S-17-9

1932588 - R8 SEMS

CHECKED OK
4.3.91

BENCH no	shot no	bh no	fire au	aa au	fire equiv (aa/ratio)	ore type	ratio	actual ratio (aa/fire)
		0						
0	0	0					95.0%	
S17	9	1		0.026	0.027	3	95.0%	
S17	9	21		0.025	0.026	3	95.0%	
S17	9	22		0.018	0.019	3	95.0%	
S17	9	41		0.007	0.007	3	95.0%	
S17	9	42		0.014	0.015	3	95.0%	
S17	9	43		0.012	0.014	2	84.0%	
S17	9	44		0.017	0.018	3	95.0%	
S17	9	61	0.010	0.011	0.010	2	100.0%	110.0%
S17	9	62		0.007	0.008	2	84.0%	
S17	9	63		0.016	0.017	3	95.0%	
S17	9	64		0.020	0.021	3	95.0%	
S17	9	65		0.018	0.019	3	95.0%	
S17	9	66		0.014	0.015	3	95.0%	
S17	9	81	0.026	0.018	0.026	3	100.0%	69.2%
S17	9	82		0.015	0.016	3	95.0%	
S17	9	83		0.013	0.014	3	95.0%	
S17	9	84		0.010	0.011	3	95.0%	
S17	9	85		0.014	0.015	3	95.0%	
S17	9	86	0.019	0.014	0.019	2	100.0%	73.7%
S17	9	87		0.026	0.027	3	95.0%	
S17	9	88	0.039	0.043	0.039	3	100.0%	110.3%
S17	9	101		0.074	0.078	3	95.0%	
S17	9	102		0.026	0.027	3	95.0%	
S17	9	103		0.054	0.057	3	95.0%	
S17	9	104	0.276	0.213	0.276	3	100.0%	77.2%
S17	9	105	0.137	0.111	0.137	3	100.0%	81.0%
S17	9	106	0.146	0.064	0.146	2	100.0%	43.8%
S17	9	107	0.026	0.020	0.026	2	100.0%	76.9%
S17	9	108	0.032	0.021	0.032	2	100.0%	65.6%
S17	9	109	0.059	0.029	0.059	1	100.0%	49.2%
S17	9	121		0.033	0.035	3	95.0%	
S17	9	122		0.031	0.033	3	95.0%	
S17	9	123		0.019	0.020	3	95.0%	
S17	9	124	0.007	0.005	0.007	3	100.0%	71.4%
S17	9	125		0.014	0.015	3	95.0%	
S17	9	126		0.021	0.022	3	95.0%	
S17	9	127		0.031	0.033	3	95.0%	
S17	9	128	0.039	0.022	0.039	1	100.0%	56.4%
S17	9	129	0.059	0.021	0.059	1	100.0%	35.6%
S17	9	141		0.019	0.020	3	95.0%	
S17	9	142	0.030	0.032	0.030	2	100.0%	106.7%
S17	9	143	0.017	0.017	0.017	3	100.0%	100.0%
S17	9	144		0.016	0.017	3	95.0%	
S17	9	145		0.015	0.016	3	95.0%	
S17	9	146	0.070	0.045	0.070	2	100.0%	64.3%
S17	9	147	0.058	0.034	0.058	2	100.0%	58.6%
S17	9	148	0.091	0.077	0.091	3	100.0%	84.6%
S17	9	149	0.068	0.033	0.068	1	100.0%	48.5%
S17	9	161		0.014	0.015	3	95.0%	
S17	9	162		0.011	0.012	3	95.0%	
S17	9	163		0.006	0.006	3	95.0%	
S17	9	164		0.029	0.031	3	95.0%	

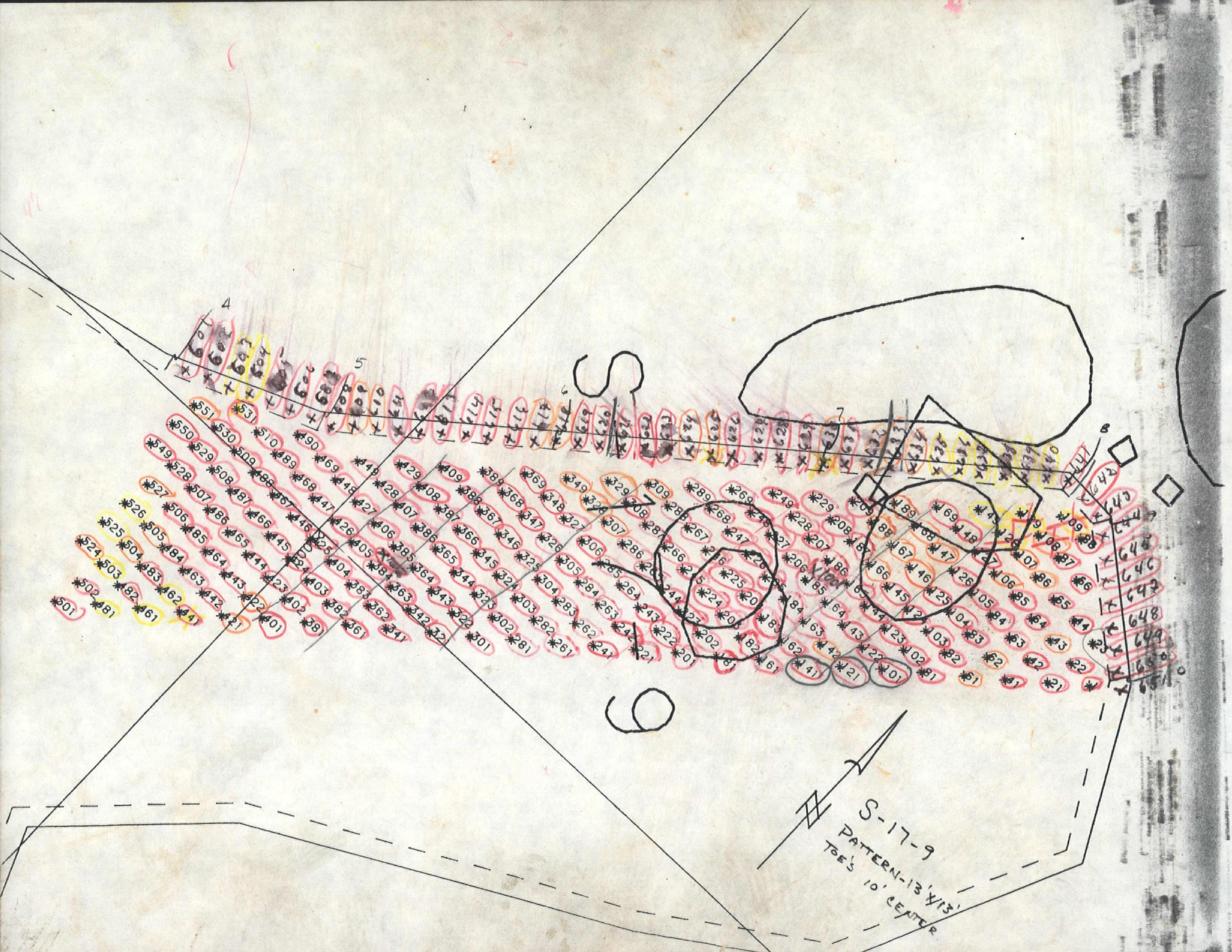
S17	9	165		0.023	0.024	3	95.0%	
S17	9	166	0.015	0.015	0.015	2	100.0%	100.0%
S17	9	167	0.100	0.049	0.100	2	100.0%	49.0%
S17	9	168	0.043	0.028	0.043	2	100.0%	65.1%
S17	9	169	0.402	0.194	0.402	3	100.0%	48.3%
S17	9	181		0.027	0.028	3	95.0%	
S17	9	182	0.045	0.049	0.045	3	100.0%	108.9%
S17	9	183	0.018	0.019	0.018	3	100.0%	105.6%
S17	9	184		0.037	0.039	3	95.0%	
S17	9	185		0.040	0.042	3	95.0%	
S17	9	186		0.037	0.039	3	95.0%	
S17	9	187		0.032	0.034	3	95.0%	
S17	9	188	0.024	0.019	0.024	2	100.0%	79.2%
S17	9	189	0.065	0.022	0.065	2	100.0%	33.8%
S17	9	201		0.011	0.012	3	95.0%	
S17	9	202		0.012	0.013	3	95.0%	
S17	9	203	0.028	0.027	0.028	3	100.0%	96.4%
S17	9	204		0.074	0.078	3	95.0%	
S17	9	205		0.090	0.095	3	95.0%	
S17	9	206	0.332	0.170	0.332	3	100.0%	51.2%
S17	9	207		0.046	0.048	3	95.0%	
S17	9	208		0.056	0.059	3	95.0%	
S17	9	209		0.018	0.019	3	95.0%	
S17	9	221		0.037	0.039	3	95.0%	
S17	9	222		0.068	0.072	3	95.0%	
S17	9	223		0.029	0.031	3	95.0%	
S17	9	224	0.021	0.020	0.021	3	100.0%	95.2%
S17	9	225		0.073	0.077	3	95.0%	
S17	9	226		0.062	0.065	3	95.0%	
S17	9	227		0.033	0.035	3	95.0%	
S17	9	228		0.056	0.059	3	95.0%	
S17	9	229		0.038	0.040	3	95.0%	
S17	9	241		0.026	0.027	3	95.0%	
S17	9	242	0.018	0.020	0.018	3	100.0%	111.1%
S17	9	243		0.035	0.037	3	95.0%	
S17	9	244		0.036	0.038	3	95.0%	
S17	9	245		0.022	0.023	3	95.0%	
S17	9	246		0.030	0.032	3	95.0%	
S17	9	247	0.086	0.089	0.086	3	100.0%	103.5%
S17	9	248		0.045	0.047	3	95.0%	
S17	9	249		0.053	0.056	3	95.0%	
S17	9	261	0.016	0.012	0.016	3	100.0%	75.0%
S17	9	262		0.030	0.032	3	95.0%	
S17	9	263		0.024	0.025	3	95.0%	
S17	9	264		0.013	0.014	3	95.0%	
S17	9	265	0.028	0.031	0.028	3	100.0%	110.7%
S17	9	266		0.012	0.013	3	95.0%	
S17	9	267		0.009	0.009	3	95.0%	
S17	9	268		0.030	0.032	3	95.0%	
S17	9	269		0.027	0.028	3	95.0%	
S17	9	281		0.039	0.041	3	95.0%	
S17	9	282	0.015	0.009	0.015	3	100.0%	60.0%
S17	9	283		0.069	0.073	3	95.0%	
S17	9	284		0.017	0.018	3	95.0%	
S17	9	285		0.017	0.018	3	95.0%	
S17	9	286		0.015	0.016	3	95.0%	

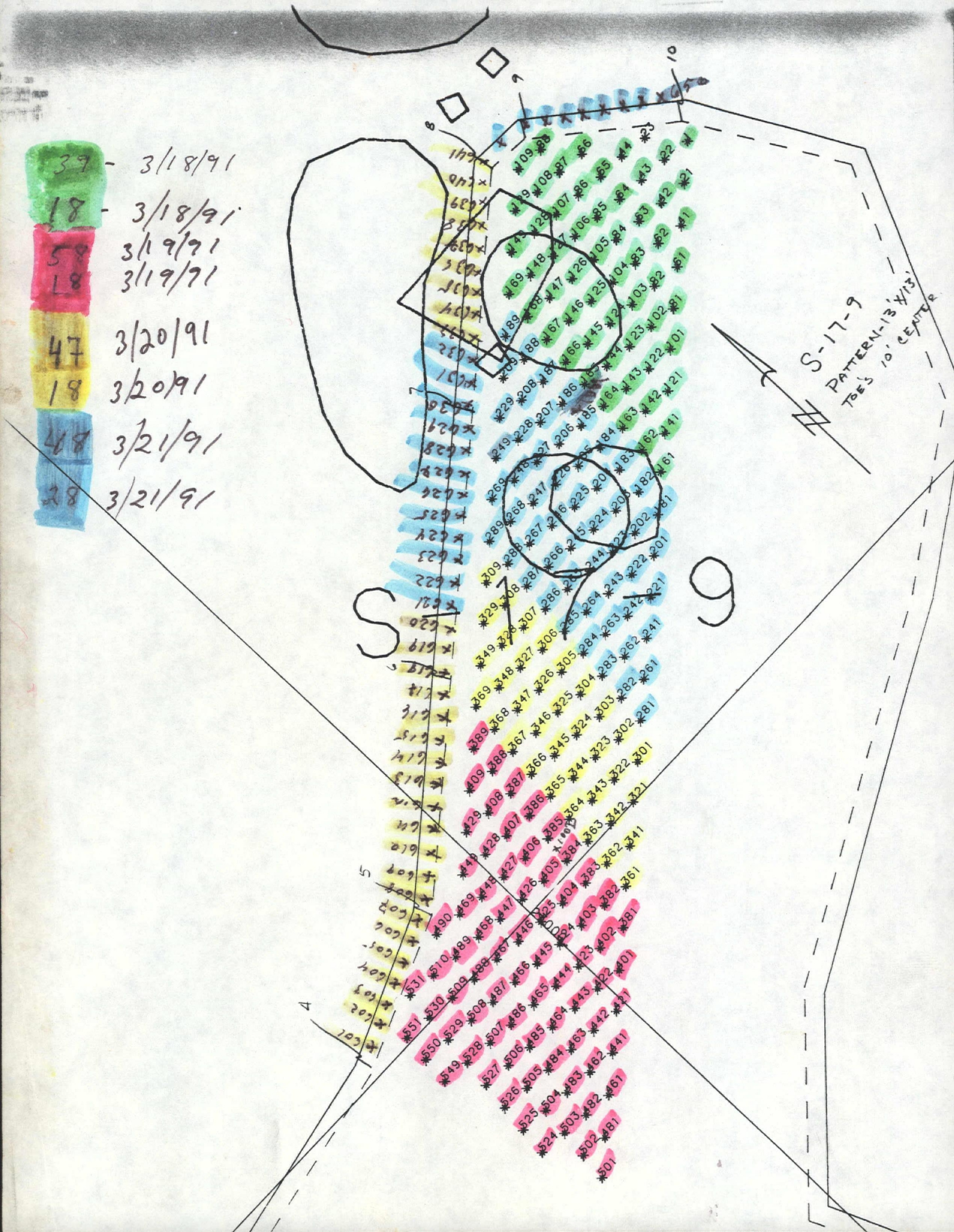
S17	9	287	0.021	0.019	0.021	3	100.0%	90.5%
S17	9	288		0.012	0.013	3	95.0%	
S17	9	289		0.037	0.039	3	95.0%	
S17	9	301		0.041	0.043	3	95.0%	
S17	9	302		0.064	0.067	3	95.0%	
S17	9	303	0.028	0.029	0.028	3	100.0%	103.6%
S17	9	304	0.016	0.016	0.016	3	100.0%	100.0%
S17	9	305		0.014	0.015	3	95.0%	
S17	9	306		0.013	0.014	3	95.0%	
S17	9	307		0.013	0.015	2	84.0%	
S17	9	308	0.017	0.017	0.017	3	100.0%	100.0%
S17	9	309	0.087	0.033	0.087	2	100.0%	37.9%
S17	9	321		0.007	0.007	3	95.0%	
S17	9	322	0.015	0.015	0.015	3	100.0%	100.0%
S17	9	323		0.027	0.028	3	95.0%	
S17	9	324		0.058	0.061	3	95.0%	
S17	9	325		0.024	0.025	3	95.0%	
S17	9	326		0.042	0.044	3	95.0%	
S17	9	327		0.049	0.052	3	95.0%	
S17	9	328		0.013	0.015	2	84.0%	
S17	9	329	0.016	0.017	0.016	2	100.0%	106.3%
S17	9	341	0.034	0.039	0.034	3	100.0%	114.7%
S17	9	342	0.010	0.008	0.010	3	100.0%	80.0%
S17	9	343		0.042	0.044	3	95.0%	
S17	9	344		0.020	0.021	3	95.0%	
S17	9	345		0.026	0.027	3	95.0%	
S17	9	346		0.026	0.027	3	95.0%	
S17	9	347		0.054	0.057	3	95.0%	
S17	9	348		0.067	0.071	3	95.0%	
S17	9	349		0.014	0.017	2	84.0%	
S17	9	361		0.037	0.039	3	95.0%	
S17	9	362	0.039	0.032	0.039	3	100.0%	82.1%
S17	9	363	0.027	0.021	0.027	3	100.0%	77.8%
S17	9	364		0.009	0.009	3	95.0%	
S17	9	365		0.065	0.068	3	95.0%	
S17	9	366		0.032	0.034	3	95.0%	
S17	9	367		0.036	0.038	3	95.0%	
S17	9	368		0.055	0.058	3	95.0%	
S17	9	369	0.129	0.114	0.129	3	100.0%	88.4%
S17	9	381		0.026	0.027	3	95.0%	
S17	9	382		0.009	0.009	3	95.0%	
S17	9	383	0.019	0.026	0.019	3	100.0%	136.8%
S17	9	384		0.040	0.042	3	95.0%	
S17	9	385		0.052	0.055	3	95.0%	
S17	9	386	0.016	0.017	0.016	3	100.0%	106.3%
S17	9	387		0.024	0.025	3	95.0%	
S17	9	388		0.028	0.029	3	95.0%	
S17	9	389		0.049	0.052	3	95.0%	
S17	9	401		0.043	0.045	3	95.0%	
S17	9	402		0.072	0.076	3	95.0%	
S17	9	403		0.032	0.034	3	95.0%	
S17	9	404	0.024	0.019	0.024	3	100.0%	79.2%
S17	9	405		0.033	0.035	3	95.0%	
S17	9	406		0.047	0.049	3	95.0%	
S17	9	407		0.050	0.053	3	95.0%	
S17	9	408		0.026	0.027	3	95.0%	

S17	9	409		0.036	0.038	3	95.0%	
S17	9	421	0.062	0.016	0.062	2	100.0%	25.8%
S17	9	422	0.046	0.040	0.046	2	100.0%	87.0%
S17	9	423		0.016	0.017	3	95.0%	
S17	9	424		0.038	0.040	3	95.0%	
S17	9	425		0.046	0.048	3	95.0%	
S17	9	426		0.032	0.034	3	95.0%	
S17	9	427		0.014	0.015	3	95.0%	
S17	9	428		0.065	0.068	3	95.0%	
S17	9	429		0.047	0.049	3	95.0%	
S17	9	441	0.069	0.059	0.069	3	100.0%	85.5%
S17	9	442		0.012	0.013	3	95.0%	
S17	9	443		0.019	0.020	3	95.0%	
S17	9	444		0.043	0.045	3	95.0%	
S17	9	445		0.027	0.028	3	95.0%	
S17	9	446		0.017	0.018	3	95.0%	
S17	9	447	0.239	0.096	0.239	3	100.0%	40.2%
S17	9	448		0.026	0.027	3	95.0%	
S17	9	449		0.029	0.031	3	95.0%	
S17	9	461		0.007	0.010	1	70.0%	
S17	9	462	0.013	0.014	0.013	1	100.0%	107.7%
S17	9	463		0.029	0.031	3	95.0%	
S17	9	464		0.044	0.046	3	95.0%	
S17	9	465		0.040	0.042	3	95.0%	
S17	9	466		0.045	0.047	3	95.0%	
S17	9	467	0.127	0.122	0.127	3	100.0%	96.1%
S17	9	468		0.053	0.056	3	95.0%	
S17	9	469		0.036	0.038	3	95.0%	
S17	9	481	0.012	0.007	0.012	1	100.0%	58.3%
S17	9	482		0.013	0.014	3	95.0%	
S17	9	483	0.021	0.019	0.021	3	100.0%	90.5%
S17	9	484		0.041	0.043	3	95.0%	
S17	9	485		0.051	0.054	3	95.0%	
S17	9	486		0.036	0.038	3	95.0%	
S17	9	487		0.037	0.039	3	95.0%	
S17	9	488		0.026	0.027	3	95.0%	
S17	9	489		0.057	0.060	3	95.0%	
S17	9	490		0.079	0.083	3	95.0%	
S17	9	501		0.009	0.009	3	95.0%	
S17	9	502	0.018	0.016	0.018	3	100.0%	88.9%
S17	9	503		0.007	0.010	1	70.0%	
S17	9	504	0.029	0.023	0.029	2	100.0%	79.3%
S17	9	505	0.020	0.016	0.020	2	100.0%	80.0%
S17	9	506		0.046	0.048	3	95.0%	
S17	9	507		0.055	0.058	3	95.0%	
S17	9	508		0.072	0.076	3	95.0%	
S17	9	509		0.035	0.037	3	95.0%	
S17	9	510		0.042	0.044	3	95.0%	
S17	9	524		0.006	0.007	2	84.0%	
S17	9	525		0.013	0.019	1	70.0%	
S17	9	526	0.037	0.028	0.037	1	100.0%	75.7%
S17	9	527	0.031	0.017	0.031	2	100.0%	54.8%
S17	9	528		0.079	0.083	3	95.0%	
S17	9	529		0.074	0.078	3	95.0%	
S17	9	530	0.130	0.134	0.130	3	100.0%	103.1%
S17	9	531		0.071	0.075	3	95.0%	

S17	9	549		0.055	0.058	3	95.0%	
S17	9	550		0.060	0.063	3	95.0%	
S17	9	551	0.059	0.027	0.059	2	100.0%	45.8%
S17	9	601	0.020	0.021	0.020	3	100.0%	105.0%
S17	9	602		0.020	0.021	3	95.0%	
S17	9	603	0.069	0.016	0.069	1	100.0%	23.2%
S17	9	604	0.054	0.024	0.054	1	100.0%	44.4%
S17	9	605		0.050	0.053	3	95.0%	
S17	9	606		0.088	0.093	3	95.0%	
S17	9	607		0.059	0.062	3	95.0%	
S17	9	608		0.034	0.036	3	95.0%	
S17	9	609	0.047	0.027	0.047	2	100.0%	57.4%
S17	9	610	0.021	0.021	0.021	2	100.0%	100.0%
S17	9	611		0.086	0.091	3	95.0%	
S17	9	612		0.058	0.061	3	95.0%	
S17	9	613	0.078	0.075	0.078	3	100.0%	96.2%
S17	9	614		0.047	0.049	3	95.0%	
S17	9	615		0.039	0.041	3	95.0%	
S17	9	616		0.087	0.092	3	95.0%	
S17	9	617	0.029	0.026	0.029	2	100.0%	89.7%
S17	9	618	0.027	0.027	0.027	2	100.0%	100.0%
S17	9	619		0.039	0.041	3	95.0%	
S17	9	620		0.044	0.046	3	95.0%	
S17	9	621	0.031	0.026	0.031	3	100.0%	83.9%
S17	9	622		0.014	0.015	3	95.0%	
S17	9	623	0.046	0.037	0.046	3	100.0%	80.4%
S17	9	624		0.009	0.011	2	84.0%	
S17	9	625		0.005	0.006	2	84.0%	
S17	9	626		0.027	0.028	3	95.0%	
S17	9	627		0.027	0.028	3	95.0%	
S17	9	628		0.028	0.029	3	95.0%	
S17	9	629		0.020	0.021	3	95.0%	
S17	9	630	0.043	0.026	0.043	2	100.0%	60.5%
S17	9	631		0.018	0.019	3	95.0%	
S17	9	632	0.051	0.026	0.051	2	100.0%	51.0%
S17	9	633	0.028	0.025	0.028	2	100.0%	89.3%
S17	9	634		0.012	0.014	2	84.0%	
S17	9	635	0.108	0.026	0.108	1	100.0%	24.1%
S17	9	636	0.124	0.013	0.124	1	100.0%	10.5%
S17	9	637		0.013	0.019	1	70.0%	
S17	9	638		0.011	0.016	1	70.0%	
S17	9	639		0.007	0.010	1	70.0%	
S17	9	640	0.706	0.122	0.706	1	100.0%	17.3%
S17	9	641		0.057	0.060	3	95.0%	
S17	9	642	0.061	0.060	0.061	3	100.0%	98.4%
S17	9	643		0.040	0.042	3	95.0%	
S17	9	644		0.052	0.055	3	95.0%	
S17	9	645		0.040	0.042	3	95.0%	
S17	9	646		0.027	0.028	3	95.0%	
S17	9	647		0.014	0.015	3	95.0%	
S17	9	648	0.020	0.016	0.020	3	100.0%	80.0%
S17	9	649		0.046	0.048	3	95.0%	
S17	9	650		0.035	0.037	3	95.0%	
S17	9	1001	0.056	0.044	0.056	3	100.0%	78.6%
S17	9	1002	0.072	0.059	0.072	3	100.0%	81.9%

mean	65.4941	35.5455	44.8623	95.6%	23.9%


S-17-9
PATTERN-13'X13'
TOE'S 10' CENTER


39 - 3/18/91
18 - 3/18/91
58 3/19/91
18 3/19/91
47 3/20/91
18 3/20/91
48 3/21/91
28 3/21/91
S-17-9
PATTERN-13'X13'
TOE'S 10' CENTER
S 17 9

Pit-Bench-Pattern #
S-17-9

Submittal Date
3-20-91 Am continued
* 3-20-91 PM *

BLAST HOLE
Hot HoCN Shake
and
FIRE DETERMINATIONS

DATE: 3-21-91
NAME: MM

	SAMPLE	FIRE Au.	HoCN Au.		SAMPLE	FIRE Au.	HoCN Au.
1.	612		Ø58 ✓	25.	Standard ✓		Ø16
2.	613	.078	Ø75 ✓	26.	635-1	.108	Ø25 ✓
3.	614		Ø47 ✓	27.	635-2		Ø26 ✓
4.	615		Ø39 ✓	28.	636	.124	Ø13 ✓
5.	616		Ø87 ✓	29.	637		Ø13 ✓
6.	617	.029	Ø26 ✓	30.	638		Ø11 ✓
7.	618	.027	Ø27 ✓	31.	639		ØØ7 ✓
8.	Standard ✓		Ø15	32.	64Ø	.706	.122 ✓
9.	619		Ø39 ✓	33.			
10.	62Ø		Ø44 ✓	34.			
11.	✓7		Ø33	35.	641		.Ø57 ✓
* 12.	3Ø1		Ø41 ✓	36.			
13.	3Ø2		Ø64 ✓	37.			
14.	3Ø3	.028	Ø29 ✓	38.			
15.	3Ø4	.016	Ø16 ✓	39.			
16.				40.			
17.				41.			
18.	3Ø5		Ø14 ✓	42.	Standard ✓		
19.	3Ø6		Ø13 ✓	43.			
20.	3Ø7		Ø13 ✓	44.			
21.	3Ø8	.017	Ø17 ✓	45.			
22.	3Ø9	.087	Ø33 ✓	46.			
23.	633	.028	Ø25 ✓	47.			
24.	634		Ø12 ✓	48.			

Pit-Bench-Pattern #
5-17-9

Submittal Date
3-21-91 8:54 Am Cont.
2:22 PM *

BLAST HOLE (2)

Bot RoCH Blake
and
FIRE DETERMINATIONS

DATE: 3-22-91

NAME: MM

End of Pattern

	SAMPLE	FIRE Au.	RoCH Au.		SAMPLE	FIRE Au.	RoCH Au.
1.	642	.061	060 ✓	25.	Standard ✓		016
2.	643		040 ✓	26.	203	.028	027 ✓
3.	644		052 ✓	27.	204		074 ✓
4.	645		040 ✓	28.	205		070 ✓
5.	646		027 ✓	29.	206	.332	.170 ✓
6.	647		014 ✓	30.	207		046 ✓
7.	648	.020	016 ✓	31.	208		056 ✓
8.	Standard ✓		015	32.	209		018 ✓
9.	649		046 ✓	33.			
10.	650		035 ✓	34.			
11.	177		032	35.	221		037 ✓
12.	181		027	36.	222		068 ✓
13.	182	.045	049 ✓	37.	223		029 ✓
14.	183	.018	019 ✓	38.	224	.021	020 ✓
15.	184		037 ✓	39.	225		073 ✓
16.				40.	226		062 ✓
17.				41.	227		033 ✓
18.	185		040 ✓	42.	Standard ✓		015
19.	186		037 ✓	43.	228		056 ✓
20.	187		032 ✓	44.	229		038 ✓
21.	188	.024	019 ✓	45.	1001-1	.056	042 ✓
22.	189	.065	022 ✓	46.	1001-2		046 ✓
23.	201		011 ✓	47.			
24.	202		012 ✓	48.			

* Bch Cil Cintrifug

8

MM

Pit-Bench-Pattern #
S-17-9

Submittal Date
3-19-91 8:36 A cont
3-19-91 pm *

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

(2)

DATE: 3-20-91

NAME: MM, KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	503		.007 ✓	25.	Standard ✓		.015
2.	504	.029	.023 ✓	26.	382		.009 ✓
3.	505	.020	.016 ✓	27.	383	.019	.026 ✓
4.	506		.046 ✓	28.	384		.040 ✓
5.	507		.055 ✓	29.	385		.052 ✓
6.	508		.072 ✓	30.	386	.016	.017 ✓
7.	509		.035 ✓	31.	387		.024 ✓
8.	Standard ✓		.014	32.	388		.028 ✓
9.	510		.042 ✓	33.	[redacted]		
10.	524		.006 ✓	34.			
11.	525		.013 ✓	35.	389		.049 ✓
12.	526	.037	.028 ✓	36.	401		.043 ✓
13.	527	.031	.017 ✓	37.	402		.072 ✓
14.	528		.079 ✓	38.	403		.032 ✓
15.	529		.074 ✓	39.	404	.024	.019 ✓
16.	[redacted]			40.	405		.033 ✓
17.				41.	406		.047 ✓
18.	530	.130	.134 ✓	42.	Standard ✓		.015
19.	531		.071 ✓	43.	407		.050 ✓
20.	✓7		.030	44.	408		.026 ✓
21.	549		.055 ✓	45.	409		.036 ✓
22.	550		.060 ✓	46.	1002-1	.072	.061 ✓
23.	551	.059	.027 ✓	47.	1002-2		.057 ✓
24.	381		.026 ✓	48.		✓ Std	.015

*

KW

x

BROHM MINING CORPORATION
BLAST HOLE ORE TYPE

PATTERN S-17-9 DATE 3/19/91

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE
421		X		505		X									
422		X		506			X								
423			X	507			X								
424			X	508			X								
425			X	509			X								
426			X	510			X								
427			X	524		X									
428			X	525	X										
429			X	526	X										
441			X	527		X									
442			X	528			X								
443			X	529			X								
444			X	530			X								
445			X	531			X								
446			X	549			X								
447			X	550			X								
448			X	551		X									
449			X												
461	X			381			X								
462	X			382			X								
463			X	383			X								
464			X	384			X								
465			X	385			X								
466			X	386			X								
467			X	387			X								
468			X	388			X								
469			X	389			X								
481	X			401			X								
482			X	402			X								
483			X	403			X								
484			X	404			X								
485			X	405			X								
486			X	406			X								
487			X	407			X								
489			X	408			X								
490			X	409			X								
501			X												
502			X												
503	X														
504		X													

PATTERN S-17-9

BLAST HOLE ORE TYPE

DATE 3/18/91

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE
1			X	142		X									
21			X	143			X								
22			X	144			X								
41			X	145			X								
42			X	146		X									
43		X		147		X									
44			X	148			X								
61		X		149	X										
62		X		161			X								
63			X	162			X								
64			X	163			X								
65			X	164			X								
66			X	165			X								
81			X	166		X									
82			X	167		X									
83			X	168		X									
84			X	169			X								
85			X												
86		X													
87			X												
88			X												
101			X												
102			X												
103			X												
104			X												
105			X												
106		X													
107		X													
108		X													
109	X														
121			X												
122			X												
123			X												
124			X												
125			X												
126			X												
127			X												
128	X														
129	X														
141			X												

ENGINEERING CORPORATION

BLAST HOLE ORE TYPE

PATTERN S-17-9 DATE 3/20/91

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE
321			X	611			X								
322			X	612			X								
323			X	613			X								
324			X	614			X								
325			X	615			X								
326			X	617		X									
327			X	618		X									
328		X		619			X								
329		X		620			X								
341			X	301			X								
342			X	302			X								
343			X	304			X								
344			X	305			X								
345			X	306			X								
346			X	307		X									
347			X	308			X								
348			X	309		X									
349		X													
				633		X									
361			X	634		X									
362			X	635	X										
363			X	636	X										
364			X	637	X										
365			X	638	X										
366			X	639	X										
367			X	640	X										
368			X	641			X								
369			X												
601			X												
602			X												
603	X														
604	X														
605			X												
606			X												
607			X												
608			X												
609		X													
610		X													

MONTANA ORE CORPORATION

PATTERN S 179 Endof Pattern — BLAST HOLE ORE TYPE — DATE 3/21/84

NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE	NO.	SULF.	MIX	OXIDE
181			X	261			X	649			X				
182			X	262			X	650			X				
183			X	263			X								
184			X	264			X	1001			X				
185			X	265			X								
186			X	266			X								
187			X	267			X								
188		X		268			X								
189		X		269			X								
201			X	281			X								
202			X	282			X								
203			X	283			X								
204			X	284			X								
205			X	285			X								
206			X	286			X								
207			X	287			X								
208			X	288			X								
209			X	289			X								
221			X	621			X								
222			X	622			X								
223			X	623			X								
224			X	624		X									
225			X	625		X									
226			X	626			X								
227			X	627			X								
228			X	628			X								
229			X	629			X								
				630		X									
241			X	631			X								
242			X	632		X									
243			X												
244			X	642			X								
245			X	643			X								
246			X	644			X								
247			X	645			X								
248			X	646			X								
249			X	647			X								
				648			X								

Pit-Bench-Pattern #
5-17-9

Submittal Date
3-21-91 8:59 Am

BLAST HOLE

Hot ReCH Blake
and
FIRE DETERMINATIONS

(1)

DATE: 3-22-91

NAME: MM

	SAMPLE	FIRE Au.	ReCH Au.		SAMPLE	FIRE Au.	ReCH Au.
1.	241		Ø26 ✓	25.	Standard ✓		Ø15
2.	242	.018	Ø20 ✓	26.	283		Ø69 ✓
3.	243		Ø35 ✓	27.	284		Ø17 ✓
4.	244		Ø36 ✓	28.	285		Ø17 ✓
5.	245		Ø22 ✓	29.	286		Ø15 ✓
6.	246		Ø30 ✓	30.	287	.021	Ø19 ✓
7.	247	.086	Ø89 ✓	31.	288		Ø12 ✓
8.	Standard ✓		Ø14	32.	289		Ø37 ✓
9.	248		Ø45 ✓	33.	[redacted]		
10.	249		Ø53 ✓	34.	[redacted]		
11.	✓7		Ø31	35.	621-1	.031	Ø23 ✓
12.	261	.016	Ø12 ✓	36.	621-2		Ø29 ✓
13.	262		Ø30 ✓	37.	622		Ø14 ✓
14.	263		Ø24 ✓	38.	623	.046	Ø37 ✓
15.	264		Ø13 ✓	39.	624		ØØ9 ✓
16.	[redacted]			40.	625		ØØ5 ✓
17.	[redacted]			41.	626		Ø27 ✓
18.	265	.028	Ø31 ✓	42.	Standard ✓		Ø14
19.	266		Ø12 ✓	43.	627		Ø27 ✓
20.	267		ØØ9 ✓	44.	628		Ø28 ✓
21.	268		Ø30 ✓	45.	629		Ø2Ø ✓
22.	269		Ø27 ✓	46.	630	.043	Ø26 ✓
23.	281		Ø39 ✓	47.	631		Ø18 ✓
24.	282	.015	ØØ9 ✓	48.	632	.051	Ø26

KW

Pit-Bench-Pattern #
S-17-9

Submittal Date
3-20-91 Am

BLAST HOLE
Hot HoCN Shake
and
FIRE DETERMINATIONS

DATE: 3-21-91
NAME: MM

	SAMPLE	FIRE Au.	HoCN Au.		SAMPLE	FIRE Au.	HoCN Au.
1.	321		007	25.	Standard		016
2.	322	.015	015	26.	363	.027	021
3.	323		027	27.	364		007
4.	324		058	28.	365		065
5.	325		024	29.	366		032
6.	326		042	30.	367		036
7.	327		049	31.	368		055
8.	Standard		015	32.	369	.129	.114
9.	328		013	33.			
10.	329	.016	017	34.			
11.	7		032	35.	601-1	.020	021
12.	341	.034	039	36.	601-2		021
13.	342	.010	008	37.	602		020
14.	343		042	38.	603	.069	016
15.	344		020	39.	604	.054	024
16.				40.	605		050
17.				41.	606		088
18.	345		026	42.	Standard		015
19.	346		026	43.	607		059
20.	347		054	44.	608		034
21.	348		067	45.	609	.047	027
22.	349		014	46.	610	.021	021
23.	361		037	47.	611		086
24.	362	.039	032	48.			

x

Pit-Bench-Pattern #
S-17-9
Submittal Date
3/19/91 8:36 Am

BLAST HOLE
Hot HoCN Shake
and
FIRE DETERMINATIONS

(1)

DATE: 3-20-91
NAME: MM, KW

	SAMPLE	FIRE Au.	HoCN Au.		SAMPLE	FIRE Au.	HoCN Au.
1.	421	.062	.016 ✓	25.	Standard ✓		.015
2.	422	.046	.040 ✓	26.	463		.029 ✓
3.	423		.016 ✓	27.	464		.044 ✓
4.	424		.038 ✓	28.	465		.040 ✓
5.	425		.046 ✓	29.	466		.045 ✓
6.	426		.032 ✓	30.	467	.127	.122 ✓
7.	427		.014 ✓	31.	468		.053 ✓
8.	Standard ✓		.014	32.	469		.036 ✓
9.	428		.065 ✓	33.			
10.	429		.047 ✓	34.			
11.	✓ 7		.032	35.	481-1	.012	.007 ✓
12.	441	.069	.059 ✓	36.	481-2		.006 ✓
13.	442		.012 ✓	37.	482		.013 ✓
14.	443		.019 ✓	38.	483	.021	.019 ✓
15.	444		.043 ✓	39.	484		.041 ✓
16.				40.	485		.051 ✓
17.				41.	486		.036 ✓
18.	445		.027 ✓	42.	Standard ✓		.015
19.	446		.017 ✓	43.	487		.037 ✓
20.	447	.239	.096 ✓	44.	488		.026 ✓
21.	448		.026 ✓	45.	489		.057 ✓
22.	449		.029 ✓	46.	490		.079 ✓
23.	461		.007 ✓	47.	501		.009 ✓
24.	462	.013	.014 ✓	48.	502	.018	.016 ✓
					Std ✓		.013

FA Rerun

KW

X

Pit-Bench-Pattern #
S-17-9

Submittal Date
3/18/91 11:49A

BLAST HOLE
Hot NaCN Strake
and
FIRE DETERMINATIONS

DATE: 3/19/91
NAME: KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	141		.019 ✓	25.	Standard ✓		
2.	142	.030	.032 ✓	26.			
3.	143-1	.017	.016 ✓	27.			
4.	143-2		.018 ✓	28.			
5.	144		.016 ✓	29.			
6.	145		.015 ✓	30.			
7.	146	.070	.045 ✓	31.			
8.	Standard ✓		.014 ✓	32.			
9.	147	.058	.034 ✓	33.			
10.	148	.091	.077 ✓	34.			
11.	149	.068	.033 ✓	35.			
12.	161		.014 ✓	36.			
13.	162		.011 ✓	37.			
14.	163		.006 ✓	38.			
15.	164		.029 ✓	39.			
16.				40.			
17.				41.			
18.	165		.023 ✓	42.	Standard ✓		
19.	166	.015	.015 ✓	43.			
20.	167	.100	.049 ✓	44.			
21.	168	.043	.028 ✓	45.			
22.	169	.402	.194 ✓	46.			
23.	17		.033 ✓	47.			
24.				48.			

FA Rerun

KW

Pit-Bench-Pattern #
S-17-9
Submittal Date
3/18/91 7:54A

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 3/19/91
NAME: KW

	SAMPLE	FIRE Au.	NaCN Au.		SAMPLE	FIRE Au.	NaCN Au.
1.	1		.026	25.	Standard ✓		.015
2.	21		.025	26.	88-1	.039	.043
3.	22		.018	27.	88-2		.042
4.	41		.007	28.	101		.074
5.	42		.014	29.	102		.026
6.	43		.012	30.	103		.054
7.	44		.017	31.	104	.276	.213
8.	Standard ✓		.015	32.	105	.137	.111
9.	61	.010	.011	33.	[redacted]		
10.	62		.007	34.			
11.	✓7		.033	35.	106	.146	.064
12.	63		.016	36.	107	.026	.020
13.	64		.020	37.	108	.032	.021
14.	65		.018	38.	109	.059	.029
15.	66		.014	39.	121		.033
16.	[redacted]			40.	122		.031
17.				41.	123		.019
18.	81	.026	.018	42.	Standard ✓		.015
19.	82		.015	43.	124	.007	.005
20.	83		.013	44.	125		.014
21.	84		.010	45.	126		.021
22.	85		.014	46.	127		.031
23.	86	.019	.014	47.	128	.039	.022
24.	87		.026	48.	129	.059	.021

Std ✓ .013