.	116	.016	.015	34.			
11.	117		.006	35.			
12.	118		.003	36.			
13.	124		.017	37.			
14.	125	.028	.030	38.			
15.	126		.032	39.			
16.	[redacted]			40.			
17.				41.			
18.	127		.040	42.	Standard ✓		
19.	128		.030	43.			
20.	✓7		.033	44.			
21.	129		.026	45.			
22.	130		.018	46.			
23.	131	.026	.023	47.			
24.	132		.024	48.			

LLD


S-12-11
13' x 13' PATTERN
10' STR. TOE'S



61 - 12-18-90 9:20 am

36 12-19-90 9:15 am

43 12-19-90 3:30 pm

140 total WRS.

BROHM MINING CORPORATION
BLAST HOLE ORE TYPE

PATTERN S-12-11

DATE

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF	MIX	OXIDE
2			X	44			X	86			X	132			X
3			X	45			X	87			X	133			X
4			X	46			X	88			X				
5			X	47			X	89			X	145			X
6			X	48		X		90			X	146		X	
7			X	49	X			91			X				
8	X			50	X			92			X	502			X
9	X			51			X	93			X	503			X
10	X			52			X	94			X	504			X
11			X	53			X	95			X	505			X
12			X	54			X	96			X	506			X
13			X	55			X	97			X	507			X
14			X	56			X	98			X	508			X
15			X	57			X					509			X
16			X	58			X	102			X	510			X
17			X					103			X	511			X
18			X	~~61~~				104			X	512			X
				62			X	105			X	513	X		
21			X	63			X	106			X	514	X		
22			X	64			X	107			X	515	X		
23			X	65			X	108			X	516	X		
24			X	66			X	109			X	517	X		
25			X	67			X	110			X	518			X
26			X	68			X	111			X	519			X
27			X	69		X		112			X	520			X
28	X			70			X	113			X	521			X
29	X			71			X	114			X	522			X
30	X			72			X	115			X	523			X
31			X	73			X	116			X	524			X
32			X	74			X	117			X	525			X
33			X	75			X	118			X	526			X
34			X	76			X					527			X
35			X	77			X	124			X				
36			X	78			X	125			X				
37			X					126			X				
38			X	~~81~~				127			X				
				~~82~~				128			X				
41			X	83			X	129			X				
42			X	84			X	130			X				
43			X	85			X	131			X				

CHECKED OK
1/7/91

BENCH NO	SHOT NO	BLASTHOLE NO	ORE TYPE	FIRE AU	AA AU	AA/FIRE	AA/RAT
S12	11	2	3	0.009	0.010	111.11%	0.009
S12	11	3	3		0.016		0.017
S12	11	4	3		0.018		0.019
S12	11	5	3	0.043	0.041	95.35%	0.043
S12	11	6	3		0.024		0.026
S12	11	7	3		0.027		0.029
S12	11	8	1		0.003		0.003
S12	11	9	1	0.004	0.003	75.00%	0.004
S12	11	10	1		0.002		0.002
S12	11	11	3	0.014	0.014	100.00%	0.014
S12	11	12	3	0.016	0.020	125.00%	0.016
S12	11	13	3		0.011		0.012
S12	11	14	3		0.003		0.003
S12	11	15	3		0.001		0.001
S12	11	16	3	0.012	0.003	25.00%	0.012
S12	11	17	3		0.003		0.003
S12	11	18	3		0.002		0.002
S12	11	21	3	0.019	0.008	42.11%	0.019
S12	11	22	3		0.013		0.014
S12	11	23	3		0.043		0.048
S12	11	24	3		0.021		0.022
S12	11	25	3	0.024	0.019	79.17%	0.024
S12	11	26	3		0.012		0.013
S12	11	27	3		0.036		0.040
S12	11	28	1	0.014	0.010	71.43%	0.014
S12	11	29	1		0.003		0.003
S12	11	30	1	0.009	0.005	55.56%	0.009
S12	11	31	3		0.020		0.021
S12	11	32	3		0.017		0.018
S12	11	33	3		0.021		0.022
S12	11	34	3		0.009		0.010
S12	11	35	3		0.001		0.001
S12	11	36	3		0.005		0.005
S12	11	37	3		0.002		0.002
S12	11	38	3		0.002		0.002
S12	11	41	3		0.010		0.011
S12	11	42	3	0.025	0.027	108.00%	0.025
S12	11	43	3		0.016		0.017
S12	11	44	3		0.024		0.026
S12	11	45	3		0.021		0.022
S12	11	46	3		0.028		0.030
S12	11	47	3		0.017		0.018
S12	11	48	2	0.017	0.021	123.53%	0.017
S12	11	49	1		0.007		0.008
S12	11	50	1	0.012	0.008	66.67%	0.012
S12	11	51	3		0.046		0.052
S12	11	52	3		0.050		0.056
S12	11	53	3	0.082	0.089	108.54%	0.082
S12	11	54	3	0.015	0.012	80.00%	0.015
S12	11	55	3		0.005		0.005
S12	11	56	3		0.012		0.013
S12	11	57	3		0.002		0.002
S12	11	58	3		0.011		0.012
S12	11	62	3	0.032	0.037	115.63%	0.032

S12	11	63	3		0.014		0.015
S12	11	64	3		0.017		0.018
S12	11	65	3		0.013		0.014
S12	11	66	3		0.019		0.020
S12	11	67	3		0.018		0.019
S12	11	68	3		0.018		0.019
S12	11	69	2	0.036	0.034	94.44%	0.036
S12	11	70	3		0.027		0.029
S12	11	71	3		0.044		0.049
S12	11	72	3		0.092		0.130
S12	11	73	3	0.162	0.057	35.19%	0.162
S12	11	74	3		0.033		0.037
S12	11	75	3		0.025		0.027
S12	11	76	3		0.005		0.005
S12	11	77	3		0.003		0.003
S12	11	78	3		0.008		0.009
S12	11	83	3	0.023	0.020	86.96%	0.023
S12	11	84	3		0.024		0.026
S12	11	85	3		0.013		0.014
S12	11	86	3	0.024	0.021	87.50%	0.024
S12	11	87	3	0.014	0.016	114.29%	0.014
S12	11	88	3		0.026		0.028
S12	11	89	3		0.011		0.012
S12	11	90	3	0.040	0.043	107.50%	0.040
S12	11	91	3		0.019		0.020
S12	11	92	3		0.027		0.029
S12	11	93	3	0.023	0.020	86.96%	0.023
S12	11	94	3		0.007		0.008
S12	11	95	3	0.008	0.012	150.00%	0.008
S12	11	96	3		0.009		0.010
S12	11	97	3		0.004		0.004
S12	11	98	3		0.004		0.004
S12	11	103	3		0.011		0.012
S12	11	104	3		0.016		0.017
S12	11	105	3	0.039	0.040	102.56%	0.039
S12	11	106	3		0.018		0.019
S12	11	107	3	0.018	0.021	116.67%	0.018
S12	11	108	3	0.074	0.076	102.70%	0.074
S12	11	109	3	0.019	0.021	110.53%	0.019
S12	11	110	3	0.009	0.007	77.78%	0.009
S12	11	111	3		0.018		0.019
S12	11	112	3		0.024		0.026
S12	11	113	3		0.047		0.053
S12	11	114	3		0.006		0.007
S12	11	115	3		0.005		0.005
S12	11	116	3	0.016	0.015	93.75%	0.016
S12	11	117	3		0.006		0.007
S12	11	118	3		0.003		0.003
S12	11	124	3		0.017		0.018
S12	11	125	3	0.028	0.030	107.14%	0.028
S12	11	126	3		0.032		0.036
S12	11	127	3		0.040		0.045
S12	11	128	3		0.030		0.034
S12	11	129	3		0.026		0.028
S12	11	130	3		0.018		0.019
S12	11	131	3	0.026	0.023	88.46%	0.026

S12	11	132	3		0.024		0.026
S12	11	133	3		0.019		0.020
S12	11	145	3		0.021		0.022
S12	11	146	2	0.029	0.015	51.72%	0.029
S12	11	502	3		0.012		0.013
S12	11	503	3		0.017		0.018
S12	11	504	3		0.011		0.012
S12	11	505	3	0.019	0.012	63.16%	0.019
S12	11	506	3		0.007		0.008
S12	11	507	3		0.008		0.009
S12	11	508	3		0.017		0.018
S12	11	509	3		0.029		0.031
S12	11	510	3		0.043		0.048
S12	11	511	3		0.027		0.029
S12	11	512	3		0.025		0.027
S12	11	513	1		0.007		0.008
S12	11	514	1	0.008	0.003	37.50%	0.008
S12	11	515	1		0.004		0.004
S12	11	516	1		0.004		0.004
S12	11	517	1	0.036	0.019	52.78%	0.036
S12	11	518	3		0.009		0.010
S12	11	519	3		0.009		0.010
S12	11	520	3		0.013		0.014
S12	11	521	3		0.004		0.004
S12	11	522	3		0.003		0.003
S12	11	523	3		0.003		0.003
S12	11	524	3		0.003		0.003
S12	11	525	3		0.004		0.004
S12	11	526	3	0.009	0.003	33.33%	0.009
S12	11	527	3		0.000		0.000
		MEAN		0.027	0.018	86.03%	0.020